

A Bayesian updating framework for calibrating the hydrological parameters of road networks using taxi GPS data

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Abstract. Hydrological parameters should pass through a careful calibration procedure before aiding decision-making. However, ~~great significant difficulties~~ difficulty is ~~are~~ encountered when applying existing calibration methods to regions in ~~which~~ where runoff data are inadequate. To ~~achieve accurate~~ fill the gap of hydrological calibration for ~~the~~ ungauged road networks, we proposed a Bayesian updating framework ~~that~~ calibrates hydrological parameters based on taxi GPS data. Hydrological parameters ~~were~~ are calibrated by adjusting their values such that the runoff generated by ~~the~~ acceptable parameter sets corresponds to ~~could yield~~ the road disruption periods during which no taxi points are observed. The proposed method was ~~is~~ validated on ~~through~~ 10 flood-prone roads in Shenzhen, and the results revealed that the trends of runoff could be correctly predicted for 8 ~~out of~~ 10 roads. This study ~~shows~~ demonstrates that the integration of hydrological models and taxi GPS data can provide ~~suggests~~ viable alternative measures for ~~the~~ model calibration to derive, ~~and provides~~ actionable insights for flood hazard mitigation.

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1 Introduction

~~In the context~~ Under the background of climate change and increased urbanization, flooding poses ~~is posing~~ far-reaching threats to ~~the~~ urban road networks of coastal ~~metropolises~~ metropolis (Balistocchi et al., 2020). In Australia, ~~around~~ approximately 53% of flood-related drowning deaths were the result of vehicles driving into flooded waters. Additionally, ~~indirect~~ losses caused by flooding, such as cancelled commutes, mandatory detours, and travel time delays, ~~even~~ often outweigh direct losses (Kasmalkar et al., 2020). Quantifying the impact of flooding exposure requires the prediction of surface runoff over ~~the~~ roads and ~~computation of~~ road disruptions induced by ~~the~~ runoff, which are critical for the implementation of ~~to~~ flood mitigation, traffic resilience improvement, and ~~risk~~ early warning systems.

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Public concerns ~~about~~ regarding road flooding hazards have created ~~the pressing need~~ pressure to develop fine-grained and accurate models for hydrological simulation. ~~The~~ hydrological modelling is, ~~as a~~ quite relatively well-established

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theory ~~that can~~; provides ~~an~~ approximations of ~~the~~ real-world hydrological system; and has been widely used in many road-related studies (Versini et al., 2010; Yin et al., 2016; Safaei-Moghadam et al., 2022). ~~As the~~ ~~Because~~ hydrological modelling is subject to uncertainty, ~~which~~ ~~that~~ arises from the ~~over-simplified~~ ~~false~~ reflection of ~~the~~ hydrological systems, ~~the~~ initial and boundary conditions, and ~~the~~ lack of true knowledge, parameters ~~for~~ ~~of~~ hydrological models ~~should~~ ~~must be carefully calibrated~~ ~~be carefully calibrated prior to their~~ ~~before~~ ~~applying~~ ~~application~~ to ~~solve~~ practical problems, so that ~~the~~ models ~~can~~ ~~is capable of~~ closely matching the historical ~~evidences~~ ~~trends~~ (Gupta et al., 1998). A ~~an~~ un-calibrated models ~~are~~ ~~is~~ indefensible and sterile, ~~so~~ ~~very~~ few models documented in the literature have been applied without ~~any~~ ~~calibrations~~ ~~a~~ ~~calibration procedure~~ (Beven, 2012).

40 ~~During~~ ~~Over~~ the ~~last~~ ~~past~~ four decades, numerous studies have been ~~conducted on~~ ~~devoted to~~ the development of calibration methods. Methodologies ~~for~~ ~~of~~ model calibration range from ~~the~~ simple trial-and-error ~~methods~~, ~~which~~ ~~that~~ adjusts one parameter value ~~in~~ each ~~turn~~ ~~iteration~~ until the differences between predicted and observed values ~~are~~ ~~is~~ satisfactory; to ~~the~~ Bayesian updating framework, ~~which~~ ~~that~~ rejected the ~~concept of a~~ ~~idea that there is~~ single correct solution. ~~To a great extent~~, ~~No matter what kinds of methods~~, hydrological models are basically calibrated based on ~~the~~ ~~runoff data alone~~ (Dembélé et al., 2020), ~~so~~ ~~the~~ success of model calibration is ~~to a great extent~~, dominated by the availability of field-observed runoff data. However, runoff data are generally ~~only~~ gathered at ~~a~~ ~~only~~ few sites; and some cities ~~even~~ never measured runoff data in ~~the~~ built-up regions (Gebremedhin et al., 2020). ~~Al~~ ~~Even~~ though ~~the~~ runoff data ~~could~~ ~~can~~ be effectively collected by administration departments ~~in some cities~~, they have ~~ved~~ no motivations to share these data ~~to~~ ~~with~~ the public. For example, among China's top 10 largest cities¹, only Shenzhen has shared runoff-related data on 50 ~~the~~ ~~an~~ open data platform. ~~FAs~~ for ~~the~~ model calibration ~~for~~ ~~at~~ the road scale, ~~the~~ runoff data are even more difficult to acquire; because ~~a~~ road networks ~~are~~ ~~is~~ far denser than ~~a~~ river networks and flood gauges are only ~~located~~ ~~installed~~ in a few flood-prone roads ~~considering~~ ~~based on their~~ high measurement cost, leaving most ~~of~~ roads ~~ungaged~~ ~~ungauged~~. As pointed out by Beven (2012, p:55), “the ungauged catchment problem is one of the real challenges for hydrological modellers.”

This lack of hydrological data ~~has~~ prompted researchers to seek ~~extra~~ ~~additional~~ data sources to support flood-related 55 decision-making. ~~In response to this need~~, ~~big data~~, ~~owing to~~ ~~Based on~~ the advancement of mobile telecommunication technologies, ~~big data~~ are emerging as alternative sources of information for coping with flood risks (Paul et al., 2018; Li et al., 2018; Gebremedhin et al., 2020). Citizens ~~can~~ voluntarily or passively ~~acting~~ ~~act~~ as human sensors ~~to~~ generate georeferenced data to improve flood monitoring. ~~Typical~~ ~~Many~~ studies ~~have leveraged~~ ~~involve the use of~~ crowdsourcing social media data (~~Brouwer and Eilander, 2017; Li et al., 2018~~) (Brouwer and Eilander, 2017; Sadler et al., 2018; Zahura et al., 2020), mobile phone data (Yabe et al., 2018; Balistrocchi et al., 2020), and taxi GPS data (She et al., 2019; Kong et al., 60 2022). However, most ~~of~~ previous works ~~have~~ concentrated on using big data either for flood mapping or mining spatiotemporal patterns (Restrepo-Estrada et al., 2018), and ~~parameter calibration for ungauged roads based on big data~~ ~~remains an open problem~~ ~~it remains an open question of how to calibrate parameters based on big data for ungauged roads~~.

¹ Rank by the resident population in 2021.

This study ~~differentiates-extends from~~ our previous study (Kong et al., 2022) by going ~~one-a~~ step further than simply recognizing ~~the-flooded~~ roads. We propose a calibration method for road-related hydrological parameters ~~using-based on~~ the taxi GPS data. Many studies have shown that vehicle-related information during ~~the-rainfall~~, ~~such-as-including~~ vehicle volume, speed, and trajectory ~~information~~, is ~~useful-critical- for~~ flooded ~~ing~~ road detection (Zhang et al., 2019; Qi et al., 2020; Yao et al., 2020). When a road segment is inundated by ~~the-heavy~~ rainfall, the vehicle volume may ~~present-exhibit~~ a sharp or gradual drop, depending on the intensity of the rainfall event. Conversely, ~~an-the~~ abnormal drop ~~in-of~~ vehicle volume during the rainfall ~~may-implies~~ that ~~the-a~~ road ~~may-has~~ experienced ~~some~~ rainfall-induced inundations. This motivates ~~us~~ to use ~~a~~ traffic-related data sources to calibrate hydrological parameters. In this study, we developed a transformation process ~~which-that~~ converts ~~the-rainfall~~ time series ~~data-into~~ ~~the-a~~ time series of ~~the-probabilities~~ that no taxis ~~will~~ drive ~~through-on~~ ~~the-a~~ road (~~no-taxi-passing probability hereafter~~) for ~~every-a~~ given hydrological parameter set, ~~and-We~~ then assigned a probability to every parameter set by integrating the no-taxi-passing probability with ~~the~~ observed taxi GPS data. We ~~not-only~~ outlined a generalized taxi-data-driven calibration framework ~~and-but-also-realize~~ ~~implemented~~ ~~the-a~~ framework with specific hydrological and transportation models.

2 Methodology

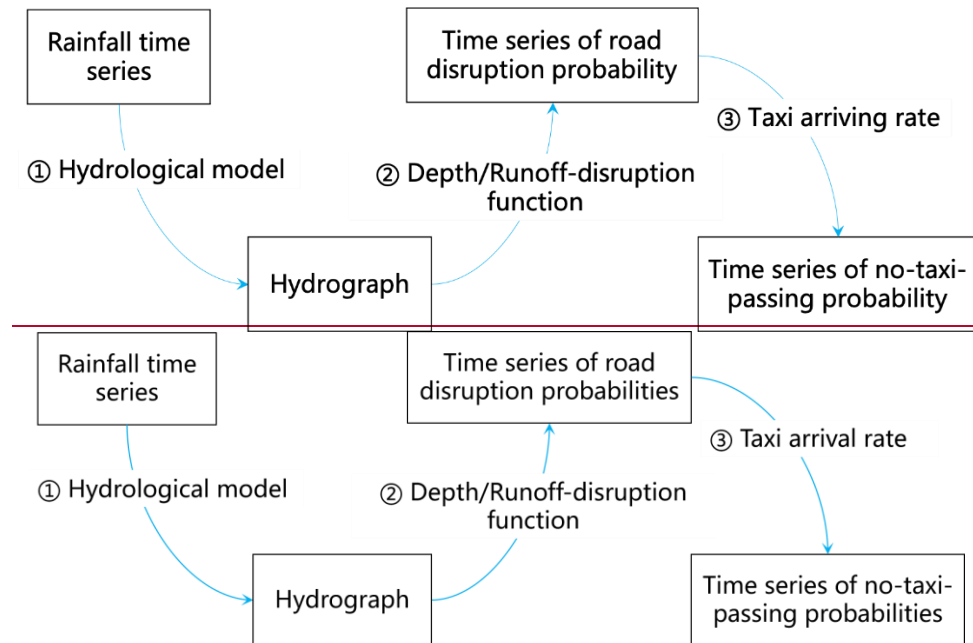
2.1 ~~A~~ Bayesian updating procedure

Observed data are not always as informative as expected and may be inconsistent with other data sources, ~~so~~ hydrologists ~~usually-typically~~ adopt the Bayesian framework to update hydrological parameters, which provides a generalized formalism that integrates prior probability representing ~~the~~ prior knowledge with ~~the~~ likelihood that reflects how ~~well-accurately~~ ~~the-presumed-a~~ model can reproduce ~~the~~ observations to form ~~the-a~~ posterior probability. Suppose we have several hydrological models, each with different sets of parameters. ~~Then,~~ the purpose of the Bayesian updating procedure ~~adopted~~ in this study is to assign a posterior probability to every hydrological parameter set as new taxi data become available.

Two components are critical for ~~the-this~~ Bayesian updating procedure. One is the prior probability, and the other is the likelihood function. ~~Regarding-For~~ the prior probability, ~~for their famous calibration model called generalized likelihood uncertainty estimation~~, Beven and Binley (1992) stated ~~in their famous calibration model, generalized likelihood uncertainty estimation (GLUE)~~, that all ~~the~~ parameter combinations are considered equally probable before ~~extra-additional~~ information is introduced. After the first updating, the prior probability of each updating ~~run-iteration~~ ~~could-can~~ be replaced by the posterior probability of the latest updating ~~iteration-run~~. ~~The-likelihood~~, ~~which-is-a~~ measurement of how well ~~the-a~~ given model conforms to the observed taxi behaviour, is not as easy to compute as the prior probability, because the parameter set to be estimated is hydrology-related, ~~whereas~~ the observed evidence is taxi-based ~~related~~. Therefore, ~~question-then-arises~~ ~~as-we-must-determine~~ how to construct a taxi-based proxy whose probability ~~equals-is-equal-to~~ ~~to-that-of~~ the associated

95 hydrological parameter and construct a function enabling the transformation from the hydrological parameters to the taxi-related proxy.

The selected proxy selected in this study was the time series of probability that no taxi drives through the road in a given time interval (short for the no-taxi-passing probability). Figure 1 illustrates presents a generalized procedure for converting the a precipitation-rainfall process-time series into the a time series of no-taxi-passing probabilities for each hydrological parameter. This procedure consists of three steps. First, a hydrological model is used to convert the a rainfall time series in process to the a hydrograph, which is a graph showing runoff with respect to time past a specific point. Second, a runoff-disruption function that, which relates the runoff to the probability that the a road is blocked, is used to transition transform the hydrograph into the a time series of road disruption probabilities. Third, the a taxi arriving-arrival rate is combined with the time series of road disruption probabilities to yield derive the a time series of no-taxi-passing probabilities. Note that the hydrological model and the taxi arrival-arrival rate are considered to be unique for every road and are invariable within a short period, while-whereas the runoff-disruption function is identical for all roads.



110 **Figure 1** A generalized procedure for converting the a rainfall time series into the a time series of no-taxi-passing probabilities.

Integrating this three-step process with the Bayesian equation enables us to compute the posterior probability of the a parameter set based on the taxi data. For a specific road, suppose there are N hydrological parameter sets to be estimated. As Because the runoff-disruption function and the taxi arrival-arrival rate are assumed to be invariant-fixed for the road, we can construct a composite function converting the i th parameter set, which is denoted as $\theta^{(i)}$, into the a time series of no-taxi-passing probabilities, which is denoted as $\Omega^{(i)}$. Therefore, the probability of $\theta^{(i)}$ to be being optimal is equals to the probability of $\Omega^{(i)}$ being to be true, which can be expressed as follows:

$$P(\boldsymbol{\theta}^{(i)}) = P(\boldsymbol{\Omega}^{(i)}) \quad (1)$$

where $P(\boldsymbol{\theta}^{(i)})$ and $P(\boldsymbol{\Omega}^{(i)})$ are the prior probabilities of $\boldsymbol{\theta}^{(i)}$ and $\boldsymbol{\Omega}^{(i)}$ respectively. As taxi observations become available, $P(\boldsymbol{\theta}^{(i)})$ (or $P(\boldsymbol{\Omega}^{(i)})$) can be updated using the Bayes theorem as:

$$P(\boldsymbol{\theta}^{(i)}|X) = P(\boldsymbol{\Omega}^{(i)}|X) \propto P(\boldsymbol{\Omega}^{(i)}) \mathcal{L}(X|\boldsymbol{\Omega}^{(i)}) \quad (2)$$

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where X is the taxi observation, and $P(\boldsymbol{\theta}^{(i)}|X)$ and $P(\boldsymbol{\Omega}^{(i)}|X)$ are the posterior probabilities of $\boldsymbol{\theta}^{(i)}$ and $\boldsymbol{\Omega}^{(i)}$ respectively under the conditional on the taxi observation, X . The $\mathcal{L}(X|\boldsymbol{\Omega}^{(i)})$ $\mathcal{L}(X|\boldsymbol{\theta}^{(i)})$ is the likelihood of X given $\boldsymbol{\Omega}^{(i)}$ $\boldsymbol{\theta}^{(i)}$. The optimal parameter set is the one that which derives yields the $\boldsymbol{\Omega}^{(i)}$ that most closely best fits the observed taxi data.

The solution of Solving Eq.(2) involves the calculation of $P(\boldsymbol{\Omega}^{(i)})$ $P(\boldsymbol{\theta}^{(i)})$ and $\mathcal{L}(X|\boldsymbol{\Omega}^{(i)})$ $\mathcal{L}(X|\boldsymbol{\theta}^{(i)})$. According to Eq.(1), $P(\boldsymbol{\Omega}^{(i)})$ can be replaced with $P(\boldsymbol{\theta}^{(i)})$, which is the prior probability of parameter sets. The derivation of $P(\boldsymbol{\theta}^{(i)})$ depends on prior knowledge regarding the parameter distribution, which is typically obtained using traditional hydrological methods. However, this prerequisite knowledge may not always be readily accessible based on limited data availability. In such cases, Beven and Binley (1992) suggested that prior to the introduction of any quantitative and qualitative information, any parameter set combination should could be considered to be equally likely. This implied that the parameter set is drawn from a uniform distribution as follows:

$$P(\boldsymbol{\Omega}^{(i)}) = P(\boldsymbol{\theta}^{(i)}) = 1/N \quad (3)$$

$$P(\boldsymbol{\theta}^{(i)}) = 1/N \quad (3)$$

In this study, we compared the effects of two types of prior parameter distributions, namely a uniform distribution and a distribution derived from digital elevation model (DEM) data, on the resulting posterior distributions.

Next, $\mathcal{L}(X|\boldsymbol{\theta}^{(i)})$ $\mathcal{L}(X|\boldsymbol{\Omega}^{(i)})$, which is a likelihood function, describes the joint probability of the observed taxi data, X , as a function of the chosen $\boldsymbol{\Omega}^{(i)}$ $\boldsymbol{\theta}^{(i)}$. Consider a rainfall event that is broken-divided into T 5 min intervals. From the taxi data, we obtained can obtain a sequence of taxi-related observations, which are denoted as $X = \{xX_1, xX_2, \dots, xX_T\}$, where $xX_t = 1$ if the observed road hasis-observed-with at least one taxi passing duringby in the t th-5 min interval, and $xX_t = 0$ otherwise. The $\boldsymbol{\Omega}^{(i)} = \{\omega_1^{(i)}, \omega_2^{(i)}, \dots, \omega_T^{(i)}\}$ is also a T -dimensional vector, where $\omega_t^{(i)}$ is the no-taxi-passing probability at-in the t th 5-mininterval taking-with $\boldsymbol{\theta}^{(i)}$ as the parameter set. Note that $\boldsymbol{\Omega}^{(i)}$ is only determined by the chosen hydrological parameter and the-rainfall proeesstime series, and is not measured from the-observed data. Considering that the arrival of taxis is independent of-with-respect-to-time, $\mathcal{L}(X|\boldsymbol{\theta}^{(i)})$ $\mathcal{L}(X|\boldsymbol{\Omega}^{(i)})$ can be formulated as:

$$\mathcal{L}(X|\boldsymbol{\Omega}^{(i)}) = \prod_{t=1}^T (1 - \omega_t^{(i)})^{X_t} (\omega_t^{(i)})^{1 - X_t} \quad (4)$$

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$$\mathcal{L}(\mathbf{X}|\boldsymbol{\theta}^{(i)}) = \mathcal{L}(\mathbf{X}|\boldsymbol{\Omega}^{(i)}) = \prod_{t=1}^T (1 - \omega_t^{(i)})^{x_t} (\omega_t^{(i)})^{1-x_t} \quad (4)$$

By substituting ~~Eq.(3) and Eq.(4) back~~ into Eq.(2), the ~~Eq.(5) is following equation can be~~ obtained:

~~$$P(\boldsymbol{\theta}^{(i)}|\mathbf{X}) \propto \frac{1}{N} \prod_{t=1}^T (1 - \omega_t^{(i)})^{x_t} (\omega_t^{(i)})^{1-x_t} \quad (5)$$~~

$$P(\boldsymbol{\theta}^{(i)}|\mathbf{X}) \propto P(\boldsymbol{\theta}^{(i)}) \prod_{t=1}^T (1 - \omega_t^{(i)})^{x_t} (\omega_t^{(i)})^{1-x_t} \quad (5)$$

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Equation (5) is the proposed Bayesian updating model ~~for~~ calibrating the hydrological parameters based on ~~the~~ taxi data, where ~~X could can~~ be directly measured and ~~$\omega_t^{(i)}$~~ $\omega_t^{(i)}$ is calculated through the three-step process ~~shown-illustrated~~ in Fig. 1, which will be discussed in detail in the ~~next following~~ section. Having ~~chosen-selected~~ an updating model, the ~~optimal~~ parameter for one period of observations may not be optimal for another period. ~~As-Because~~ the model may have ~~a~~ continuing inputs of new taxi observations, the posterior probability for $\boldsymbol{\theta}^{(i)}$ should be updated as new evidence becomes

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available. For the second update, the posterior probability from the first observation becomes the prior probability for the second observation, and the posterior probability for $\boldsymbol{\theta}^{(i)}$ is recursively updated as:

$$P(\boldsymbol{\theta}^{(i)}|\mathbf{X}_2) \propto \mathcal{L}(\mathbf{X}_2|\boldsymbol{\theta}^{(i)})P(\boldsymbol{\theta}^{(i)}|\mathbf{X}_1) \quad (6)$$

where \mathbf{X}_1 and \mathbf{X}_2 are the first and the second taxi observations.

2.2 ~~Instantiation Instantization~~ of the three-step procedure

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Section 2.1 presents a generalized three-step procedure ~~which for~~ converting the a rainfall time series into the a time series of no-taxi-passing probabilities. In this section, we specialize ~~this~~ process by integrating existing theories with our model. ~~The (Three conceptualized steps shown-illustrated in Fig. 1 are-were replaced-substituted-~~ with three ~~more~~ concrete sub-models. First~~ly~~, a Soil Conservation Service (SCS) unit hydrograph ~~was~~ used to ~~turn-convert the~~ rainfall excess into the a hydrograph of the target road. Second~~ly~~, an empirical runoff-disruption function based on, ~~whose~~ data extracted from

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various experimental, observational, and modelling studies, ~~is was~~ applied to convert the hydrograph into the a time series of ~~the~~ road disruption probabilities. Third~~ly~~, a Poisson distribution, representing the distribution of taxi arrival ~~arriving~~ rate, ~~is was~~ combined with the road disruption probability time series to yield-derive the a no-taxi-passing probability time series.

Step 1: Converting rainfall into runoff based on the SCS unit hydrograph

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Not all rainfall will produces runoff because ~~storage from~~ soils storage can absorb a certain amount of rain ~~light~~ shower. ~~While-However,~~ in the urbanized areas, only a small proportion of rainfall infiltrates into the soil or is retained on the land surface, leaving most ~~of the~~ rain to flow across the urban surfaces and ~~becomes-become the~~ direct runoff. The rainfall that ~~yields-becomes the~~ direct runoff is termed-referred to as rainfall excess. The Natural Resources Conservation Service

(NRCS)² developed a method to estimate ~~the~~ rainfall excess based on ~~the~~ soil types and land uses using the following curve number equation:

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$$P_e = \begin{cases} (P_a - 0.2S)/(P_a + 0.8S) & P_a > 0.2S \\ 0 & P_a \leq 0.2S \end{cases} \quad (7)$$

where P_e is the accumulated rainfall excess in cm, P_a is the accumulated rainfall in cm, and S is the potential retention after runoff begins, which is defined as a function of the curve number as follows:

$$S = 2.54 \times (1000/CN - 10) \quad (8)$$

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where CN is the curve number. For urban and residential land, the curve number varies from ~~65-40~~ to ~~85-95~~, depending on the impervious areas (Natural Resources Conservation Service, 2010a). Because prior knowledge on the CN is unavailable, it was considered as a calibrated parameter in this study. ~~For sake of brevity, the curve number will not be regarded as a parameter to be calibrated in this study but as a given parameter with the value of 85.~~

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~~Next, t~~The rainfall excess derived using by Eq. (7) was inputted in to the unit hydrograph to ~~produce-derive~~ the runoff. The unit hydrograph is a commonly used rainfall-runoff model that converts rainfall excess into a temporal distribution of direct runoff ~~converts rainfall excess to direct runoff~~. First proposed by Sherman in 1932, the unit hydrograph is defined as the hydrograph resulting from one unit of rainfall excess distributed uniformly over a catchment area. It assumes ~~the-that~~ rainfall is uniform over the catchment area and that runoff increases linearly with ~~the~~ rainfall excess. Although ~~under most conditions~~ these assumptions cannot be perfectly satisfied under most conditions, the results obtained from the unit hydrograph are generally acceptable for most practical uses/cases. The model, ~~was~~ originally designed for larger watersheds, ~~but it~~ has been found to be applicable to some catchments areas less than 5,000 m² in size (Chow et al., 1988).

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The unit hydrograph ~~applies is only~~ applicable to ~~for the~~ watershed areas where ~~the~~ runoff data ~~are~~ were measured. The paucity of ~~the~~ runoff data motivated/sparked the idea development of the synthetic unit hydrograph (SUH) concept. The term “synthetic” in SUH ~~denotes the-refers to a~~ unit hydrograph derived from watershed characteristics, rather than empirical rainfall-runoff relationships. In this study, we utilized the SCS unit hydrograph, which is a dimensionless SUH proposed by the NRCS. For the dimensionless SUH, the discharge (i.e., y-axis) is expressed as the ratio of discharge q to ~~the~~ peak discharge q_p and the time (i.e., x-axis) is expressed as the ratio of time t to ~~the~~ peak time t_p . Therefore, the SCS unit hydrograph, ~~rigorously speaking,~~ is not exactly an SUH itself, but is a useful tool for constructing an SUH.

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The shape of an SCS unit hydrograph is ~~totally-entirely~~ determined by the peak rate factor. A standard value of 2.08 for the peak rate factor is recommended and commonly used by the NRCS (Fig. 2). To construct an SUH from ~~the-an~~ SCS unit hydrograph, the x-axis of the SCS unit hydrograph is multiplied by t_p and the y-axis is multiplied by q_p . The values of q_p and t_p are functions of the catchment area and ~~the~~ time of concentration as follows:

$$t_p = 0.6t_c + D/2 \quad (9)$$

$$q_p = 2.08A/t_p \quad (10)$$

² The NRCS ~~used to be-was originally~~ called the US Soil Conservation Service-~~(SCS)~~.

where t_c is the time of concentration in hours, A is the catchment area in km^2 , and D is the duration of unit rainfall excess in hours, which ~~was set to 1/12 h one-twelfth of an hour~~ (i.e., 5 min) in this study. ~~Notably As can be seen,~~ the catchment area and time of concentration are required to construct an SUH, and they are the ~~other~~ two hydrological parameters ~~we would that should be~~ calibrated based on ~~the~~ taxi data. ~~Although numerous tools and theories have been developed for estimating catchment area and time of concentration, these two parameters are still prone to significant errors, particularly in urban areas, because of challenges in accurately delineating urban catchments~~ (Huang and Jin, 2019; Li et al., 2020). ~~Urban catchment delineation is more complex than natural catchment delineation. Urban catchments have spatially heterogeneous surface cover types, which change with city development and construction, and modify runoff parameters (Goodwin et al., 2009). High densities of residential and commercial buildings obstruct flow paths and alter flow directions of storm water runoff, complicating rainfall-runoff and overland flow processes in urban areas (Ji and Qiuwen, 2015). Additionally, accurate urban catchment delineation necessitates high-resolution DEMs, which are not always available. In many Chinese cities, high-resolution DEMs are considered confidential data and are generally inaccessible to non-governmental organizations. Based on these challenges, deriving accurate catchment area and time of concentration data in urban areas is difficult in Shenzhen.~~

For ~~the~~ sake of simplicity, the peak rate factor ~~would was~~ not be calibrated and ~~be was fixed as at~~ 2.08, although some studies have ~~showed indicated~~ that it has a ~~much wider~~ range from 0.43 for steep terrain to 2.58 for very flat terrain (Chow et al., 1988). After t_c and A ~~were are~~ chosen, an SUH ~~could can~~ be constructed, and ~~then we used~~ it to convert ~~the~~ rainfall excess ~~into the~~ runoff by applying the discrete convolution equation. The detailed computation process of the discrete convolution equation can be found in most hydrological textbooks (e.g., ~~see~~ Chow et al., (1988) ~~pp: 211-213~~), and will not be discussed here. ~~To be clear, a~~ The graphical workflow in Fig. 3 ~~shows illustrates the transformation of how the~~ rainfall time series ~~is data transformed into the a~~ hydrograph for every parameter set.

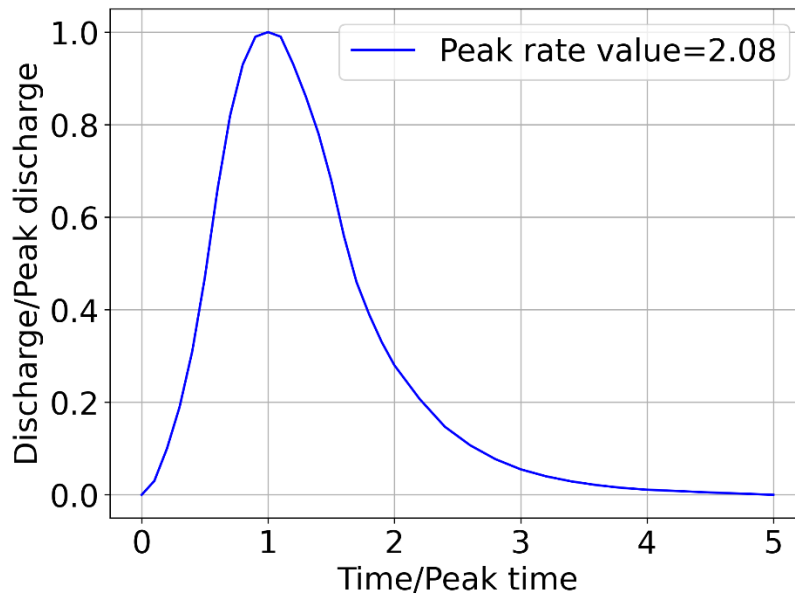


Figure 2 The standard SCS unit hydrograph. Data provided by the NRCS (2007).

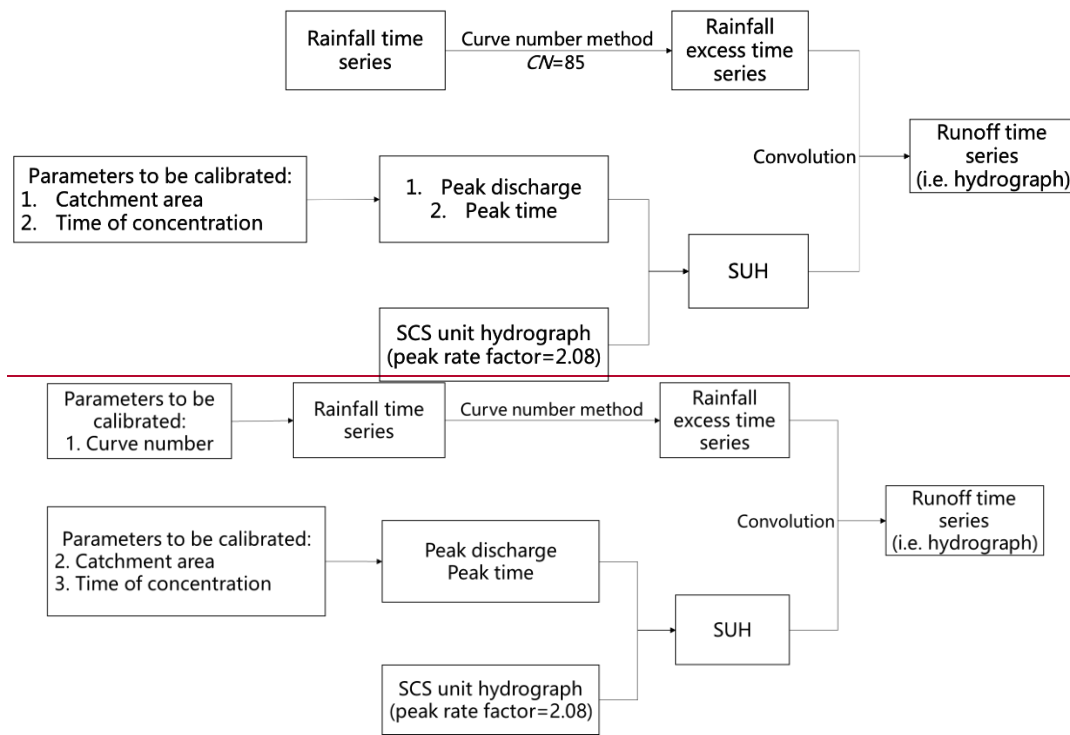


Figure 3 Workflow of the SCS unit hydrograph for converting rainfall into runoff.

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Step 2: Derivation of the road disruption probability using the runoff-disruption function

The goal of Step 2 is to convert the hydrograph generated in Step 1 into the a time series of road disruption probabilities, or more specifically, the probability that a taxi driver chooses to turn the ir car when arriving at a flooded road. Most models in the literature assume that a road is either open or closed, which usually does not correspond to the empirical evidence that many drivers may take risks to drive on inundated roads along the road even though it is inundated. In order to transition from a binary view of a flooded road being considered “open” or “closed,”; Pregnolato et al. (2017) proposed to the use of a curve that relates the depth of floodwater to a reduction in vehicle speed to show indicate the probability of road disruption, and such This idea was is soon followed adopted by Contreras-Jara et al. (2018) and Nieto et al. (2021).

A driver will turn around when he believes that the flow rate is too risky for their overcomes the vehicle configuration. From this perspective, the road disruption probability is equals to equal to the probability that the vehicle performance is lower less than the flow rate perceived by a driver. However, it is a difficult task to quantify the factors that influence common belief of what guide people’s willingness of people to drive through a flooded waterway roadway, and is also impossible difficult to obtain the precise knowledge of regarding all taxi-flood intersections. Alternatively, to ensure the vehicle stability in flood flows, guidelines are usually typically recommended based on the limiting values of depth times velocity, and in Many studies researchers have carried out conducted laboratory testing on the stability of different kinds types of vehicle models exposed to different combinations of depth and velocity (Merz and Thielen, 2009; Shah et al., 2018). As s Suggested by Pregnolato et al. (2017), we constructed the our runoff-disruption function by integrating data from reviewed the literatures and some authoritative guidelines. In this study, the road disruption probability was is defined as the probability that the product of flow velocity and flow depth is higher was greater than the stability limits extracted eding from the literature existing studies, which are shown listed in Table 1 and plotted in Fig. 4. The expression of the fitting curve is:

$$y = [1 + \exp(-16.6(x - 0.48)^2)]^{-1} \quad (11)$$

where x is the product of flow velocity and flow depth, and y is the disruption probability. According to Eq. (11), a road has a disruption probability of 50% when the product of flow velocity and flow depth is $0.47 \text{ m}^2 \text{ s}^{-1}$; and is totally disrupted when the product is higher greater than $0.80 \text{ m}^2 \text{ s}^{-1}$. By A applying the fitting curve, we can easily convert the flood runoff into the disruption probability as follows:

$$P(\text{Disrupt})_t^{(i)} = [1 + \exp(-16.6(q_t^{(i)}/W - 0.48)^2)]^{-1} \quad (12)$$

where $P(\text{Disrupt})_t^{(i)}$ and $q_t^{(i)}$ are the road disruption probability and discharge at in the t th interval 5 min derived by from the hydrological model with the parameter set $\theta^{(i)}$, respectively, and W is the road width.

Table 1 Guidelines recommended by in the existing literatures.

Reference	Vehicle type	Feature	Recommended limits for vehicle stability ($\text{m}^2 \text{ s}^{-1}$)
Shah et al. (2018)	Volkswagen Scirocco	Flow direction = 0°	velocity \times depth < 0.014
Al-Qadami et al. (2022)	Perodua Viva	Ground clearance = 0.18 m	velocity \times depth < 0.39

Calculated according to Kramer et al. (2016)	VW Golf III	<u>Not mention</u>	velocity×depth<0.42
Shand et al. (2016)	Large passenger	Ground clearance >0.12 m	velocity×depth<0.45
Martínez-Gomariz et al. (2017)	Mini Cooper	Ground clearance =0.12 m	velocity×depth<0.49
Martínez-Gomariz et al. (2017)	BMW i3	Ground clearance =0.10 m	velocity×depth<0.49
Martínez-Gomariz et al. (2017)	BMW 650	Ground clearance =0.08 m	velocity×depth <0.50
Martínez-Gomariz et al. (2017)	Mercedes GLA	Ground clearance =0.17 m	velocity×depth <0.59
Moore and Power (2002)	All but very small cars	<u>Not mention</u>	velocity×depth <0.60
Calculated according to Xia et al. (2014)	Honda Accord	<u>Not mention</u>	velocity×depth <0.65

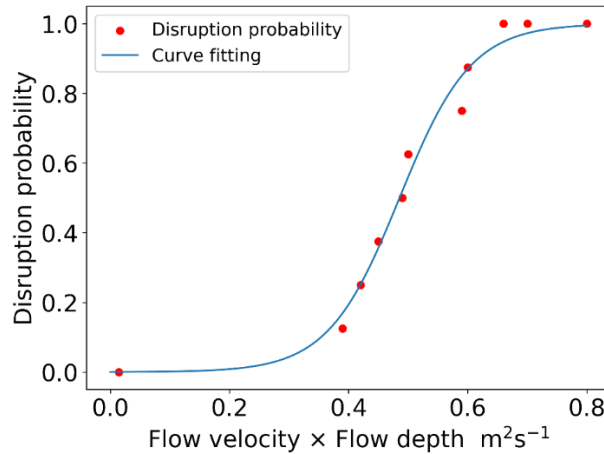


Figure 4 Empirical runoff-disruption function derived from the existing literature.^s

Step 3: Derivation of the time series of no-taxi-passing probabilities^y

A road has is considered to have no taxis passing by in a fixed time step interval if the road has no taxis visiting arriving or if every taxi that arrives at the road turns around.^z Therefore, the no-taxi-passing probability can be inferred calculated by using the following equation:

~~$$\omega_t^{(i)} = \sum_{n=0}^{\infty} P(\text{Arrival_taxi}=n) \times (P(\text{Disrupt})_t^{(i)})^n \quad (13)$$~~

$$\omega_t^{(i)} = \sum_{n=0}^{\infty} P(\text{Arrival_taxi} = n)_t \times (P(\text{Disrupt})_t^{(i)})^n \quad (13)$$

where $\omega_t^{(i)}$ is the no-taxi-passing probability in the t th interval-5 min, and $P(Arrival_taxi = n)$
 $(Arrival_taxi = n)_t$ is the probability that n taxis arrives at the road segment during the t th 5-min interval. Equation (13)
 270 indicates that if every taxi that arrives at the road segment makes a turn because of the flooded waterway/roadway, then the
 taxi volume of-on the road will be zero. In this study, $P(Arrival_taxi = n)(Arrival_taxi = n)_t$ $P(Arrival_taxi = n)$ wasis
 assumed to follow the Poisson distribution:

~~$$P(Arrival_taxi = n) = e^{-\lambda} \lambda^n / n! \quad (14)$$~~

$$P(Arrival_taxi = n)_t = e^{-\lambda_t} \lambda_t^n / n! \quad (14)$$

275 where λ_t is the average number of taxis arriving at the road during the t th interval. By Ssubstituting Eq. (14) into Eq. (13),
 we deriveobtain:

~~$$\omega_t^{(i)} = \sum_{n=0}^{\infty} (e^{-\lambda} \lambda^n / n!) \times (P(Disrupt)_t^{(i)})^n \quad (15)$$~~

$$\omega_t^{(i)} = \sum_{n=0}^{\infty} (e^{-\lambda_t} \lambda_t^n / n!) \times (P(Disrupt)_t^{(i)})^n \quad (15)$$

By Applying $e^x = \sum_{n=0}^{\infty} x^n / n!$, Eq. (15) can be further converted into:

~~$$\omega_t^{(i)} = e^{-\lambda} \sum_{n=0}^{\infty} (P(Disrupt)_t^{(i)} \lambda)^n / n! = \exp(\lambda (P(Disrupt)_t^{(i)} - 1)) \quad (16)$$~~

$$\omega_t^{(i)} = e^{-\lambda_t} \sum_{n=0}^{\infty} (P(Disrupt)_t^{(i)} \lambda_t)^n / n! = \exp(\lambda_t (P(Disrupt)_t^{(i)} - 1)) \quad (16)$$

Equation (16) indicates that $\omega_t^{(i)}$ is totally-entirely determined by λ_t and $P(Disrupt)_t^{(i)}$. Since-Because $P(Disrupt)_t^{(i)}$
 is given-obtained through-from Step 2, what is left to determine is the value of λ_t . The value of λ_t fluctuates according to
the time of day, indicating higher taxi volume during congested periods and lower volume during non-congested periods.
 285 Therefore, we calculate λ_t by averaging the taxi volume during the t th interval to account for time-of-day variations. It should
be noted that As the intensity of rain increases-gets heavier, experienced taxi drivers will avoid flood-prone roads in advance,
which-meanings that strictly speaking, λ_t ,-strictly speaking, is a decreasing function of rainfall intensity. However, fitting
 the rainfall- λ_t curve requires substantial-many taxi GPS trajectories to inspect the route choices of taxi drivers under heavy
 rain, which is currently-unfeasible in/outside the scope of this study. We assume that λ is a constant quantity which keeps
 290 unchanged with respect to rainfall. The value of λ can be calculated by averaging all 5 min taxi volume using the historical
taxi-GPS data. Therefore, we assumed that λ_t was independent of rainfall.

Finally, Table 2 lists all the sub-models and parameters used in/of the three-step process. The core principle of the three-
 step process iwas to calculate the time series of no-taxi-passing probabilities, $\Omega^{(i)}$, givenfor each parameter set, $\theta^{(i)}$.
AsBecause the best choice of a model is often data-specific, it is probable-likely that the model combination proposed in this
 295 study is not optimal for other studiesscenarios. To apply the proposed calibration method in practicel-use, one-must-specify

the sub-models ~~for~~ in the three-step process must be specified according to the available data, prior knowledge, and accuracy requirements.

Table 2 Specific sub-models and parameters used in the three-step process.

Purpose of the each step	Specific model	Parameter	Source of parameters
Step 1: Convert the rainfall data into the a hydrograph	Curve number equation	1. Curve number	<u>Parameters to be calibrated</u> <u>Existing literature</u>
	SCS unit hydrograph	2. Peak rate factor 2. Catchment area <u>3. Time of concentration</u>	<u>Existing literature</u> <u>Parameters to be calibrated</u>
3. Catchment area 4. Time of concentration <u>4. Peak rate factor</u>		<u>Parameters to be calibrated</u> <u>Existing literature</u>	
Step 2: Convert the hydrograph into the a time series of disruption probabilities	Empirical runoff-disruption function	5. Limit of product of flow velocity and depth	Existing literatures
Step 3: Convert the time series of disruption probabilities into the a time series of no-taxi probabilities	Taxi arrival rate following the Poisson distribution	6. Average taxi volumes in 5 min periods	Taxi GPS data

3 A ~~w~~ Working example

300 The method outlined above was tested on ~~an~~ the intersection ~~of~~ located in Xinzhou R₁ road and Hongli R₂ road in Shenzhen, which is recognized as a waterlogging-flood-prone point by the Water Authority of Shenzhen Municipality. Recall that the parameters to be calibrated are the curve number CN, catchment area, A , and time of concentration, t_c . The parameter spaces for CN, A, and t_c are determined by DEMs and other prior knowledge, which will be discussed in Section 4. ~~The range of parameters should be wide enough to encompass most possible values. After several rounds of testing, the~~
 305 ~~maximum value for A is set as 0.5 km², and the maximum value for t_c is 5 h. Optimal parameter sets for most roads would fall into the region enclosed by the maximum parameter sets.~~ Table 3 ~~shows~~ presents the details information of the parameter sets to be calibrated, which ~~totally~~ form $3,0008 \times 20 \times 30 = 4,800$ possible combinations. For ease of exposition, we assume that all parameters are uniformly distributed.

Table 3 Detailed information ~~of~~ on parameter sets to be calibrated.

Parameter	Annotation	Minimum	Maximum	Incremental	Number of possible parameter values
<u>Curve number</u>	<u>CN</u>	<u>40</u>	<u>75</u>	<u>5</u>	<u>8</u>
Catchment area	A	<u>0.1 km²</u> 0.01 km²	<u>0.29 km²</u> 0.5 km²	0.01 km ²	<u>20</u> 50
Time of concentration	t_c	<u>0.75 h</u> 4/12 h	<u>3.2 h</u> 5 h	1/12 h	<u>30</u> 60

310 ~~The~~ Taxi GPS data collected during two storm events that ~~occurred~~ ing on 9-May 9, 2015 and 23-May 23, 2015 ~~were~~ are used to calibrate the parameter sets ~~of~~ for the target intersection. Rainfall time series data and taxi observations under during ~~two~~ these two storms are ~~shown~~ presented in Fig. 5. Each taxi observation contains two time series: ~~One~~ is the time

series of 5-min taxi volumes at 5 min intervals, and the other is the 5-min time series of road statuses at 5 min intervals, which is These were derived from the taxi volumes, with the a value of one to be 1 if the taxi volume was higher greater than 0-zero and a value of zero 0 if the taxi volume is was 0-zero.

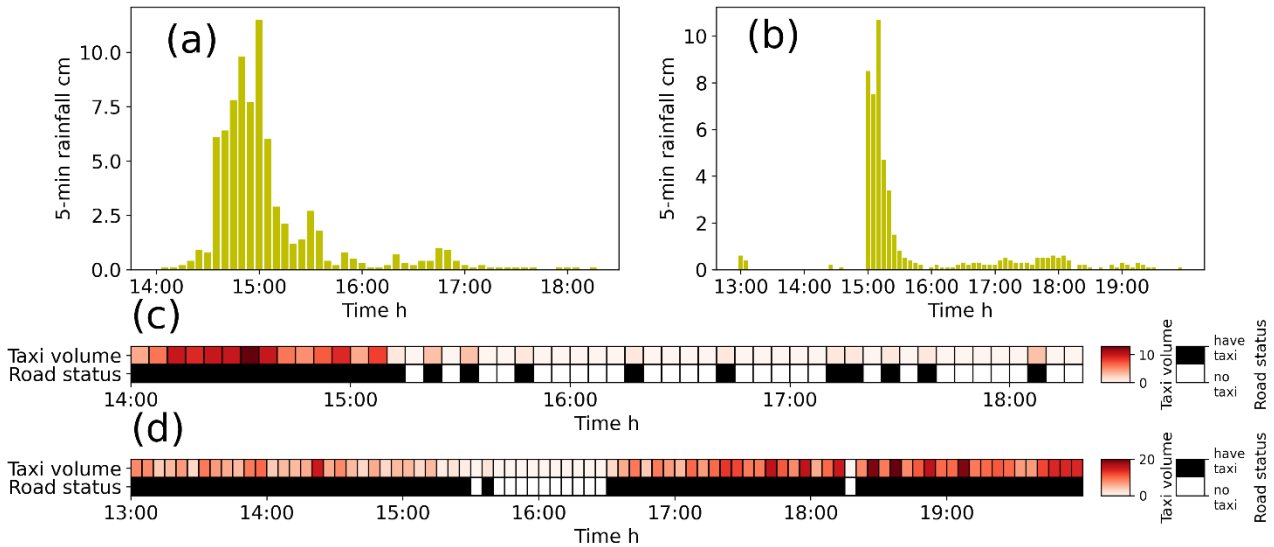


Figure 5 Rainfall and taxi observations used to calibrate the hydrological parameters: (a) 5-min rainfall time series in 5 min intervals on May 9, 2015, (b) 5-min rainfall time series in 5 min intervals on May 23, 2015, (c) Taxi observations on May 9, 2015, and (d) Taxi observations on May 23, 2015.

Given the rainfall on May 9, 2015, we should must calculate the time series of no-taxi-passing probabilities possibility for each parameter combination. Because there are 4,800 parameter sets, we can derive 4,800 possible time series of no-taxi-passing probabilities. For simplicity, we only present the 3,120th parameter set (i.e., $CN = 65$, $A = 0.2 \text{ km}^2$, and $t_c = 2.75 \text{ h}$) as an example to demonstrate the working of the proposed method. According to the three-step process, the first step is to convert the original rainfall into the rainfall excess using the curve number method given $CN = 65$ (Fig. 6(a)). Then, for each combination of A and t_c , we construct a SUH. As there are 3,000 parameter sets, we can construct 3,000 different SUHs. For simplicity, we only chose the 1,170th parameter set, i.e. $A = 0.2 \text{ km}^2$ and $t_c = 2.75 \text{ h}$, as examples to show the calibration works. Using Eq.(9) and Eq.(10), the we calculated the peak discharge q_p and peak time t_p using Eqs. (9) and (10) can be calculated as:

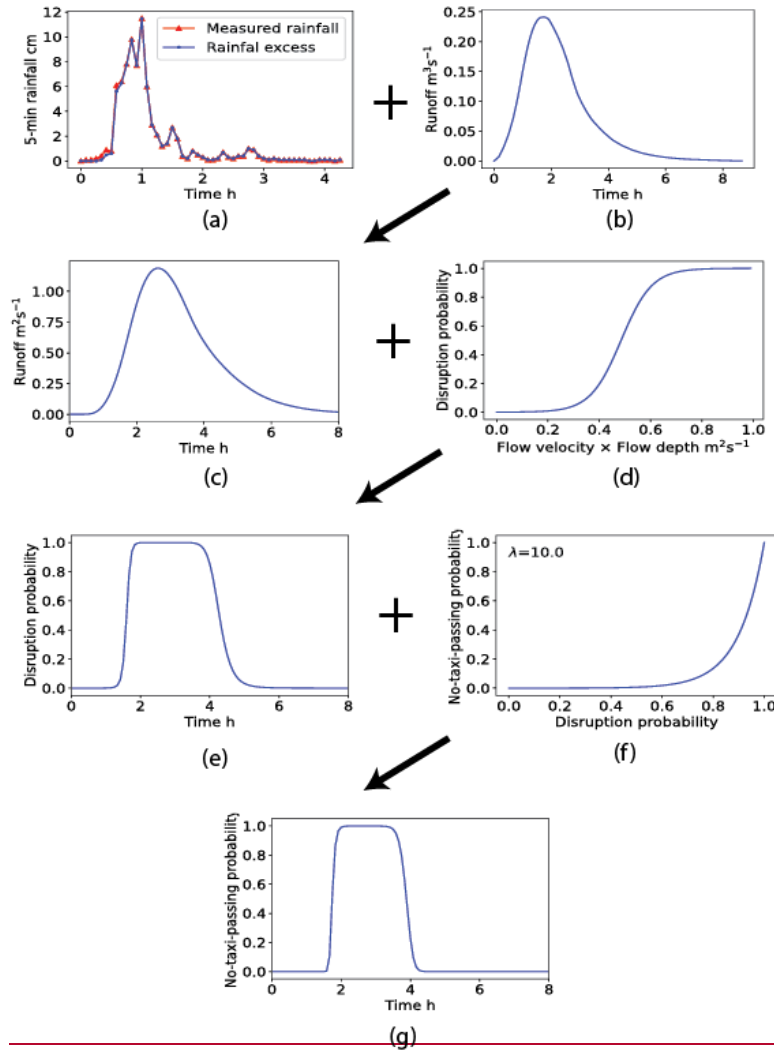
$$t_p = 0.6 \times 2.75 + \frac{1}{2 \times 12} \approx 1.69 \text{ h}$$

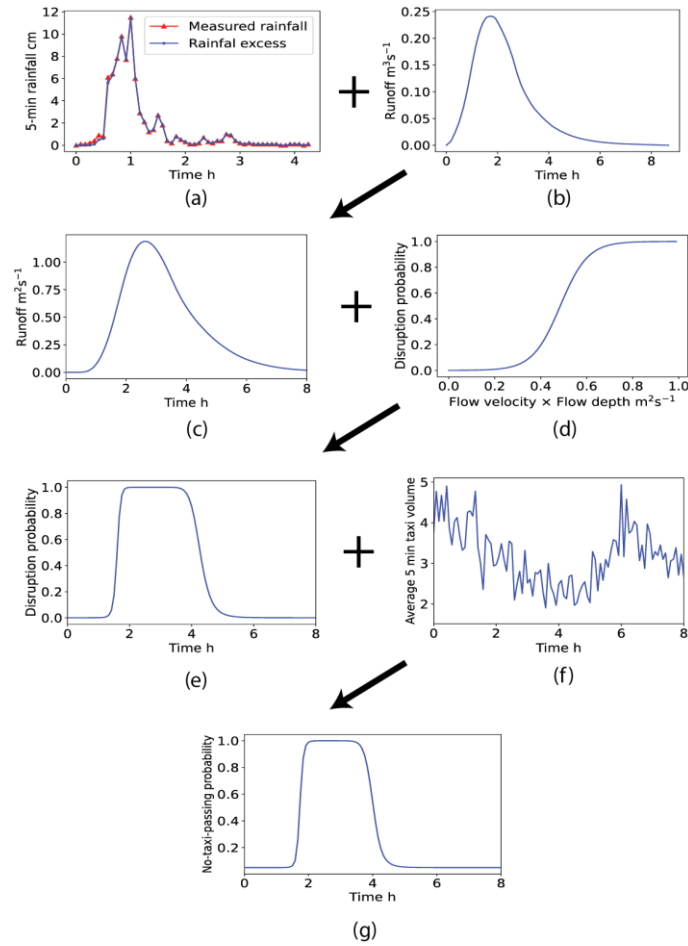
$$q_p = 2.08 \times \frac{0.2}{1.69} \approx 0.24 \text{ m}^3\text{s}^{-1}$$

The SUH was derived by through multiplication multiplied by t_p on the x-axis and by q_p on the y-axis of the standard SCS unit hydrograph (Fig. 6(b)). Next, the rainfall excess shown presented in Fig. 6(a) was combined with the derived SUH to yield obtain the a hydrograph through the convolution (Fig. 6(c)).

In the second step, the runoff ~~was~~ transformed ~~into~~ ~~the~~ a time series of road disruption probabilities based on the runoff-disruption function (Fig. 6(d)). ~~Note that~~ ~~t~~ The runoff-disruption function takes the production of water depth and velocity (in ~~the~~ units of $\text{m}^2 \text{s}^{-1}$) as inputs. Therefore, the original runoff (in ~~the~~ units of $\text{m}^3 \text{s}^{-1}$) ~~produced by~~ ~~derived in~~ the first step should be divided by the road width before inputting ~~it in~~ to the runoff-disruption function.

In the third step, the time series of road disruption probabilities (Fig. 6(e)) ~~was~~ converted to ~~that of~~ no-taxi-passing probabilities using Eq. (16) (Fig. 6(f)). ~~According to the historical taxi GPS data, the average number of taxis arriving at the road, λ , is 10.0 taxi per 5 min.~~ The average number of taxis during the flooding period is presented in Fig. (6f), and ~~t~~ The derived time series of no-taxi-passing ~~probabilities~~ ~~possibility~~ ~~is shown~~ ~~presented~~ in Fig. 6(g).





345 **Figure 6** An example transformation of how the a rainfall time series is transformed into the no-taxi-passing probabilities using the three-step procedure for the 1170th-3,120th parameter set: (a) Time series of rainfall and rainfall excess, (b) SUH constructed using the 3,120th-1170th parameter set, (c) Derived runoff, (d) Empirical runoff-disruption function, (e) Derived time series of disruption probabilities, (f) Disruption no-taxi-passing probability function average taxi volume in 5 min intervals, and (g) Derived no-taxi-passing probabilities.

350 After the time series of no-taxi-passing probabilities for every parameter set were derived, we can calculate the degree of belief that a given parameter set is optimal was calculated by integrating it with the taxi observations on 9-May 9, 2015. According to Eq. (5), the posterior probability of the 1,170,3,120th parameter set is calculated as:

~~$$P(\theta^{(1170)}|X) \propto P(\Omega^{(1170)}) \mathcal{L}(X|\Omega^{(1170)}) = \frac{1}{3000} \prod_{t=1}^T (1 - \omega_t^{(1170)})^{X_t} (\omega_t^{(1170)})^{1-X_t}$$~~

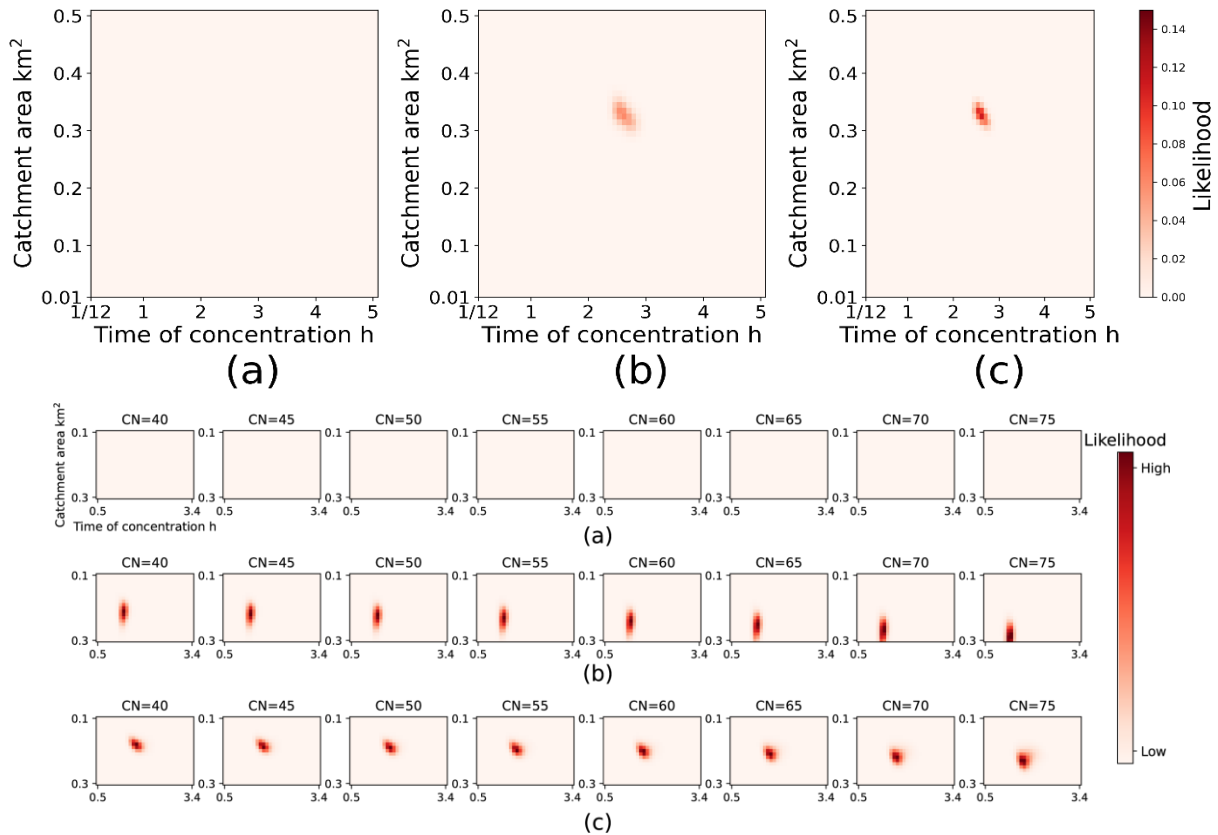
$$P(\theta^{(3120)}|X) \propto L(X|\theta^{(3120)})P(\theta^{(3120)}) = 1/4800 \times \prod_{t=1}^T (1 - \omega_t^{(3120)})^{X_t} (\omega_t^{(3120)})^{1-X_t}$$

where $\mathcal{L}(\theta^{(1170)}|X) \mathcal{L}(\theta^{(3120)}|X)$ is the likelihood-posterior distribution of probabilities that the 1,170,120th parameter set is optimal conditioning conditional on X , which represents the taxi observations on 9-May 9, 2015 shown-presented in Fig. 5(c). The $P(\theta^{(1170)}) P(\theta^{(3120)})$ is the prior probability of the 1,170,120th parameter set to being optimal, and its values is 1/30001 / 4,800 because there are 3,0004,800 possible combinations.

By Following the above process, we can calculate the posterior probabilities for every parameter set. Furthermore Additionally, the posterior probability distribution of a parameter set could-can be updated using the taxi observations and rainfall data on 23-May 23, 2015 as:

$$P(\theta^{(i)}|X_2) \propto \mathcal{L}(X_2|\theta^{(i)})P(\theta^{(i)}|X_1)$$

where $P(\theta^{(i)}|X_1)$ is the original posterior probability distribution calculated-calibrated based on the storm on 9-May 9, 2015, and $P(\theta^{(i)}|X_2)$ is the updated posterior distribution after the data of storm from 23-May 23, 2015 are added. Fig. 7 illustrates the evolution of the probability distribution with the availability of more-additional taxi data. The first row in Fig. 7 represents the prior joint distribution of hydrological parameter sets, and the second and third rows represent the posterior distribution after each round of updating. The posterior distribution dominates the uniform prior distribution after the first updating, and the distribution is refined slightly a little bit after the second updating.



370 **Figure 7** Evolution of the posterior probability distribution of hydrological parameter sets: (a) Prior distribution before updating, (b) Posterior distribution after the first updating, and (c) Posterior distribution after the second updating.

4 Method Validation and result

4.1 Method validation Data description

375 The proposed method was validated upon-on flood-prone roads located in Shenzhen, China, which is a coastal city frequently hit by extreme storms in-during summer. Another reason that Shenzhen is chosen is that only Shenzhen, as far as we known, To the best of our knowledge, Shenzhen is the only city that has shared the-runoff-related data to-with the public in China. Three data sources, which-namely are-taxi GPS data, rainfall data, and authoritative water level data, were are used to validate the-our parameter calibration method. Hydrological parameters are-were calibrated using the first two data sources, and the water level data acts as the ground truth to validate the proposed method. Taxi GPS data were-are anonymized and aggregated to-in-the-road-every-5 min intervals. The-rainfall data, which are-were also collected every-in-5 min intervals, are-were measured at 115 gauging stations citywide, and are-mapped to the road network throughout Shenzhen using the Ordinary Kriging spatial interpolation algorithm. The water level data are-were only measured at some-certain waterlogging-flood-prone points, with a dynamic sampling interval ranging from 5 min when the weather was rainy to 1 h when the weather was clear-rainless. The proposed calibration method was validated by checking-analyzing the hydrographs 385 derived from the calibrated hydrological models and-against the authoritative water levels for 10 selected roads. Detailed information of-on-the three data sources is provided-are-listed-in Table 4.

Table 4 Detailed information of-on-the three data sources.

Item	Taxi GPS data ¹	Rainfall data ¹	Water level data ²
Source	Transport Commission of Shenzhen Municipality	Meteorological Bureau of Shenzhen Municipality	Shenzhen Municipal Government Data Open Platform ¹
Record	Taxi volume of each road	5 min accumulative rainfall	Water level
Data collection period	May 2015	2015 and 2019	2019
Data collection interval	5 min	5 min	5 min -1 h
Location	Citywide	115 rainfall gaging stations	171 flooding gaging sites

¹ The complete taxi GPS data and rainfall data are not openly accessible due-owing to the requirements of data policy. To validate the-our research findings, we have uploaded the necessary data in-to Zenodo (Kong, 2022).

390 ² Openly available at the-site: https://opendata.sz.gov.cn/data/dataSet/toDataDetails/29200_01403147.

The-Two storm events, occurred on 9-May 9, 2015 and 23-May 23, 2015 are-were treated as calibration events and the-a storm occurred on 11-June 11, 2019, was retained for testing. Obviously-Clearly, there is a four4 year span-gap between the calibration data and validation data due-to-based on the data availability. The hydrological environments of flood-prone roads may have changed during these years, which could render the parameters calibrated based on data from 2015 inaccurate for

395 ~~analysis in 2019.~~ To reduce the validation error caused by ~~this~~ the time ~~difference~~ gap, the roads to be validated should ~~have~~ ~~been~~ vulnerable to flooding ~~on~~ in both 2015 and 2019 so that ~~the~~ hydrological parameters of these roads ~~would~~ have a higher chance ~~to~~ of remaining unchanged. Therefore, ~~in~~ a total of 10 flood-prone roads, ~~which~~ ~~that~~ were labelled as ~~flood-prone roads~~ such in ~~on~~ both the List of 2015 Flood-prone Roads in Shenzhen (Water Authority of Shenzhen Municipality, 2015) and the List of 2019 Flood-prone Roads in Shenzhen (Water Authority of Shenzhen Municipality, 2019), were carefully selected (Fig. 8).

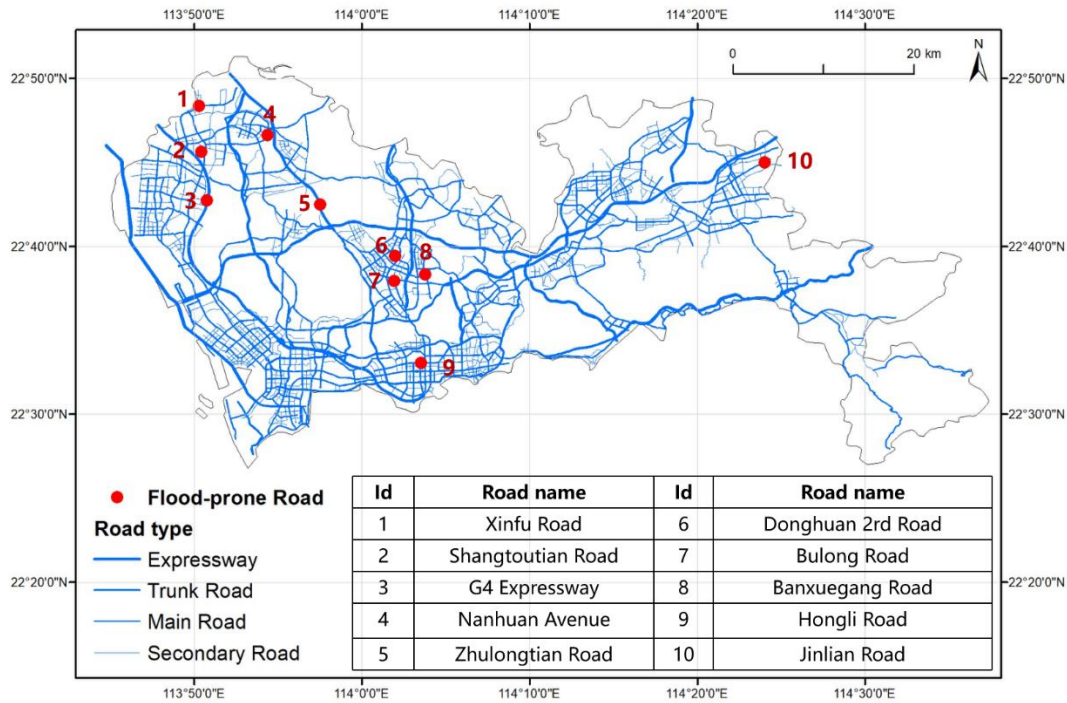


Figure 8 Spatial distribution of 10 flood-prone roads in Shenzhen.

405 Next, the posterior probability of parameter sets after calibration for the 10 roads are illustrated in Fig.9. As shown in Fig.9, the posterior probability distribution of parameter sets for most flood-prone roads are clustered around the optimal parameter set after two runs of updating, indicating that the uncertainty of parameter sets is refined to a much smaller area when taxi observations are added. It should also be noted that the posterior probability of parameter set for the Jinlian Road (Road ID=10) is evenly distributed on a triangular region (Fig.9j). By examining the taxi data of the road, we found that the taxi volume was greater than 0 for most 5-min intervals during two storms, indicating that the road was not disrupted during two storms. As hydrological parameters are calibrated by adjusting their values such that the runoff generated by the acceptable parameter sets could yield the disruption period during which no taxi points are observed, the lack of no-taxi passing period would provide less information for calibration compared with when no-taxi passing period is observed. This explains why the posterior probability is not refined to a small area domain. However, we can still get some valuable information from Fig.9j. First, the catchment area for the Jinlian Road should not be too large to generate the runoff which may cause the road disruption.

Second, the catchment area is highly intercorrelated with time of concentration. As the catchment area gets larger, the time of concentration is more likely to increase so that the high runoff volume could not converge in a short time.

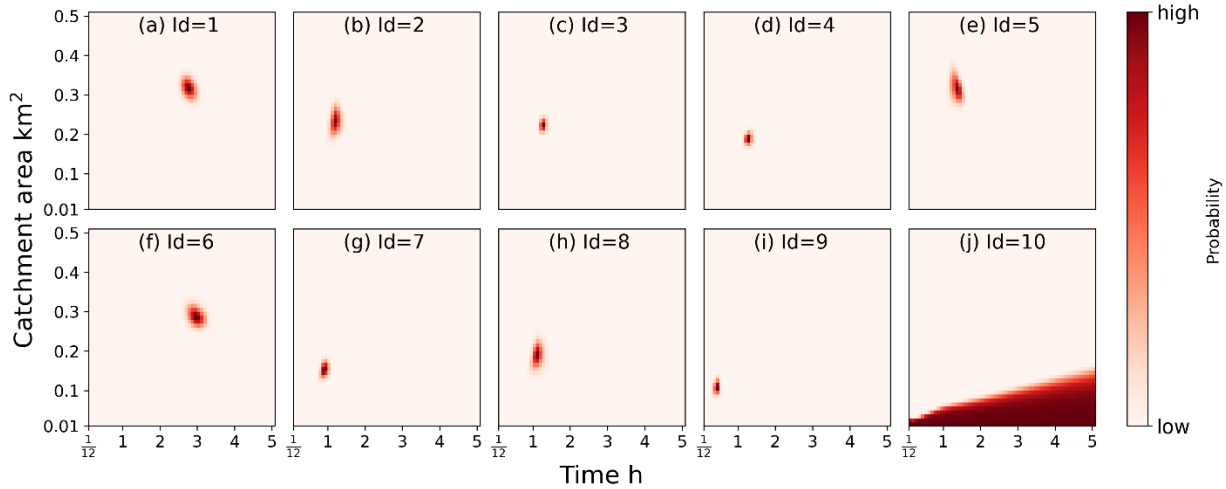


Figure 9 Posterior probability distribution of hydrological parameter sets after the first updating for 10 flood-prone roads. Subplots (a)–(j) represent the probability distribution for Road 1–10.

4.2 Prior distributions of calibrated parameters

We introduced two types of prior distributions to demonstrate the effects of prior distributions on calibrated parameters. The first prior distribution was determined based on prior knowledge and DEMs from Shenzhen, which were obtained from ASTER GDEM V3, which is a product of NASA and Japan’s Ministry of Economy, Trade, and Industry (METI) (ASTER Global Digital Elevation Map, 2023). This global DEM covers the entire land surface of the earth with a 30 m resolution, exhibiting notable improvements in horizontal and vertical accuracy while reducing anomalies compared to previous versions. We inputted the DEMs from Shenzhen into the hydrological software PCSWMM to delineate catchments and calculate the catchment area. Subsequently, we computed the time of concentration using the watershed lag method (Natural Resources Conservation Service, 2010b). As suggested by Zhang and Huang (2018), we used the average curve number for Shenzhen in 2015, which was assessed to be 60, as the estimated curve number for each road under validation.

We then constructed a discretized parameter space for the three parameters for each road as follows. For the curve number, we examined eight possible values centered on 60 with steps of five. For the catchment area, we considered 20 possible values centered on the estimated value with steps of 0.01 km². For the time of concentration, we considered 30 possible values centered on the estimated value with steps of 5 min. After constructing the parameter space for the parameters, we assigned a triangular prior distribution to each, which assumed the maximum probability at the estimated value and linearly decreased to zero at the parameter space boundaries, as depicted in Fig. 9.

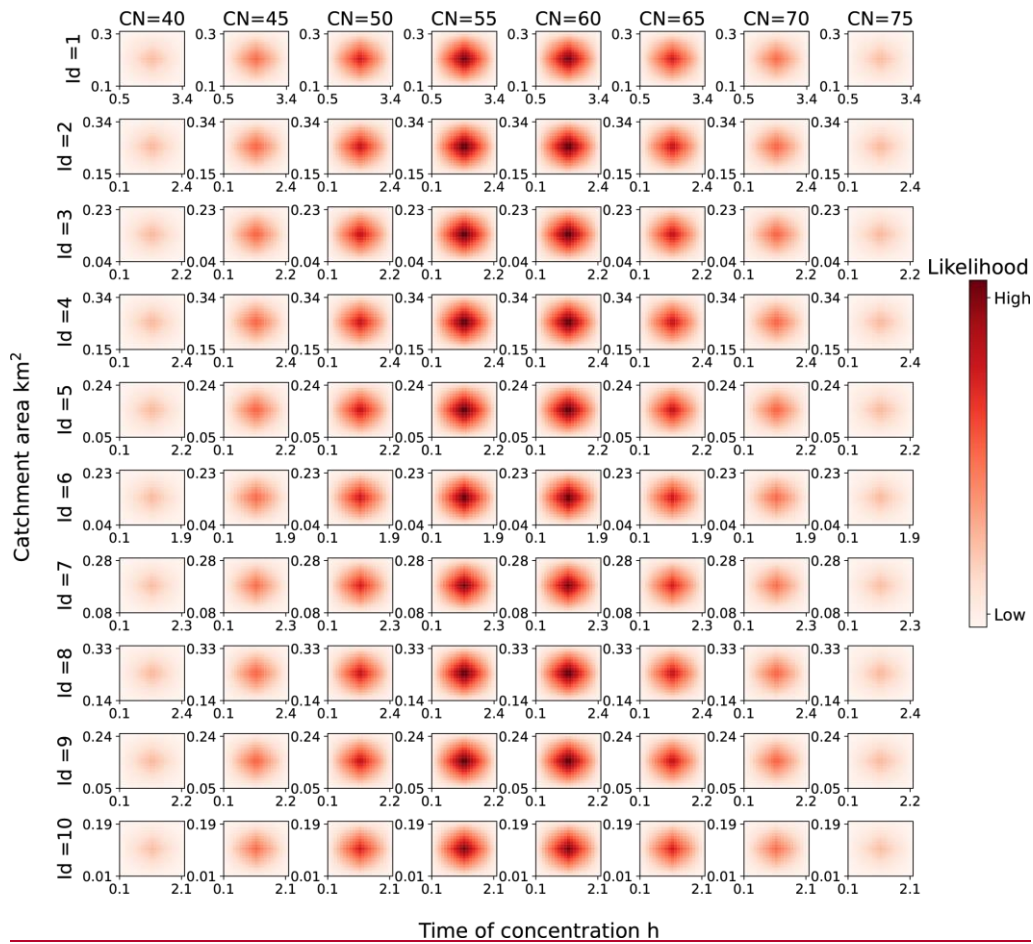


Figure 9 Prior probability distributions of hydrological parameter sets based on DEMs and other prior knowledge for 10 flood-prone roads.

The second prior distribution assumed that the three parameters all follow uniform distributions. The parameter spaces for the second prior distribution were the same as those for the first. As a result, the joint probability of each parameter set was equal to $(1 / 20) \times (1 / 30) \times (1 / 8)$. To facilitate comparisons, we present the detailed information on the two types of prior distributions in Table 4.

Table 4 Detailed information of the two types of prior distributions.

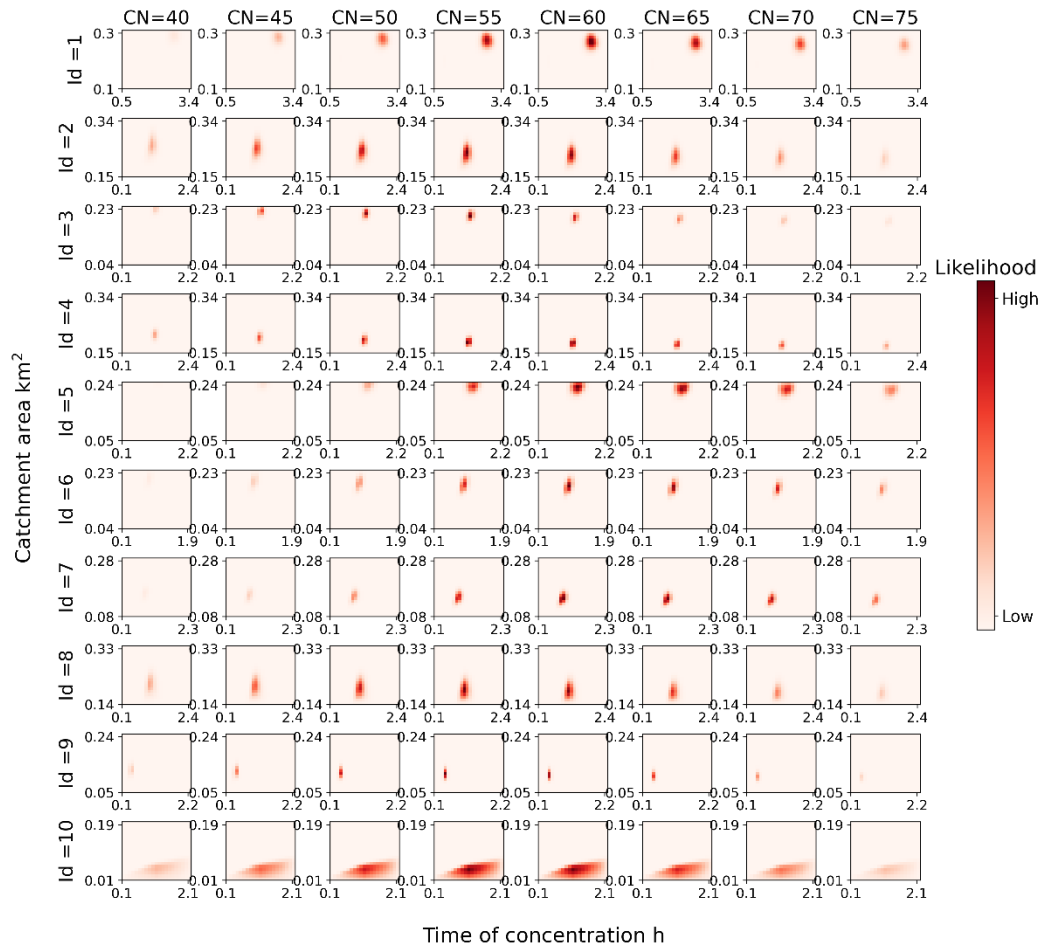
Item	Prior probability distributions based on DEM and other knowledge			Uniform distributions		
	Number of possible values	Parameter interval	Prior marginal distribution	Number of possible values	Parameter interval	Prior marginal distribution

<u>Curve number</u>	<u>8</u>	<u>5</u>	<u>Maximum probability at 60 and linearly reduces to zero at the parameter space boundaries</u>	<u>8</u>	<u>5</u>	<u>1/8 for each possible value</u>
<u>Catchment area</u>	<u>20</u>	<u>0.01</u>	<u>Maximum probability at the estimated value and linearly reduces to zero at the parameter space boundaries</u>	<u>20</u>	<u>0.01</u>	<u>1/20 for each possible value</u>
<u>Time of concentration</u>	<u>30</u>	<u>1/12</u>	<u>Maximum probability at the estimated value and linearly reduces to zero at the parameter space boundaries</u>	<u>30</u>	<u>1/12</u>	<u>1/30 for each possible value</u>

4.3 Posterior distributions after calibration

445 We first calibrated the parameters based on the prior distributions calculated according to the DEMs and other prior knowledge. The resulting posterior distributions are presented in Fig. 10. Each row in Fig. 10 represents a different road, and each column represents a curve number. Each subplot presents the joint probability distribution of the catchment area and time of concentration for a given curve number. The color intensity in Fig. 10 represents the magnitude of the probabilities. Following two iterations of updating, the posterior probability distributions for both the catchment area and time of
450 concentration converge around the optimal parameter sets for most flood-prone roads. This demonstrates that incorporating taxi observations significantly reduces the uncertainty associated with catchment area and time of concentration. The probability typically achieves its maximum value when the curve number is either 55 or 60. Furthermore, each subplot contains a salient cluster with higher probability than other regions, suggesting that there may be multiple acceptable parameter sets.

455 Furthermore, the optimal catchment area under a given curve number decreases as the curve number increases, whereas the optimal time of concentration under a given curve number increases with the curve number. This is logical, because a higher curve number corresponds to increased rainfall excess under identical rainfall conditions, requiring a reduction in catchment area to maintain the runoff that best aligns with the taxi observations. Similarly, an increase in the time of concentration diminishes the peak runoff produced by the additional runoff generated by a higher curve number, thereby preserving the optimal runoff status.



460

Figure 10 Posterior probability distributions of hydrological parameter sets for 10 flood-prone roads after calibration. The prior probability distributions were derived from the DEMs and additional prior knowledge.

We also present the marginal distributions of the three parameters for 10 roads before and after calibration in Fig. 11. In Fig. 11, the marginal posterior distributions of the curve number appear relatively similar to the marginal prior distributions. It seems that the proposed method employing taxi data provides limited information regarding the distribution of curve numbers compared to the catchment area and time of concentration. This outcome may be a result of the range and discretization granularity of the parameter spaces. Catchment area and time of concentration encompass 20 and 30 possible values, respectively, whereas the curve number has only 8 potential values. The smaller parameter space of the curve number reduces the search space, and its impact on the no-taxi-passing probability is comparatively lower than that of the catchment area and time of concentration.

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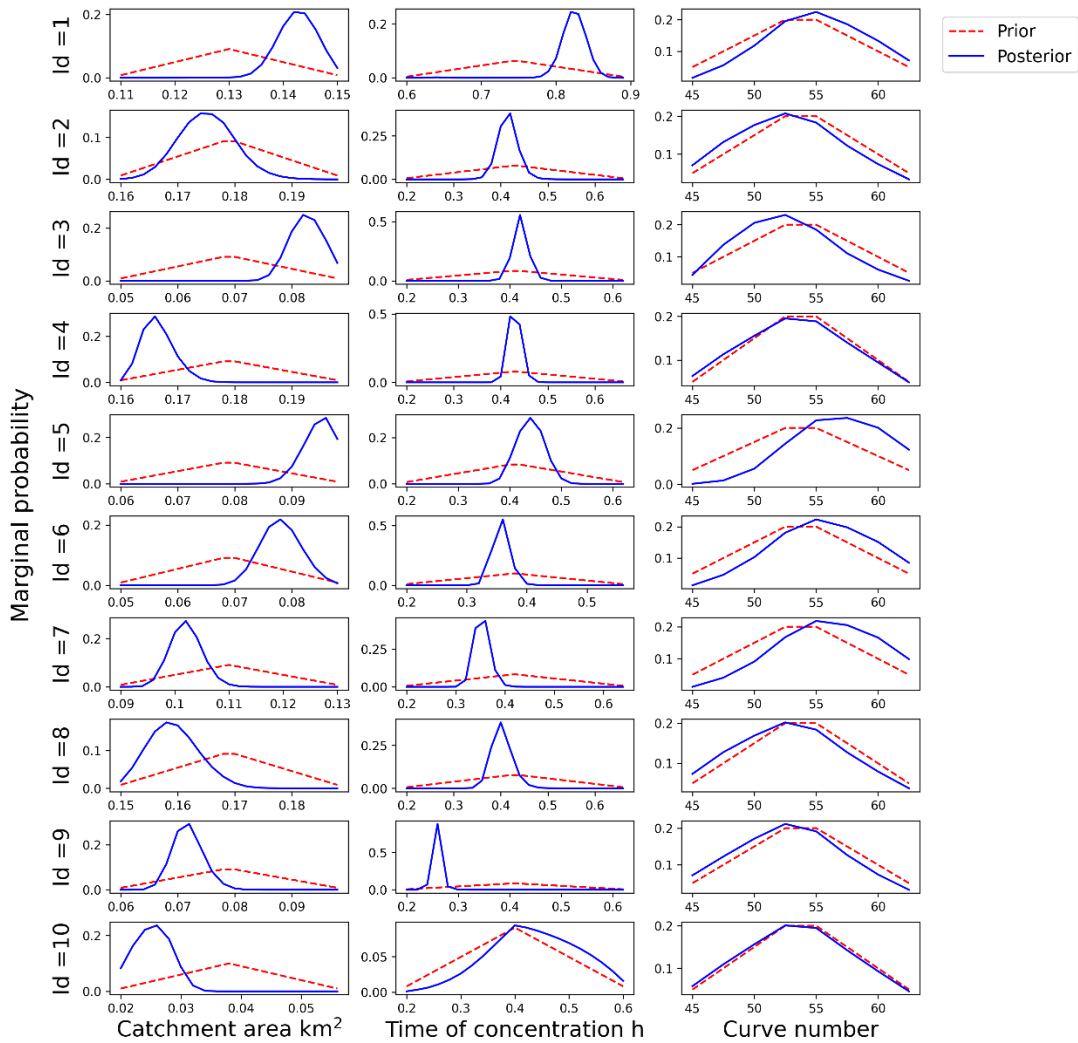
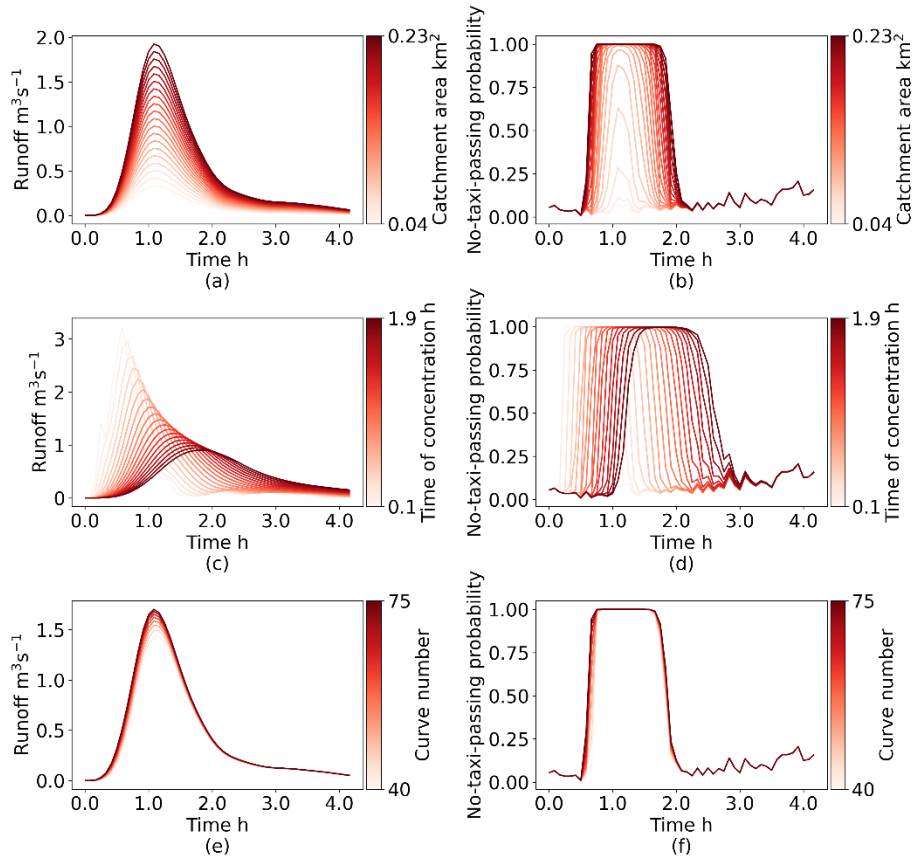


Figure 11 Marginal prior and posterior probability distributions of the curve number for 10 flood-prone roads.

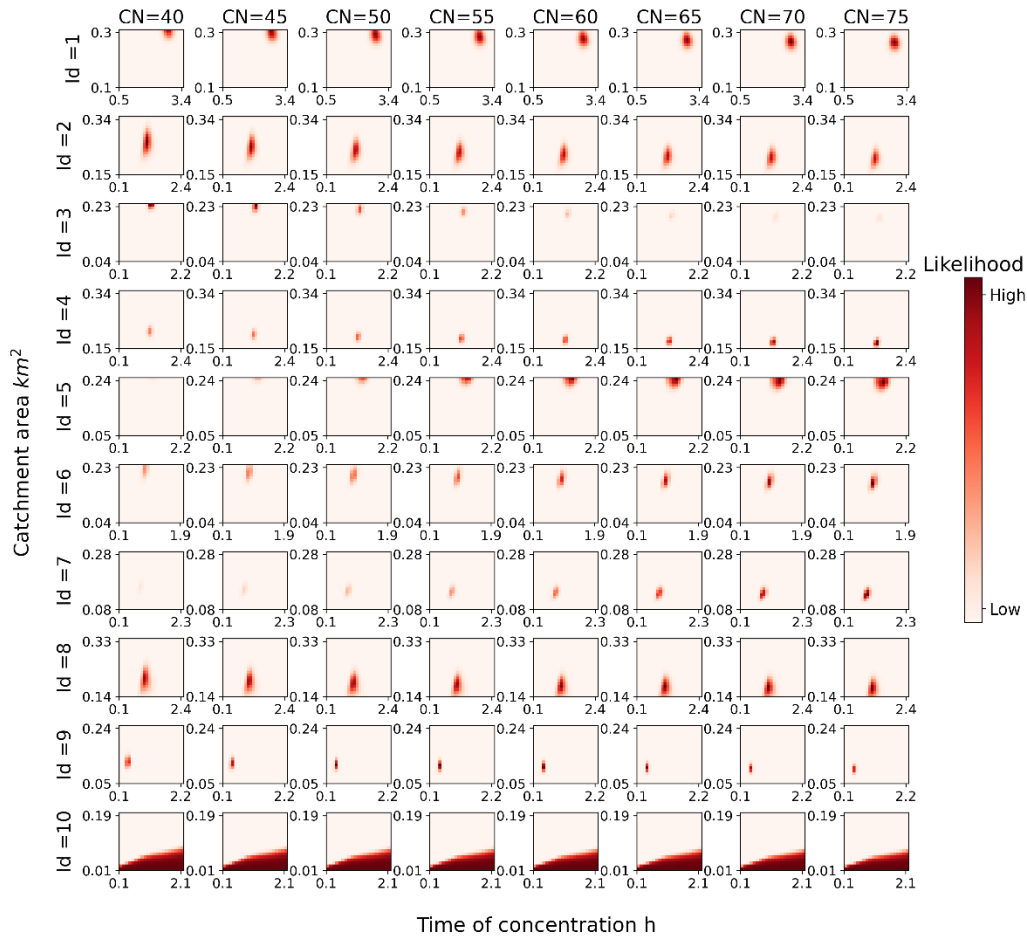
For example, for road ID = 6, the optimal parameter set consists of a catchment area of 0.19 km², time of concentration of 0.9 h, and curve number of 55. To investigate the effects of these parameters on the hydrograph and time series of no-taxi-passing probabilities, we held two parameters constant at their optimal values and observed the impact of changing the third parameter. Our findings are presented in Fig. 12. One can see that when the catchment area varies from 0.04 to 0.23 km², the maximum no-taxi-passing probability increases from 20% to 100% and the duration for which the no-taxi-passing probability exceeds 0.5 increases from 0.0 to 1.3 h. Similarly, when the time of concentration fluctuates from 0.1 to 1.9 h, the peak time of the no-taxi-passing probability varies from 0.5 to 1.8 h. In contrast, when the curve number varies from 40 to 75, the maximum no-taxi-passing probability is fixed at 100%, the duration for which the no-taxi-passing probability exceeds 0.5 extends from 1.1 to 1.3 h, and the peak time of the no-taxi-passing probability remains fixed at the 1.1 h. These

small fluctuations in the time series of no-taxi-passing probabilities are representative of why the distribution of curve numbers remains relatively stable after calibration compared to the catchment area and time of concentration.



485 **Figure 12** Impacts of three parameters on the variation of the time series of runoff and no-taxi-passing probabilities: (a) catchment area conditional on runoff, (b) catchment area conditional on the no-taxi-passing probability, (c) time of concentration conditional on runoff, (d) time of concentration conditional on the no-taxi-passing probability, (e) curve number conditional on runoff, and (f) curve number conditional on the no-taxi-passing probability.

490 The posterior distributions calibrated based on the uniform prior distribution are presented in Fig. 13. When comparing two posterior distributions derived from two prior distributions, it is clear that the posterior distributions of the catchment area and time of concentration are very similar, indicating that the impact of prior distributions on these parameters rapidly diminishes after taxi-related knowledge is added. As stated by Beven and Binley (1992 pp: 286), “as soon as information is added in terms of comparisons between observed and predicted responses then, if this information has value, the distribution of calculated likelihood values should dominate the uniform prior distribution when uncertainty estimates are recalculated.”



495

Figure 13 Posterior probability distributions of hydrological parameter sets for 10 flood-prone roads after calibration. The prior probability distributions were derived from a uniform distribution.

4.4 Validation results

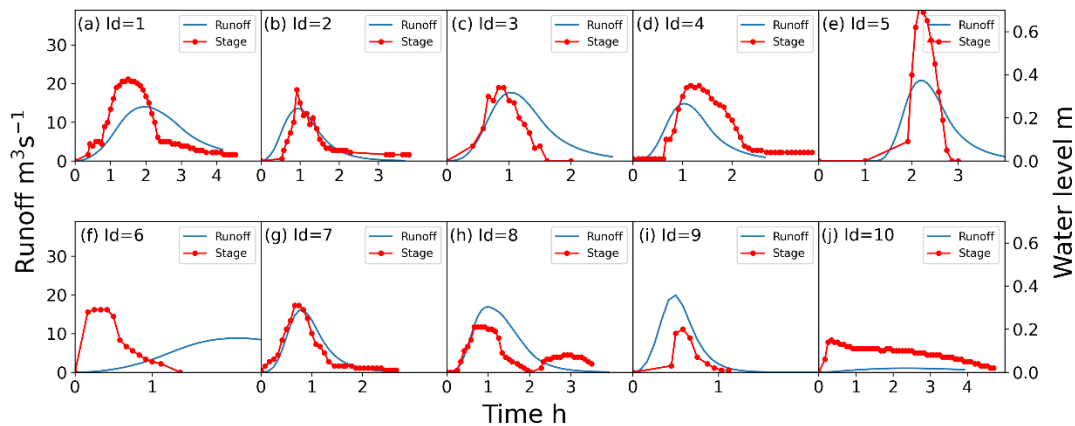
After the parameter sets were calibrated, they were combined with ~~the an~~ SCS unit hydrograph to construct ~~the an~~ SUH, which ~~were was further~~ combined with the rainfall data ~~occurring from on 11~~ June 11, 2019 to produce the predicted hydrograph. ~~As Because~~ the posterior probability associated with each parameter set can be regarded as a fuzzy measure reflecting the degree of belief that the parameter set is true, the weighted runoff ~~s values~~ for each parameter set were summed to ~~produce calculate~~ the final predicted runoff:

$$Q = \sum_{i=1}^N P(\theta^{(i)}|X)Q^{(i)} \quad (17)$$

505 ~~where-Here.~~ Q is the final predicted runoff, $Q^{(i)}$ is the simulated runoff derived from the i th parameter set, and $P(\theta^{(i)}|X)$ is the posterior probability of the i th parameter set, ~~which acting-acts as the-a~~ weight.

The output of the calibrated hydrological model is runoff (with ~~the-units~~ of $\text{m}^3 \text{s}^{-1}$), whereas the validation data ~~areis~~ water level ~~data~~ (with ~~the-units~~ of m). ~~BecauseAs~~ the calibration data and validation data ~~arise-came~~ from multiple sources and have different units, conventional error-based statistics such as the mean absolute error (~~MAE~~)~~wereare~~ not suitable ~~forin~~ this study. ~~Most-often,-t~~The discharge of a stream is rarely measured directly. Instead, streamflow is typically determined by converting measured water depth (i.e., ~~water~~ stage) into discharge through a rating curve, which provides a functional relationship between ~~the water~~ stage and discharge at a specified point (Le Coz et al., 2014). Inspired by the application of the rating curve, we validated ~~the-our~~ method by ~~developing-the-rating-curve-for-every-road,-and-then-estimate-estimating~~ the goodness-of-fit ~~between-the-water-level-which-was-measured-in-the-field-and-the-corresponding-runoff-which-was-predicted~~ ~~based-on-the-proposed-calibration-method,-of-those-rating-curves.-A-higher-goodness-of-fit-indicates-synchronous-trends~~ ~~between-the-runoff-and-water-level,-which-indirectly-demonstrates-the-feasibility-of-the-proposed-method.~~

~~Because-the-posterior-distributions-derived-from-the-two-types-of-prior-distributions-were-very-similar,-we-only-considered-the-posterior-distribution-calibrated-based-on-prior-distributions-derived-from-DEMs-and-other-prior-knowledge-for-validation.~~ Comparisons between the observed water depth and ~~the-simulated-runoff~~ for 10 selected roads are ~~shown~~ presented in Fig. 140, and ~~rating-corresponding-curves-scatter-plots-constructed-by-fitting-the-runoff-stage-scatter-plot-are~~ ~~shown-presented~~ in Fig. 154. We use the Pearson correlation coefficient, which measures the linear correlation between two variables, as ~~the-a~~ goodness-of-fit indicator. ~~The-result-showsOne-can-see~~ that 8 of 10 roads ~~have-rating-curves-with-are~~ ~~characterized-by~~ significant positive Pearson coefficients, indicating that the runoff and water have similar and consistent variation ~~processtrends~~.



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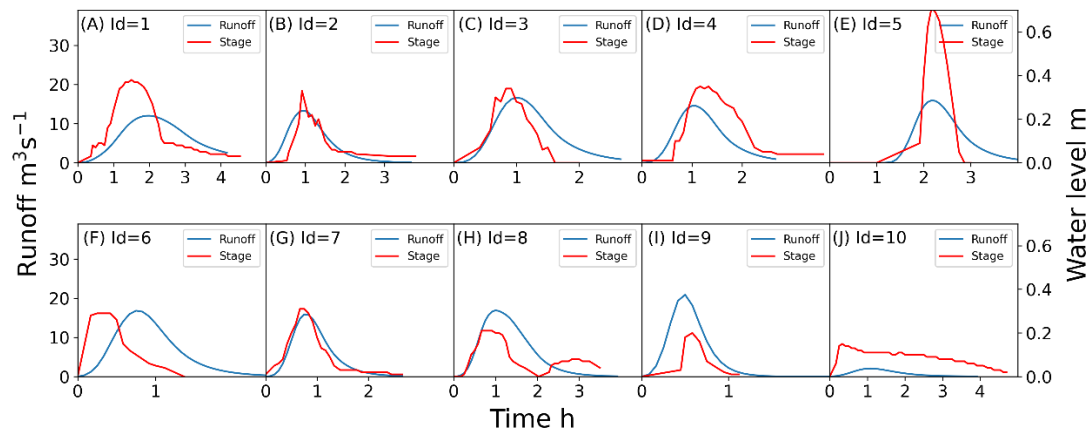


Figure 10-14 Comparisons between the observed water depth and the simulated runoff for roads 1 to-10. The maximum value is $30 \text{ m}^3 \text{ s}^{-1}$ on the left y-axis (i.e., runoff) and 0.6 m on the right y-axis (i.e., stage) for every each subplot.

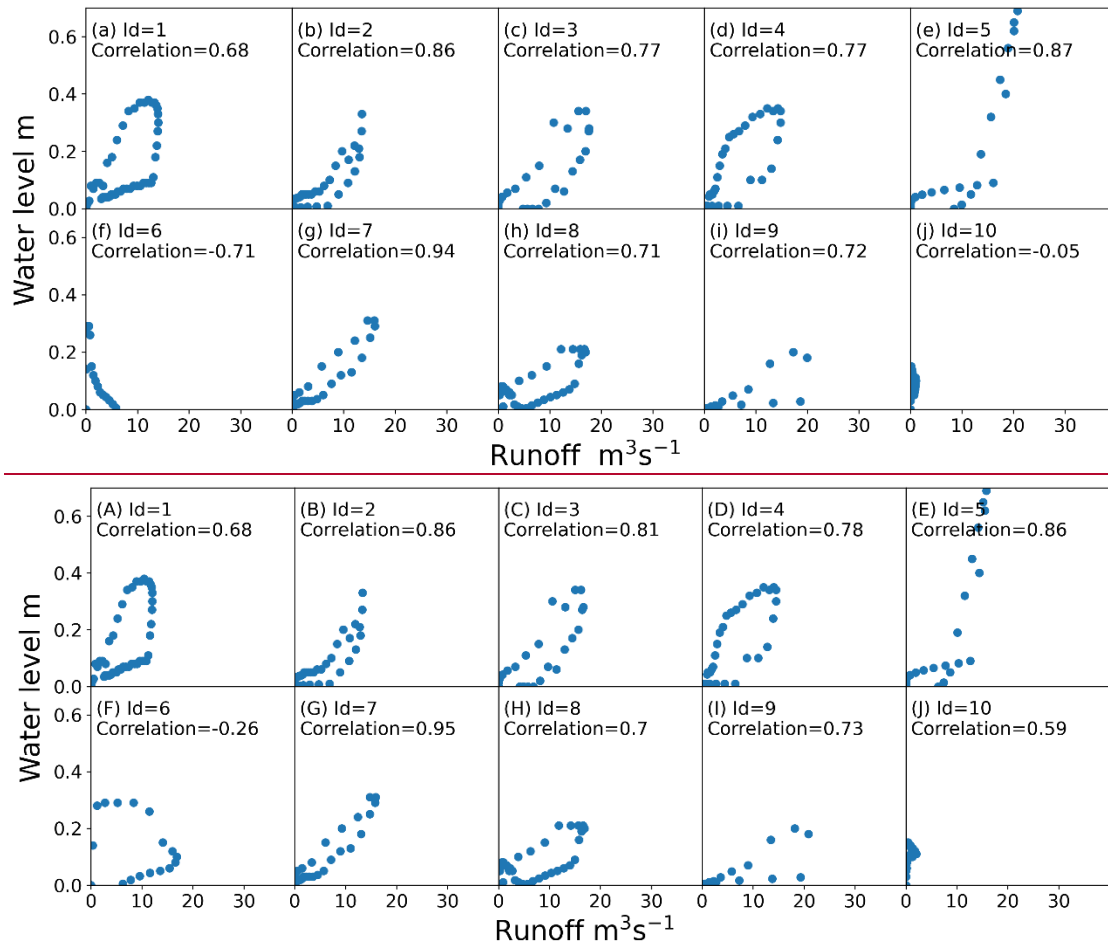


Figure 11-15 Scatter plots (a-j) of the observed water depth and the simulated runoff for roads 1-10.

535 It is ~~worth-noteworthy~~ing that goodness-of-fit ~~solely-simply~~ describes the degree of correlation between the observed and simulated data, and may contain validation bias. As suggested by Legates and McCabe (1999), correlation-based statistics ~~are~~is insensitive to additive and proportional differences between ~~the~~simulations and observations. Therefore, ~~the~~ fitting of a rating curve ~~is only a partial~~reveals part of the validation truth, and the usefulness of the ~~proposed~~ calibration method ~~needs~~ requires further ~~inspection~~analysis.

4.2 Application of the method to plot flooding maps in Shenzhen

540 Based on the ~~proposed calibration method~~, we simulated how the road network experiences flooding for different rainfall return periods. Three storm events of different return periods ($T=2, 10,$ and 50 years) were designed according to the Rainfall Intensity Formula of Shenzhen (Meteorological Bureau of Shenzhen Municipality, 2015). Each storm lasts 3 hours, with an accumulative rainfall amount of 159 mm, 230 mm, and 283 mm for the 2, 10, and 50 year return period. Hydrological parameters of high level flood prone roads, including expressway, main road, and secondary road, are calibrated using the taxi data on 9 May 2015 and 23 May 2015. The flood prone roads are identified based on the algorithm proposed in our previous studies (Kong et al., 2022). The road discharges under different rainfall return periods are simulated by inputting the designed rainfall to the calibrated hydrologic models. As an example, Fig.12 shows the spatio-temporal evolution of simulated discharge of parts of the road network, which locate in Baoan District, Shenzhen, for different return periods. With the return periods rising from 2 year to 50 year, the average peak discharge for flood prone roads increases by 80.6%, with the value from $13.9 \text{ m}^3\cdot\text{s}^{-1}$ to $25.1 \text{ m}^3\cdot\text{s}^{-1}$. Inputting the simulated runoff to the empirical runoff disruption function, expressed in Eq.(12), the time series of disruption probability for every road could be derived³. To facilitate discussion, we temporarily define the disruption period as the time when disruption probability is higher than 0.5. The average disruption period for flood prone roads increases from 1.67 h to 3.15 h as the return period increases from 2 year to 50 year.

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³Original runoff should be divided by the road width before inputting to the empirical runoff disruption function.

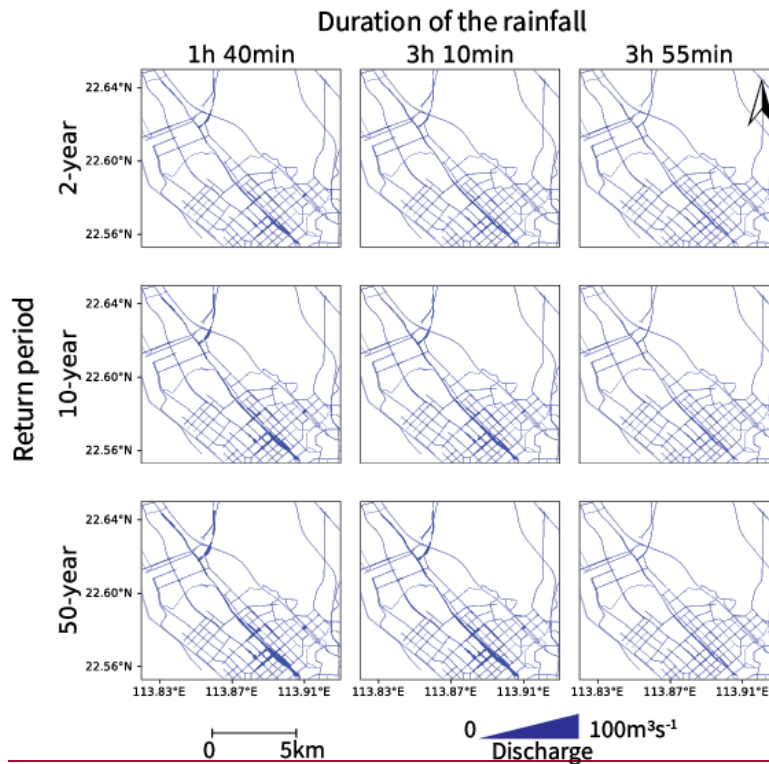


Figure 12 Spatio-temporal evolution of simulated runoff for different return periods in Baoan District, Shenzhen.

5 Discussion

555 Three main points ~~are worth discussing~~ about the proposed calibration method are worthy of further discussion. The first is that, although the presented validation results support the use of taxi GPS data to calibrate hydrological parameters for poorly gauged road networks, the proposed method is more applicable to ~~the roads which that are~~ frequently visited by taxis. Uncertainty increases as the taxi volume ~~of on~~ a road decreases. A road is considered to be passable when at least one taxi GPS points ~~is are~~ observed during ~~the a~~ time interval, ~~while but~~ we cannot assert that ~~the a~~ road is disrupted when the

560 taxi volume is zero. When a road with frequent taxis ~~traffic frequently passing by~~ is observed with no taxi GPS points during ~~the a~~ storm, it is highly probable that the road is disrupted by ~~the~~ flooding, which provides relatively reliable information for parameter calibration. Conversely, when a road with ~~few little~~ taxis ~~visiting traffic~~ has no taxi points during ~~the a~~ storm, there is a ~~great relatively chance high likelihood~~ that the road remains passable and is simply exhibiting its typical trend of just has no taxis ~~as usual~~. Therefore, The the proposed calibration method ~~thus~~ becomes relatively unreliable considering

565 ~~that when the a~~ “no-taxi-passing period” is no longer a good proxy for of the “disruption period” ~~for the taxi data sparse road on a road with sparse taxi data~~. To compensate for ~~the a~~ shortage of ~~the a~~ taxi GPS data, extra additional data sources, such as ride-hailing data and bus data, should be incorporated in ~~the~~ future work.

Secondly, the disruption of one road may cause cascading failures, so that where the disruption is may be rapidly propagating from the inundated road to the adjacent non-inundated roads under the constraints of the road connectivity. For a road which that is disrupted, but not inundated by the a storm, the implementation of the proposed calibration method may be subject to structural errors. Assume Consider there are two connected roads called, namely Road 1 and Road 2, which that are both disrupted during a storm, and have taxi volumes of two roads are therefore of zero (Fig. 13 16). The difference lies in that In this case, Road 1 is disrupted by the flooding, while whereas Road 2 is only disrupted due to because it is connected to the disrupted road, i.e. Road 1. If taxi data are is the only data source used for calibration, then the posterior distributions of the hydrological parameters for Road 1 and Road 2 should will be identical after calibration, because the sequences of taxi volume are identical for both roads. Clearly However, we know that the hydrological parameters for of these two roads could are not be the same, because only one road is flooded otherwise Road 1 and Road 2 should be both flooded. Just like we cannot simply treat the “no-taxi-passing period” as the “disruption period”, we cannot confuse the “disruption period” with the “flooded period.” In the future work, an algorithm that facilitates enabling to distinguishing the flooding-induced disruption and the from connectivity-induced disruption should be developed.

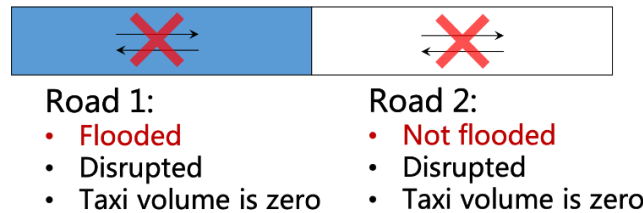


Figure 13-16 A graphical representation to show highlighting the difference between the “disruption period” and flooded period the “no-taxi-passing period.”

Thirdly, the specific-proposed three-step process, which consists of the an SCS unit hydrograph, the empirical runoff-disruption function, and the Poisson distribution, is performs as a realization of the generalized framework shown-presented in Fig. 1. The sSub-models used in of the three-step process are not deterministic, and can be flexibly substituted-replaced with by other sub-models according to the needed-complexity requirements and data availability. For example, an alternative to the SCS unit hydrograph is the distributed hydrological model. Unlike Compared with the SCS unit hydrograph, the distributed hydrological model partitions a watershed into physically homogeneous units and captures the complex spatial variation induced by human activity in high resolution, which may be more applicable to the urbanized environments, such as the road networks. However, considering that some critical data such as including the road drainage data and land use data are missing, as well as the calibration procedure will become extremely computationally intensive cost associated with the distributed hydrological model, we did not use the distributed hydrological model adopt this model in this study. Another assumption we made in this study is that the number of taxis arriving at a road follows a Poisson distribution. By conducting the Chi-square goodness of fit test, we found that the frequency distribution of taxi volumes adheres to a Poisson distribution for more than 50% of 5 min intervals for 7 of the 10 roads presented in Fig. 8, indicating that the Poisson model appears to be a suitable

assumption. However, this hypothesis may not be universally applicable, particularly in different urban contexts, where alternate distributions such as the Weibull distribution may provide a more accurate representation.

6 Conclusion

600 An urban flooding model requires various types of data for calibration. In this study, we proposed a Bayesian calibration framework for the hydrological parameters of ~~the a~~ road network based on ~~the~~ taxi GPS data. A three-step procedure, consisting of a rainfall-runoff model, ~~a~~ runoff-disruption ~~model~~function, and ~~a~~ ~~disruption~~ no-taxi-passing probability model, ~~enables~~ enabled us to transform ~~the a~~ given rainfall time series into the a time series of no-taxi-passing probabilities for each parameter set, which is key to ~~the~~ taxi-data-driven model calibration. The calculated no-taxi-passing probabilities, which acting-acted as a proxy ~~for~~ the associated hydrological parameter sets, ~~is further were~~ compared ~~with the~~ observed taxi data ~~through~~ based on the Bayes equation to assess the posterior probability distributions of the hydrological parameter sets. Three parameters, namely the curve number, catchment area, and time of concentration, were calibrated. The proposed calibration method ~~was~~ instantiated by combining ~~some~~ classical hydrological ~~models and with~~ traffic flow models, and ~~is was~~ validated on 10 flood-prone roads in Shenzhen. The validation results ~~show indicate~~ that the trends of runoff could be correctly predicted
610 for ~~eight~~ roads, which demonstrates the potential of calibrating hydrological parameters based on taxi GPS data indicating a good performance for hydrological parameter calibration.

This study ~~illustrates highlights~~ the great potential of integrating transportation-related data with hydrological theory for ~~the~~ transportation resilience improvement and flood risk management ~~for of the~~ road networks. We hope that our study can provides a flexible calibration framework for countries ~~which that are short of~~ have little runoff data, but rich ~~of~~ taxi data. We
615 ~~accept acknowledge~~ that the application of the proposed method is currently limited by the heterogeneous spatial distributions of taxis citywide and ~~the~~ cascading effects of road inundation, but expect this to change with the increasing availability of vehicle data and continuously optimization of modelling approaches.

Code and data availability

The data and code used to validate the proposed method are available ~~on at~~ Zenodo
620 (<https://doi.org/10.5281/zenodo.7894921><https://doi.org/10.5281/zenodo.7294849>).

Author contributions

JY ~~conceptualised~~ conceptualized the article and collected ~~the~~ field data. XK designed the methodology and was responsible for ~~the~~ code compilation. KX plotted the figures and revised the manuscript. BD ~~managed~~ managed the

implementation of research activities. SJ discussed ~~the~~ results and contributed to ~~the~~ method validation. XK wrote the final
625 version of the article with contributions from all co-authors.

Competing interests

The ~~contact-corresponding~~ author ~~has declared~~ ~~declares~~ that none of the authors ~~have~~s any competing interests.

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