# Technical note: A sigmoidal soil water retention curve without asymptote that is robust when dry–range data are unreliable

Gerrit Huibert de Rooij<sup>1</sup>

<sup>1</sup> Helmholtz Centre for Environmental Research – UFZ GmbH, Soil System Science Dept.,
 5 Theodor–Lieser–Strasse 4, 06120 Halle (Saale), Germany

Correspondence to: Gerrit H. de Rooij (gerrit.derooij@ufz.de)

**Abstract.** In a recently introduced parameterization for the soil water retention curve (SWRC) with a sigmoid wet branch and a logarithmic dry branch, the matric potential at the junction point of the sigmoid and the logarithmic branch ( $h_i$ ) was a fitting parameter, while that at oven-dryness ( $h_d$ ) was derived from

- 10 the fitting parameters. The latter is undesirable, especially if reliable data in the dry range are limited. Therefore, an alternative is presented in which shape parameter  $\alpha$  instead of  $h_d$  is a derived parameter, and  $h_d$  can be fitted or fixed. The resulting relationship between  $\alpha$  and  $h_j$  is such that it prevents correct fits for  $h_j$ . Fortunately, an expression for  $h_j$  is found that allows it to be replaced by  $\alpha$  as a fitting parameter. The corresponding parameter space is well-behaved and has fewer internal bounds defined by restraining
- 15 relationships between parameters than the space for  $h_j$  as a fitting parameter. The few available values of  $h_j$ in the literature are in line with those according to the new expression. The reformulated SWRC is fitted to data of 21 soils by shuffled complex evolution. The paper gives the main features of an accompanying opensource fitting code. The curves fit the data well, except for some clayey soils. A theoretical value of  $h_d$ performs well for a wide range of soils. The new SWRC simplifies to an earlier junction model of the SWRC
- 20 based on a well-known power-law SWRC if  $\alpha$  is very large.

# 1 Introduction

Recently, de Rooij et al. (2021) proposed a closed-form expression for the SWRC with a distinct air-entry value, like the SWRC proposed by Ippisch et al. (2006), a sigmoid shape in the intermediate range
according to van Genuchten (1980), and a logarithmic dry branch terminating at a finite matric potential (*h<sub>d</sub>* (L)) at which the soil was oven-dry, with the water content essentially zero. The volumetric water contents and derivatives of the sigmoid and logarithmic branches were matched at the matric potential of their junction according to Rossi and Nimmo (1994). The rationale for developing the function was to preserve the desirable sigmoid shape of van Genuchten's (1980) curve while removing the physically unrealistic asymptote at some non-zero residual water content (Du, 2020), eliminating the non-converging integral of the SWRC for commonly occurring parameter values (Fuentes et al., 1991), and avoiding the detrimental effect of the non-zero slope at saturation on hydraulic conductivity near saturation (Durner, 1994; Assouline and Or, 2013; Wang et al., 2022).

Erroneous measurements in the dry range can lead to unrealistically low values of the matric 35 potential at oven dryness,  $h_d$  (L) (de Rooij et al., 2021). Unfortunately,  $h_d$  was not fitted independently but expressed as a function of other parameters that were fitted. Data in the dry range can be unreliable due to lack of equilibrium or other causes (Bittelli and Flury, 2009; Solone et al., 2012). If they are, it would be helpful to fix  $h_d$  at a reasonable value, e.g.  $-10^{6.8}$  cm H<sub>2</sub>O (Schneider and Goss, 2012), and either give the unreliable data points a lower weight during the fitting process or remove them altogether. An SWRC with 40 improved behavior in the dry range even if dry-range data are scant can help improve the behavior of

- Richards' solvers (e.g. SWAP Soil Water Atmosphere Plant, 2022; Šimůnek et al., 2016), be useful to improve conceptualizations of the soil reservoirs in large scale hydrological models (e.g., Lawrence et al., 2019), and for investigating dielectric properties of dry soil and associated soil backscatter (Ferré and Topp, 2002; Davis and Annan, 2002).
- 45 This note presents an alternative to de Rooij et al.'s (2021) model in which  $h_d$  is a fitting parameter. In doing so, it uncovers the peculiar behavior of shape parameter  $\alpha$  (L<sup>-1</sup>), which makes it essentially impossible for any fitting algorithm to avoid a local minimum with very inaccurate parameter values. The main objective is therefore to elucidate the behavior of  $\alpha$  and formulate a version of de Rooij's (2021) SWRC that has  $h_d$  as a fitting parameter but avoids the difficulties caused by the behavior of shape parameter  $\alpha$ .
- 50 In the testing phase, it was found that a commonly used convergence criterion used in parameter optimization not necessarily gave the best parameter values if the objective function was challenging. The second objective is therefore to present a parameter fitting algorithm that employs multiple convergence

2

criteria, and optionally explores the parameter space prior to the fitting operation to reduce the search area during fitting. The corresponding open–source code for fitting the improved SWRC is provided.

#### 55 2 Theory

De Rooij et al. (2021) introduced a unimodal model for the SWRC by combining those of Rossi and Nimmo (1994) and Ippisch et al. (2006), dubbed 'RIA'.

$$\theta(h) = \begin{cases} 0, & h \le h_{d} \\ \theta_{s}\beta \ln\left(\frac{h_{d}}{h}\right), & h_{d} < h \le h_{j} \\ \theta_{s}\left(\frac{1+|\alpha h|^{n}}{1+|\alpha h_{ae}|^{n}}\right)^{\frac{1}{n}-1}, & h_{j} < h \le h_{ae} \\ \theta_{s}, & h > h_{ae} \end{cases}$$
(1)

60

Here *h* denotes the matric potential in equivalent water column (L), subscripts 'd' and 'ae' denote the value at which the water content reaches zero and the air–entry value, respectively, and subscript 'j' indicates the value of *h* at which the logarithmic and sigmoid branch are joined. The volumetric water content is denoted by  $\theta$ , with the subscript 's' denoting its value at saturation. Parameters  $\alpha$  (L<sup>-1</sup>) and *n* determine the shape of the sigmoid branch are joined as for the logarithmic here  $\theta$ .

65 the sigmoid branch (van Genuchten, 1980), while parameter *β* does so for the logarithmic branch. By assuming that for  $h \le h_j$ , all water is adsorbed and for  $h > h_j$ , the adsorbed water content is equal to  $\theta(h_j)$ , the total water content can be partitioned in a capillary water content  $\theta_c$  and an adsorbed water content  $\theta_a$ .

By requiring the derivatives of the sigmoidal and logarithmic branches to match at  $h_{j}$ , parameter  $\beta$  can be expressed in terms of the other parameters (de Rooij et al., 2021).

70

75

$$\beta = (n-1) \left| \alpha h_j \right|^n (1 + \left| \alpha h_{ae} \right|^n)^{1 - \frac{1}{n}} \left( 1 + \left| \alpha h_j \right|^n \right)^{\frac{1}{n} - 2}$$
(2)

Using this expression to eliminate  $\beta$  from the equality that arises when the values of both branches are matched at  $h_i$ , the resulting expression can be solved for  $\alpha$  to establish  $h_d$  as one of the fitting parameters. The expression can also be found by rearranging Eq. (9) of de Rooij et al., (2021).

$$\alpha = |h_j|^{-1} \left[ (n-1) \ln\left(\frac{h_d}{h_j}\right) - 1 \right]^{-\frac{1}{n}}$$
(3)

The five fitting parameters are:  $h_{ae}$ ,  $h_{j}$ ,  $h_{d}$ ,  $\theta_{s}$ , and n. Equation (3) is only valid if the bracketed term is positive. 80 This is the case if the following criterion is met.

$$\left|h_{\rm j}\right| < \left|h_{\rm d}\right| {\rm e}^{\frac{1}{1-n}} \tag{4}$$

Many soils for which SWRCs of van Genuchten (1980) or de Rooij et al. (2021) are fitted have values for  $\alpha$  between roughly 0.001 and 0.3, with sandy soils generally having higher values than fine-textured soils (e.g., de Rooij et al., 2021). When  $h_d$  is fixed at  $-10^{6.8}$  cm H<sub>2</sub>O,  $\alpha$  is a function of *n* and  $h_j$  only. Its contour map is depicted in Fig. 1. De Rooij et al. (2021) reported four soils with data sets without suspect data points above pF 3 for soils with n > 1.2 (soils 1142, 1143, 2110, and 2126, all sands or loamy sands). De Rooij et al.'s (2021) values of  $\alpha$  and *n* for these soils give values of  $h_j$  that are all larger (closer to zero) than -150 cm, which is unrealistic. For soil 2126 the value even exceeds  $h_{ae}$ , which is not physically acceptable.



Figure 1: The logarithm of shape factor  $\alpha$  (cm<sup>-1</sup>) as a function of shape factor *n* and the matric potential at the junction point  $h_1$  (cm H<sub>2</sub>O) according to Eq. (3), with  $h_4$  fixed at  $-10^{6.8}$  cm. The labels of the contour lines

95 represent log(*a*). The transparent yellow curve is the limit of the valid domain according to Eq. (4). The black area is the invalid part of the domain.

It therefore appears from Fig. 1 that plausible combinations of  $\alpha$  and  $h_j$  are not feasible, but Eq. (3) reveals that the relationship  $\alpha(h_j)$  is non–monotonous. A combination of large values of both  $\alpha$  and  $h_j$  is

100 possible in a band too narrow to be visible in Fig. 1, located immediately below the maximum allowed value of  $h_j$ , marked by the transparent yellow curve in Fig. 1. In that band,  $\alpha$  goes to infinity when  $h_j$  approximates its limiting value defined in Eq. (4) (Fig. 2). The partial derivative of Eq. (3) with respect to  $h_j$  is as follows.

$$\frac{\partial \alpha}{\partial h_{j}} = \frac{1}{h_{j}^{2}} \left[ (n-1) \ln\left(\frac{h_{d}}{h_{j}}\right) - 1 \right]^{-\frac{1}{n}} + \frac{1-n}{n} \frac{1}{h_{j}^{2}} \left[ (n-1) \ln\left(\frac{h_{d}}{h_{j}}\right) - 1 \right]^{-\frac{n+1}{n}}$$
(5)  
105



Figure 2: A transect of Figure 1 for n = 1.4 that shows the sharp increase of shape factor  $\alpha$  (cm<sup>-1</sup>) as the 110 matric potential at the junction point  $h_1$  (cm H<sub>2</sub>O) reaches its physical limit defined in Eq. (4).

The value of  $\alpha$  is at its minimum where its derivative is zero. From Eq. (5) follows this occurs when the following equality holds.

115 
$$\ln\left(\frac{h_{\rm d}}{h_{\rm j}}\right) = \frac{2n-1}{n^2 - n} \tag{6}$$

Because Fig. 1 shows that realistic values of  $\alpha$  require excessively low values of  $h_j$  in much of the parameter space, it may be better to use Eq. (6) to set a lower limit on the permissible values of  $h_j$  as follows.

120 
$$|h_j| > |h_d| e^{\frac{2n-1}{n-n^2}}$$
 (7)

Figure 3 shows the band of valid values of  $h_i$  enveloped by the limits set by Eqs. (4) and (7). A large part of the parameter space between these limits of  $h_i$  has an excessively large  $\partial \alpha / \partial h_i$ . Finding the optimum will therefore be very difficult for any parameter fitting algorithm. But if the lower limit is not enforced, trial

125 fits showed that the shuffled complex evolution algorithm (SCE, Duan et al., 1992, 1993) consistently ended up in the region of Fig. 1 corresponding to the area below the lower limit in Fig. 3.



Figure 3: The limits imposed on the matric potential at the junction point  $h_j$  (scaled by the matric potential at 130 oven-dryness  $h_d$ ) by the requirement that shape factor  $\alpha$  be positive (upper limit) and by the minimum value of  $\alpha$  for any specific value of n (lower limit). The shading indicates the area with plausible parameter

# combinations. The dots represent de Rooij et al.'s (2021) fits of Eq. (1) with $\alpha$ instead of $h_d$ as a fitting parameter for 21 soils.

135 De Rooij et al. (2021) already fitted Eq. (1) with  $\alpha$  instead of  $h_d$  as a fitting parameter and without any restrictions other than minimum and maximum values imposed on any of the fitting parameters. By calculating  $h_d$  from the fitted values of  $\alpha$ , n, and  $h_j$  according to their Eq. (10), it was possible to see if their fits fell within the limits defined above. Figure 3 shows that the values of all 21 soils fell on the upper limit. This opens the possibility to eliminate  $h_j$  as a fitting parameter and replace it by its upper limit. This leads 140 to the following additional equation augmenting Eq. (1).

$$h_{\rm j} = h_{\rm d} \mathrm{e}^{\frac{1}{1-n}} \tag{8}$$

Combining Eq. (8) with Eq. (3) leads to an infinite  $\alpha$ , consistent with Fig. 2. But Fig. 2 also shows that a

145 minute change in h<sub>j</sub> (much smaller than a realistic number of significant digits would be able to represent) allows α to vary beyond the range of values reported in the literature. In other words: If, for given values of h<sub>d</sub> and n, h<sub>j</sub> is determined from Eq. (8), α can vary over its entire range. It is therefore better to treat α as a fitting parameter and h<sub>j</sub> as a derived parameter, by replacing Eq. (3) by Eq. (8). This has the added advantage that the entire parameter space defined by the minimum and maximum values of the fitting parameters is valid, provided the physical and mathematical limits of each parameter are respected, and

the fitted or fixed value of  $h_{d}$  is smaller (more negative) than  $h_{ae}$ .

In the limit as  $\alpha$  approximates infinity, the expression for the sigmoid branch of the SWRC simplifies to the power law proposed by Brooks and Corey (1964).

155 
$$\lim_{\alpha \to \infty} \theta_{s} \left( \frac{1 + |\alpha h|^{n}}{1 + |\alpha h_{ae}|^{n}} \right)^{\frac{1}{n} - 1} = \theta_{s} \left( \frac{h}{h_{ae}} \right)^{1 - n}$$
(9)

It can be easily shown that both the values and the derivatives of the dry and the wet branch match at  $h_j$  if Eq. (9) is used for the latter. Equation (9) establishes that Rossi and Nimmo's (1994) junction model (without the parabolic smoothing near saturation that Madi et al. (2018) showed to be detrimental to the

160 hydraulic conductivity function) is a special case of the RIA parameterization. Incidentally, this implies that Brooks and Corey's model (1964) is a special case of that of Ippisch et al. (2006). If Eq. (8) replaces Eq. (3), the fitted value of  $\alpha$  no longer ensures continuity at the junction point. The ensuing continuity gap can be closed by applying a correction factor *c* to the value of  $h_d$  used in the logarithmic branch as follows.

165

$$\theta = \theta_{\rm s} \beta \ln \left[ \frac{(1+c)h_{\rm d}}{h} \right] \tag{10}$$

The correction factor *c* is defined by the following expression, which is found by replacing  $h_d$  in Eq. (1) by  $(1+c)h_d$ , requiring the logarithmic and sigmoid branches of Eq. (1) to be equal at  $h_j$ , and replacing the ratio 170  $h_d/h_j$  in the resulting equality by  $\exp[1/(n-1)]$  according to Eq. (8).

$$c = \exp\left[\frac{1}{\beta} \left(\frac{1+|\alpha h_{j}|^{n}}{1+|\alpha h_{ae}|^{n}}\right)^{\frac{1}{n}-1} + \frac{1}{1-n}\right] - 1$$
(11)

In the expression for  $\beta$ ,  $h_d$  appears indirectly. Its value should not be corrected there because  $\beta$  ensures 175 continuity of the derivatives only if its expression is not modified. Trial calculations showed that c is negligible, except when both  $\alpha$  and n are small.

Rossi and Nimmo (1994) fitted  $h_j$  values for their parameterization of the SWRC between  $-2.6 \cdot 10^6$ and  $-2.0 \cdot 10^4$  cm H<sub>2</sub>O for seven soils, with only the one clayey soil having a value more negative than  $-1.9 \cdot 10^5$ cm H<sub>2</sub>O. Tuller and Or (2005) tentatively set the matric potential at which the capillary-bound water

- 180 content becomes negligible 10<sup>5</sup> cm H<sub>2</sub>O, based on data from a sand mixture and six soils that mostly overlap with those of Rossi and Nimmo (1994) (Or and Tuller, 1999). Beyond this there is little guidance on the value of  $h_j$  in the literature. When Eq. (8) is used, such guidance is not necessary. The map of  $h_j$  as defined by Eq. (8) in Fig. 4 shows that for *n* below 1.4,  $h_j$  is very sensitive to the value of *n*. For n > 2, log(– $h_j$ ) is roughly proportional to log(– $h_d$ ) for a given value of *n*. When  $h_d$  is close to –10<sup>6.8</sup> cm H<sub>2</sub>O (Schneider and
- 185 Goss, 2012), values of  $h_j$  in the range of those reported in the literature occur for  $n \ge 1.25$ .





For completeness, the multimodal version of Eq. (1) is provided as well. The multimodality is limited to the sigmoid branch, so that the multimodal SWRC has only one value for  $h_{\rm l}$ . Because Eq. (8) allows only a single value of n in that case, only  $\alpha$  can be varied between the constituting sigmoid curve sections.

195

190

$$\theta(h) = \begin{cases} 0, & h \le h_{\rm d} \\ \theta_{\rm s} \beta_{\rm m} \ln\left(\frac{h_{\rm d}}{h}\right), & h_{\rm d} < h \le h_{\rm j} \\ \theta_{\rm s} \sum_{i=1}^{k} w_i \left(\frac{F_i(h)}{F_i(h_{\rm ae})}\right)^{\frac{1}{n-1}}, & h_{\rm j} < h \le h_{\rm ae} \\ \theta_{\rm s}, & h > h_{\rm ae} \end{cases}$$
(12)

For brevity, the following function was introduced in Eq. (12).

200 
$$F_i(x) = 1 + |\alpha_i x|^n$$
 (13)

Here, *k* denotes the modality,  $w_i$  is the weighting factor (adding up to one) of the *k*<sup>th</sup> constituting curve, and  $\alpha_i$  (L<sup>-1</sup>) its shape factor. The expression for the multimodal  $\beta_m$  is found be setting the derivatives of the logarithmic and the sigmoid branch equal at  $h_i$  and invoking Eq. (8).

205

$$\beta_{\rm m} = \frac{n-1}{\rm e} |h_{\rm d}|^{n-1} \sum_{i=1}^{k} w_i \alpha_i^n F_i(h_{\rm ae})^{1-\frac{1}{n}} G_i(h_{\rm d})^{\frac{1}{n}-2}$$
(14)

Function *G* is defined as follows.

210 
$$G_i(x) = 1 + |\alpha_i x|^n e^{\frac{n}{1-n}}$$
 (15)

The continuity correction factor  $c_m$  can be found by requiring that the logarithmic and sigmoid branch join at  $h_{j}$ .

215 
$$c_{\rm m} = \exp\left[\frac{1}{\beta_{\rm m}}\sum_{i=1}^{k} w_i \left(\frac{G_i(h_{\rm d})}{F_i(h_{\rm ae})}\right)^{\frac{1}{n}-1} + \frac{1}{1-n}\right] - 1$$
 (16)

Above, the subscript 'm' is used to distinguish multimodal versions of  $\beta$  and *c* from their single-mode equivalents.

# **3 Materials and Methods**

# 220 3.1 Selected soils

The SWRC has five fitting parameters:  $\theta_s$ ,  $h_{ae}$ ,  $h_d$ ,  $\alpha$ , and n. These were fitted to data of the 21 soils selected from the UNSODA database (Nemes et al., 2001) by de Rooij et al. (2021), with  $h_d$  either fixed at – 10<sup>6.8</sup> cm H<sub>2</sub>O, or its lower limit set at that value. These soils cover a wide range of textures (see Madi et al. (2018) and de Rooij et al. (2021) for details). At the time the data base was created, the the pressure plate

apparatus was widely used in the dry range. Therefore, the standard deviation (SD) of the matric potential of any data point with  $h \le -1000$  cm H<sub>2</sub>O was set to half the its value, thereby drastically reducing its weight

in the objective function. The SD of *h* for 0 > h > -1000 cm H<sub>2</sub>O was set to 1.0 cm , that for h = 0 at 0.05 cm. The SD for the volumetric water content was set at 0.01 when h = 0, and to 0.02 otherwise. The sample height was set to zero for  $h \le -1000$  cm because the variation in the water content can be neglected at low

230 matric potentials. For h = 0 cm, it was assumed that the water pressure in the sample was positive everywhere, or that the porosity was measured. In both cases, there is no effect of the matric potential on the local water content, hence the sample height was set to zero to reflect this. For the intermediate values of *h*, the sample height was set to the value specified in the UNSODA database. If a sample height was not reported, it was set to 3.0 cm.

#### 235 3.2 Parameter fitting

The parameters were fitted using the SCE algorithm (Duan et al., 1992, 1993), implemented in Fortran in a code that accompanies this paper. The most important features of the code are summarized here. The code itself, further details of the code and the algorithm, as well as a user manual, can be downloaded (de Rooij, 2022). For each case, the code performs three optimization runs by minimizing the

240 objective function: the root mean square error (RMSE) of the differences between fitted and observed volumetric water contents, weighted according to the error standard deviations of the observed matric potentials and corresponding water contents provided on input, as detailed by de Rooij (2022).

Ten convergence criteria are evaluated. Criteria 1 and 2 take into account the results of the last few shuffles. The number of shuffles considered is twice the number of fitting parameters or an internally set number (5), whichever is larger.

- 1. In the best fits from the last set of shuffles, the range of a parameter exceeds neither the absolute nor the relative user–specified tolerance.
- 2. In the best fits from the last set of shuffles, the range of the objective function does not exceed its absolute user–specified tolerance.
- 250 3. The parameter range in the final complexes does not exceed the maximum internally set permissible value.
  - 4. The volume of the hypercube enveloping the final complexes does not exceed the maximum internally set permissible value.
  - 5. The parameter range in the most successful complex (minus the point with the highest RMSE) does not exceed the internally set maximum permissible value.

11

255

245

- 6. The volume of the hypercube enveloping the most successful complex (minus the point with the highest RMSE) does not exceed the internally set maximum permissible value.
- 7. A parameter does not exceed both the absolute and the relative user–specified tolerance in the final complexes.
- 260 8. A parameter does not exceed both the absolute and the relative user-specified tolerance in the most successful complex (without the point with the highest RMSE).
  - 9. The change of the objective function between consecutive shuffles does not exceed the userspecified tolerance.
  - 10. The Root Mean Square Error of the fit does not exceed a user-specified tolerance.

265

A relative improvement criterion similar to criterion 9 is often used as the sole criterion (e.g., in the Rpackage SoilHyp, Dettmann, 2021). Criteria 1, 3, 5, 7, and 8 are evaluated separately for each parameter. Convergence is achieved when no more than a user-prescribed number of these criteria failed for any of the parameters. The code keeps evolving and shuffling complexes until convergence is achieved or the user-specified maximum allowed number of evaluations of the objective function is exceeded. If not all criteria are considered relevant, the user can either set their thresholds unrealistically strict and increase the number of criteria that are allowed to fail, or set them excessively loose and decrease the number of

criteria that are allowed to fail accordingly.

- 275 The algorithm generates large numbers of sets of fitted parameter values. A random sample of these is used to determine the correlation matrix of the parameters. The best fit, its RMSE and its correlation matrix are reported by the code for each of the three runs, and the run with the overall lowest RMSE is identified. The code returns a table of the fitted curve based on the best run, and reports the correction factor *c* used to compile this table. These tables are the basis for the plots shown below. If desired, the code
- 280 also calculates the objective function on points of a regular grid covering the parameter space (map points) and writes a random sample of these to output. Even if this is not desired, a map is calculated based on a three-point grid along each principal axis of the parameter space. This resulting output is helpful if a user wishes to verify if the objective function is correctly calculated.
- Normally, the first complexes of each run are filled with randomly selected points in the valid regions of the parameter space. Optionally, only the complexes of run 3 are filled with randomly selected points, while the first complexes of run 1 are filled with the map points with the lowest RMSE. The first

complexes of run 2 then contain these map points perturbed by adding random noise to the parameter values.

- For each fitting parameter, a maximum and minimum value need to be provided. If these values are equal, the parameter is treated as a fixed value, and the dimensionality of the parameter space is reduced accordingly. The number of complexes is two (for 8 of fewer fitting parameters) or four (see Duan et al. (1994)). If this leads to frequent convergence at local minima, the number of complexes can be set to twice the number of fitting parameters. The number of individuals in a complex and the number of evolution steps are twice the number of fitting parameters plus one. The number of individuals in the subcomplexes is the number of fitting parameter plus one. The number of offspring in each evolution step is one. These settings
  - are all in accordance with Duan et al. (1994).

When the user chooses to use the map of regularly–spaced points in the parameter space to set the initial guesses of the first two runs, the code adapts the parameter ranges based on their ranges among the map points selected to fill the initial complexes.

- 300 The permitted parameter range for  $\theta_s$  enveloped the range of observed saturated water contents, with a limited buffer on either side of the range. The range of  $h_{ae}$  was determined based on the wettest unsaturated data point and the driest saturated point, with a generous buffer. The range limit at the wet end was often set to zero. The value of  $h_d$  was mostly fixed and occasionally varied over a relatively wide range depending on visual examination of the data points. The permitted range for  $\alpha$  was 0.001 to 0.5, 205 event for 1142, where alpha could go as high as 100.0. After some trial and error, the range of pures set
- 305 except for 1142, where alpha could go as high as 100.0. After some trial and error, the range of *n* was set relatively narrow (between 1.05 and 2) because even with wider ranges the fitted values fell within this range. Any time a fitted value was close to one of its limits, the fit was repeated with an expanded range.

No more than four convergence criteria were allowed to fail for convergence to be achieved. If convergence was not achieved, up to 20000 evaluations of the objective function evaluations would be 310 performed. The actual number could be slightly higher because it was checked each time a shuffle had been completed. A map was not created, and therefore, all three optimization runs started with random parameter combinations filling the complexes. The maximum allowed relative change of the RMSE between consecutive shuffles was  $10^{-6}$ . The maximum allowed value of the RMSE was 0.1. For the parameters, the absolute tolerances for  $\theta_s$ ,  $h_{ae}$ ,  $h_d$ ,  $\alpha$ , and n were 0.001, 0.1, 1000.0, 0.1, and 0.01, respectively. The relative

315 tolerances were 0.1 for  $\alpha$  and 0.01 for the others. This choice reflects the limited sensitivity to  $\alpha$ .

The internally set relative tolerance for parameter variations for all complexes and for the most successful complex were both 0.01. The internally set required maximum size of the hypercube enveloping

the range of fitted parameter values (again for all complexes as well as the most successful one), scaled by the volume of the hypercube defined by the minimum and maximum allowed parameter values, equals  $0.01^{d}$ , with *d* the number of fitting parameters that were not set at fixed values by the user.

#### **4** Results and Discussion

320

325

In the tables that follow, the soil texture classification according to Twarakavi et al. (2010) is provided. The advantage of this classification over the conventional USDA soil texture classification is that it better recognizes differences in hydraulic behavior between its textural classes. This makes it more relevant for soil water flow studies for which the SWRCs are typically used.

Table 1 shows the fitted parameter values of the best fits, the resulting RMSE and the corresponding value of *h*j. The value of  $\alpha$  for soil 1142 stands out. As explained above, high values of  $\alpha$  lead to a power–law type of SWRC between  $h_{ae}$  and  $h_{j}$ . An additional fit with  $\alpha$  capped at 1.0 confirmed that the shape of the SWRC is not very sensitive to large values of  $\alpha$ . The increase in the RMSE caused by limiting the range of  $\alpha$ 

330 was  $10^{-4}$ , and the changes in  $\theta_s$ ,  $h_{ae}$ , and n did not occur before the fourth significant digit. One can also switch from a sigmoidal model to a power–law model by invoking Eq. (9) if  $\alpha$  is very large, keeping the fitted values of the other parameters.

Fuentes et al. (1991) showed that for values of *n* smaller than 2, the asymptotic dry branch of the original parameterization of van Genuchten (1980) would lead to physically unacceptable behaviour. All

335 soils in Table 1 have values of *n* in this range. This highlights the importance of avoiding a dry branch with an asymptote at a residual water content.

The range of values of  $h_j$  in Table 1 is only slightly beyond the range reported by Rossi and Nimmo (1994) for a smaller number of soils. This lends credibility to Eq. (8). In the few cases where  $h_d$  was fitted, the resulting values in Table 1 are close to the value proposed by Schneider and Goss (2012). Table 2 shows

340 the the correction factor *c* of Eqs. (10) and (11), which ensures continuity of the SWRC. Seven of the 21 soils need a correction of  $h_d$  that exceeds 1%. The resulting shift of the dry–branch pF is also shown. For most soils, the shift is negligible. Only for soils 1122 and 1123 (both fine–textured soils with small values for both  $\alpha$  and *n*), the shift exceeds 0.1 pF unit, but never more than 0.2 unit.

Only the optimizations for soils 1142 and 2104 converged, with convergence criteria 4, 6, 8, 9, and 345 10 satisfied for all parameters for soil 1142, and criteria 4 through 10 for soil 2104. None of the correlation coefficients of the parameter pairs for either soil exceeded 0.31. The other optimizations ran until the maximum number of objective function evaluations was exceeded. For soil 1120, criteria 9 and 10 were met for all parameters. For the remaining soils, criteria 1, 2, and 9 were satisfied in all cases. For 14 soils, criterion 10 was met as well. For soil 3250, criterion 8 was also satisfied. The lack of convergence forced

350 the code to keep exploring the parameter space, leading to a large proportion of randomly selected points because the reflection and contraction points determined by the SCE algorithm did not improve the fit. If the majority of points is randomly selected, there is no correlation between the parameters, and the correlation matrix does not provide any information.

Table 1. Fitted parameter values and the Root Mean Square Error (RMSE) of the best fits for 21 soils. The corresponding values of the derived parameter  $h_j$  are given as well. If parameter  $h_d$  was fixed during the fitting operation, its value is denoted in italic font.

Soil (UNSODA identifier and	$ heta_{ m s}$	h <sub>ae</sub> (cm	$log(-h_d)$ ( $h_d$ in cm	$\alpha$ (cm <sup>-1</sup> )	п	RMSE	$log(-h_j)$ ( $h_i$ in cm
classification		H₂O)	H <sub>2</sub> O)				H <sub>2</sub> O)
according to		-	,				
Twarakavi et							
al., 2010)							
2126 A1	0.3808	-3.999	6.8000	0.1332	1.8319	0.1434	6.2779
1142 A2	0.2404	-25.90	6.5623	561.2	1.3882	0.0545	5.4435
2104 A2	0.3980	-2.990	6.8000	0.1156	1.4400	0.0715	5.8129
1120 A3	0.3076	-0.012	6.8000	0.02803	1.3016	0.0796	5.3601
1143 A3	0.2761	-5.017	6.8000	0.08308	1.2214	0.0589	4.8384
2110 A3	0.3634	-0.014	6.8000	0.03268	1.3431	0.0930	5.5343
2132 A3	0.3058	-0.004	6.8000	0.06055	1.1413	0.0417	3.7264
1121 A4	0.3441	-13.97	6.7811	0.04667	1.1560	0.0830	3.9970
1133 A4	0.3280	-240.5	6.8000	0.001366	1.1985	0.0477	4.6126
3260 B2	0.4740	-0.009	6.4711	0.02055	1.3234	0.0510	5.1281
3261 B2	0.4934	-0.015	6.8000	0.02379	1.3549	0.0731	5.5763
3263 B2	0.4628	-0.014	6.8000	0.01920	1.2925	0.0737	5.3151
3250 B4	0.5400	-3.796	6.8000	0.01236	1.2636	0.0611	5.1525
3251 B4	0.4980	-0.582	6.7479	0.01321	1.1576	0.0857	3.9918
4450 B4	0.3705	-0.548	6.8000	0.03784	1.1577	0.1150	4.0459
1135 C2	0.4147	-174.8	6.8000	0.001791	1.1763	0.0478	4.3361
1182 C2	0.5307	-8.131	6.8000	0.01349	1.1551	0.2484	3.9991
1122 C4	0.3571	-8.664	6.8000	0.001385	1.1550	0.0497	3.9976
1123 C4	0.3575	-67.17	6.8000	0.001008	1.1554	0.0663	4.0054
1180 C4	0.4885	-2.005	6.8000	0.1319	1.1549	0.2514	3.9962
1181 C4	0.4407	-7.282	6.8000	0.006671	1.1552	0.1593	4.0012

In all cases, the fitted parameter values for the runs with  $h_d$  fixed and  $h_d$  free as well as the three individual runs for each optimization were essentially in agreement, and the parameter values did not look suspect. Therefore, it was considered unnecessary to run the optimizations with modified convergence requirements in order to obtain more meaningful correlation matrices.

360

The reduced weights assigned to data points with pF > 3 are reflected in the plots of Figs. 5 through 8, which show the fitted curves with  $h_d$  fixed and  $h_d$  fitted. In these plots, the fit with the lowest RMSE is plotted in red, and the corresponding curves for  $\theta_c$  and  $\theta_a$  are included. The other curve is shown in black. To illustrate how small the continuity correction *c* is, this curve is shown without this correction. The discontinuity at the junction point is only visible for soils 1133 (Fig. 6) and 1122 (Fig. 8).

365

Table 2. The continuity correction factor c (Eq.(11)) and the corresponding shift on the pF scale of the dry–branch correction for 21 soils.

Soil (UNSODA identifier and classification	Correction factor	pF–shift dry	
according to Twarakavi et al., 2010)	С	branch	
2126 A1	1.525E-10	6.62E-11	
1142 A2	1.092E-11	4.74E-12	
2104 A2	2.164E-07	9.40E-08	
1120 A3	3.666E-05	1.59E-05	
1143 A3	1.162E-04	5.04E-05	
2110 A3	1.063E-05	4.62E-06	
2132 A3	0.009750	0.00421	
1121 A4	0.005323	0.00231	
1133 A4	0.04130	0.0176	
3260 B2	8.647E-05	3.76E-05	
3261 B2	1.243E-05	5.40E-06	
3263 B2	7.641E-05	3.32E-05	
3250 B4	3.015E-04	1.31E-04	
3251 B4	0.02300	0.00988	
4450 B4	0.005833	0.00253	
1135 C2	0.07969	0.0333	
1182 C2	0.02266	0.00973	
1122 C4	0.3664	0.136	
1123 C4	0.5566	0.192	
1180 C4	0.001627	7.06E-04	
1181 C4	0.05147	0.0218	

The fraction of adsorbed water increases when moving from sands (Figs. 5 and 6) through loams (Fig. 6 and 7) to clays (Fig. 8). Because the separation between capillary and adsorbed water is abrupt and binary at  $h_{j}$ , this should not be interpreted as representative for the more smooth transition in natural soils. Nevertheless, the direction of the trend is physically plausible.

Most soils (2126 and 1142 in Fig. 5; 1120, 1121, 1143, 2110, and 2132 In Fig. 6; 1142 and 2126 in Fig. 7; 1122, 1180, and 1182 in Fig. 8) have observed saturated water contents that seem to be too large compared to the other data points. The causes (e.g., macropores or air inclusion) are not known. Data points at saturation were assumed to be very accurate and therefore had a high weight, which the plots reflect. It sometimes results in relatively low (more negative) air–entry values in coarse soils (Figs. 5 and 6 and Table



1, most notably soil 1142).

370

375

0.25

Figure 5: Soil water retention data and fitted curves for soils of classes A1 and A2 of Twarakavi et al. (2010).

- 380 Curves fitted with h₁ fixed at -10<sup>6.8</sup> cm H₂O, and with h₁ fitted with a cap at that value are shown. The one with the lowest Root Mean Square Error is shown as a red solid line. The volume fractions of capillary–bound water and water adsorbed in films is shown for this curve. The other curve is shown as black dash–dot line. This curve has not been corrected for continuity at the junction point. The vertical axes denote the logarithm (base 10) of the absolute value of the matric potential in cm H₂O.
- 385

All B2 soils (silt loams) and two out of three B4 soils (both silty clay loams) have high values of  $h_{ae}$ , indicating that the maximum pore size is large (Table 1). Although one would suspect that such fine-textured soils would have a low (more negative) air-entry value, the results are consistent with the data, as Fig. 7 shows.

390 Some of the C2 and C4 soils (1180–1182) have high RMSE values (Table 1). Their plots in Fig. 8 reveal that the multimodal shape of the curves was not captured well by Eq. (1). The remaining soils in Fig. 8 had very few points in the dry range, and fixing  $h_d$  was very effective in guiding the dry branch of the SWRC.

This paper focuses on mineral soils with unimodal SWRCs. If an extension to multimodality is 395 desired, Eqs. (12–16) provide a starting point. Further testing on soils with specific characteristics, such as volcanic or organic soils, may be worthwhile. In the case of organic soils, the risk of irreversible changes will require some caution when measuring points on the SWRC.



400 Figure 6: As Fig. 5, for soils of classes A3 and A4 of Twarakavi et al. (2010).



Figure 7: As Fig. 5, for soils of classes B2 and B4 of Twarakavi et al. (2010).



Figure 8: As Fig. 5, for soils of classes C2 and C4 of Twarakavi et al. (2010).

# **Competing interests**

410 GdR is a member of the HESS Editorial Board. The peer–review process was guided by an independent editor, and the author has no other competing interests to declare.

#### Data availability

415 The UNSODA database with the soil data can be downloaded at https://data.nal.usda.gov/dataset/unsoda-20-unsaturated-soil-hydraulic-database-database-and-program-indirect-methods-estimatingunsaturated-hydraulic-properties. (National Agricultural Library, 2015)

# Code availability

420

430

The Fortran code for fitting the SWRC parameters and post processing as well as its user manual are available from the Zenodo repository (de Rooij, 2022).

#### References

- 425 Assouline, S., and Or, D., Conceptual and parametric representation of soil hydraulic properties: a review, Vadose Zone J.,12, https://doi.org/10.2136/vzj2013.07.0121, 2013.
  - Bittelli, M., and Flury, M.: Errors in water retention curves determined with pressure plates, Soil Sci. Soc. Am. J., 73,1453-1460, https://doi.org/10.2136/sssaj2008.0082, 2009.

Brooks, R. H. and Corey, A. T.: Hydraulic properties of porous media, Colorado State University, Hydrology Paper No. 3, 27 pp., 1964.

Davis, J. L., and Annan, A. P.: Ground penetrating radar to measure soil water content, in: Methods of soil analysis. Part 4 – Physical methods, edited by Dane, J. H., and Topp, G. C., Soil Science Society of America, Inc., Madison, Wisconsin, U.S.A., 446–463, 2002.

22

405

Dettmann, U., SoilHyp: Soil Hydraulic Properties, https://rdrr.io/cran/SoilHyP/, access date April 1<sup>st</sup>, 2022,

435

455

2021.

- de Rooij, G.: Fitting the parameters of the RIA parameterization of the soil water retention curve (1.0). Zenodo. https://doi.org/10.5281/zenodo.6491979, access date April 26<sup>th</sup>, 2022.
- de Rooij, G. H., Mai, J., and Madi, R.: Sigmoidal water retention function with improved behaviour in dry and wet soils, Hydrol. Earth Syst. Sci., 25, 983–1007, https://doi.org/10.5194/hess-25-983-2021, 2021.
- 440 Du, C.: Comparison of the performance of 22 models describing soil water retention curves from saturation to oven dryness, Vadose Zone J., 19, e20072, https://doi.org/10.1002/vzj2.20072, 2020.
  - Duan, Q. Y., Gupta, V. K., and Sorooshian, S.: Shuffled complex evolution approach for effective and efficient global minimization, Journal of Optimization Theory and Applications, 76, 501–521, 1993.
- Duan, Q., Sorooshian, S., and Gupta, V.: Effective and efficient global optimization for conceptual rainfall– runoff models, Water Resour. Res., 28, 1015–1031, 1992.
  - Duan, Q., Sorooshian, S. and Gupta, V.: Optimal use of the SCE–UA global optimization method for calibrating watershed models, J. Hydrol., 158, 265–284, 1994.
  - Durner, W.: Hydraulic conductivity estimation for soils with heterogeneous pore structure, Water Resour. Res., 30,211–223, 1994.
- 450 Ferré, P. A., and Topp, G. C.: Time domain reflectometry, in: Methods of soil analysis. Part 4 Physical methods, edited by Dane, J. H., and Topp, G. C., Soil Science Society of America, Inc., Madison, Wisconsin, U.S.A., 434–446, 2002.
  - Fuentes, C., Haverkamp, R., Parlange, J. –Y., Brutsaert, W., Zayani, K., and Vachaud, G.: Constraints on parameters in three soil–water capillary retention functions, Transport in Porous Media, 6, 445–449, 1991.
  - Ippisch, O., Vogel, H. –J., and Bastian, P.: Validity limits for the van Genuchten–Mualem model and implications for parameter estimation and numerical simulation, Adv. Water Resour., 29, 1780–1789, https://doi.org/10.1016/j.advwatres.2005.12.011, 2006.
- Lawrence, D. M., Fisher, R. A., Koven, C. D., Oleson, K. W., Swenson, S. C., Bonan, G., et al.: The Community Land
   Model version 5: Description of new features, benchmarking, and impact of forcing uncertainty,
   Journal of Advances in Modeling Earth Systems, 11, 4245–4287,
   https://doi.org/10.1029/2018MS001583, 2019.

Madi, R., de Rooij, G. H., Mielenz, H., and Mai, J.: Parametric soil water retention models: a critical evaluation of expressions for the full moisture range, Hydrol. Earth Syst. Sci., 22, 1193–1219, https://doi.org/10.5194/hess-22-1193-2018, 2018.

465

- National Agricultural Library, UNSODA Database, https://data.nal.usda.gov/dataset/unsoda-20unsaturated-soil-hydraulic-database-database-and-program-indirect-methods-estimatingunsaturated-hydraulic-properties, last access 22 July 2020.
- Nemes, A., Schaap, M. G., Leij, F. J., and Wösten, J. H. M.: Description of the unsaturated soil hydraulic
- 470 database UNSODA version 2.0, J. Hydrol., 251, 152–162, https://doi.org/10.1016/S0022-1694(01)00465-6, 2001.
  - Or, D., and Tuller, M.: Liquid retention and interfacial area in variably saturated porous media: Upscaling from single–pore to sample–scale model, Water Resour. Res. 35, 3591–3605, 1999.
- Rossi, C., and Nimmo. J. R.: Modeling of soil water retention from saturation to oven dryness, Water Resour.
   Res., 30, 701–708, 1994.
  - Schneider, M., and Goss, K. –U.: Prediction of the water sorption term in air dry soils, Geoderma, 170, 64–69, https://doi.org/10.1016/j.geoderma.2011.10.008, 2012.
- Šimůnek, J., M. Th. van Genuchten, M. Th., and Šejna, M.: Recent developments and applications of the HYDRUS computer software packages, Vadose Zone Journal, 15, 1–25, https://doi.org/10.2136/vzj2016.04.0033, 2016.
  - Solone, R., Bittelli, M., Tomei, F., and Morari, F.: Errors in water retention curves determined with pressure plates: Effects on the soil water balance, J. Hydrol., 470–471, 65–74, https://doi.org/10.1016/j.jhydrol.2012.08.017, 2012.
  - SWAP Soil Water Atmosphere Plant, https://www.swap.alterra.nl/, last access: 10 August, 2022.
- 485 Tuller, M., and Or, D.: Water films and scaling of soil characteristic curves at low water contents, Water Resour. Res., 41, W09403, https://doi.org/10.1029/2005WR004142, 2005.
  - Twarakavi, N. K. C., Šimůnek, J., and Schaap, M. G.: Can texture–based classification optimally classify soils with respect to soil hydraulics?, Water Resour. Res. 46, W01501, https://doi.org/10.1029/2009WR007939, 2010.
- 490 van Genuchten, M. Th.: A closed-form equation for predicting the hydraulic conductivity for unsaturated soils, Soil Sci. Soc. Am. J., 44, 892–898, 1980.
  - Wang, Y., Ma, R., and Zhu, G.: Improved prediction of hydraulic conductivity with a soil water retention curve that accounts for both capillary and adsorption forces, Water Resour. Res., 58, e2021WR031297, https://doi.org/10.1029/2021WR031297, 2022.