

Supplement data for:
Calibrating macro-scale hydrological models in poorly gauged and heavily regulated basins

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Table S1. Design specifications of the hydropower dams on the mainstream of the Lancang River. Data retrieved from Do et al. (2020).

| Name | COM | Height (m) | MWL (m) | DWL (m) | MWA (km ²) | Dead storage (MCM) | Full storage (MCM) | Hydropower capacity (MW) |
|-------------|------|---------------|------------|------------|---------------------------|-----------------------|-----------------------|-----------------------------|
| Jinghong | 2009 | 108 | 602 | 595 | 510 | 810 | 1119 | 1750 |
| Nuozhadu | 2014 | 262 | 812 | 756 | 320 | 10414 | 21749 | 5850 |
| Dachaoshan | 2003 | 115 | 899 | 887 | 826 | 465 | 740 | 1350 |
| Manwan | 1992 | 132 | 994 | 982 | 415 | 630 | 887 | 1670 |
| Xiaowan | 2010 | 292 | 1236 | 1162 | 194 | 4750 | 14645 | 4200 |
| Gongguoqiao | 2012 | 105 | 1319 | 1311 | 343 | 196 | 316 | 900 |
| Miaowei | 2016 | 140 | 1408 | 1373 | 171 | 359 | 660 | 1400 |
| Dahuaqiao | 2018 | 106 | 1477 | 1466 | 148 | 252 | 293 | 920 |
| Huangdeng | 2017 | 203 | 1619 | 1604 | 199 | 1031 | 1418 | 1900 |
| Wunonglong | 2018 | 138 | 1906 | 1894 | 163 | 236 | 272 | 990 |

COM Year of commission

MWL Maximum water level

DWL Dead water level

MWA Maximum water surface area

Table S2. List of Landsat-5 images used to identify the river cross-section at the virtual station.

| ID | Collection Date (dd/mm/yyyy) | River Width | Water Level* |
|--|---------------------------------|-------------|--------------|
| | | (m) | (m) |
| LT05_L1TP_129046_20080929_20161029_01_T1 | 29/09/2008 | 240 | 298.36 |
| LT05_L1TP_129046_20081015_20161029_01_T1 | 15/10/2008 | 240 | 297.47 |
| LT05_L1TP_129046_20081202_20170111_01_T1 | 02/12/2008 | 210 | 291.89 |
| LT05_L1TP_129046_20081218_20170111_01_T1 | 18/12/2008 | 210 | 290.75 |
| LT05_L1TP_129046_20090119_20161028_01_T1 | 19/01/2009 | 210 | 288.80 |
| LT05_L1TP_129046_20090220_20161027_01_T1 | 20/02/2009 | 180 | 287.39 |
| LT05_L1TP_129046_20090308_20161029_01_T1 | 08/03/2009 | 180 | 286.77 |
| LT05_L1TP_129046_20091018_20161019_01_T1 | 18/10/2009 | 210 | 293.50 |
| LT05_L1TP_129046_20091103_20161023_01_T1 | 03/11/2009 | 210 | 292.51 |
| LT05_L1TP_129046_20091205_20161017_01_T1 | 05/12/2009 | 210 | 288.93 |
| LT05_L1TP_129046_20100207_20161017_01_T1 | 07/02/2010 | 180 | 285.88 |
| LT05_L1TP_129046_20100223_20161016_01_T1 | 23/02/2010 | 180 | 284.06 |
| LT05_L1TP_129046_20100428_20161015_01_T1 | 28/04/2010 | 180 | 287.85 |
| LT05_L1TP_129046_20100514_20161015_01_T1 | 14/05/2010 | 180 | 287.22 |
| LT05_L1TP_129046_20100903_20161014_01_T1 | 03/09/2010 | 240 | 297.37 |
| LT05_L1TP_129046_20101106_20161012_01_T1 | 06/11/2010 | 210 | 293.59 |
| LT05_L1TP_129046_20110125_20161010_01_T1 | 25/01/2011 | 210 | 288.38 |
| LT05_L1TP_129046_20110210_20161010_01_T1 | 10/02/2011 | 180 | 287.45 |
| LT05_L1TP_129046_20110415_20161209_01_T1 | 15/04/2011 | 180 | 287.74 |

* obtained by Jason-2/3 on the corresponding day

Table S3. Model calibration performance calculated for twelve selected solutions, i.e., those yielding the top 25% performance in terms of NSE, TRMSE, MSDE, and ROCE. The performance metrics are calculated by comparing simulated and remote-sensed discharge at the virtual station.

| No. | NSE | TRMSE | MSDE | ROCE |
|-----|-------|-------|--------|-------|
| 1 | 0.689 | 3.353 | 891526 | 0.035 |
| 2 | 0.689 | 3.353 | 891388 | 0.035 |
| 3 | 0.689 | 3.354 | 890904 | 0.035 |
| 4 | 0.688 | 3.360 | 897298 | 0.040 |
| 5 | 0.687 | 3.356 | 891553 | 0.030 |
| 6 | 0.687 | 3.345 | 908805 | 0.033 |
| 7 | 0.687 | 3.345 | 908805 | 0.033 |
| 8 | 0.686 | 3.343 | 891400 | 0.036 |
| 9 | 0.686 | 3.343 | 891400 | 0.036 |
| 10 | 0.686 | 3.343 | 890948 | 0.036 |
| 11 | 0.686 | 3.343 | 891457 | 0.036 |
| 12 | 0.686 | 3.337 | 891369 | 0.039 |

Table S4. Model validation performance calculated for the twelve selected solutions. The performance metrics are calculated by comparing simulated and observed discharge at Chiang Saen station.

| No. | NSE | TRMSE | MSDE | ROCE |
|-----|-------|-------|---------|-------|
| 1 | 0.616 | 3.908 | 1062099 | 0.169 |
| 2 | 0.608 | 3.919 | 1058180 | 0.183 |
| 3 | 0.608 | 3.919 | 1058419 | 0.183 |
| 4 | 0.608 | 3.920 | 1057966 | 0.183 |
| 5 | 0.599 | 3.891 | 1058223 | 0.170 |
| 6 | 0.598 | 3.904 | 1058282 | 0.177 |
| 7 | 0.598 | 3.904 | 1058282 | 0.177 |
| 8 | 0.598 | 3.906 | 1058083 | 0.178 |
| 9 | 0.598 | 3.905 | 1058305 | 0.178 |
| 10 | 0.596 | 3.935 | 1058645 | 0.195 |
| 11 | 0.594 | 3.911 | 1071282 | 0.187 |
| 12 | 0.594 | 3.911 | 1071282 | 0.187 |

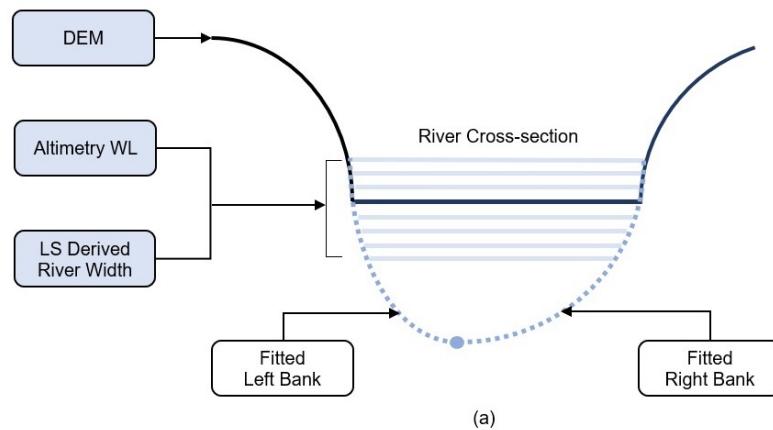
Table S5. Model calibration performance, calculated for the 58 selected solutions (the Pareto front) from model calibration. The performance metrics are calculated between simulated and remote-sensed discharge at the virtual station.

| No. | NSE | TRMSE | MSDE | ROCE | No. | NSE | TRMSE | MSDE | ROCE |
|-----|-------|-------|---------|-------|-----|-------|-------|---------|-------|
| 1 | 0.698 | 3.375 | 1065802 | 0.041 | 30 | 0.688 | 3.330 | 1119978 | 0.027 |
| 2 | 0.697 | 3.363 | 1064265 | 0.046 | 31 | 0.688 | 3.372 | 883766 | 0.038 |
| 3 | 0.696 | 3.420 | 1104404 | 0.013 | 32 | 0.687 | 3.265 | 1240258 | 0.057 |
| 4 | 0.696 | 3.333 | 1296485 | 0.022 | 33 | 0.687 | 3.356 | 891553 | 0.030 |
| 5 | 0.696 | 3.374 | 1061290 | 0.042 | 34 | 0.687 | 3.336 | 897516 | 0.047 |
| 6 | 0.695 | 3.377 | 1060950 | 0.041 | 35 | 0.687 | 3.410 | 884122 | 0.035 |
| 7 | 0.695 | 3.379 | 1039961 | 0.040 | 36 | 0.687 | 3.407 | 885826 | 0.036 |
| 8 | 0.695 | 3.301 | 1298463 | 0.032 | 37 | 0.687 | 3.345 | 908805 | 0.033 |
| 9 | 0.694 | 3.366 | 1172060 | 0.028 | 38 | 0.687 | 3.398 | 883010 | 0.037 |
| 10 | 0.694 | 3.300 | 1296746 | 0.032 | 39 | 0.686 | 3.432 | 854452 | 0.038 |
| 11 | 0.694 | 3.301 | 1297546 | 0.032 | 40 | 0.686 | 3.343 | 891400 | 0.036 |
| 12 | 0.693 | 3.329 | 973419 | 0.041 | 41 | 0.686 | 3.343 | 890948 | 0.036 |
| 13 | 0.693 | 3.324 | 963126 | 0.041 | 42 | 0.686 | 3.420 | 883425 | 0.037 |
| 14 | 0.693 | 3.311 | 1300094 | 0.024 | 43 | 0.686 | 3.337 | 891369 | 0.039 |
| 15 | 0.692 | 3.310 | 1298422 | 0.024 | 44 | 0.685 | 3.271 | 1238422 | 0.059 |
| 16 | 0.692 | 3.303 | 1121617 | 0.032 | 45 | 0.685 | 3.447 | 864589 | 0.037 |
| 17 | 0.692 | 3.305 | 1118386 | 0.031 | 46 | 0.685 | 3.465 | 858494 | 0.037 |
| 18 | 0.692 | 3.286 | 1237423 | 0.039 | 47 | 0.681 | 3.422 | 880224 | 0.045 |
| 19 | 0.691 | 3.307 | 977172 | 0.043 | 48 | 0.680 | 3.348 | 1286568 | 0.024 |
| 20 | 0.691 | 3.387 | 1170933 | 0.018 | 49 | 0.679 | 3.363 | 1269557 | 0.018 |
| 21 | 0.691 | 3.308 | 1230897 | 0.025 | 50 | 0.679 | 3.379 | 1254975 | 0.014 |
| 22 | 0.690 | 3.386 | 1174178 | 0.019 | 51 | 0.673 | 3.452 | 793084 | 0.037 |
| 23 | 0.690 | 3.387 | 1174042 | 0.019 | 52 | 0.672 | 3.425 | 792973 | 0.028 |
| 24 | 0.690 | 3.295 | 1244238 | 0.038 | 53 | 0.670 | 3.428 | 793443 | 0.026 |
| 25 | 0.690 | 3.324 | 962490 | 0.049 | 54 | 0.670 | 3.428 | 793443 | 0.026 |
| 26 | 0.689 | 3.299 | 1244769 | 0.037 | 55 | 0.670 | 3.428 | 793443 | 0.026 |
| 27 | 0.689 | 3.353 | 891526 | 0.035 | 56 | 0.670 | 3.428 | 793443 | 0.026 |
| 28 | 0.689 | 3.353 | 891388 | 0.035 | 57 | 0.656 | 3.545 | 1285269 | 0.007 |
| 29 | 0.689 | 3.354 | 890904 | 0.035 | 58 | 0.646 | 3.588 | 892415 | 0.001 |

Table S6. Model validation performance, calculated for the 58 selected solutions (the Pareto front) from model calibration. The performance metrics are calculated between simulated and observed discharge at Chiang Saen station.

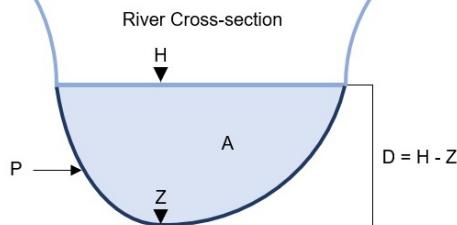
| No. | NSE | TRMSE | MSDE | ROCE | No. | NSE | TRMSE | MSDE | ROCE |
|-----|-------|-------|---------|-------|-----|-------|-------|---------|-------|
| 1 | 0.637 | 3.928 | 989984 | 0.174 | 30 | 0.594 | 3.911 | 1071282 | 0.187 |
| 2 | 0.635 | 3.897 | 988499 | 0.170 | 31 | 0.592 | 3.871 | 1211314 | 0.223 |
| 3 | 0.634 | 3.924 | 1002652 | 0.173 | 32 | 0.592 | 3.872 | 1211245 | 0.223 |
| 4 | 0.632 | 3.716 | 1093794 | 0.139 | 33 | 0.591 | 3.846 | 1335416 | 0.117 |
| 5 | 0.631 | 3.745 | 1093664 | 0.157 | 34 | 0.588 | 4.032 | 993374 | 0.201 |
| 6 | 0.625 | 3.944 | 1047262 | 0.158 | 35 | 0.586 | 3.845 | 1336296 | 0.123 |
| 7 | 0.624 | 3.731 | 1094157 | 0.152 | 36 | 0.581 | 4.041 | 994241 | 0.206 |
| 8 | 0.623 | 3.733 | 1094213 | 0.154 | 37 | 0.581 | 4.041 | 994241 | 0.206 |
| 9 | 0.622 | 3.737 | 1081727 | 0.156 | 38 | 0.581 | 4.041 | 994241 | 0.206 |
| 10 | 0.621 | 3.967 | 1050516 | 0.180 | 39 | 0.581 | 4.041 | 994241 | 0.206 |
| 11 | 0.620 | 3.851 | 1108955 | 0.143 | 40 | 0.574 | 3.923 | 1334334 | 0.174 |
| 12 | 0.619 | 3.957 | 1052596 | 0.180 | 41 | 0.570 | 3.950 | 1376977 | 0.192 |
| 13 | 0.619 | 3.948 | 1050599 | 0.177 | 42 | 0.569 | 3.928 | 1337789 | 0.177 |
| 14 | 0.619 | 3.963 | 1051327 | 0.183 | 43 | 0.568 | 3.960 | 949657 | 0.292 |
| 15 | 0.618 | 3.861 | 1059505 | 0.148 | 44 | 0.567 | 3.932 | 1337865 | 0.179 |
| 16 | 0.616 | 3.927 | 1051718 | 0.176 | 45 | 0.567 | 3.947 | 1248912 | 0.193 |
| 17 | 0.614 | 3.885 | 1119650 | 0.166 | 46 | 0.567 | 3.942 | 1386466 | 0.187 |
| 18 | 0.613 | 3.880 | 1112699 | 0.165 | 47 | 0.566 | 3.944 | 1386968 | 0.187 |
| 19 | 0.610 | 3.842 | 1207660 | 0.197 | 48 | 0.566 | 3.953 | 1246566 | 0.196 |
| 20 | 0.609 | 4.022 | 990455 | 0.180 | 49 | 0.566 | 3.942 | 1388012 | 0.188 |
| 21 | 0.608 | 3.919 | 1058180 | 0.183 | 50 | 0.564 | 4.001 | 1389071 | 0.218 |
| 22 | 0.608 | 3.919 | 1058419 | 0.183 | 51 | 0.561 | 3.970 | 1327052 | 0.214 |
| 23 | 0.605 | 3.883 | 1088908 | 0.171 | 52 | 0.557 | 3.977 | 1246317 | 0.205 |
| 24 | 0.602 | 3.847 | 1119397 | 0.159 | 53 | 0.553 | 3.981 | 1318489 | 0.243 |
| 25 | 0.599 | 3.891 | 1058223 | 0.170 | 54 | 0.552 | 3.975 | 1388532 | 0.211 |
| 26 | 0.598 | 3.904 | 1058282 | 0.177 | 55 | 0.551 | 3.973 | 1389883 | 0.210 |
| 27 | 0.598 | 3.841 | 1133345 | 0.236 | 56 | 0.545 | 3.992 | 1368735 | 0.216 |
| 28 | 0.598 | 3.906 | 1058083 | 0.178 | 57 | 0.539 | 4.015 | 1353742 | 0.232 |
| 29 | 0.596 | 3.935 | 1058645 | 0.195 | 58 | 0.512 | 4.190 | 1053505 | 0.276 |

Figure S1. Approach for constructing the river cross-section at the virtual station (a) and elements of the river cross-section used to construct the rating curve (b). Note that the approach builds on multiple satellite data, namely DEM, altimetry, and river width (derived from Landsat images).



(a)

A : Cross-section Area
P : Wet Perimeter
D : Water Depth
H : Water Level
Z : River Bed Elevation



(b)

Figure S2. Comparison between remote sensed (RS) and simulated discharge at the virtual station. The range of variability of the RS discharge is represented by the medium blue band, while the range of simulated discharge (corresponding to a range of Manning's coefficient $n \in [0.04-0.052]$) is represented by the light green band. The RS discharge estimated with $n = 0.046$ is illustrated by the dark blue line. Finally, the dotted orange line illustrates the discharge estimated by scaling the discharge observed at Chiang Saen by the area ratio.

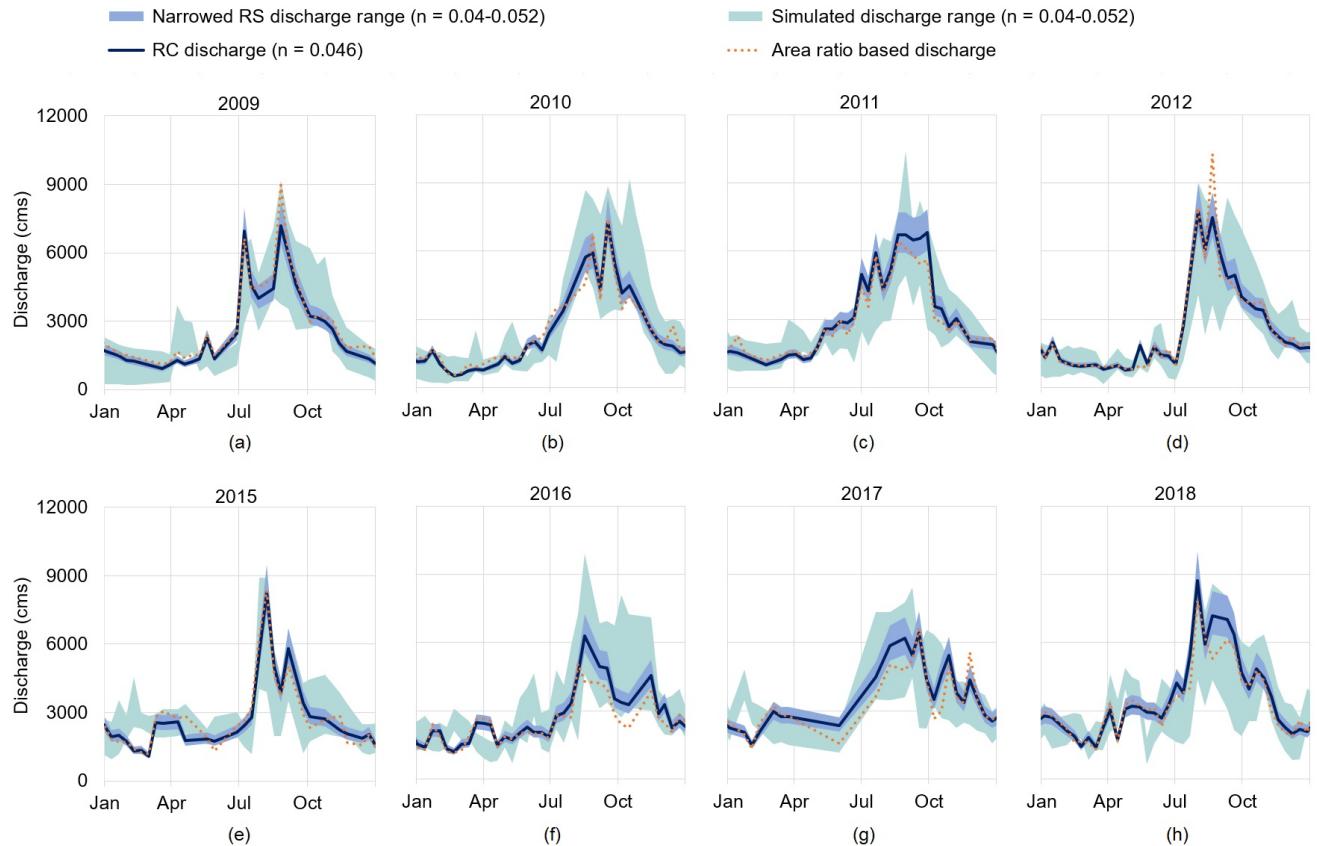
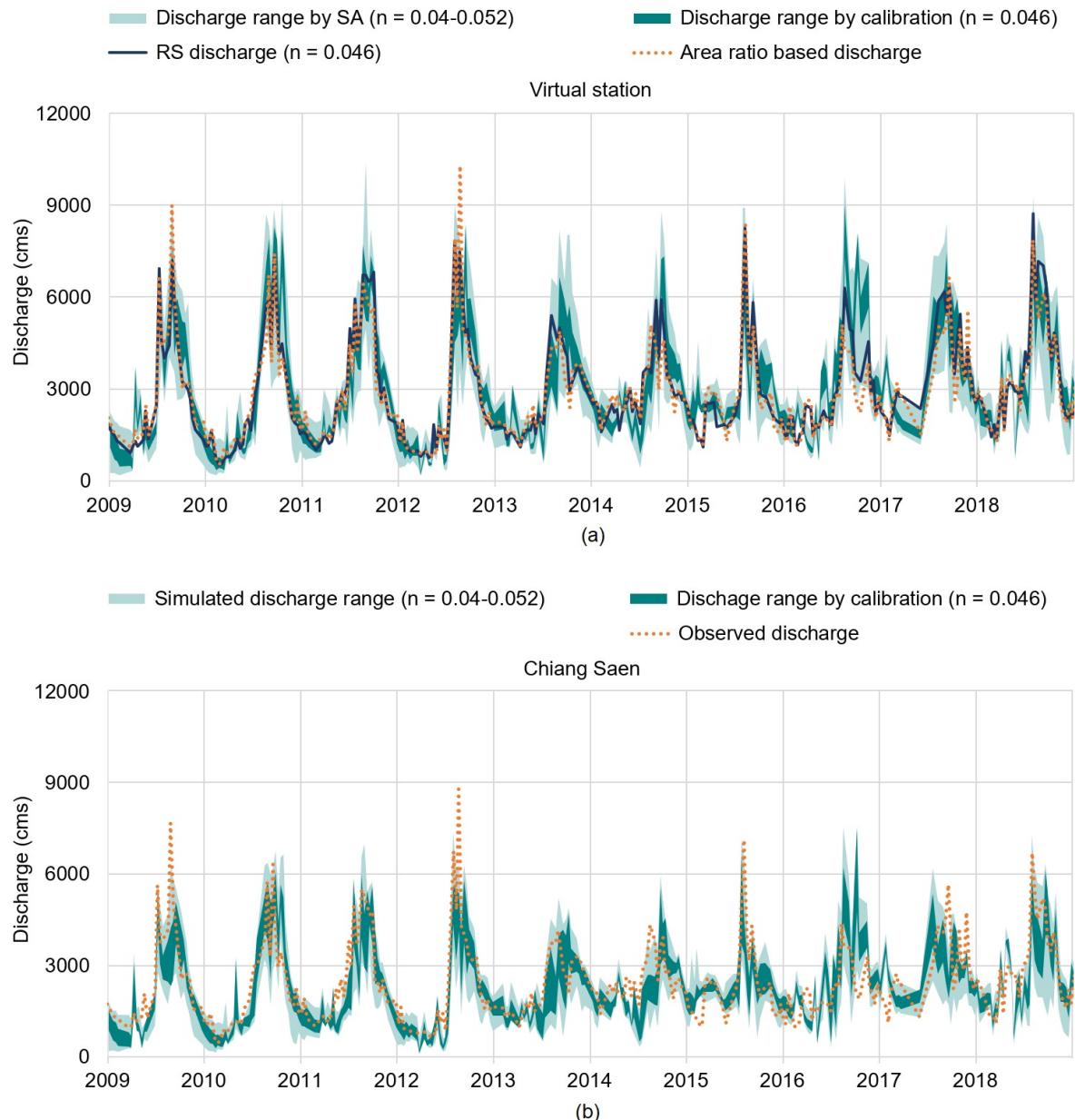


Figure S3. Comparison of discharge time series obtained during calibration at the virtual station (a) and validation at Chiang Saen station (b). The dark green band depicts the range of variability of 58 selected solutions (corresponding to the Pareto front), while the light green band corresponds to the range of variability of 40 solutions selected in the sensitivity analysis. In panel (a), the dark blue line represents the remote sensed discharge at the virtual station (with $n = 0.046$), while the dotted orange line corresponds to the discharge estimated by scaling the discharge observed at Chiang Saen by the area ratio. In panel (b), the dotted orange line illustrates the observed discharge at Chiang Saen.



5 References

Do, P., Tian, F., Zhu, T., Zohidov, B., Ni, G., Lu, H., and Liu, H.: Exploring synergies in the water-food-energy nexus by using an integrated hydro-economic optimization model for the Lancang-Mekong River Basin, *Science of The Total Environment*, 728, 137996, <https://doi.org/10.1016/j.scitotenv.2020.137996>, 2020.