

1 **Karst aquifer discharge response to rainfall interpreted as anomalous transport**

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13 **Abstract**

14 The discharge measured in karst springs is known to exhibit distinctive long tails during
15 recession times following distinct discharge peaks of short duration. The long-tail behavior is
16 generally attributed to the occurrence of tortuous, ramified flow paths that develop in the
17 underground structure of karst systems. Modeling the discharge behavior poses unique
18 difficulties because of the poorly-delineated flow path geometry and generally scarce
19 information on the hydraulic properties of catchment-scale systems. In a different context,
20 modeling of long-tailed behavior has been addressed in studies of chemical transport. Here, an
21 adaptation of a continuous time random walk – particle tracking (CTRW-PT) framework for
22 anomalous transport is proposed, which offers a robust means to quantify long-tailed
23 breakthrough curves that often arise during chemical species transport under various flow
24 scenarios. A theoretical analogy is first established between partially water-saturated karst flow,
25 characterized by temporally varying water storage, and chemical transport involving
26 accumulation and release of a chemical tracer. This analogy is then used to develop and
27 implement a CTRW-PT model. Application of this numerical model to examination of three
28 years of summer rainfall and discharge data from a karst aquifer system – the Disnergshroef
29 high alpine site in the Austrian Alps – is shown to yield robust fits between modeled and
30 measured discharge values. In particular, the analysis underscores the predominance of slow
31 diffusive flow over rapid conduit flow. The study affirms the analogy between partially
32 saturated karst flow and chemical transport, exemplifying the compatibility of the CTRW-PT
33 model for this purpose. Within the specific context of the Disnergshroef karst system, these
34 findings highlight the predominance of slow diffusive flow over rapid conduit flow. The
35 agreement between measured and simulated data supports the proposed analogy between
36 partially saturated karst flow and chemical transport; it also highlights the potential ability of
37 the anomalous transport framework to further enhance modeling of flow and transport in karst
38 systems.

39 1 Introduction

40 Aquifers consist of various geological formations through which water can flow and carry
41 chemical species. The abundance of structural heterogeneities, ranging from intricate grain
42 arrangements at the pore scale to larger geologic structures and discontinuities at the meso- and
43 macroscopic scales, introduces irregular and tortuous flow paths that cannot be delineated
44 without a full physical description of the system. Achieving an accurate representation of flow
45 and transport therefore becomes increasingly difficult with an increase in the scale and
46 complexity of the groundwater system.

47 Karst systems, in particular, are known as structurally complex aquifers. They are composed
48 of many interconnected conduits, fractures and voids formed through the dissolution of soluble
49 rocks like limestone, dolostone and gypsum, which leads to the occurrence of multiple and
50 ramified flow paths (Bakalowicz, 2005). Karst terrains are usually described, in a vertical
51 cross-section, by distinct hydrological layers whose structure affect the response of the system
52 to incoming precipitation: (1) the surface soil layer; (2) the interface between the soil layer and
53 the deeper saturated zone (epikarst); and (3) the deep underground, mostly phreatic, zone
54 (endokarst). The soil and epikarst layers, known collectively as the exokarst, are known to
55 exhibit lateral flow of water above and below ground, until water reaches fractures or conduits
56 that allow them to flow rapidly to the endokarst. This allows for some water to infiltrate
57 downwards, while some may remain in the vadose zone and be subjected to both percolation
58 and evapotranspiration (Jukić and Denić-Jukić, 2009). The epikarst and endokarst layers each
59 consist of a primary (matrix) porosity composed of all bulk pores, a secondary porosity
60 composed of the smaller joints and fissure developed during diagenesis and/or by tectonic
61 processes, and a tertiary porosity of large fractures and voids (conduits) created due to
62 karstification (Ford and Williams, 2007). The different types of porosities usually exhibit
63 distinct flow patterns: rapid flow in the conduits and slow diffusive flow in the smaller fissures
64 and the matrix. The different karst layers may exhibit a changing role in facilitating the flow or
65 retention of water through the system as a function of water level or recharge intensity
66 (Hartmann et al., 2014). Furthermore, the connectivity of the different porosities often results
67 in a fracture-cave network, which dominates the flow structures in karst systems (Zhang et al.,
68 2022).

69 To date, various hydrological models have been developed specifically for karst systems, to
70 describe the commonly observed flow and transport patterns that are specific to karst systems.

71 In particular, distributed models rely on creating a grid of cells with different hydrological
72 parameters (e.g., Anderson & Radić, 2022; Chen et al., 2017; Kaufmann & Turk, 2016), while
73 lumped parameter models parameterize the characteristics of the system. Lumped parameter
74 models are based on different system conceptualizations (e.g., Chen and Goldscheider, 2014;
75 Cinkus et al., 2023b; Fleury et al., 2009; Jukić and Denić-Jukić, 2009; Mazzilli et al., 2019;
76 Rimmer and Salinger, 2006; Tritz et al., 2011), as well as neural network approaches (e.g.,
77 Afzaal et al., 2020; Cinkus et al., 2023b; Kratzert et al., 2018; Renard and Bertrand, 2017;
78 Wunsch et al., 2022). A common, significant feature encountered in karst systems – which is
79 difficult to capture in models – is the interplay of rapid and slow flow which manifests as long-
80 tailed measurements of both discharge rates (e.g., Frank et al., 2021) and chemical tracer
81 concentrations (e.g., Goepfert et al., 2020) observed at karst springs.

82 In many systems that exhibit highly variable spatial velocity distributions or temporal
83 behaviors, measurements of long tails in arrival times may be encountered. In the context of
84 chemical transport in porous media, long tails in the arrival time of chemical tracers have long
85 been a subject of study. Anomalous transport, which describes chemical transport that deviates
86 from the behavior described by the traditional Advection-Dispersion Equation (ADE), is
87 prevalent in many system and transport scenarios (Berkowitz et al., 2006); deviations from
88 solutions of traditional transport equations were observed even for non-dispersive diffusion
89 (Cortis and Knudby, 2006). It has been shown that higher subsurface heterogeneity increases
90 the degree of anomalous transport by inducing longer than expected (for Fickian transport)
91 arrival times (Edery et al., 2016, 2014). Traditional ADE based models, which rely on
92 averaging the physical traits of the medium into a single coefficient, do not accurately predict
93 transport in many cases. To correctly describe long-tailed events, various modeling approaches
94 have been developed. Among these, the Continuous Time Random Walk (CTRW) framework
95 has emerged as suitable for simulating diverse transport scenarios, including the behavior of a
96 long-time field-scale hydrological catchment (Dentz et al., 2023). The CTRW framework
97 accounts for anomalous transport behavior and offers a more physically realistic representation
98 of the transport processes that are encountered in real-world groundwater systems. The
99 framework defines waiting time and step length distributions that are applied in random walks
100 which are continuous in time, thereby capturing the complexity of transport processes
101 (Berkowitz et al., 2006).

102 In the current study, the CTRW framework, which has been developed to model anomalous
103 chemical transport, is utilized to quantify long-tailing of water flow in karst systems. In this

104 context, data from the Disnergenschroef alpine study site in Vorarlberg, Austria are revisited
105 (Frank et al., 2021). This high-alpine karst system has been thoroughly studied and offers a
106 well defined spatial catchment with a well-defined spatial boundary. The surface of the karst
107 system is composed mainly of bare limestone with very limited soil coverage, resulting in
108 negligible surface runoff. The plateau is characterized by dolines and depressions, further
109 facilitating the direct flow of water into the subsurface. The vadose zone is estimated to be
110 several hundred meters thick (Frank et al., 2021). The known extent of its recharge basin and
111 the corresponding single spring which serves as its outlet allow for measurements of both
112 recharge and discharge. Previous studies (e.g., Frank et al., 2021) identified a distinct discharge
113 response approximately 5.5 hours after a rainfall event, with variations in electrical
114 conductivity, indicative of fresh rainfall arriving at the spring outlet, observed ~8 hours post-
115 event. While existing models provided a good overall fit and illuminated the divide between
116 epikarst-to-conduit and matrix-to-conduit flows, they were less effective in matching the long
117 tails.

118 Accurate modeling of water movement in these complex subsurface landscapes is crucial, as
119 many regions rely on karst systems for drinking water (Stevanović, 2019). Here, a theoretical
120 and practical development of the CTRW framework is proposed as an approach to simulate the
121 intricate dynamics of water movement in karst environments.

122 **2 Conceptual and mathematical development**

123 The conceptual development of the CTRW framework to model water flow in karst systems is
124 founded on a proposed ansatz, in which water flow is conceptualized as distinct “water parcels”
125 (i.e., infinitesimal volumes of water) that travel along the available flow paths. Local volumes
126 along the flow paths, e.g., caverns, conduits, and voids, allow for the accumulation and release
127 of water parcels, and define mobile and immobile zones for water flow. The ansatz asserts that
128 the accumulation and release of water parcels in the various volumes in the karst system
129 resemble the accumulation and release of “parcels” of a chemical tracer (i.e., infinitesimal
130 volumes of tracer) over time in a porous medium. As shown in Fig. 1, a cavern acting as a
131 storage region for water parcels is analogous to tracer parcels accumulating in an immobile (or
132 less mobile) zone. For both cases, it should be noted that local accumulation of water parcels
133 or increase in concentration of a chemical will increase their respective fluxes in the immediate
134 local vicinity. Under similar hydraulic conditions both fluxes create distinctive long tails when

135 measured over a control plane at the system outlet, which is primarily a result of the structural
 136 heterogeneity of the system.

137 Characterizing the flow of water through an infinitesimal control volume can be formulated in
 138 terms of a mass balance equation that equates the net rate of fluid flow in the control volume
 139 to the time rate of change of fluid mass storage within it:

$$140 \quad -\frac{\partial(\rho q_x)}{\partial x} - \frac{\partial(\rho q_y)}{\partial y} - \frac{\partial(\rho q_z)}{\partial z} = \frac{\partial(\rho n)}{\partial t} \quad (1)$$

141 where n is porosity, ρ water density, and the three components of the specific discharge \mathbf{q} are
 142 described as q_x , q_y and q_z . This equation describes the mass balance in a fully saturated domain,
 143 in which the void volume (V_v) is completely filled with water ($V_w=V_v$). The moisture content
 144 ($\theta = \frac{V_w}{V_{tot}}$) in these cases is equal to the porosity, and the degree of saturation ($\theta' = \frac{\theta}{n}$) is equal
 145 to 1.

146 For partially saturated flow, the degree of saturation is less than 1 and the moisture content is
 147 smaller than n (as $V_w < V_v$). Adjusting the equation for partially saturated transient flow yields
 148 (allowing for water compressibility, to retain generality):

$$149 \quad -\frac{\partial(\rho q_x)}{\partial x} - \frac{\partial(\rho q_y)}{\partial y} - \frac{\partial(\rho q_z)}{\partial z} = \frac{\partial(\rho \theta' n)}{\partial t} \quad (2)$$

150 Substituting $\theta = \theta' n = \frac{\theta}{\theta'}$:

$$151 \quad -\frac{\partial(\rho q_x)}{\partial x} - \frac{\partial(\rho q_y)}{\partial y} - \frac{\partial(\rho q_z)}{\partial z} = \frac{\partial(\rho \theta)}{\partial t} \quad (3)$$

152 Deriving a description for the a-transport of a chemical tracer transport in a fully saturated
 153 porous medium within a similar control volume is achieved by a mass balance equation:

$$154 \quad -\frac{\partial F_x}{\partial x} - \frac{\partial F_y}{\partial y} - \frac{\partial F_z}{\partial z} = n \frac{\partial C}{\partial t} \quad (4)$$

155 The chemical mass flux (in one direction) is defined by advection and diffusion terms:

$$156 \quad F_i = q_i C - n D_i \frac{\partial C}{\partial i} \quad (5)$$

157 Substituting (5) into (4) yields

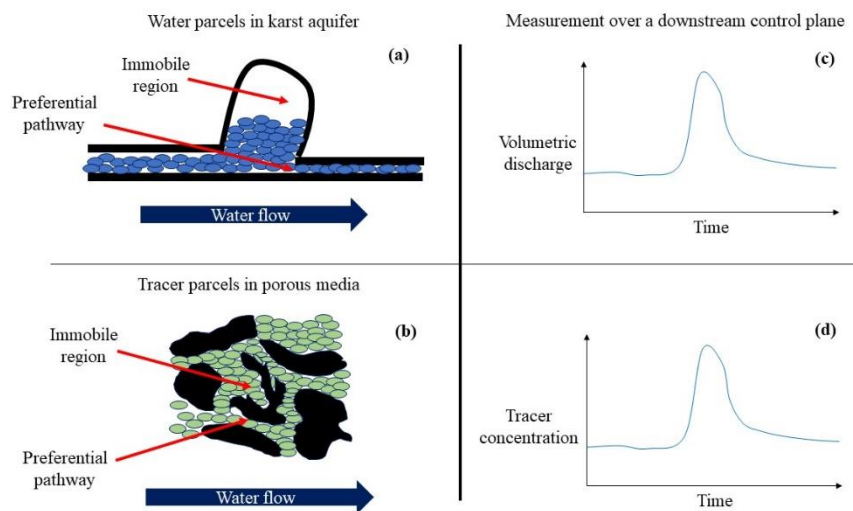
$$158 \quad \frac{\partial}{\partial x} \left(n D_x \frac{\partial C}{\partial x} \right) - \frac{\partial}{\partial x} (q_x C) + \frac{\partial}{\partial y} \left(n D_y \frac{\partial C}{\partial y} \right) - \frac{\partial}{\partial y} (q_y C) + \frac{\partial}{\partial z} \left(n D_z \frac{\partial C}{\partial z} \right) - \frac{\partial}{\partial z} (q_z C) = n \frac{\partial C}{\partial t} \quad (6)$$

159 (Note that the appearance of the porosity variable, n , in the terms of Eqs. (4)-(6) is easily
 160 rearranged, and that these equations can be simplified if n is assumed constant in space.)

161 By drawing the analogy in the ansatz between the dynamics of water parcels and chemical
 162 tracers, and noting the similar forms of Eqs. (3) and (4), the description of the mass balance of

163 water in a partially saturated domain is (at least) mathematically analogous to the description
 164 of the mass balance of a chemical tracer in a saturated domain. This results in the intrinsic
 165 connection of $C \Leftrightarrow \rho\theta$, both with units of mass per volume. In a 1D direction, the analogy of
 166 the mass flux can be thus defined: $\rho q_x \equiv nD_x \frac{\partial C}{\partial x} - q_x C$. This connection incorporates
 167 hydrodynamic dispersion, which is inherent in chemical transport resulting in observed long
 168 tails, into the description of the partially saturated water parcels moving within the conceptual
 169 karst domain. Thus, the analogy of chemical transport and water flow is expected to show long
 170 tailing in simple flow scenarios, and was established even for pure diffusion (Cortis and
 171 Knudby, 2006).

172



173

174 **Figure 1.** Schematic illustration of (a) water parcels (blue ovals) in a karst aquifer, and (b)
 175 chemical tracer parcels (green ovals) in a porous medium (black grains) flowing through
 176 preferential pathways and accumulating in adjunct immobile regions. The resulting
 177 (schematic) measurements of the (c) temporal volumetric discharge, and (d) tracer
 178 concentration that are measured at the spring outlet further downstream.

179

180 Thus, transport equations – either advection-dispersion equations (ADE; Eq. (6)) for Fickian
 181 transport, or a CTRW formulation for non-Fickian transport (see Sect. 3.1) can be used, where
 182 the chemical tracer concentrations that these equations solve for $C(x,t)$ are conceptually
 183 identical to the relative concentration of water parcels. The concentration at a specific point is
 184 analogous to the moisture content, and the classical $C(t)$ breakthrough curve is analogous to

185 ~~the translated to a volume of water, so that a classical breakthrough curve $C(t)$ is reinterpreted~~
 186 ~~as the~~ (volumetric) amount of water per time reaching the domain outlet (or measurement
 187 plane).

188 3 Methods

189 3.1 CTRW-PT simulations

190 In this study, a particle tracking (PT) implementation of the CTRW framework was employed
 191 to devise a model capable of simulating spring discharge using the rainfall data as input. The
 192 CTRW-PT model, characterized by stochastically defined particle transitions, is a Lagrangian
 193 approach to solving the partial differential equations defined in the CTRW mathematical
 194 framework. The movement of the particles, representing water parcels as described in the
 195 ansatz (see Sect. 2), is described by equations that define the probability of particles to make
 196 transitions in both space and time (Elhanati et al., 2023). For 1D cases, the transport is governed
 197 by two probability density functions, $p(s)$ and $\psi(t)$, which define the particle movement in space
 198 and time, respectively. An exponential form for $p(s)$ and a truncated power law (TPL) form for
 199 $\psi(t)$ are used:

$$200 \quad p(s) = \lambda_s^2 \exp(-\lambda_s s) , \quad (7)$$

$$201 \quad \psi(t) = C \frac{\exp(-t/t_2)}{(1+t/t_1)^{1+\beta}} . \quad (8)$$

202 Here, λ_s^2 and C serve as normalization factors for $p(s)$ and $\psi(t)$, respectively. The TPL is
 203 governed by β , the power law exponent ($0 < \beta < 2$), which is a measure of the non-Fickian
 204 nature of the transport, t_1 , the characteristic transition time, and t_2 , the cutoff time to initiate
 205 transition to Fickian transport. The particle velocity, v_ψ , and the generalized dispersion, D_ψ ,
 206 are defined as the first and second spatial moments of the chemical species plume in the flow
 207 direction (Berkowitz et al., 2006) For a 1D system:

$$208 \quad v_\psi = \frac{\overline{s_x}}{\bar{t}} = \frac{\int_0^\infty p(s)s^2 ds}{\int_0^\infty \psi(t)t dt} , \quad (9)$$

$$209 \quad D_\psi = \frac{1}{2} \frac{\overline{s_x^2}}{\bar{t}} = \frac{1}{2} \frac{\int_0^\infty p(s)s^3 ds}{\int_0^\infty \psi(t)t dt} , \quad (10)$$

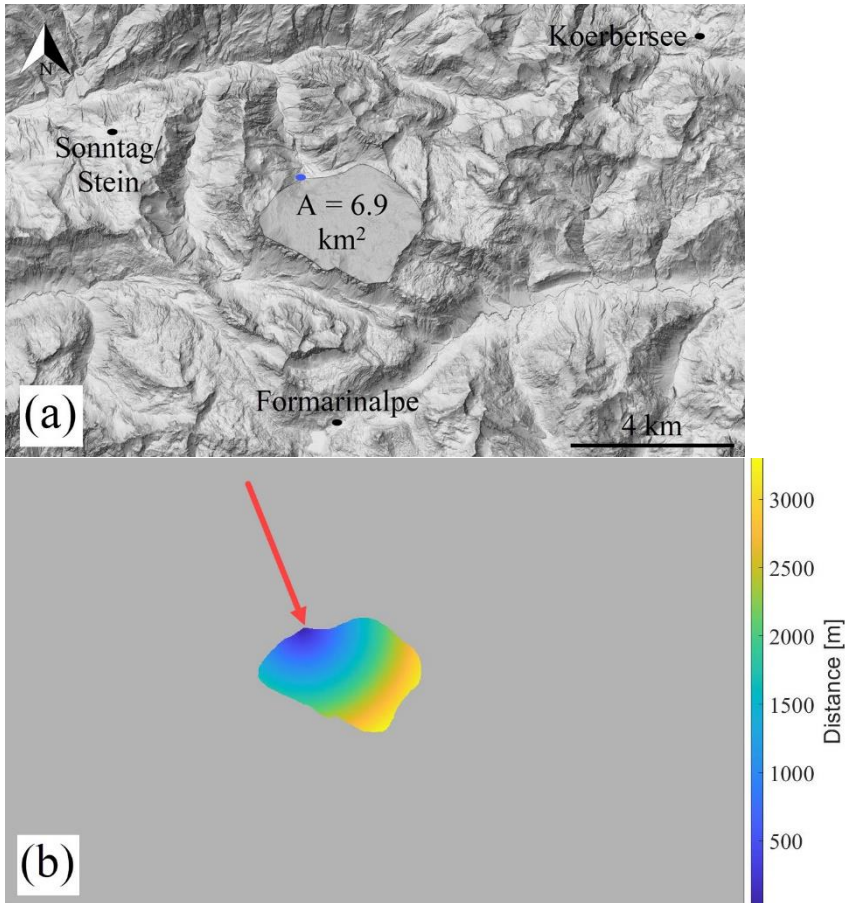
210 where $\overline{s_x}$ and \bar{t} are the mean step size and time, respectively.

211 Inserting the probability density functions (Eqs. 7 and 8) into Eqs. 9 and 10, and defining $\tau_2 \equiv$
212 t_2/t_1 yields a mathematical relation among v_ψ , D_ψ , β , τ_2 , t_1 , t_2 and λ_s (see Nissan et al., 2017
213 for a full mathematical development). By treating the first four variables (v_ψ , D_ψ , β , τ_2) as
214 fitting parameters, the other three (t_1 , t_2 , λ_s) are immediately determined, allowing
215 optimization of the CTRW-PT model to a specific flow scenario (see Table 1).

216 The intricate three-dimensional flow field of a karst system can be conceptualized in a model
217 that considers the relationships between storage and discharge. These kinds of models, known
218 as lumped models, have been extensively used in simulation of karst systems (Hartmann et al.,
219 2014). Herein, a similar approach is applied, i.e., conceptualizing the system as a series of
220 specific physical transitions. However, in the context of the CTRW-PT model, an equivalent
221 medium to the karst system is defined in the form of a one-dimensional domain. Water is
222 introduced into the domain along its entire extent and flows to the domain outlet.

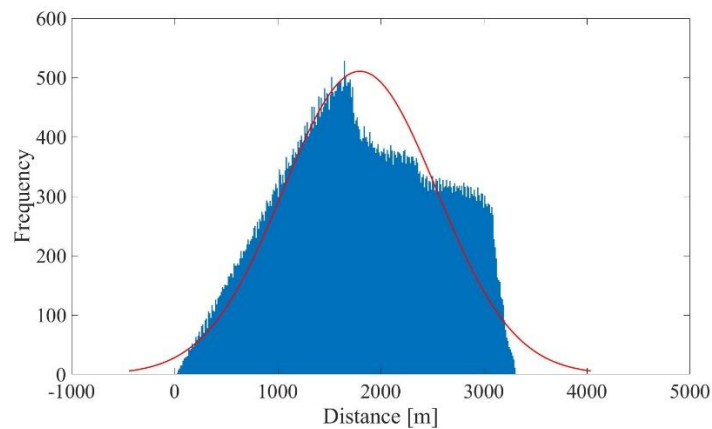
223 The 1D conceptualization is facilitated by the well-defined spatial characteristics of the system,
224 namely the catchment area and spring outlet (Fig. 2a). The distance of each point on the surface
225 of the catchment to the spring outlet is calculated (Fig. 2b), which yields a frequency histogram
226 of distances ~~frequency histogram~~ (Fig. 3). ~~A~~ The histogram shape is dependent upon the initial
227 image resolution and the chosen bin size and yields discrete distances. To sample continuum
228 particle entry locations without dependence on bin size, a distance ~~normal~~-distribution, fitted
229 to the histogram using MATLAB, dictates how new particles are introduced into the system
230 along the 1D domain (physically unrealistic, negative sampled values are set to 0). A normal
231 distribution was chosen as a simplified representation of the distance distribution; preliminary
232 simulation results were similar for different skewed distributions. The actual underground flow
233 path between each point and the outlet spring is longer than the linear distance between the two
234 points, as the water must travel through the tortuous path through the existing conduits and
235 fissures. The distances are therefore multiplied by an empirical tortuosity factor (L), which
236 serves as an optimization parameter (see Table 1).

237



238

239 **Figure 2.** (a) Map of the Disnergschroef study area. The three weather stations in which rainfall
 240 was measured are marked with black dots, the measured spring outlet is marked with a blue
 241 dot (basemap: Land Vorarlberg – data.vorarlberg.gv.at); (b) Distances from the catchment
 242 area to the spring outlet. The distances are marked by a color scale. The spring outlet is marked
 243 by a red arrow.

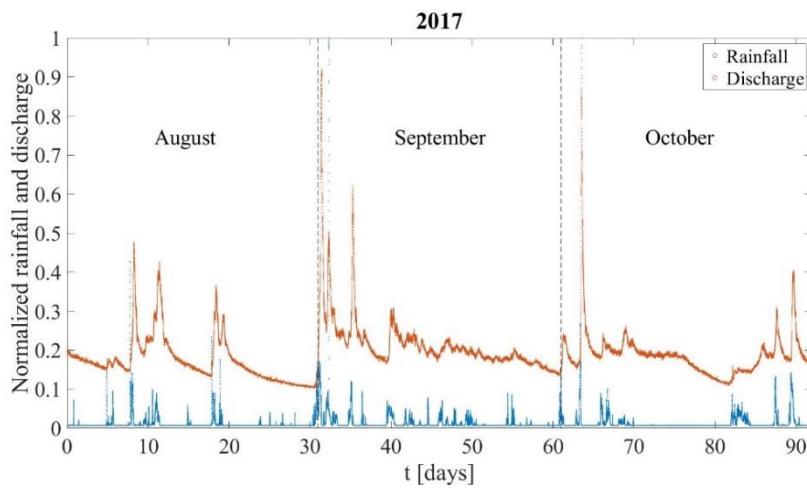
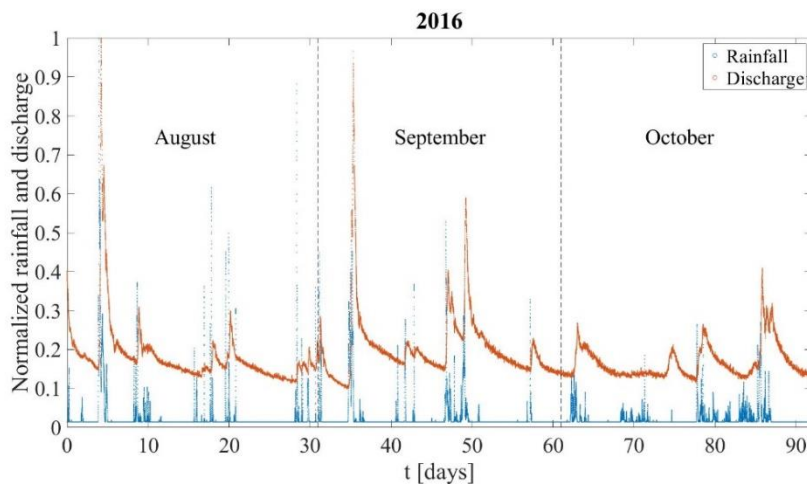


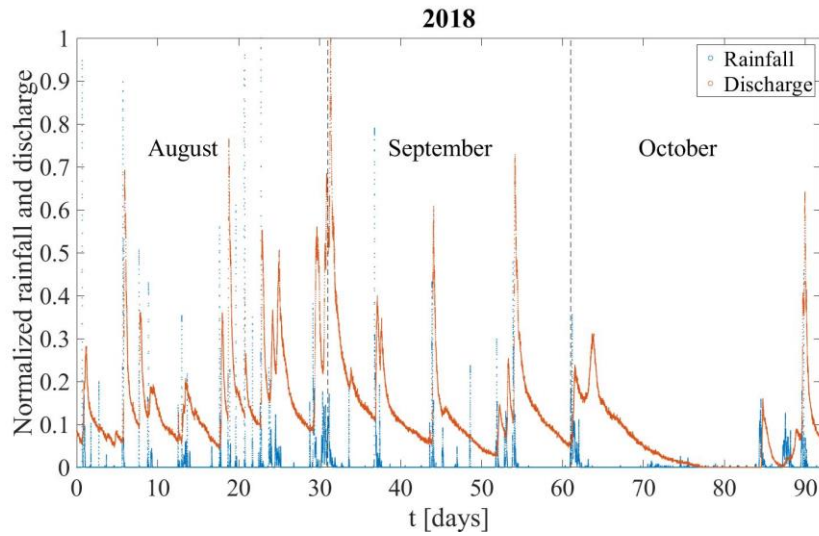
244

245 **Figure 3.** Distribution of distances from catchment area to spring outlet. The red line represents
 246 a fitted normal distribution ($\mu=1.8 \times 10^3$; $\sigma=747$).

247 Discharge at the spring is sampled every 15 minutes ($L s^{-1}$). The minimum measured discharge
248 minimum measured represents the baseflow discharge conditions. Raw rainfall data from three
249 nearby weather stations (Fig. 2a) are measured in millimeters per 15 minutes. The data from
250 the three stations are averaged, and the catchment area is used to convert the data into liters per
251 second (Fig. 4). To achieve higher temporal simulation resolution, linear interpolation was used
252 to resample the time series to match a smaller simulation time step (100 s).

253





256

257 **Figure 4.** Rainfall and discharge curves for the 2016, 2017 and 2018 datasets. The data are
 258 normalized according to the maximum rainfall and discharge values, respectively, for each of
 259 the three years.

260

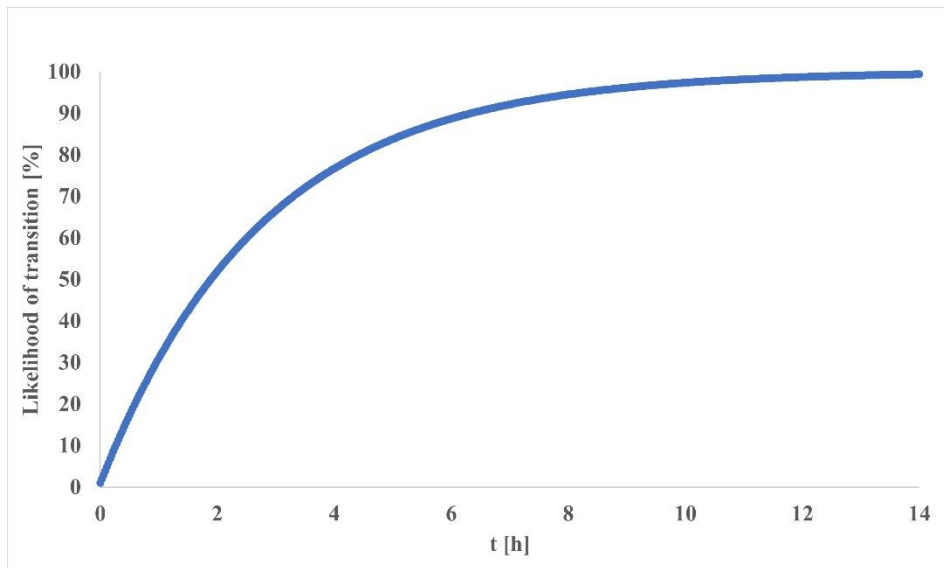
261 For an ideal system, in which all incoming rainwater is discharged through the spring outlet,
 262 the ratio of total rainwater to total discharge is expected to be unity. However, considering the
 263 uncertainty in the contributions of hydraulic parameters to the catchment water budget, e.g.,
 264 flow to deeper parts of the aquifer and/or other springs, and evapotranspiration, the rainfall
 265 function must be adjusted by a calculated observed recharge capacity to yield the recharge
 266 function:

267
$$recharge(t) = rainfall(t) \times \frac{\sum discharge(t) - baseflow}{\sum rainfall(t)} \quad (11)$$

268 where $rainfall(t)$ and $discharge(t)$ are the measured rainfall and discharge time series. The ratio
 269 multiplying the rainfall function is defined here as the recharge capacity parameter. The
 270 baseflow was subtracted from the total discharge for the recharge capacity calculation, to
 271 account for the background discharge not related to the spring response to rainfall. While a
 272 constant recharge capacity factor is employed in this study, due to the negligible surface runoff,
 273 it is important to note that the rainfall-to-recharge ratio may be influenced by temporal
 274 variations, rainfall intensity, and spatial characteristics. Future research should consider the
 275 sensitivity of these variables for the specific scenarios considered. In cases where there is
 276 significant variability among them, other temporal and/or spatial ratios may be applied.

277 A common procedure in lumped karst models separates the flow into slow and fast components,
278 representing the diffusive flow in the matrix and smaller fissures and the rapid flow in the
279 conduits, respectively (Hartmann et al., 2014). The CTRW-PT, as opposed to lumped models,
280 does not utilize water flow reservoirs, and operates by tracking the motion of particles that
281 represent water parcels. Therefore, the model was adapted to implement a similar approach:
282 two different sets of CTRW parameters, which govern the probability density functions for
283 particle movement (see Eqs. 7-10), are defined to represent the two flow regimes. Each particle
284 in the simulation is defined as “slow” or “fast”, and therefore obeys the corresponding set of
285 CTRW parameters (see Table 1). Newly introduced particles are divided between fast and slow
286 flow, according to a set ratio (SF_r), and they advance in space and time by their corresponding
287 set of CTRW parameters. Furthermore, each slow particle has a likelihood to transition into a
288 fast particle (SF_f) in each simulation iteration, by changing the set of CTRW parameters that
289 the particle obeys. The transition from slow to fast flow illustrates the flow of water from the
290 matrix/fissures to the conduits. While transition of fast to slow flow is also possible in karst
291 aquifers, i.e., when the pressure gradient allows water from the conduits to enter the matrix,
292 the slow to fast transition is more prominent for this site. Thus, the likelihood of transition
293 represents the net transition from slow to fast flow. When more particles transition back from
294 fast to slow flow, the transition likelihood is lower. In this context, it is important to note that
295 the CTRW-PT is a stochastic approach, in which the system parameters are represented by
296 statistical properties. The results of CTRW-PT simulations are, therefore, representative of an
297 ensemble average of many realizations.

298 As depicted in Fig. 5, the likelihood of particle transition increases rapidly, with slow particles
299 consistently transitioning into fast particles. For a transition likelihood of 0.01% and a
300 simulation time step of 100 s, the likelihood for a single particle to make a transition surpasses
301 99% after 458 steps which amount to 45,800 seconds (~12.7 hours). In comparison, the data
302 and simulations presented in this study span a duration of 7,951,400 seconds (~92 days). These
303 two parameters, governing the division of water between fast and slow flow and the transition
304 of water from the matrix/fissures to the conduits, are pivotal in allowing the CTRW-PT model
305 to simulate karst data.



306

307 **Figure 5.** Likelihood of particle transition from slow regime to fast regime (SF_i) as a function
 308 time for $SF_i=0.01\%$, representing a particle transition from slow matrix/fissure flow to fast
 309 conduit flow.

310

311 3.2 Model optimization and comparison to field measurements

312 Each particle represents a volume of water. The volume per particle was calculated by dividing
 313 the total observed rainfall volume by the number of simulation particles. This enables a
 314 comparison between simulated and observed recharge by volume. Given the presence of
 315 numerous-multiple model parameters (refer to Table 1), optimization is achieved by applying
 316 a bound constraint version of the Matlab's MATLAB fminsearch function (D'Errico, 2024) to
 317 minimizing-minimize the Root Mean Squared Error (RMSE) between observed and simulated
 318 discharge using different combinations of parameter values. A broad range of constrained
 319 parameters were investigated, as detailed in Table 1. The 2016 dataset was first utilized-used
 320 for model parameter optimizationestimation, while the 2017 and 2018 datasets served as targets
 321 for validation, by considering them for prediction using the optimized parameters from the
 322 2016 dataset.

323 The Nash-Sutcliffe efficiency (NSE) and modified balance error (BE) was-were calculated for
 324 the optimized simulations, as a measure of the goodness of fit. The NSE and BE are the
 325 performance criteria utilized, for example, by the widely used KarstMod software (Frank et al.,
 326 2021). They are defined It is described as a the normalized variant of the mean squared error
 327 and the relative bias of the simulated and observed flow durations, respectively:

328

$$NSE = 1 - \frac{\sum(x_s(t) - x_o(t))^2}{\sum(x_o(t) - \mu_o)^2} \quad (12)$$

329

$$BE = 1 - \left| \frac{\sum(x_o(t) - x_s(t))}{\sum x_o(t)} \right| \quad (13)$$

330

where x_s is the simulated discharge, x_o is the observed discharge and μ_o is the observed mean.

331

The NSE performance criterion is widely used in hydrological studies and does not induce

332

counterbalancing errors. However, it should be noted that the NSE has limitations when there

333

is large variability in the data, and in some cases other performance criteria may be more

334

relevant for different datasets (see Cinkus et al., 2023a for a comparison of different

335

performance criteria).

336

4 Results and Discussion

337

4.1 Optimized simulations of measured discharge

338

The optimized simulation for the 2016 dataset yields a fit (Fig. 6) that captures both the rapid

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response of the spring discharge to rainfall events and the protracted relaxation times

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characterized by the long tails evident after rainfall events. The optimized model parameters

341

for the slow diffusive and fast conduit flow components are detailed in Table 1.

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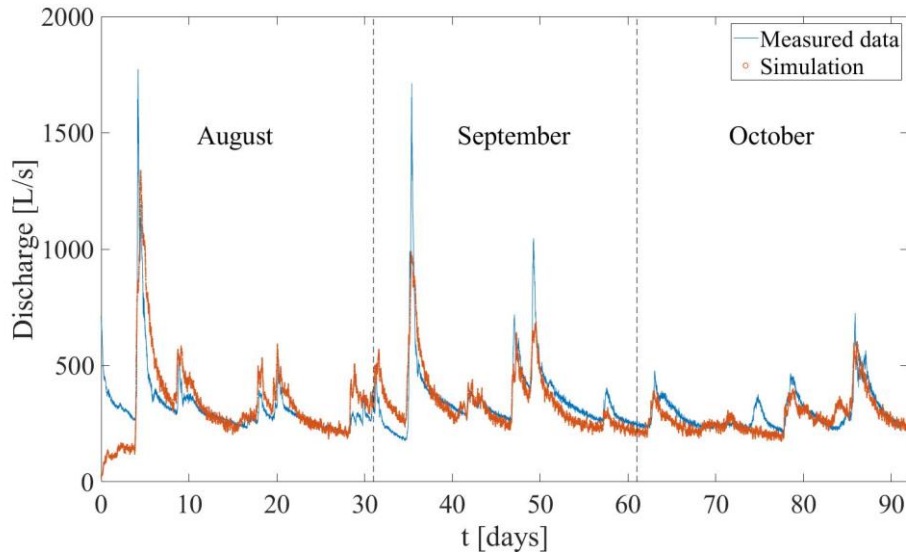
Table 1. The investigated parameter space and optimized values found. *Optimized model*

343

parameters.

Parameter	Minimum value	Optimized value	Maximum value	Description
v_{ψ}^f	<u>10 m h⁻¹</u>	360 m h ⁻¹	<u>3000 m h⁻¹</u>	Fast v_{ψ}
D_{ψ}^f	<u>10 m h⁻¹</u>	360 m ² h ⁻¹	<u>3000 m h⁻¹</u>	Fast D_{ψ}
β^f	<u>1.4</u>	1.7	<u>2</u>	Fast β
τ_2^f	<u>10³</u>	10 ⁶	<u>10⁹</u>	Fast τ_2
v_{ψ}^s	<u>0.1 m h⁻¹</u>	18 m h ⁻¹	<u>1000 m h⁻¹</u>	Slow v_{ψ}
D_{ψ}^s	<u>1 x 10⁷ m² h⁻¹</u>	3.6 x 10 ⁸ m ² h ⁻¹	<u>1 x 10⁹ m² h⁻¹</u>	Slow D_{ψ}
β^s	<u>1</u>	1.2	<u>1.8</u>	Slow β
τ_2^s	<u>10⁵</u>	10 ⁸	<u>10¹¹</u>	Slow τ_2
L	<u>1.2</u>	1.6	<u>2</u>	Tortuosity
SF_r	<u>0</u>	0.95	<u>1</u>	Slow to fast particle ratio
SF_l	<u>0 %</u>	0.01 %	<u>10 %</u>	Slow to fast particle transition likelihood

344



345

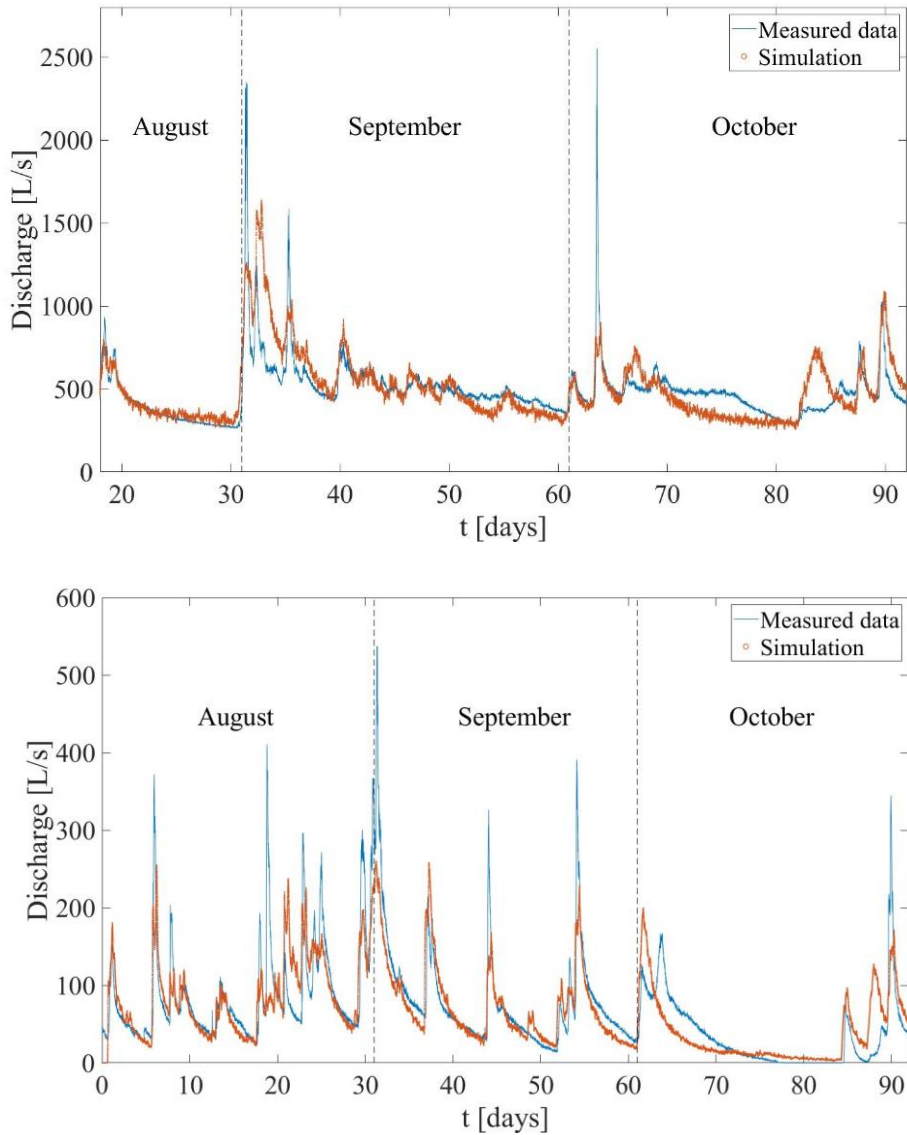
346 **Figure 6.** Measured and simulated spring discharge for the 2016 dataset ($NSE=0.5$; $BE=0.98$).

347 The differences between the fast and slow flow components, as illustrated by the respective
 348 optimized CTRW parameters, elucidate the contribution of each flow component to the
 349 volumetric discharge. The fast flow velocity parameter ($v_{\psi}^f = 360 \text{ m h}^{-1}$) is much larger than
 350 the slow flow velocity parameter ($v_{\psi}^s = 18 \text{ m h}^{-1}$), and shows showing how incoming rain
 351 can rapidly flow to the spring outlet, when travelling through the large conduits. The slow
 352 diffusive flow, however, has a much longer travel time than the fast flow. Another clear
 353 difference between the two components which is evident from the optimized values is the
 354 degree of anomalous transport. The fast flow β (1.7) and τ_2 (10^6) parameters lead to a more
 355 symmetrical contribution to the resulting discharge around the peak following the recharge
 356 event, compared to the slow flow parameters ($\beta=1.2$, $\tau_2=10^8$), which create a long tail after the
 357 discharge peak. The slow flow is also much more dispersive ($D_{\psi}^s = 3.6 \times 10^8 \text{ m}^2 \text{ h}^{-1}$)
 358 compared to the fast flow ($D_{\psi}^f = 36 \text{ m}^2 \text{ h}^{-1}$), which contributes further to the long discharge
 359 tails. The optimized parameters show a strong prominence of the slow flow over the fast flow:
 360 95% of newly introduced particles are introduced as slow particles (SF_r), with a 0.01%
 361 likelihood for a slow particle to transition at each iteration to a fast regime (SF_1). The optimized
 362 tortuosity factor of 1.6 found for the Disnergschroef system is somewhat higher than that found
 363 in some cases (~ 1.2 - 1.4 , e.g., Jouvès et al., 2017; Collon et al., 2017), but well within the range
 364 (1.1 - 3.9) reported for karst systems (e.g., Assari and Mohammadi, 2017). The higher value can
 365 be attributed to the morphology of the specific system, and also to the fact that while tortuosity
 366 is often calculated at the cave branch scale (e.g., Jouvès et al., 2017; Collon et al., 2017), the

367 CTRW-PT model uses a catchment scale tortuosity factor. The variability of tortuosity in
368 different karst morphologies should therefore be recognized when considering different
369 modeling scenarios.

370 The fit obtained for the 2016 dataset modeling is satisfactory considering the inherent
371 uncertainty associated with the input data. The three weather stations used to measure the
372 precipitation are not located inside the catchment area, and different precipitation data were
373 measured at each station, which can be seen by examining the cross-correlation coefficients
374 between the 2016 discharge and rainfall data: 0.20, 0.22 and 0.15 for stations Koerbersee,
375 Formarinalpe, Sonntag/Stein, respectively (Fig. 2a). While an average of the three stations
376 provides an acceptable estimate of the recharge over the given time period, the variability of
377 local rain events is overlooked, which may be common in the high mountainous topography.
378 ~~This is especially true in extreme rain events, in which variations of onset, duration, and total~~
379 ~~discharge of an event can induce different responses of the modeled discharge.~~

380 The same set of CTRW parameters optimized for the 2016 data – without further adjustment –
381 was employed to interpret the 2017 and 2018 datasets (Fig. 7). Both datasets show that the
382 simulated discharge after rainfall events predicts the onset, length and volume of the measured
383 discharge. This is especially true for the many discharge peaks exhibited by the 2018 data.



384

385 **Figure 7.** Measured and simulated spring discharge for the 2017 (top; $NSE=0.33$; $BE=0.98$)
 386 and 2018 (bottom; $NSE=0.63$; $BE=0.96$) datasets. Note that due to the large differences in
 387 maximum discharge between the three years, the vertical scales in Fig. 6 and in Fig. 7 are
 388 adjusted accordingly.

389

390 The recharge capacity parameter (applied to calculate the recharge function from the measured
 391 rainwater; see Eq. 11) was calculated as 0.43 and 0.45 for the 2016 and 2017 datasets,
 392 respectively. These values suggest that $\sim 40\%$ of the incoming rainfall reaches the outlet spring,
 393 with the remaining water reaching deeper parts of the aquifer that are less mobile. The drier
 394 2018 dataset, however, displayed a much lower value of 0.19. The variability of the recharge
 395 capacity parameter in different time periods, as a function of the rainfall pattern and amount,

396 highlights the importance of this parameter to the correct prediction of the system discharge
397 response to rainfall.

398 **4.2 Prominence of the slow flow component in the Disnerg Schroef system**

399 The prominence of the slow component in this karst system is evident from both the high SF_r
400 and low SF_1 . The consistency of this finding, across the three datasets (Fig. 6 and 7), agrees
401 with the analysis by Frank et al. (2021) of the recharge/discharge relationship. They observed
402 that while the flow from epikarst to conduit and matrix is highly variable and rainfall-
403 dependent, the matrix to conduit flow remains relatively constant up to a threshold. The
404 coupling of the two flow processes produces a distinctive discharge pattern characterized by a
405 sharp rapid peak after a rainfall event, followed by a long tail during recession and a return to
406 baseflow. The current analysis is similar and further emphasizes that the volumetric
407 contribution of the slow flow is substantial, particularly influencing the extended tails. In
408 contrast, the fast flow plays a more straightforward role, contributing predominantly to
409 discharge peaks by quickly expelling introduced rainwater from the system.

410 Given the importance of karst systems for human consumption, monitoring and prediction of
411 system discharge is especially important during high and low flow scenarios. These extreme
412 events can have consequences on water quality, including over-consumption during dry periods
413 and increases in turbidity and bacterial activity in high flow conditions (Pronk et al., 2006).
414 The frequency of both dry periods and heavy rainfall events has been shown to rise due to
415 climate change (Stoll et al., 2011), and this may well increase in the near future. In this context,
416 the high peaks and long tails associated with these flow conditions have proven to be the most
417 difficult to correctly predict, across different karst modeling approaches (Jeannin et al., 2021).
418 The results presented of the CTRW modeling ~~exhibit~~ the long tails associated with low
419 water flow. The 2018 dataset, in particular, which represents a dry summer compared to the
420 other two datasets, exemplifies the robustness of the model in predicting low flow conditions.

421 **4.3 The contribution of the slow and fast flow components to simulated discharge**

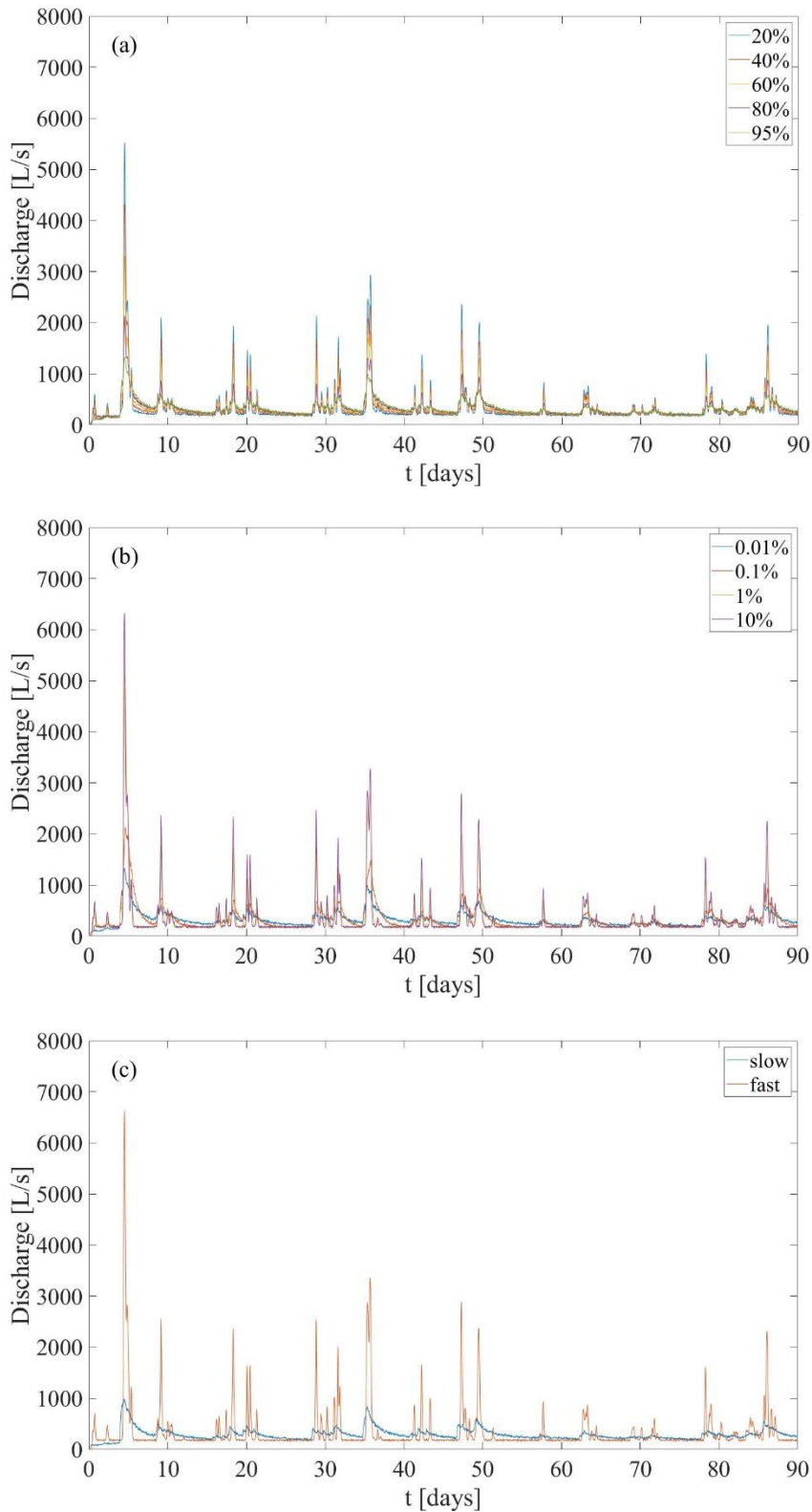
422 The results for all three datasets do not show agreement between the maximum simulated and
423 observed discharge values that are found immediately after high recharge events. ~~The better fit
424 of the long tails compared to the high peaks is evident in the improvement of the NSE values
425 presented above (0.50, 0.33, 0.63 for 2016, 2017 and 2018, respectively), when calculated for
426 the data without the prominent peaks (0.75, 0.60, 0.65 for 2016, 2017 and 2018, respectively).
427 The dry 2018 dataset is the least affected from removing the peak for the NSE calculation~~

428 ~~because the peaks are low relatively to the 2016 and 2017 datasets.~~ The fast response of
429 discharge to the incoming rain in karst systems after high recharge events has been described
430 in previous studies as a piston effect (Aquilina et al., 2006; Hartmann et al., 2014). Incoming
431 rain creates a rise in discharge before the rainwater reaches the outlet, as the increase in
432 hydraulic head pushes out water that was retained in the system before the rain.

433 This effect was shown specifically in the Disnerg Schroef system by Frank et al. (2021) which
434 measured a 2.5-hour difference between the first response of spring discharge to a rainfall
435 event, to the arrival of the rainwater to the outlet. The model herein does not explicitly take this
436 effect into account, which creates the negative bias in modeling the high peaks. While outside
437 the scope of this study, this feature might can be addressed in the future by adding a third flow
438 component, or by altering further refining the CTRW parameters of the particles present in the
439 system prior to the rainfall event to represent the increase in flow velocity.

440 To further examine the effect of both the slow and fast flow components on the simulated
441 discharge, simulations that examine the SF_l and SF_r parameters across a wider range were
442 conducted (Fig. 8). Simulations that contained only fast or slow particles (Fig. 8a), clearly show
443 that fast flow discharge responds very quickly to rainfall and produces no observable tails. In
444 contrast, the slow flow produces very long tails. It is noteworthy that the first response of the
445 slow flow is similar to the fast flow, as particles that are introduced to the system close to the
446 outlet have a very short length to travel to reach the outlet. Mixing of both flow regimes, either
447 by directly splitting the particles between the two regimes as they are introduced (Fig. 8b) or
448 by changing the transition likelihood (Fig. 8c) produces an intermediate response: as more of
449 the flow is slow, longer tails are found but the peaks are smaller. The SF_l and SF_r are thus
450 important parameters as they allow application of the CTRW-PT model to different karst
451 systems. The Disnerg Schroef system, presented here as a case study, is characterized by a thick
452 vadose zone and negligible surface runoff. Different karst systems are likely to show different
453 SF_l and SF_r parameters.

454



455

456 **Figure 8.** Simulation sensitivity to slow and fast particle contributions, based on the 2016
 457 rainfall data. Simulations that compare different SF_r values (a), different SF_l values (b) and
 458 only fast/slow particles (c), demonstrate the containing only one kind of particle (a), Slow/Fast

459 ~~ratio (b) and transition likelihood from slow to fast (c) demonstrate the~~ importance of the slow
460 flow for the observed long tails in the discharge data.

461 **5 Conclusions**

462 An analogy between partially saturated water flow in karst aquifers and anomalous chemical
463 transport is established, allowing for the adaptation of the CTRW-PT model to water flow in
464 general, and for karst discharge response to rainfall specifically. The model was calibrated on
465 one summer season of measurements of spring outlet discharge response to incoming rain; it
466 was then used to predict the long tails observed in discharge measurements following rainfall
467 events in two subsequent summer seasons.

468 The investigation of the Disnergshroef karst system has ~~showed~~shown that slow diffusive
469 flow is a predominant contributor to the volumetric discharge response to recharge events, in
470 comparison to fast conduit flow. This finding highlights the nuanced interplay between fast and
471 slow flow components in karst systems, and how they both evolve over time and as a function
472 of the recharge intensity.

473 The theoretical and practical advancements presented here offer a potentially robust tool to
474 further assess long-tailed rainfall-discharge responses in karst systems and other complex,
475 catchment-scale systems. The application of the CTRW-PT model for the Disnergshroef
476 system, specifically, has shown that it is particularly advantageous in predicting the long tails
477 observed in discharge data, compared to other modeling approaches.

478

479

480 **Data availability**

481 The data on which this article is based are available online on Zenodo:
482 <https://zenodo.org/doi/10.5281/zenodo.10635639> (Elhanati and Berkowitz, 2024).

483 **Author contribution**

484 DE, NG and BB formulated the ideas which originated the project and defined the goals and
485 aims of the study. DE developed and implemented the methodology and carried out the data
486 analysis. DE and BB drafted the initial manuscript. All authors took part in reviewing and
487 editing the final manuscript.

488 **Competing interests**

489 BB is a member of the editorial board of the journal.

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499

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