



1 **Reinforce lake water balance components estimations by integrating water isotope**
2 **compositions with a hydrological model**

3 Nariman Mahmoodi^{1,2*}, Ulrich Struck³, Michael Schneider¹ Christoph Merz^{1,2}

4 ¹ Department of Hydrogeology, Institute of Geological Sciences, Freie Universität Berlin, Berlin, Germany

5 ² Lowland Hydrology and Water Management Group, Leibniz Centre for Agricultural Landscape Research
6 (ZALF), Müncheberg, Germany

7 ³ Museum für Naturkunde, Leibniz-Institut für Evolutions- und Biodiversitätsforschung, Berlin, Germany

8 *Corresponding author, email: n.mahmoodi@fu-berlin.de

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10 **Abstract:**

11 Accurate estimation of water balance components of groundwater-fed lakes, including
12 subsurface inflow, as well as actual evaporation from lakes, poses a complex task for
13 hydrologists employing hydrological models. Hence, an alternative approach was used to
14 capture the dynamic behavior of the hydrological groundwater/surface water system, which
15 can be used for integration with the hydrological model and serves as a validation for the
16 hydrological model estimates of the water balance components. The approach, based on
17 measurements of the stable isotopes ($\delta^{18}\text{O}$ and δD) enables the quantitative estimation of the
18 individual water flux and evapotranspiration rates. An isotope-mass-balance model was used
19 to quantify lake water balances over a one-year sampling period. The approach is based on the
20 global relationship between the $\delta^{18}\text{O}$ and δD values of the precipitation and kinetic isotopic
21 fractionation in the lake water during evaporation. Assuming that the lake is hydrostatically
22 connected to the groundwater the isotope mass-balance model accounts for the quantification
23 of the **evapotranspiration** rate considering the groundwater inflow compensating the
24 evaporation loss. The study addresses the model-based quantification of subsurface-
25 groundwater inflow and evaporation losses of a young glacial groundwater lake (Lake Gross
26 Glienicke (GG), southwest of Berlin in the Havel catchment), over the period from 2015 to
27 2023 with the integrated hydrological model HydroGeoSphere. Utilizing the isotopic mass
28 balance model, HydroCalculator, under steady-state hydrologic regime conditions, the
29 evaporation-to-inflow (E/I) ratio is determined for the period of one year spanning August
30 2022 to September 2023. Employing the fully integrated hydrological model, calibrated and
31 validated under monthly normal transient flow conditions from 2008 to 2023 for the lake



32 catchment, subsurface, and groundwater inflows to the lake are calculated and compared to
33 the calculated E/I ratios based on the isotopic measurement of the lake water. Isotopic
34 signatures of surface water, groundwater, and rainwater ($\delta^{18}\text{O}$ and δD) confirm **a flow-**
35 **through type for the lake**. The calculated E/I ratio for GG Lake is around 40%. The calculated
36 evaporation for the years 2022 and 2023, within the isotopic mass balance model framework
37 ($E_{\text{iso}22} = 601$ mm, $E_{\text{iso}23} = 553$ mm), aligns well with the **actual evaporation from the lakes**
38 calculated by the HGS model ($E_{\text{HGS}22} = 688$ mm, $E_{\text{HGS}23} = 659$ mm). The change in the ratio
39 of evaporation to inflow (E/I) leads to a significantly improved estimation of evaporation
40 rates after correction for temperature fluctuations and inflow data from previous years (2015-
41 2021). With a correlation coefficient of 0.81, these revised estimates show a high degree of
42 agreement with the evaporation rates predicted by the **HydroGeoSphere (HGS)** model for the
43 corresponding years. Despite the uncertainties associated with the analysis of the water
44 isotope signature, its integration into the hydrological model serves to validate the
45 hydrological model calculations of the water balance components.

46 **Keywords:** HydroGeoSphere, HydroCalculator, Lake Water Exchange, Evaporation Loses,
47 **Stable Isotope**, Gross Glienicke Lake

48

49 1. Introduction

50 Hydrological models have undergone substantial advancements in past decades (Singh, 2018;
51 Herrera et al., 2022), but still face unsolved problems and uncertainties in depicting
52 hydrological processes (Liu and Gupta, 2007; Renard et al., 2010). Recently, a wide range of
53 monitoring and modeling techniques have emerged for investigating water fluxes at different
54 scales (Fekete et al., 2006, Windhorst et al., 2014). However, limitations in the hydrological
55 model parametrizations lead to insufficient quantification of water flows, and therefore a
56 quantitatively and qualitatively incorrect interpretation of hydrodynamic processes and, as a
57 result, inaccurate assumptions for water management purposes (Müller Schmied et al., 2014).
58 Improving the informative value of the models, representing complex hydrological processes
59 is needed to enhance the applicability of the models for future estimations and scenario
60 analyses. The optimal adaptation of hydrological models to real conditions for a precise
61 determination of water balance components is often considered unattainable within the
62 current technical possibilities due to the overwhelming amount of work associated with field
63 measurements. Particularly the quantification of groundwater-surface water exchange using



64 the hydrological models faces pronounced uncertainties in considering geostructural
65 heterogeneities in different scales. To validate the model results, arduous monitoring surveys
66 are required to measure for example the groundwater-surface water interactions along rivers'
67 banks or lakes' shorelines (Partington, 2020). Hence, a combination of hydrogeological
68 modeling, field measurements, and innovative isotopic-based studies along with appropriate
69 linkage between these approaches will be a concrete way to achieve optimal parameterization
70 and validation capabilities for modeling hydrological processes in complex geohydraulic
71 systems.

72 Recent studies show that the stable water isotope mass balance on different water sources
73 together with the numerical models improve the model performance in simulating the
74 interactions between groundwater and surface water (e.g., Jafari et al., 2021). The isotopic
75 insights enhance hydrogeologists' efforts to calculate water balance components such as the
76 groundwater inflow to the surface water resources and water losses due to evaporation
77 (Skrzypek et al., 2015; Vyse et al., 2020). This method is based on the fractionation of heavier
78 isotopes caused by evaporation from surface water, provoking a disparity in isotopic
79 composition between groundwater and surface water. However, a limitation of this approach
80 is that the stable water isotope mass balance **is restricted to the sampling time**, making it
81 incapable of accounting for the transient behavior of groundwater-surface water exchange
82 over different time periods. Although water isotope tests can describe the changes in water
83 fluxes in specific time frame intervals (e.g. monthly), **deficiency in providing spatial**
84 **exchanges between groundwater and surface** water can be also introduced as their limitation.
85 These gaps can be addressed by integrating water isotope analyses with physical-based
86 hydrogeological models.

87 Water isotope **analyses** are helpful techniques to evaluate the model's performance. For
88 instance, Ala-Aho et al. (2015) assess the hydrogeological model performance by comparing
89 the simulated groundwater inflow to lakes in the middle of Finland with calculated recharge
90 by water isotope analyses.

91 In the northeast of Germany, groundwater levels and landscape runoff have largely been in
92 decline for over three decades (Lahmer 2003; Germer et al., 2011; Merz and Pekdeger, 2011);
93 regional climate studies suggest further decreases over the next decades (Gerstengarbe et al.,
94 2003, 2013). Thus, water resource management for this region requires a thorough assessment
95 of possible adaptations and measures to counteract or mitigate severe consequences, such as
96 decreasing groundwater heads and surface water levels and declining groundwater and surface



97 water quality. The development of integrated management schemes for groundwater-
98 dependent ecosystems such as lakes under climate changes, requires a more comprehensive
99 understanding of hydrological dynamics and a better estimation of ecologically relevant water
100 fluxes are of prime importance. Therefore, an alternative approach was developed to capture
101 the complex behavior of the hydrological groundwater-surface water system. This approach
102 can be integrated with hydrological models to improve parameterization and validate model
103 calculations in water balance components.

104

105 2. Materials and methods

106 2.1 Study area

107 Gross Glienicke Lake (GGS) with an area of 0.59 km² and a maximum depth of 10 meters is
108 located in Berlin-Brandenburg state, Germany (30–87 m.s.l., Fig. 1a). It is a young glacial
109 lowland lake that is exclusively fed by groundwater. The lake's water levels have shown
110 significant seasonal variability (around 0.4 m) over recent decades (Fig. 2). Since 2014 the
111 lake's water level has faced severe drops (Fig. 2) around 1.28 meters. GGS as a seepage lake
112 (lake without an outlet) is surrounded by low-density residences (Fig. 1). In the north and
113 northwestern areas, grassland and farmland are the dominant surface cover and directly overly
114 sandy soils. The aquifers are recharged in the Döberitzer-Heide region where fine sandy soil
115 with a hydraulic conductivity ranging from 8×10^{-5} to 12×10^{-5} m/s can be found according to
116 the lab analysis. The root zone within the grassland ranges in depth from the surface to 30 cm.
117 The groundwater monitoring measurements illustrate a smooth hydraulic head gradient from
118 West to East, highlighting connections between the lake and the aquifer recharge area from
119 the Döberitzer-Heide region (Fig. 3). On the east side of the lake catchment, a regulated river,
120 the Havel, has been flowing from northeast to southwest. Continuous stratigraphic units have
121 been delineated throughout the lakes' catchment based on the geological features information
122 collected from 480 boreholes (Fig. 2, The Federal Institute for Geosciences and Natural
123 Resources - BGR 2022). The geology in the study area is formed by a series of layered
124 Pleistocene and Tertiary sediments that are approximately 150 to 200 m thick, with a lower
125 confining bed of Oligocene marine Rupel clay. The series consists of a complex interplay of
126 glacial deposits from the Pleistocene and permeable marine and limnic sediments of the
127 Upper Oligocene and Miocene. The series can be divided into an upper unconfined aquifer
128 system of shallow Weichselian and late Saalian sediments. In general, a shallow (i.e., 5 to 10

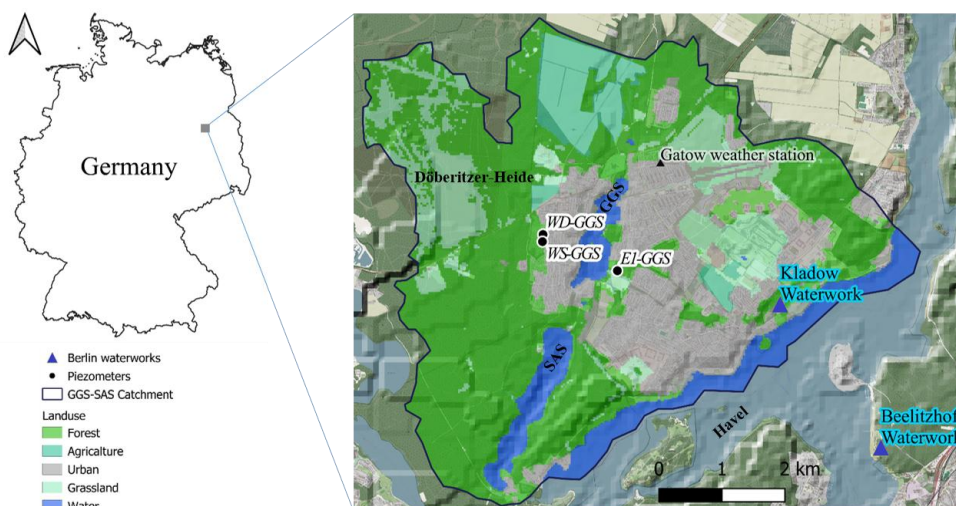


129 m) unconfined aquifer is separated from the thick (140 to 190 m) lower confined aquifer by a
130 15 to 20 m thick layer of Saalian sediments. The confined and unconfined aquifers consist of
131 multiple permeable sediment layers partially disconnected by layers of till, but still
132 hydraulically connected. The hydraulic connection to the lakes is mainly controlled by these
133 aquifer layers. Underneath these sediments is a thick confined aquifer system of the early
134 Saalian and Elster layers, and Upper Oligocene and Miocene sediments. The first shallow,
135 unconfined aquifer in the catchment area is characterized by highly permeable glacial sand
136 and gravel deposits (Holocene and Weichselian). A till layer (Weichselian age, Fig. 3) is
137 found in the underlying layers. The till is underlain by late Warthe sandy sediments forming
138 the second aquifer.

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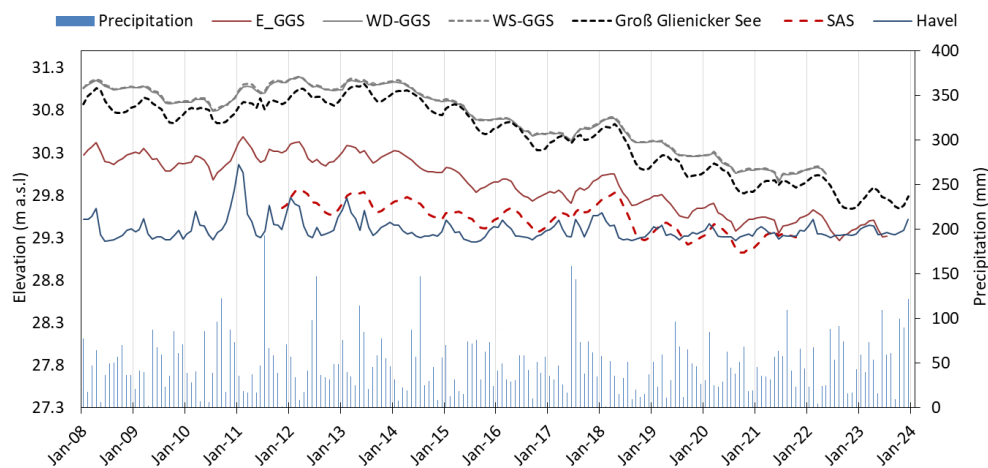
140 **2.2 Available meteorological data**

141 From 1990 to 2023, radar-based CER v2 data (The Central Europe Refined Analysis version
142 2, details on the data pre- and post-processing are provided by Jänicke et al., 2017) generated
143 a mean daily temperature of 10.4 °C and average annual precipitation of 612 mm, with an
144 average annual **actual evapotranspiration (PET)** of 639, 646, and 670 mm for farmland and
145 grassland, forest, and urban areas respectively. The annual mean humidity in Gatow station
146 varies from 50% to 70% over the last two decades (2000-2023). During the hydrological year
147 of the survey (August 2022 to September 2023), the mean precipitation, temperature, and
148 humidity in the study region were **51.9 mm**, 12.3 °C (Potsdam weather station, DWD, 2024;),
149 and 69 % respectively (recorded in Gatow weather station of The Berlin Measurement
150 Network (MEVIS, Fig. 1). Precipitation data as one of the boundary conditions in the
151 modeling work has been obtained from the Potsdam station of the German Weather Service
152 (DWD, 2024).



153

154 **Fig. 1.** Location of the study area, highlighting Gross Glienicke Lake (GGS), Sacrow Lake (SAS), Havel
155 channel, piezometers on the east (E-GGS) and west (WD-GGS and WS-GGS) side of GGS, Berlin waterworks,
156 and land use classifications. © OpenStreetMap contributors 2023. Distributed under the Open Data Commons
157 Open Database License (ODbL) v1.0..

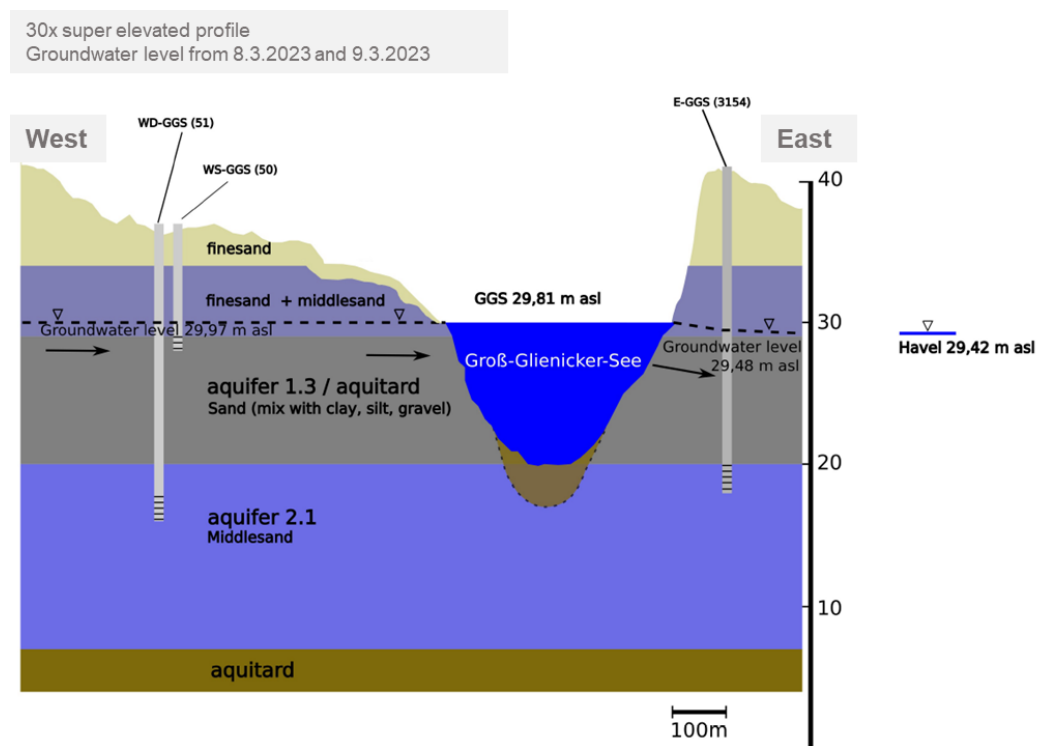


158

159 **Fig. 2.** Lakes water level fluctuations and precipitation variations during the period of 2008 to 2023.

160

161



162

163 **Fig. 3.** Conceptual cross-section of the aquifer demonstrating the geological structure, the hydraulic head, and
164 water flow direction from the groundwater recharge area towards Gross Glienicke Lake (GGS) and the
165 groundwater discharge area with a lower altitude. WD-GGS, WS-GGS, and E-GGS are the piezometers on the
166 west and east sides of GGS.

167

168 2.2 Stable isotope analysis

169 Surface water samples were collected for one year (from August 2022 to September 2023) on
170 a monthly time interval from GGS and three piezometers installed in the first two aquifers,
171 encompassing the lakes, and from two rainwater samplers. The total depth and well water
172 volume of the monitoring well, and the stability of in-situ parameters such as temperature,
173 pH, and electrical conductivity (EC) were monitored as guidance of appropriate timing for
174 water sampling from the piezometers. All water samples collected in clusters within two-day
175 excursions were filtered through a membrane filter (0.2 and 0.45- μm pore) and stored at 6 °C
176 to prevent evaporation before laboratory analysis. Stable isotope ratios of oxygen ($^{18}\text{O}/^{16}\text{O}$)
177 and hydrogen ($^2\text{H}/^1\text{H}$) in H_2O in water samples were measured with a PICARRO L1102-i
178 isotope analyzer. The L1102-i is based on the WS-CRDS (wavelength-scanned cavity ring-



179 down spectroscopy) technique (Gupta et al., 2009). Measurements were calibrated by the
180 application of linear regression of the analyses of IAEA calibration material VSMOW,
181 VSLAP, and GISP. The stable isotope ratios of oxygen and hydrogen are expressed in the
182 conventional delta notation ($\delta^{18}\text{O}$, δD) per mil (‰) versus VSMOW. For each sample 6
183 replicate injections were performed and arithmetic average and standard deviations (1 sigma)
184 were calculated. The reproducibility of replicate measurements is generally better than 0.1 ‰
185 for oxygen and 0.5 ‰ for hydrogen.

186

187 2.3 Isotope mass balance model

188 The evaporation loss from a lake such as GGS Lake can be calculated by knowing the
189 transient stable water isotope compositions of inflow and moisture in ambient air and climate
190 data (air temperature and humidity) for the specific period of time and considering a steady-
191 state hydrologic condition (no additional water inflows, Tweed et al. 2009; Gibson and Reid,
192 2010). The isotope mass balance model (Hydrocalculator) whose capability has been verified
193 through various field experiments globally (Skrzypek et al. 2015; Vyse et al., 2020) was
194 applied to estimate evaporation over inflow ratio (E/I) for the GGS Lake in the steady state
195 condition. The differences between stable isotope compositions of water samples reflect the
196 isotopic phases: enrichment (heavier isotope) or dilution (lighter isotope). Hence, a series of
197 time-based analyses enables the assessment of evaporation progress. Climate data from
198 nearby weather stations (Gatow and Potsdam) were utilized to address uncertainties arising
199 from the distance to the points of water samplings (Gibson and Reid, 2014; Skrzypek et al.
200 2015). The stable isotope composition of moisture in ambient air (δ_{air}) is estimated from the
201 mean monthly weighted averages from the stable isotope composition of precipitation (δ_{pcp})
202 of GNIP station (GNIP/Berlin (DWD, BFG, BGR & HHZM, Stumpp et al. 2014 and Schmidt
203 et al. 2020) which were corrected by local precipitation stable isotope composition. The δ_{air} is
204 calculated based on the rain and rain-LEL as follows (Gibson and Reid, 2014):

$$205 \delta_{\text{air}} = (\delta_{\text{pcp}} - \epsilon^+) / (1 + \epsilon^+ \times 10^{-3}) \quad \text{Eq.}$$

206 1

207 where ϵ^+ is an isotope fractionation factor that is solely temperature-dependent. ϵ is the total
208 fractionation factor, and equals the sum of the equilibrium isotope fractionation factor ϵ^+ , as
209 given above plus the kinetic isotope fractionation factor ϵ_k (Gibson and Reid, 2010):



210 $\varepsilon = \varepsilon^+ / (1 + \varepsilon^+ \times 10^{-3}) + \varepsilon_k$ Eq.

211 **2**

212 The kinetic fractionation ε_k is defined as (Gat 1995):

213 $\varepsilon_k = (1 - h) \times C_k$ Eq.

214 **3**

215 According to Gonfiantini, 1986 and Araguas-Araguas et al., 2000, the kinetic fractionation
 216 constant (C_k) is 12.5 percent for δD and 14.2 percent for $\delta^{18}O$. Air relative humidity (h) is
 217 given as a fraction.

218 Based on the local climate conditions the enrichment of stable isotope compositions can be
 219 limited. According to Gat and Levy (1978) and Gat, (1981), this **limitation threshold (δ^*)** can
 220 be estimated by considering air humidity (h), δ_{air} , and a total enrichment factor (ε).

221 $\delta^* = (h \times \delta_{air} + \varepsilon) / (h - \varepsilon \times 10^{-3})$ Eq.

222 **4**

223 When this limitation exceeds, further evaporation does not result in isotope enrichment.

224 The ratio of evaporation over inflow (E/I) can be calculated using the following reformulated
 225 equation (e.g. as by Mayr et al. (2007)) under steady-state hydrological conditions. E/I is the
 226 fraction of inflowing water evaporated from GGS Lake:

227 $E/I = ((\delta_{inflow} - \delta_{outflow}) / (\delta^* - \delta_{inflow}) \times E_s)$ Eq. 5

228 enrichment slope (E_s) is defined by Welhan and Fritz, 1977 and Allison and Leaney, 1982
 229 accordingly:

230 $E_s = (h - (\varepsilon \times 10^{-3})) / (1 - h + (\varepsilon \times 10^{-3}))$ Eq.

231 **6**

232 The model calculates the evaporative losses based on the theory behind the Craig–Gordon
 233 model (Gibson and Reid (2014)). The variables used in the Hydrocalculator model are listed
 234 in Table 1.

235 **Table 1.** The list of variables used in the Hydrocalculator model

Variable	Description	Unit
T	temperature	°C
h	air relative humidity	-



δ_{air}	stable isotope composition of moisture in ambient air	%
δ_{pcp}	stable isotope composition of precipitation	%
LEL	slope of the local evaporation line	
ϵ	total isotope fractionation	%
ϵ^+	equilibrium isotope fractionation factor	%
ϵ_k	kinetic isotope fractionation factor	%
C_k	kinetic fractionation constant	
δ^*	limiting isotopic composition	%
E/I	Evaporation over inflow ratio	%
δ_{inflow}	stable isotope composition of inflow (groundwater)	%
$\delta_{outflow}$	stable isotope composition of outflow (lake)	%
E_s	enrichment slope	-

236

237 2.4 Model domain configuration and boundary conditions

238 2.4.1 Surface – subsurface flows

239 The HydroGeoSphere (HGS) modeling code (Aquanty Inc, 2023) was used to simulate the
 240 hydrological processes in the GGS Lake catchment. HGS is a 3-D, fully integrated, and
 241 physically-based model with the capacity to simulate the interwoven flow mechanisms of
 242 subsurface and surface water by coupling solutions obtained from the diffusion-wave of the
 243 two-dimensional, depth-integrated diffusion-wave of the Saint Venant equation governing
 244 surface water flow (Eq. 8, Viessman Jr. and Lewis, 1996) and the Richards' equation
 245 governing three-dimensional unsaturated and saturated subsurface flows (Eq. 9).

246

Eq. 7

$$247 \frac{\partial \phi_0 h_0}{\partial t} - \frac{\partial}{\partial x} \left(d_0 K_{0x} \frac{\partial h_0}{\partial x} \right) - \frac{\partial}{\partial y} \left(d_0 K_{0y} \frac{\partial h_0}{\partial y} \right) + d_0 \Gamma_0 \pm Q_0 = 0$$

248 ϕ_0 represents the porosity (dimensionless) of the surface flow domain, which varies based on
 249 the presence of rills and obstructions. h_0 stands for the water surface elevation (L). t denotes
 250 time (T). d_0 indicates the depth of flow (L). K_{0x} and K_{0y} represent surface conductance. Γ_0 is
 251 the water exchange rate ($L^3 L^{-3} T^{-1}$) occurring between the surface and subsurface systems.
 252 Q_0 represents external sources or sinks.

253 The interaction between the two flow domains is facilitated by the exchange term Γ_0 through:

254

Eq. 8



$$255 \quad d_0 \Gamma_0 = \frac{k_r K_{zz}}{l_{exch}} (h - h_0)$$

256 k_r symbolizes the exchange's relative permeability. K_{zz} represents the saturated hydraulic
257 conductivity in the vertical direction. l_{exch} corresponds to the coupling length.

258 *Eq. 9*

$$259 \quad \nabla \cdot (W_m \mathbf{q}) + \sum \Gamma_{ex} \pm Q = W_m \left(\frac{\partial}{\partial t} \right) (\theta_s S_w)$$

260 In the given context: W_m (dimensionless) represents the volumetric porosity fraction within
261 the porous media domain. Γ_{ex} stands for the volumetric exchange rate ($L^3 L^{-3} T^{-1}$) occurring
262 between the porous media and other flow domains. Q denotes the source or sink term. t
263 signifies time (T). θ_s corresponds to porosity (dimensionless). S_w refers to the degree of water
264 saturation (dimensionless).

265 The flow rate q ($L T^{-1}$) is portrayed as:

266 *Eq. 10*

$$267 \quad \mathbf{q} = -K \cdot k_r \nabla h$$

268 K signifies the hydraulic conductivity ($L T^{-1}$). k_r represents the relative permeability
269 (dimensionless), which is dependent on water saturation. h corresponds to the hydraulic head
270 (L), calculated as the sum of the elevation head and pressure head.

271 The three-dimensional surface-subsurface flows in porous media and saturated zones were
272 solved with the control volume finite element method. Nonlinear equations were linearized
273 using Newton-Raphson and solved iteratively at each time step for the entire hydrologic
274 system.

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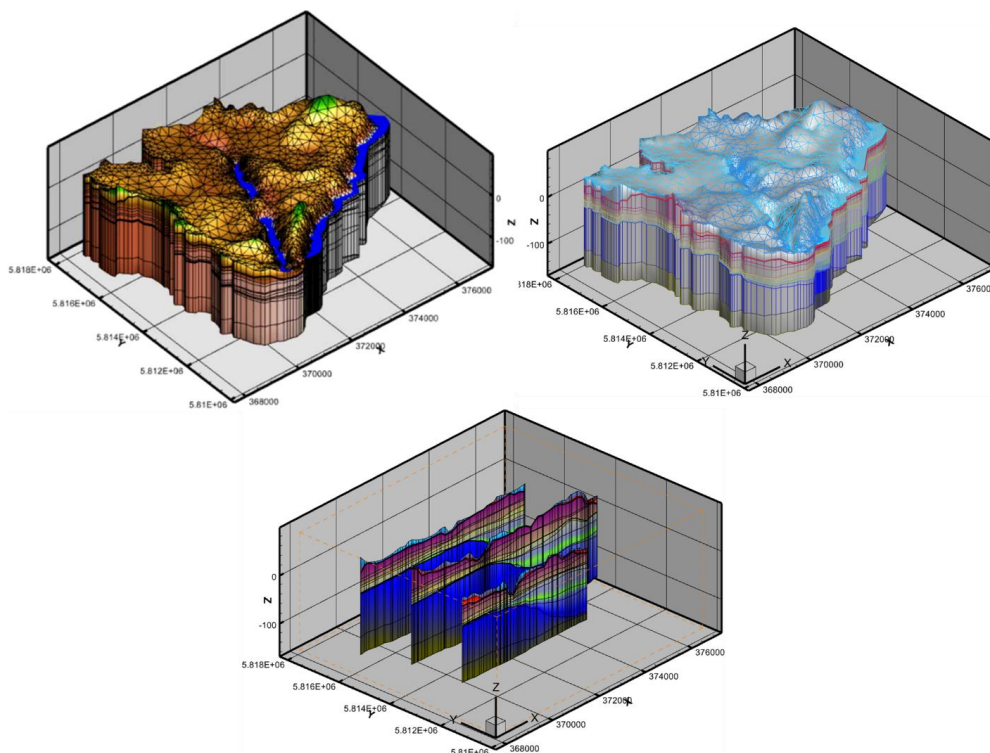
276 **2.4.2 Evapotranspiration**

277 The evapotranspiration process needs specific prerequisites for accurate parameterization as it
278 is treated to play a dual role in the HGS as both a boundary condition and a distinct domain.
279 Within this framework, the evapotranspiration fluxes encounter a restriction governed by a
280 potential evapotranspiration flux (PET) which is defined by the modeler. The PET values are
281 designated a boundary condition, serving its purpose on the surface domain. With each
282 subsequent time step, a condition emerges, if the calculated actual evapotranspiration (AET)



283 surpasses the PET, then the PET value is employed as a flux directed toward the relevant
284 model faces. Conversely, if the calculated AET falls short of the PET, the computed AET
285 value itself becomes the applied flux. Additional details on the evapotranspiration process
286 formulations within the HGS model are presented in Kristensen and Jensen (Kristensen and
287 Jensen, 1975). The two-dimensional PET database used in this research is calculated using the
288 energy balance method and covers the period 2000 - 2022. The method is a balance of the
289 energy terms which are the net radiation, the change in the heat content of the lake, and the
290 latent and sensible heat fluxes. The equation is based on measurements of global radiation, air
291 and water temperature, cloud cover, and vapor pressure. The latent heat flux, which represents
292 the energy used for evaporation, was determined by subtracting the sensible heat fluxes and
293 the change in the heat content of the lake from the net radiation. The evaporation rate was
294 then calculated by dividing the latent heat flux by the latent heat of vaporization of the water.
295 A maximum evaporation threshold of 15 mm/day was set. More details are given by Ölmez et
296 al., 2024.

297 The simulation domain encompasses the entire GGS Lake catchment (Fig. 4) which is defined
298 based on the surface topography considering the equipotential lines derived from the lakes'
299 levels and measurements of the hydraulic head surrounding the lakes (piezometers). The
300 surface topography across the catchment was produced by stitching a digital elevation model
301 (DEM) from The Shuttle Radar Topography Mission (SRTM) with a resolution of 30 m, and
302 the bathymetry data of GGS (Wolter, 2010) and Sacrow Lake (SAS) (Lüder et al., 2006,
303 Bluszcz et al., 2008). Due to the high vegetation density, flat elevations, and the substantial
304 hydraulic conductivity of the predominantly sandy soil, the absence of river formation is
305 currently observed in the catchment. The foundational 2-D triangular mesh supporting the
306 comprehensive 3-D triangular prism grid within the HGS model was created using AlgoMesh
307 (Merrick, 2017). Each 2-D mesh layer encompasses a total of 2837 mesh nodes and 5300
308 triangular finite elements (Fig. 4). The complete 3-D model (Fig. 4) grid extends the 2-D
309 mesh across 15 subsurface layers, broadly categorized as one soil layer, 14 Quaternary
310 material layers, and one competent bedrock layer (Rupel clay).



311

312 **Fig. 4.** Hydrostratigraphic units and enlarged view of the mesh within the Gross Glienicke
313 Lake catchment

314 Spatially distributed land cover data (Fig. 1) were utilized to capture a broad range of factors
315 influencing evapotranspiration and overland flow, including evaporation depth, root depth,
316 leaf area index (LAI), surface roughness, rill storage height, and obstruction storage height.
317 Specific parameters for evapotranspiration (ET) and overland flow are tailored to each land
318 cover type. To accurately reflect the impact of vegetation growth on water demand through
319 evapotranspiration, the Leaf Area Index (LAI) during winter (January) and summer (July)
320 using the Sun Sacan device type SS1 were measured, capturing both maximum and minimum
321 current LAI values. The measured LAI indices were then compared with data from the
322 MCD15A2H Version 61 Moderate Resolution Imaging Spectroradiometer (MODIS), which
323 provides a 4-day composite with a pixel size of 500 m for January and July (Myneni et al.,
324 2021). Corrected monthly average MODIS LAI values for each land cover type, spanning
325 from 2000 to 2023, were subsequently integrated into the HGS model.

326 2.4.3 Unsaturated zone



327 The top subsurface layer in the 3-D mesh with spatial varying depths shows the distribution of
328 soil materials across the catchment. The soil data were obtained from the soil map with a
329 scale of 1:200,000 (BUEK200) which was prepared by the Federal Institute for Geosciences
330 and Natural Resources (BGR, 2007). The soil samples were collected from various depths,
331 extending up to 3 meters, at 10 different sites, primarily in the groundwater recharge area
332 (Döberitzer-Heide region) and natural conservation zones. The sampling locations were
333 selected based on soil types. The percentages of sand, silt, and clay for each soil type were
334 determined in the laboratory to classify the soil textural types, using the United States
335 Department of Agriculture (USDA) soil textural calculator. A set of 2 soil textural types,
336 sand, and loamy sand has been recognized. Unsaturated soil hydraulic parameters and soil
337 moisture retention properties required for the van Genuchten application with the HGS model
338 were uniquely estimated for each soil type using the ROSETTA program, version 1 (Schaap
339 et al., 2001).

340 Underlying the soil layers are 14 Quaternary geology layers that overlie bedrock. To represent
341 the topography of the subsurface in the lake catchment, relevant data was extracted from the
342 groundwater model provided by Berliner Wasserbetriebe. This model (software FEFLOW)
343 was calibrated in 2012 and updated in 2013 (BWB, 2012 and 2013) using measured data from
344 the year 2010. The model focuses on analyses of the waterworks at Beelitzhof, Tiefwerder,
345 and Kladow. It, therefore, covers areas along both banks of the river Havel. Additional
346 datasets from boreholes were merged into a single surficial geology dataset using the
347 Rockware model setup for the GGS Lake catchment (Hermanns, 2022). The initial hydraulic
348 conductivity values for each type of Quaternary material were taken from the FEFLOW
349 model. The hydraulic properties of the unsaturated zone were manually adjusted during
350 manual model calibration.

351 **2.4.4 Groundwater – lake levels loggers**

352 A total of 8 groundwater monitoring wells scattered within the catchments, along with two
353 loggers set on the lakes, provide a well spatially distributed dataset of groundwater-lake level
354 dynamics for evaluating model simulations. The groundwater monitoring wells were selected
355 based on location, catchment area, and data availability spanning from 2000 to 2023. GGS
356 has been monitored since 1964. Moreover, within the study catchment, the regulated flow
357 system of the river Havel is maintained to facilitate water conveyance. Since 1980, an
358 established logger has been operational to meticulously monitor the water level dynamics
359 within this river. For the presented study particular interest lies in loggers No. 51, 52 (WD-



360 GGS and WS-GGS), and 3154 (E-GGS). WD-GGS(50) and WS-GGS(51) belong to two
361 different aquifers (shallow(WS-GGS) and deep aquifer (WD-GGS) and are situated on the
362 western side of GGS (Brandenburg, Fig. 3). These loggers in the recharge area of the GGS
363 lake consistently maintain water levels averaging 15-20 cm higher than the GGS.
364 Additionally, logger E-GGS, located close to the eastern shoreline downstream of GGS
365 (Berlin), consistently registers water levels averaging 30-40 cm lower than the GGS lake (Fig.
366 3).

367 **2.4.5 Groundwater abstractions**

368 Two major drinking water supply systems, Kladow and Beelitzhof, located alongside Havel
369 on the southwest side of Berlin have been in operation since 1888 and 1932 respectively by
370 BWB. Kladow comprises 16 wells up to 93 meters deep and a maximum pumping rate of
371 30,000 m³/day, while Beelitzhof has 85 wells up to 170 meters deep and a maximum pumping
372 rate of 160,000 m³/day. To assess the impact of groundwater withdrawals from deeper layers,
373 the model domain was extended to a depth of 150 meters below sea level. According to
374 studies BWB, upto 80 percent of the water extracted by Kladow originates from bank
375 filtration along the river Havel. The remaining 20 percent of the extracted water originates
376 directly from groundwater recharge as well as outflow from GGS. As various water resources
377 contribute to the overall drinking water production in the main waterworks in this area
378 (Beelitzhof, located on the western side of the Havel), a detailed analysis was conducted to
379 assess the share of the GGS Lake catchment. The analysis involved the implementation of
380 distinct scenarios within the hydrologic model.

381 **2.4.6 Model evaluations**

382 This study emphasizes the importance of a multifaceted approach to evaluate hydrological
383 model performance, utilizing both traditional and innovative methodologies. Initially to
384 evaluate model performance the simulated seasonal and long-term groundwater and lake level
385 fluctuations will be compared to observed water levels of the lakes and piezometers around
386 the lakes. The performance evaluation of hydrological models commonly relies on various
387 metrics such as the Nash-Sutcliffe efficiency (NSE), percent bias (PBIAS), root mean squared
388 error (RMSE), and the Kling-Gupta efficiency (KGE). The KGE, introduced by Gupta et al.
389 (2009), offers a comprehensive assessment by considering bias, correlation, and variability
390 separately. Given the specific hydrological focus of each metric, a multi-metric approach was
391 adopted for calibrating the HGS model parameters, as demonstrated to efficiently balance



392 model performance by previous studies (Pfannerstill et al., 2014; Mahmoodi et al., 2020). For
393 model assessment, NSE, PBIAS, RMSE, and KGE were employed as performance metrics on
394 a monthly basis. Calibration runs were evaluated based on predefined thresholds for NSE
395 (0.65), PBIAS (-25% to 25%), and KGE (0.65) to identify the most suitable configurations.
396 The calibration process was carried out manually due to the model's long execution time and
397 limited computational capacity. Emphasis was placed on calibrating model parameters of the
398 unsaturated zone which governs water movement into the soil and subsequently into or out of
399 the aquifer. The initial hydraulic conductivity values for each type of soil were determined
400 from existing literature (Steidl et al 2023) and lab analysis and later manually adjusted during
401 model calibration. The model parameterization for the saturated zone was initially derived
402 from the FEFLOW model calibrated by the **BWB** (BWB, 2012/2013). The calibration and
403 validation periods chosen for the simulation runs were 2008-2018 and 2019–2023,
404 respectively, preceded by an eight-year spin-up phase before 2008 to reach quasi-steady state
405 condition fitting to the conditions in 2008.

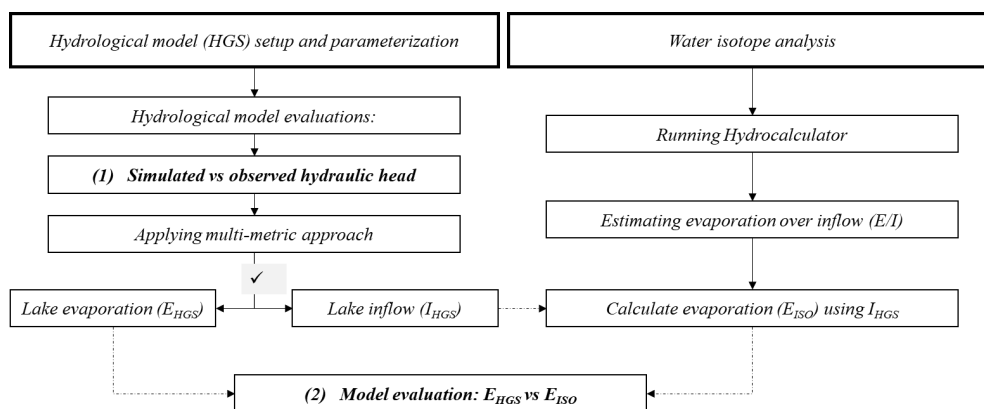
406 To evaluate the performance of the HydroGeoSphere (HGS) model on different angles, a
407 detailed assessment involving the simulation of the inflow to GGS Lake (denoted as I_{HGS}) was
408 undertaken. This parameter (I_{HGS}) was subsequently used as a testing parameter to evaluate
409 the model's performance in calculating evaporation rates for the years 2022 and 2023 using **an**
410 **independently determined E/I ratio**. The evaporation rate (E_{ISO}) can be expressed as:

411 *Eq. 11*

$$412 \quad E_{ISO} = \frac{1}{A} \cdot I_{HGS} \cdot P$$

413 Where A is the area of the lake water body (m^2), I_{HGS} represents the **annual inflow** to the lake
414 (m^3) and **P is the percentage of losses** of inflow due to evaporation derived from the isotope
415 analysis (E/I). Figure 5 shows the methodology used to evaluate the model performance
416 across different dimensions. The underlying assumption for this evaluation is that an accurate
417 simulation of inflow to the lake by the HGS model (I_{HGS}) would yield evaporation rates (E_{ISO})
418 comparable to those calculated by the HGS model (E_{HGS}). Thus, the consistency between
419 evaporation estimates derived from both approaches serves as a validation of the HGS
420 model's capability to simulate other water balance components precisely.

421



422

423 **Fig. 5.** Flow chart of the methodology employed to evaluate the model performance

424 The well-captured inflow and subsequent evaporation rates for the years 2022 and 2023 by
425 the HGS model, allow us to extend this approach for estimating evaporations during the
426 earlier period from 2015 to 2021. This period is crucial as it encompasses years without water
427 isotope analyses, during which significant drops in lake and groundwater levels were
428 observed. However, the E/I ratio derived from recent years (2022 and 2023) cannot be
429 directly applied to earlier years due to variations in temperature and inflow, which are key
430 factors influencing isotopic signatures (dilution and enrichment). To **adjust the E/I ratio** for
431 earlier years, we incorporated annual temperature variations and inflow data into our model.
432 Specifically, we compared **the temperature and inflow of each specific year (y_x)** to the
433 corresponding values from 2022 and 2023 (y_{22-23}). This comparison yielded ratios for
434 **temperature ($T_{y_x}/T_{y_{22-23}}$)** and inflow ($I_{y_{2023}}/I_{y_x}$), which were used to modify the E/I ratio
435 accordingly. For instance, to apply the $E/I_{y_{22-23}}$ to the year 2015, we multiplied the $E/I_{y_{22-23}}$
436 ratio by the temperature ratio ($T_{y_{15}}/T_{y_{22-23}}$) and the inflow ratio ($I_{y_{2023}}/I_{y_{15}}$). A temperature
437 ratio greater than 1 indicates higher temperatures in 2015 compared to 2023, suggesting a
438 higher E/I ratio, greater evaporation, and enrichment. An inflow ratio greater than 1,
439 indicating lower inflow in 2015 compared to 2023, would lead to a greater E/I ratio, reflecting
440 greater evaporation and enrichment. **The adjusted E/I ratios were then applied to refine the**
441 **initial evaporation estimates from the isotopic mass balance model.** These revised evaporation
442 estimates were subsequently compared to the evaporation rates calculated by the HGS model
443 for the period 2015-2021.

444

445 3. Results

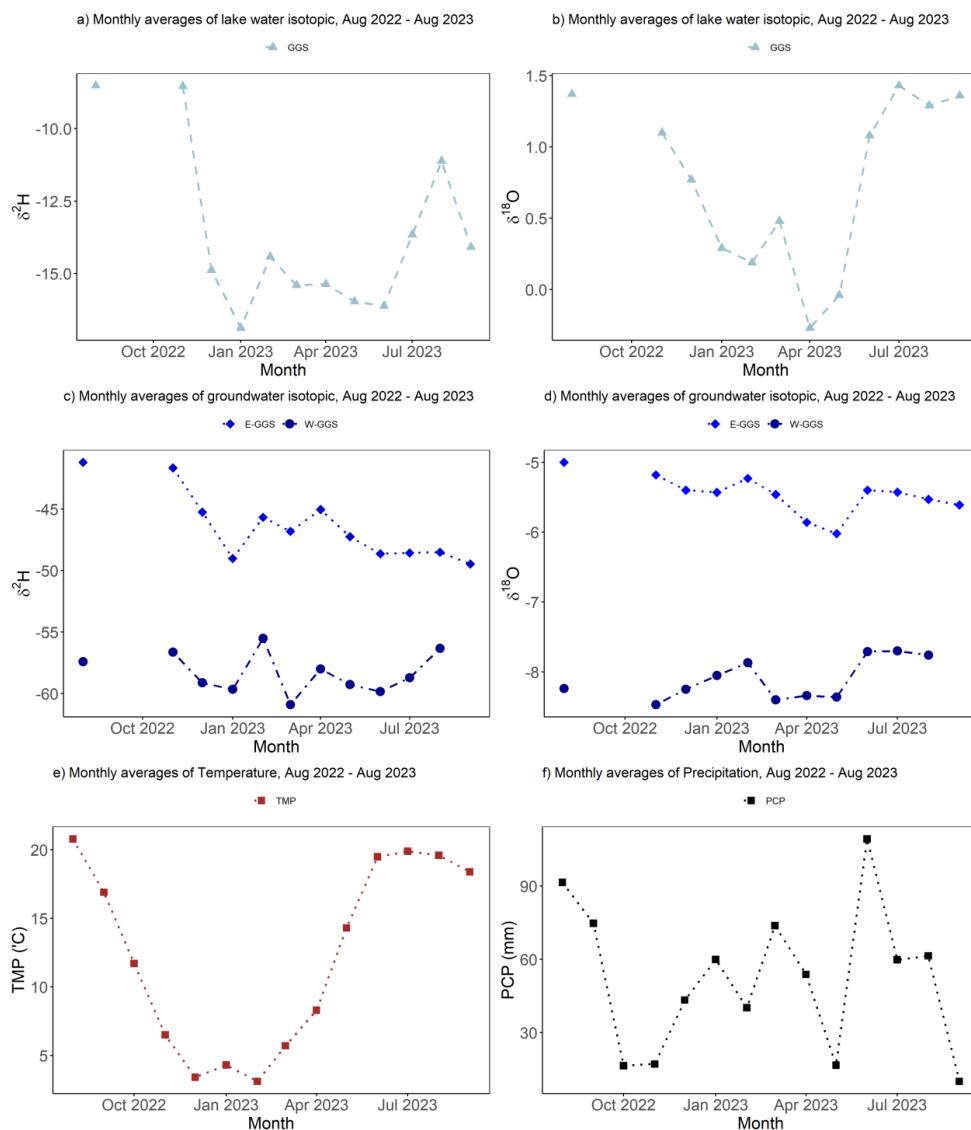


446 **Isotopic analysis**

447 Alterations in the mean monthly isotopic compositions of lake water and groundwater, along
448 with **temperature** and precipitation data, from August 2022 to August 2023 is presented in
449 Figure 6. The δD values for GGS (Fig. 6a), show significant variability, showing a
450 pronounced drop in δD values from around -8‰ in August 2022 to -17‰ in January 2023,
451 followed by a gradual decrease (except February) to approximately -16‰ by June 2023,
452 which represent a strong dilution phase. The period from July to September demonstrates
453 enriched values of δD alongside rising temperature and evaporation as a consequence. The
454 $\delta^{18} O$ values for GGS (Fig. 6b) record a fluctuating pattern, ranging from -0.27‰ to 1.4‰ ,
455 with peaks observed in August 2022 and July 2023, but experienced noticeable drops in April
456 and May 2023. **Overall, the isotopic data indicate that GGS experiences great isotopic**
457 **enrichment (heavier isotopic composition).**

458 The $\delta^2 H$ values of groundwater on the east side of GGS (E-GGS, Fig. 6c) range from
459 approximately -40‰ to -50‰ , with notable fluctuations throughout the year. The isotopic
460 composition of groundwater on the west side of GGS (W-GGS, Fig. 6c) has less variability,
461 with δD values mostly remaining between -55‰ and -60‰ , suggesting a rather stable
462 isotopic environment. Despite the fluctuations in δD values, **the $\delta^{18} O$ values (Fig. 6d) show**
463 **less variation, indicating some degree of isotopic stability in the oxygen isotopes in the**
464 **groundwater of both sides of lakes.** E-GGS presents a relatively stable trend with $\delta^{18} O$ values
465 fluctuating between -5‰ and -6‰ . W-GGS, with a seasonal pattern similar to E-GGS, shows
466 a consistent range of $\delta^{18} O$ values between -8‰ and -8.5‰ with minimal fluctuations (Fig.
467 6d). **Overall, the E-GGS with heavier isotopic signatures experiences greater isotopic**
468 **variability, meanwhile, the W-GGS site maintains a more consistent isotopic signature,**
469 **indicative of a more stable hydrological regime.** These observations (Fig. 6a,b,c,d) indicate
470 that the isotopic composition of both lake water and groundwater was generally heavier
471 (stronger enrichments) **during the summer of 2022 compared to the summer of 2023.**

472 The monthly average temperature (TMP, Fig. 6e), follows a clear seasonal pattern. It drops
473 from around $20^\circ C$ in August 2022 to a low of $5^\circ C$ in January 2023, then rises again to about
474 $20^\circ C$ by July 2023. Alongside temperature, precipitation values fluctuate significantly, with
475 peaks exceeding 90 mm in August 2022 and June 2023, and lower values around 20 mm
476 observed in Oct and November 2022 and May and Septemeber 2023.



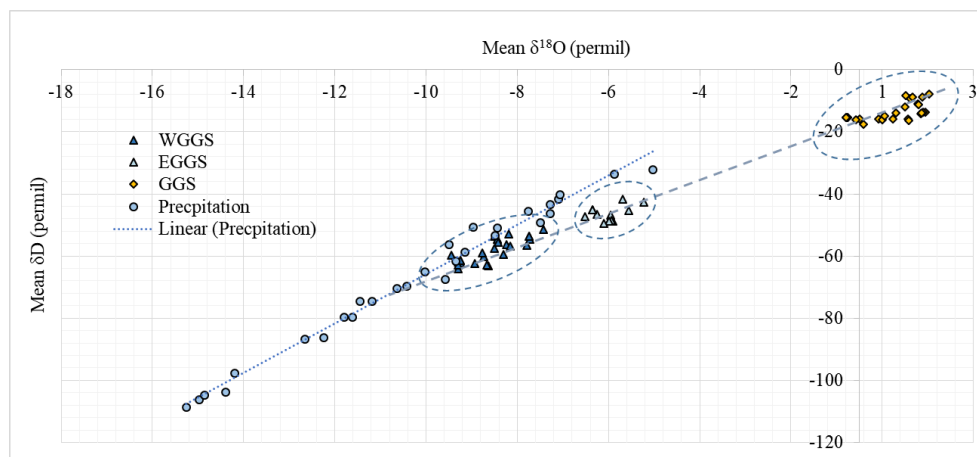
477

478 **Fig. 6.** Monthly averages of lake water isotopic compositions (a: δD and b: $\delta^{18}\text{O}$), groundwater isotopic
479 compositions (c: δD and d: $\delta^{18}\text{O}$), temperature (e), and precipitation (f) data from August 2022 to September
480 2023.

481 The relationship between δD and $\delta^{18}\text{O}$ values for lake water (GGS) and groundwater (WGGS
482 and EGGs) from August 2022 to September 2023 are illustrated in Figure 7. The isotopic
483 values for lake water are significantly clustered, with δD values between -25‰ and -5‰ and
484 $\delta^{18}\text{O}$ values from 2‰ to -2‰ and are isotopically heavier compared to precipitation and
485 groundwater, suggesting significant evaporative enrichment. WGGS exhibits $\delta^2\text{H}$ values from



486 -50‰ to -65‰ and $\delta^{18}\text{O}$ values from -9‰ to -7‰ . EGGS $\delta^2\text{H}$ values range from
487 approximately -50‰ to -40‰ , with $\delta^{18}\text{O}$ values between -7‰ and -5‰ , indicating less
488 enrichment compared to lake water and higher enrichment compared to the groundwater on
489 the west side.



490

491 **Fig. 7.** Isotopic composition of lake water and groundwater measured on the west (WGGS) and east (EGGS)
492 sides of Groß Glienicke from August 2022 to September 2023. The local meteoric water line (LMWL) is driven
493 from (GNIP/Berlin (DWD, BFG, BGR & HHZM, Stumpp et al. 2014).

494

495 Variables used for the calculation of evaporative losses and evaporation over inflow ratio
496 (E/I) ratios calculated for GGS during the August 2022–September 2023 period are presented
497 in Table 2. The winterwater isotopic compositions (dilution phase) served as the initial
498 sampling point for calculating the E/I ratio in both years 2022 and 2023. The δ_A -value of the
499 ambient air moisture was calculated based on the stable isotope composition of local
500 precipitation sampled in the Groß Glienicke region and the Lankwitz campus of the Freie
501 University Berlin. The calculated evaporative losses over inflow were equal to 43.4% and
502 42.3% based on δD and 30.11% and 29.4% based on $\delta^{18}\text{O}$ in 2022 and 2023 respectively. The
503 E/I ratio calculated based on δD is around 12% higher compared to the E/I based on $\delta^{18}\text{O}$.
504 Therefore, as a mean ratio, an average of 37% will be used for further analyses.

505

506 **Table 2.** Variables used for calculation of evaporative losses and the ratio of total evaporation to inflow (E/I) as
507 a function of the measured δD and $\delta^{18}\text{O}$ isotope enrichments for Lake Gross Glienicke (GGS) surveyed during
508 the August 2022–September 2023.



Parameters	Description	δD	$\delta^{18}O$
$\epsilon \square$	Kinetic isotope fractionation factor [‰] (h dependent)	-887.5	-1008.2
ϵ^*	Equilibrium isotope fractionation factor [‰] (T dependent)	78.7465	9.3468
ϵ	Total isotope fractionation [‰]	-814.5018	-998.9398
Ck	Kinetic isotope fractionation constant [‰]	12.5	14.2
α^*	Equilibrium isotope fractionation factor [‰] (T dependent)	1.0787	1.0093
δ^*	Limiting isotope composition	-134.7724	-30.2151
m	Enrichment slope	-1.0129	-1.0138
δ_A	Ambient air moisture	-124.9844	-16.7601
E/I_{y2022}	Evaporation over inflow ratio [‰] of Groß Glienicke Lake in 2022	43.37	29.63
E/I_{y2023}	Evaporation over inflow ratio [‰] of Groß Glienicke Lake in 2023	42.28	29.07

509

510

511 Hydrological modeling and model evaluations

512 Figure 8 illustrates the simulated vs. observed hydraulic heads (meters above sea level: m
 513 a.s.l.) at West-GGS Piezometer (W-GGS), Lake Gross Glienicke (GGS), and East-GGS
 514 Piezometer (E-GGS) over the period from January 2008 to December 2023. The model's
 515 performance is evaluated using several metrics, including the Kling-Gupta Efficiency (KGE),
 516 Percent Bias (PBIAS), and Root Mean Square Error (RMSE), as shown in Table 3. A strong
 517 alignment is evident between simulated and observed hydraulic heads, both in terms of
 518 magnitude and seasonality.

519 The simulated groundwater levels on the west side of the lakes, despite some over- and
 520 underestimations, showed very good agreement with the observed data. For the calibration
 521 period (2008-2018), the performance metrics are KGE of 0.86, PBIAS of 0.0%, and RMSE of
 522 0.13 m. During the validation period (2019-2023), the model maintained high performance
 523 with a KGE of 0.82, PBIAS of -0.1%, and RMSE of 0.07 m. Both observed and simulated
 524 data exhibit a general declining trend over the study period, with hydraulic heads decreasing
 525 from approximately 30.15 m to 30 m.

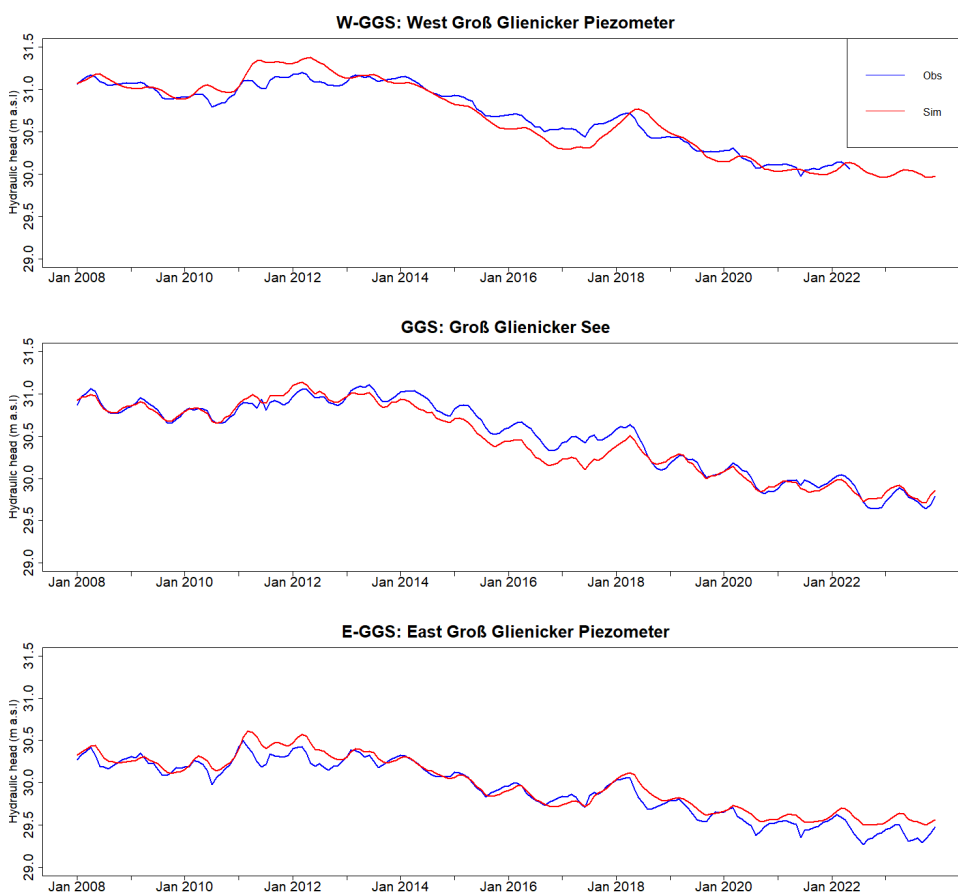
526 For GGS, similar to W-GGS, both observed and simulated values show a decreasing trend
 527 from around 31 m in 2008 to approximately 29.80 m in 2023. The model simulations closely
 528 follow the observed data, with minor deviations. The performance metrics for GGS during the
 529 calibration period are KGE of 0.78, PBIAS of -0.2%, and RMSE of 0.13 m. In the validation
 530 period, the metrics are KGE of 0.75, PBIAS of 0.0%, and RMSE of 0.06 m, indicating high
 531 accuracy in representing the hydraulic behavior of the lake.

532 The observed and simulated groundwater dynamics on the east side of GGS show good
 533 agreement. During the calibration period, the performance metrics are KGE of 0.84, PBIAS
 534 of 0.1%, and RMSE of 0.09 m. In the validation period, the metrics are KGE of 0.70, PBIAS



535 of 0.2%, and RMSE of 0.09 m. Overall, the high-performance metrics confirm the model's
 536 reliability and accuracy in capturing both the long-term trends and seasonal variations of
 537 groundwater-surface water dynamics within the study area, providing valuable insights into
 538 groundwater-surface water interactions.

539



540

541 **Fig. 8.** Time series of observed and simulated hydraulic heads at three locations: (a) West Gross Glienicke
 542 Piezometer (W-GGS), (b) Lake Gross Glienicke (GGS), and (c) East Gross Glienicke Piezometer (E-GGS) from
 543 January 2008 to December 2023.

544 **Table 3.** Model performance evaluation using several metrics for both calibration (2008-2008) and validation
 545 (2018-2023) periods

		West Gross Glienicke	East Gross Glienicke	Gross Glienicke Lake
Calibration	KGE	0.86	0.84	0.78

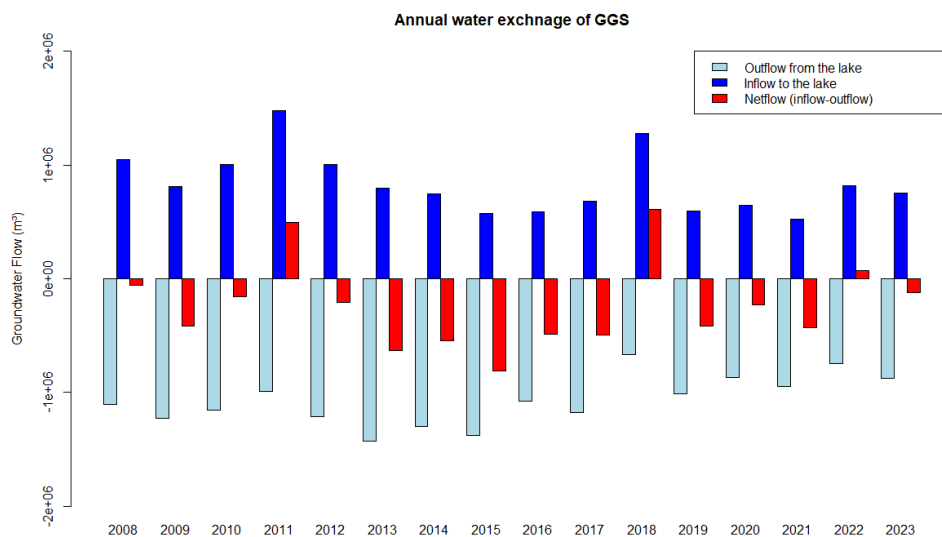


2008-2018	PBIAS	0.0	0.1	-0.2
	RMSE	0.13	0.09	0.13
Validation 2019-2023	KGE	0.82	0.7	0.75
	PBIAS	-0.1	0.2	0
	RMSE	0.07	0.09	0.06

546

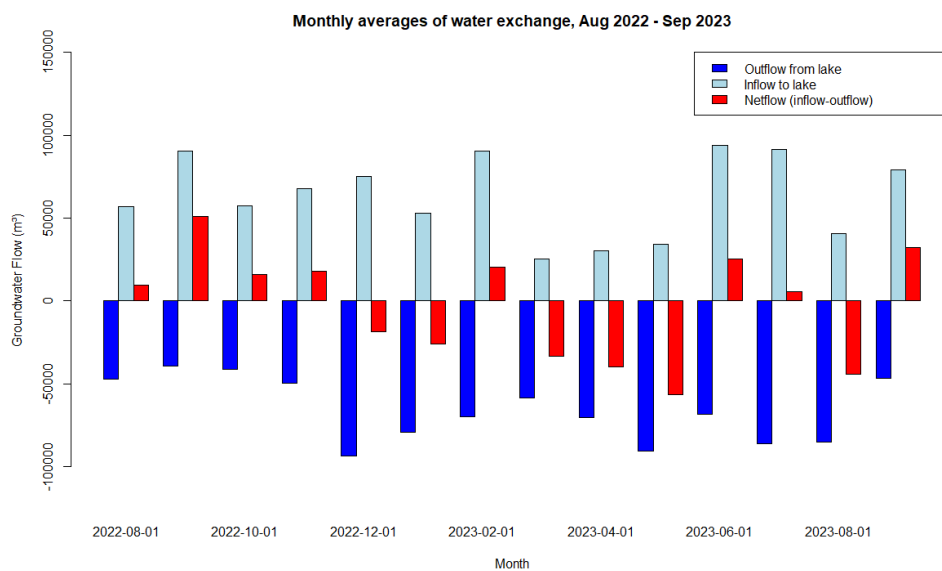
547 The calculated annual water exchange for GGS from 2008 to 2023, detailing the inflow to the
548 lake, outflow from the lake, and their differences (net flow = inflow - outflow) are presented
549 in Figure 9. The inflow to GGS demonstrates substantial annual variability. For instance,
550 years such as 2008, 2011, 2012, and 2018 show relatively higher inflows compared to other
551 years. Notably, there is a discernible decreasing trend in inflow from 2011 to 2021, with 2018
552 being an exception. This trend indicates a progressive reduction in the hydrological inputs to
553 the lake over the decade. Simultaneously, the outflow from GGS shows significant annual
554 variability, with the highest outflow occurring between 2012 and 2017. This increased
555 outflow, coupled with the decreasing inflow, points to a period of significant net water loss
556 for GGS, potentially impacting the lake's water levels. Positive net flow values in years 2011,
557 2018, and 2022 indicate years when inflow exceeds outflow, contributing to the lake's water
558 gain. Variation in both water gain and loss over the study period, reflects the complex
559 interplay of natural hydrological processes governing the lake's water balance.

560 Figure 10 illustrates the water exchange dynamics of GGS over the period from August 2022
561 to September 2023, highlighting seasonal patterns in inflow, outflow, and net flow. During
562 the warmer months, particularly June and July, the inflow to the lake peaks at approximately
563 90,000 m³, indicating a significant increase in water input during this period. Among the
564 summer months (July to September), August has the lowest amount of inflow, with an
565 average of approximately 40,000 m³. In contrast, the inflow is pronouncedly lower during the
566 months of March, April, and May, averaging around 20,000 m³. The lake experiences positive
567 net flow, reflecting water gain, during the months of June and July. From December to May
568 (except February), the net flow is predominantly negative, indicating that outflow exceeds
569 inflow. During these months, the lake loses water, with outflow reaching its highest levels.



570

571 **Fig. 9.** Annual water exchange of Lake Groß Glienicke (GGS) from 2008 to 2023, showing the inflow to the
572 lake, outflow from the lake, and net flow (Outflow - Inflow)



573

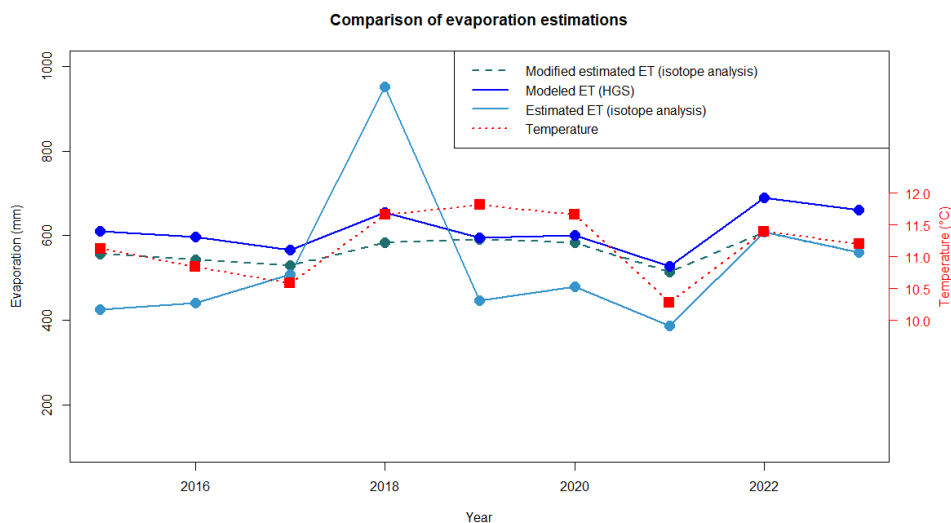
574 **Fig. 10.** Monthly water exchange of Lake Gross Glienicke (GGS) from August 2022 to September 2023

575



576 To compare the lake evaporation values calculated by the HGS model and the results of the
577 isotopic signature of lake water actual evaporation (E) from GGS for the years 2022 and 2023
578 was calculated using Eq. 11, which incorporates simulated annual water inflow to GGS (I_{HGS})
579 from the HGS model and the E/I ratio derived from isotope analysis (mean ratio: 37%). These
580 results were compared to the evaporation rates from GGS simulated by the HGS model (Fig.
581 11). The annual evaporation estimates from the isotope analysis for the years 2022 and 2023
582 show good agreement. The values calculated by the HGS model (E_{HGS}) are slightly lower
583 (around 80 mm). The general agreement between the evaporation rates simulated by the HGS
584 model and the values derived from the isotope approach indicates accurate inflow simulation
585 by the HGS model. Transferring the E/I ratios from 2022 and 2023 to calculate evaporation
586 for earlier years (2015-2021, Fig. 11) results in notable discrepancies, particularly evident in
587 2015 and 2018, where evaporation reaches 450 and 1000 mm, respectively, compared to E_{HGS}
588 values of 590 and 614 mm for those years. However, modified isotope analysis (considering
589 annual variations in inflow and temperature, see Eq.11) demonstrates good agreement with
590 the HydroGeoSphere model, emphasizing our approach of incorporating temperature and
591 inflow data for accurate evaporation predictions for earlier years. This suggests that while the
592 E/I ratio obtained from 2022 and 2023 can be applied to estimate evaporation in previous
593 years, adjustments for differences in inflow and temperature between those years and 2022-
594 2023 are crucial for enhanced estimations of evaporations in years without isotope analysis
595 (E/I).

596



597
598 **Fig. 11.** Comparison of actual evaporation from Lake Gross Glienicke (GGs) estimated by Hydroeosphere
599 model (HGE) and isotope analyses (E/I ratio), and modification of isotope analyses (E/I ratio) considering
600 annual temperature and inflows to the lake. Annual temperatures are indicated, corresponding to the secondary
601 y-axis.

602

603 4. Discussion

604 The comparison of actual evaporation (E) from GGS for 2022 and 2023, derived from isotope
605 analysis (E/I) and HydroGeoSphere (HGS) model calculations, demonstrates the
606 comparability of these methods. Despite slight differences in the results, likely due to the
607 influence of direct precipitation with lighter isotope signatures diluting the lake water, the
608 general consistency between the methods underscores the accurate simulation of inflows by
609 the HGS model. Seasonal variations in water isotopic compositions offer a valuable
610 perspective for evaluating hydrological model simulations. Higher outflow observed from
611 December 2022 to May 2023 provides insights into the dilution phase of groundwater
612 isotopic compositions on the eastern side of GGS during these months. Notably, GGS water
613 isotopes reached their heaviest form in August 2023, contrasting with other summer months
614 with similar temperatures and precipitation, suggesting lower inflow during that particular
615 month as simulated by the HGS model. This approach highlights the value of using isotopic
616 data to evaluate model simulations, providing a complementary angle to traditional methods.
617 Considering the higher precipitation and warmer temperatures in the summer of 2022
618 compared to the summer of 2023, the isotopic composition of both lake water and east



619 groundwater was heavier during the summer of 2022. This indicates that isotopic “light”
620 rainwater, which directly recharged the lakes in the summer of 2022, was insufficient to
621 counterbalance the influence of the higher temperatures, resulting in a heavier isotopic
622 composition in the lakes. Despite the high precipitation in summer 2022, which would
623 typically dilute the isotopic signature of the lake, the higher temperatures (evaporation) led to
624 an enrichment of water isotopes. This phenomenon can be attributed to the large water body
625 of the lake (approximately 4 million m³ considering the average water depth of 6.5 m reported
626 by Wolter and Ripl (1999) compared to the rain amount (0.05 million m³), where the
627 relatively small volume of rainwater was not enough to significantly alter the isotopic
628 composition of the much larger lake volume. This is in line with the findings of the study by
629 Vyse et al. 2020 where they discovered a more significant influence of rain on shallow water
630 bodies compared to larger water bodies in the State of Brandenburg (NE-Germany). The low
631 impacts of rainwater on the isotope composition of the lake can also be interpreted to mean
632 that GGS is a groundwater-dominated lake with a very good hydraulic connection to the
633 groundwater, which keeps the lake water fresh and diluted by providing a source of
634 isotopically-depleted water. This underlines the robustness of the isotopic approach against
635 the variations of meteorological factors influencing the isotopic signature.

636 The isotopic differences between lake water and groundwater on both side of the GGS,
637 highlight the complex interactions and distinct hydrological processes occurring within the
638 study area. Considering that the groundwater samples from the east and west of GGS belong
639 to the same depth (9-10 m below surface) and same aquifer, the isotopically-enriched
640 groundwater in the east side can only be explained by a well-mixed interaction of lake water
641 and groundwater in this area. This underlines that GGS is a flow-through lake, a conclusion
642 supported by the E/I ratio being up to 37% (e.i., mean ratio) in 2022 and 2023. The E/I ratio
643 of GGS aligns with the E/I ratio reported for wetlands and lake water bodies downstream of
644 the Spree catchment showing similar climate conditions. In 2021, the E/I ratio in this area was
645 up to 34% (Chen et al., 2023). Vyse et al. (2020) reported that the wetlands with lower
646 landscape elevations located in northern Brandenburg typically possessed higher E/I ratios
647 than the ones with higher elevations. This is due to the hydrological function of small
648 waterbodies in the Pleistocene landscape. Higher wetlands have a more recharge/flow
649 through character whereas lower positions show a discharge character. Moreover, Cluett and
650 Thomas (2020) highlighted that the sensitivity of lake water isotopes to inflow and
651 evaporation can vary significantly over time, influenced by regional hydroclimate (e.g., direct
652 precipitation and humidity) and local hydrology (e.g., type of the lake). The uncertainty in



653 evaporative loss calculated using the code embedded in the Hydrocalculator is mainly due to
654 uncertainties in the required inputs, temperature, and humidity, which can cause variations of
655 up to 2% (E/I) according to Skrzypek et al. (2015). Despite these potential measurement
656 variations, the calculated E/I ratio for GGS provides a reliable estimate that aligns with
657 known hydrological behaviors in similar regions.

658 For the period 2015-2021, evaporation estimates derived from the isotope analysis (E/I) of
659 2022 and 2023 generally show lower values compared to the HGS model's evaporation
660 estimates, except 2018. This year saw a strong inflow peaking due to heavy rainfall events in
661 the summer 2017. This suggests that using the E/I ratios from 2022 and 2023 for earlier years
662 without adjustments can lead to significant inaccuracies. The modified isotope analysis (E/I),
663 which incorporates annual variations in inflow and temperature, shows a better agreement
664 with the HGS model evaporation calculates, especially in the earlier years. This finding
665 underscores the importance of including both temperature and inflow data for more accurate
666 evaporation predictions. Comparing these results with previous studies, Herbst and Kappen
667 (1999) reported evaporation from the Bornhöved Lake, which covers 1.1 km² in northern
668 Germany and has a maximum depth of 26 m, to be around 650 mm for the years 1992-1995.
669 The evaporation estimates for GGS from both the HGS model and the modified isotope
670 analysis fall within a similar range reported by Herbst and Kappen (1999), suggesting that
671 despite differences in geographical and hydrological characteristics, the annual evaporation
672 rates for German lowland lakes are comparable. These findings support the use of
673 comprehensive, multi-faceted approaches in hydrological studies to improve the precision of
674 evaporation estimates and enhance water resource management.

675

676 **5. Conclusion**

677 This study has addressed the challenge of accurate estimation of water balance components
678 comprehensively through the quantification of subsurface-groundwater inflow and
679 evaporation losses to Gross Glienicke Lake (GG), located in northeast Germany. Through the
680 combined use of the isotopic mass balance model, HydroCalculator, alongside the fully
681 integrated hydrological model, HydroGeoSphere (HGS), a detailed understanding of the
682 hydrological dynamics governing GG Lake was attained. The calculated evaporation rates
683 derived from the isotopic mass balance model, exhibit strong alignment with the actual
684 evaporation rates calculated by the HGS model. This alignment underscores on one hand the
685 reliability and efficacy of the integrated hydrologic modeling approach in predictions of water



686 balance components such as inflow to the lake in a complex hydrogeological setting. On the
687 other hand, incorporating evaporation rate estimations given by isotope analysis corrected by
688 temperature variations and historical inflows leads to an improvement of the inflow results
689 even for the years without measured isotope data. Despite inherent uncertainties associated
690 with water isotope signature analyses, the integration of isotopic data with hydrological
691 modeling has provided valuable validation for the estimation of water balance components.
692 Moving forward, this integrated approach holds promise for enhancing the robustness of
693 hydrological models and facilitating more accurate assessments of water resources and
694 ecosystem dynamics in similar lake environments.

695

696 **Data availability:** All data (except the data provided by Berliner Wasserbetriebe) used to
697 process and set up the models will be available upon request. Data provided by Berliner
698 Wasserbetriebe can be requested through a separate usage agreement with Berliner
699 Wasserbetriebe.

700 **Author contributions:** Data collection, fieldwork, HGS model setup, and code development,
701 model input-output analysis, writing (original draft, review, and editing). JS: Isotopic
702 laboratory analysis, writing (review and editing). MS: Model input-output analysis, writing
703 (original draft, review, and editing). CM: Model input-output analysis, writing (original draft,
704 review, and editing).

705 **Competing interests:** The authors declare that they have no conflict of interest.

706 **Acknowledgments:** This investigation was funded through the Einstein Research Unit
707 ‘Climate and Water under Change’ from the Einstein Foundation Berlin and Berlin University
708 Alliance (ERU-2020-609). We would like to thank Reinhard Hinkelmann, Franziska Tügel,
709 and Can Ölmez from the Technical University of Berlin for providing potential evaporation
710 data. We like to thank Dr. Gunnar Lorenzen and Bertram Monnkinkhoff (Berliner
711 Wasserbetriebe) for providing us with the FEFLOW model as well as the actual data on the
712 drinking water extraction rates around the Havel River. We are grateful to our colleague,
713 Dieter Scherer his rainwater sampling assistance, and Patrick Zentel for his field and
714 laboratory assistance.

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716 **References**



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