



## Technical note: A sigmoidal soil water retention curve with a logarithmic dry branch that is robust when reliable dry-range data are lacking

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**Abstract.** In a recently introduced parameterization for the soil water retention curve (SWRC) with a sigmoid wet branch and a logarithmic dry branch, the matric potential at the junction point of the sigmoid and the logarithmic branch ( $h_j$ ) was a fitting parameter, while that at oven-dryness ( $h_d$ ) was derived from the fitting parameters. The latter is undesirable, especially if reliable data in the dry range are limited. Therefore, an alternative is presented in which shape parameter  $\alpha$  instead of  $h_d$  is a derived parameter, and  $h_d$  can be fitted or fixed. The resulting relationship between  $\alpha$  and  $h_j$  is such that it prevents correct fits for  $h_j$ . Fortunately, an expression for  $h_j$  is found that allows it to be replaced by  $\alpha$  as a fitting parameter. The corresponding parameter space is well-behaved and has fewer internal bounds defined by restraining relationships between parameters. The few available values of  $h_j$  in the literature are in line with those according to the new expression. The reformulated SWRC is fitted to data of 21 soils by shuffled complex evolution. The paper gives the main features of an accompanying open-source fitting code. The fits are good, except for some clayey soils. A theoretical value of  $h_d$  performs well for a wide range of soils. For some soils,  $\alpha$  is very large. If this is the case, the new SWRC simplifies to an earlier junction model of the SWRC based on a well-known power-law SWRC.



## 20 1 Introduction

Recently, de Rooij et al. (2021) proposed a closed-form expression for the SWRC with a distinct air-entry value, like the SWRC proposed by Ippisch et al. (2006), a sigmoid shape in the intermediate range according to van Genuchten (1980), and a logarithmic dry branch terminating at a finite matric potential ( $h_d(L)$ ) at which the soil was oven-dry, with the water content essentially zero. The volumetric water contents and derivatives of the sigmoid and  
 25 logarithmic branches were matched at the matric potential of their junction according to Rossi and Nimmo (1994). The rationale for developing the function was to preserve the desirable sigmoid shape of van Genuchten's (1980) curve while removing the physically unrealistic asymptote at some non-zero residual water content (Du, 2020), eliminating the non-converging integral of the SWRC for commonly occurring parameter values (Fuentes et al., 1991), and avoiding the detrimental effect of the non-zero slope at saturation on hydraulic conductivity near saturation (Durner, 1994;  
 30 Wang et al., 2022).

De Rooij et al. (2021) showed that erroneous measurements in the dry range could lead to unrealistically low values of the matric potential at oven dryness,  $h_d(L)$ . Unfortunately, in their formulation of the model,  $h_d$  was not fitted independently but expressed as a function of other parameters that were fitted. Data in the dry range can be unreliable due to lack of equilibrium or other causes (Bittelli and Flury, 2009; Solone et al., 2012). If they are, it would be very  
 35 helpful to fix  $h_d$  at a reasonable value, e.g.  $-10^{6.8}$  cm H<sub>2</sub>O (Schneider and Goss, 2012), and either give the unreliable data points a lower weight during the fitting process or remove them altogether.

This note presents an alternative of de Rooij et al.'s (2021) model in which  $h_d$  is a fitting parameter. In doing so, it uncovers the peculiar behavior of shape parameter  $\alpha (L^{-1})$ , which makes it essentially impossible for any fitting algorithm to avoid a local minimum with very inaccurate parameter values. The main objective is therefore to formulate  
 40 a version of de Rooij's (2021) SWRC that has  $h_d$  as a fitting parameter but avoids the difficulties caused by the nature of shape parameter  $\alpha$ .

In the testing phase, it was found that a commonly used convergence criterion used in parameter optimization not necessarily gave the best parameter values if the objective function was challenging. The second objective is therefore to present a parameter fitting algorithm that employs multiple convergence criteria, and optionally explores  
 45 the parameter space prior to the fitting operation to reduce the search area during fitting. The corresponding open-source code for fitting the improved SWRC is provided.

## 2 Theory

De Rooij et al. (2021) introduced a unimodal model for the SWRC by combining those of Rossi and Nimmo (1994) and Ippisch et al. (2006), dubbed 'RIA'.



$$\theta(h) = \begin{cases} 0, & h \leq h_d \\ \theta_s \beta \ln\left(\frac{h_d}{h}\right), & h_d < h \leq h_j \\ \theta_s \left(\frac{1+|\alpha h|^n}{1+|\alpha h_{ae}|^n}\right)^{\frac{1}{n}-1}, & h_j < h \leq h_{ae} \\ \theta_s, & h > h_{ae} \end{cases} \quad (1)$$

Here  $h$  denotes the matric potential in equivalent water column (L), subscripts ‘d’ and ‘ae’ denote the value at which the water content reaches zero and the air-entry value, respectively, and subscript ‘j’ indicates the value of  $h$  at which the logarithmic and sigmoid branch are joined. The volumetric water content is denoted by  $\theta$ , with the subscript ‘s’ denoting its value at saturation. Parameters  $\alpha$  ( $L^{-1}$ ) and  $n$  determine the shape of the sigmoid branch (van Genuchten, 1980), while parameter  $\beta$  does so for the logarithmic branch. By assuming that for  $h \leq h_j$ , all water is adsorbed and for  $h > h_j$ , the adsorbed water content is equal to  $\theta(h_j)$ , the total water content can be partitioned in a capillary water content  $\theta_c$  and an adsorbed water content  $\theta_a$ .

Data points in the dry range are often unreliable due to lack of hydraulic equilibrium or other causes (Bittelli and Flury, 2009; Solone et al., 2012). De Rooij et al. (2021) showed this could lead to unrealistically large negative values of  $h_d$ . If that is the case it would be preferable to fix  $h_d$  at a realistic value, e.g.  $-10^{6.8}$  cm H<sub>2</sub>O (Schneider and Goss, 2012), but de Rooij et al. (2021) expressed  $h_d$  as a function of other parameters, not as an independent fitting parameter.

By requiring the derivatives of the sigmoidal and logarithmic branches to match at  $h_j$ , parameter  $\beta$  can be expressed in terms of the other parameters (de Rooij et al., 2021).

$$\beta = (n-1)|\alpha h_j|^n (1+|\alpha h_{ae}|^n)^{1-\frac{1}{n}} (1+|\alpha h_j|^n)^{\frac{1}{n}-2} \quad (2)$$

Using this expression to eliminate  $\beta$  from the equality that arises when the values of both branches are matched at  $h_j$ , we can then solve the resulting expression for  $\alpha$  to establish  $h_d$  as one of the fitting parameters.

$$\alpha = |h_j|^{-1} \left[ (n-1) \ln\left(\frac{h_d}{h_j}\right) - 1 \right]^{-\frac{1}{n}} \quad (3)$$

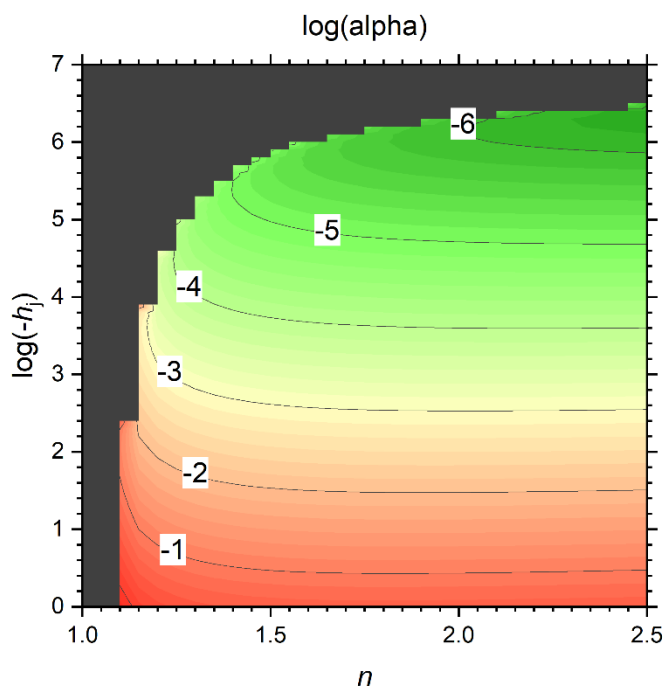
The five fitting parameters are:  $h_{ae}$ ,  $h_j$ ,  $h_d$ ,  $\theta_s$ , and  $n$ . Equation (3) is only valid if the bracketed term is positive. This is the case if the following criterion is met.

$$|h_j| < |h_d| e^{\frac{1}{1-n}} \quad (4)$$



80 Many soils have values for  $\alpha$  between roughly 0.001 and 0.3, with sandy soils generally having higher values than fine-textured soils (e.g., de Rooij et al., 2021). When  $h_d$  is fixed at  $-10^{6.8}$  cm H<sub>2</sub>O,  $\alpha$  is a function of  $n$  and  $h_j$  only. Its contour map is depicted in Fig. 1. The map shows that combinations of realistic but large  $n$  and ( $n > \sim 1.4$  and  $\alpha > \sim 0.01$ ) require values of  $h_j$  that are unrealistically close to zero ( $-10^2$  cm). Such large values of  $n$  indicate a chair-shaped SWRC and are frequently fitted for coarse soils in which the water content changes rapidly within a narrow range of

85 the matric potential. De Rooij et al. (2021) reported four soils with data sets without suspect data points above pF 3 for soils with  $n > 1.2$  (soils 1142, 1143, 2110, and 2126, all sands or loamy sands). De Rooij et al.'s (2021) values of  $\alpha$  and  $n$  for these soils give values of  $h_j$  that are all larger (closer to zero) than  $-150$  cm, which is unrealistic. For soil ~~soil~~ 2126 the value even exceeds  $h_{ae}$ , which is not physically acceptable.



90 **Figure 1:** The logarithm of shape factor  $\alpha$  (cm<sup>-1</sup>) as a function of shape factor  $n$  and the matric potential at the junction point  $h_j$  (cm H<sub>2</sub>O) according to Eq. (3), with  $h_d$  fixed at  $-10^{6.8}$  cm. The labels of the contour lines represent  $\log(\alpha)$ . The black area is the invalid part of the domain defined by Eq. (4).

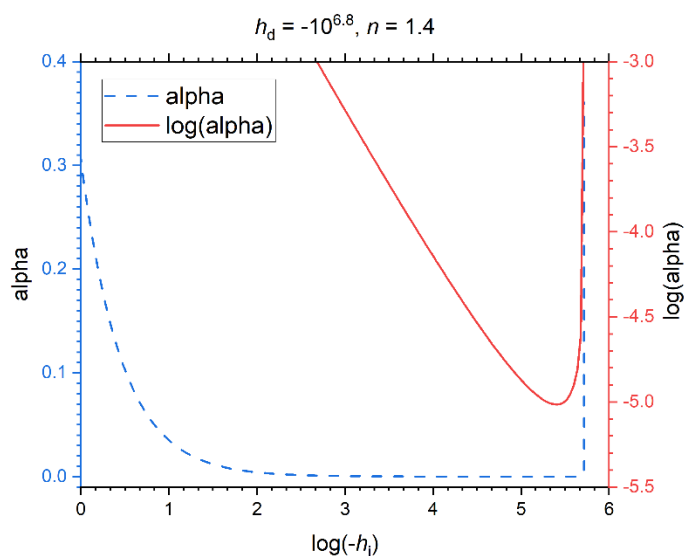
It therefore appears from Fig. 1 that plausible combinations of  $\alpha$  and  $h_j$  are not feasible, but closer inspection

95 of Eq. (3) reveals that the relationship  $\alpha(h_j)$  is non-monotonous. A combination of large values of both  $\alpha$  and  $h_j$  is possible in a band too narrow to be visible in Fig. 1, where  $h_j$  is very close to its maximum allowed value. In that narrow



band,  $\alpha$  goes to infinity when  $h_j$  approximates its limiting value defined in Eq. (4) (Fig. 2). The partial derivative of Eq. (3) with respect to  $h_j$  is as follows.

$$100 \quad \frac{\partial \alpha}{\partial h_j} = \frac{1}{h_j^2} \left[ (n-1) \ln \left( \frac{h_d}{h_j} \right) - 1 \right]^{-\frac{1}{n}} + \frac{1-n}{n} \frac{1}{h_j^2} \left[ (n-1) \ln \left( \frac{h_d}{h_j} \right) - 1 \right]^{-\frac{n+1}{n}} \quad (5)$$



**Figure 2:** A transect of Figure 1 for  $n = 1.4$  that shows the sharp increase of shape factor  $\alpha$  (cm<sup>-1</sup>) as the matric potential at the junction point  $h_j$  (cm H<sub>2</sub>O) reaches its physical limit defined in Eq. (4).

The value of  $\alpha$  is at its minimum where its derivative is zero. From Eq. (5) follows this occurs when the following equality holds.

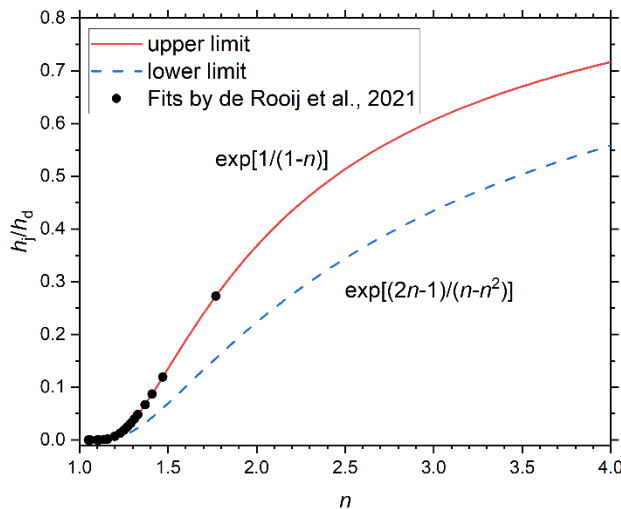
$$110 \quad \ln \left( \frac{h_d}{h_j} \right) = \frac{2n-1}{n^2-n} \quad (6)$$

Because Fig. 1 shows that realistic values of  $\alpha$  require excessively low values of  $h_j$  in much of the parameter space, it may be better to use Eq. (6) to set a lower limit on the permissible values of  $h_j$  as follows.

$$115 \quad |h_j| > |h_d| e^{\frac{2n-1}{n^2-n}} \quad (7)$$



Figure 3 shows the band of valid values of  $h_j$  enveloped by the limits set by Eqs. (4) and (7). Exploring the parameter space between these limits of  $h_j$ , with an excessively large  $\partial\alpha/\partial h_j$  in a large part of it, will be very difficult for any parameter fitting algorithm. But if the lower limit is not enforced, trial fits showed that the shuffled complex evolution algorithm (SCE, Duan et al., 1992, 1993) consistently ended up in the lower region of Fig. 1.



**Figure 3:** The limits imposed on the matric potential at the junction point  $h_j$  (scaled by the matric potential at oven-dryness  $h_d$ ) by the requirement that shape factor  $\alpha$  be positive (upper limit) and by the minimum value of  $\alpha$  for any specific value of  $n$  (lower limit). The dots represent de Rooij et al.'s (2021) fits of Eq. (1) with  $\alpha$  instead of  $h_d$  as a fitting parameter for 21 soils.

De Rooij et al. (2021) already fitted Eq. (1) with  $\alpha$  instead of  $h_d$  as a fitting parameter and without any restrictions other than minimum and maximum values imposed on any of the fitting parameters. By calculating  $h_d$  from the fitted values of  $\alpha$ ,  $n$ , and  $h_j$  according to their Eq. (10) it was possible to see if their fits fell within the limits defined above. Figure 3 shows that the values of all 21 soils fell on the upper limit. This opens the possibility to eliminate  $h_j$  as a fitting parameter and replace it by its upper limit. This leads to the following additional equation augmenting Eq. (1).

$$h_j = h_d e^{\frac{1}{1-n}} \quad (8)$$

Combining Eq. (8) with Eq. (3) leads to an infinite  $\alpha$ , consistent with Fig. 2. But Fig. 2 also shows that a minute change in  $h_j$  (much smaller than a realistic number of significant digits would be able to represent) allows  $\alpha$  to vary beyond the range of values reported in the literature. In other words: If, for given values of  $h_d$  and  $n$ ,  $h_j$  is determined from Eq. (8),



$\alpha$  can vary over its entire range. It is therefore better to treat  $\alpha$  as a fitting parameter and  $h_i$  as a derived parameter, by replacing Eq. (3) by Eq. (8). This has the added advantage that the entire parameter space defined by the minimum and maximum values of the fitting parameters is valid, provided the physical and mathematical limits of each parameter are respected, and the fitted or fixed value of  $h_d$  is smaller (more negative) than  $h_{ae}$ .

It is worth noticing that the expression for the sigmoid branch of the SWRC remains well-behaved in the limit as  $\alpha$  approximates infinity. The expression in that case simplifies to the power law proposed by Brooks and Corey (1964).

$$\lim_{\alpha \rightarrow \infty} \theta_s \left( \frac{1+|\alpha h_i|^n}{1+|\alpha h_{ae}|^n} \right)^{\frac{1}{n}-1} = \theta_s \left( \frac{h}{h_{ae}} \right)^{1-n} \quad (9)$$

It can be easily shown that both the values and the derivatives of the dry and the wet branch match at  $h_i$  if Eq. (9) is used for the latter. Equation (9) establishes that Rossi and Nimmo's (1994) junction model (without the parabolic smoothing near saturation that Madi et al. (2018) showed to be detrimental to the hydraulic conductivity function) is a special case of the RIA parameterization. Incidentally, this implies that Brooks and Corey's model (1964) is a special case of that of Ippisch et al. (2006).

If Eq. (8) replaces Eq. (3), the fitted value of  $\alpha$  no longer ensures continuity at the junction point. The ensuing continuity gap can be closed by applying a correction factor  $c$  to the value of  $h_d$  used in the logarithmic branch as follows.

$$\theta = \theta_s \beta \ln \left[ \frac{(1+c)h_d}{h} \right] \quad (10)$$

The correction factor  $c$  is defined by the following expression.

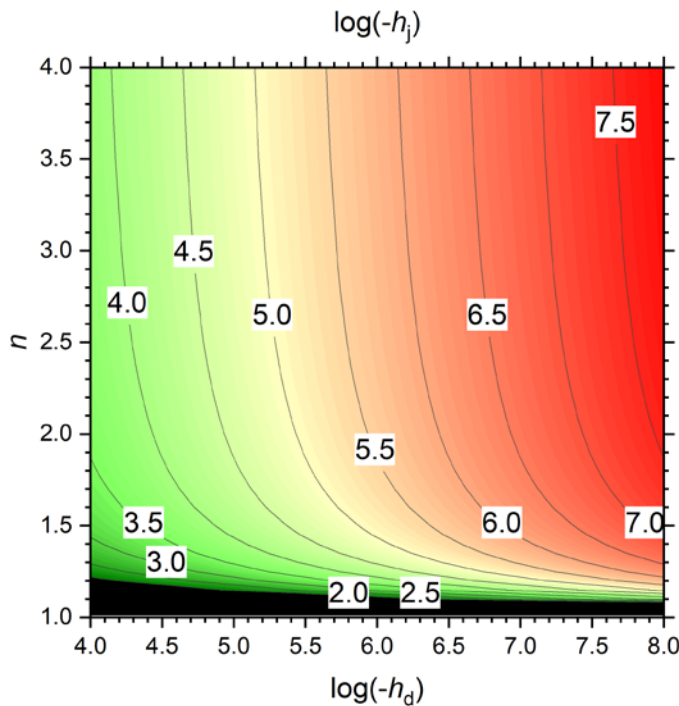
$$c = \exp \left[ \frac{1}{\beta} \left( \frac{1+|\alpha h_i|^n}{1+|\alpha h_{ae}|^n} \right)^{\frac{1}{n}-1} + \frac{1}{1-n} \right] - 1 \quad (11)$$

In the expression for  $\beta$ ,  $h_d$  appears indirectly. Its value should not be corrected there because  $\beta$  ensures continuity of the derivatives only if its expression is not modified. Trial calculations showed that  $c$  is negligible, except when both  $\alpha$  and  $n$  are small.

Rossi and Nimmo (1994) fitted  $h_i$  values for their parameterization of the SWRC between  $-2.6 \cdot 10^6$  and  $-2.0 \cdot 10^4$  cm H<sub>2</sub>O for seven soils, with only the one clayey soil having a value more negative than  $-1.9 \cdot 10^5$  cm H<sub>2</sub>O. Tuller and Or (2005) tentatively set the matric potential at which the capillary-bound water content becomes negligible  $-10^5$  cm H<sub>2</sub>O, based on data from a sand mixture and six soils that mostly overlap with those of Rossi and Nimmo (1994) (Or and



170 Tuller, 1999). Beyond this there is little guidance on the value of  $h_j$  in the literature. When Eq. (8) is used, such guidance is not necessary. The map of  $h_j$  as defined by Eq. (8) in Fig. 4 shows that for  $n$  below 1.4,  $h_j$  is very sensitive to the value of  $n$ . For  $n > 2$ ,  $\log(-h_j)$  is roughly proportional to  $\log(-h_d)$  for a given value of  $n$ . When  $h_d$  is close to  $-10^{6.8}$  cm H<sub>2</sub>O (Schneider and Goss, 2012), values of  $h_j$  in the range of those reported in the literature occur for  $n \geq 1.25$ .



175 **Figure 4: The logarithm of the absolute value of the matric potential at the junction point ( $h_j$ , cm H<sub>2</sub>O) as a function of the matric potential at oven-dryness ( $h_d$ , cm H<sub>2</sub>O) and shape factor  $n$ , according to Eq. (8). The labels of the contour lines denote  $\log(-h_j)$ . In the black region,  $h_j > -100$  cm.**

For completeness, the multimodal version of Eq. (1) is provided as well. Like de Rooij et al. (2021), the multimodality is limited to the sigmoid branch, so that the multimodal SWRC has only one value for  $h_j$ . Because Eq. (8) allows only a single value of  $n$  in that case, only  $\alpha$  can be varied between the constituting sigmoid curve sections.

$$\theta(h) = \begin{cases} 0, & h \leq h_d \\ \theta_s \beta_m \ln\left(\frac{h_d}{h}\right), & h_d < h \leq h_j \\ \theta_s \sum_{i=1}^k w_i \left(\frac{F_i(h)}{F_i(h_{ae})}\right)^{\frac{1}{n}-1}, & h_j < h \leq h_{ae} \\ \theta_s, & h > h_{ae} \end{cases} \quad (12)$$





For brevity, the following function was introduced in Eq. (12).

$$F_i(x) = 1 + |\alpha_i x|^n \quad (13)$$

Here,  $k$  denotes the modality,  $w_i$  is the weighting factor (adding up to one) of the  $k^{\text{th}}$  constituting curve, and  $\alpha_i$  ( $L^{-1}$ ) its shape factor. The expression for the multimodal  $\beta_m$  is found by setting the derivatives of the logarithmic and the sigmoid branch equal at  $h_i$  and invoking Eq. (8).

$$\beta_m = \frac{n-1}{e} |h_d|^{n-1} \sum_{i=1}^k w_i \alpha_i^n F_i(h_{ae})^{1-\frac{1}{n}} G_i(h_d)^{\frac{1}{n}-2} \quad (14)$$

Function  $G$  is defined as follows.

$$G_i(x) = 1 + |\alpha_i x|^n e^{\frac{n}{1-n}} \quad (15)$$

The continuity correction factor  $c_m$  can be found by requiring that the logarithmic and sigmoid branch join at  $h_i$ .

$$c_m = \exp \left[ \frac{1}{n-1} (e |h_d|^{1-n} - 1) \frac{\sum_{i=1}^k w_i \left( \frac{G_i(h_d)}{F_i(h_{ae})} \right)^{\frac{1}{n}-1}}{\sum_{i=1}^k w_i \alpha_i^n F_i(h_{ae})^{1-\frac{1}{n}} G_i(h_d)^{\frac{1}{n}-2}} \right] - 1 \quad (16)$$

Above, the subscript ‘m’ is used to distinguish multimodal versions of  $\beta$  and  $c$  from their single-mode equivalents.

### 3 Materials and Methods

#### 3.1 Selected soils

The SWRC has five fitting parameters:  $\theta_s$ ,  $h_{ae}$ ,  $h_d$ ,  $\alpha$ , and  $n$ . These were fitted to data of the 21 soils selected from the UNSODA database (Nemes et al., 2001) by de Rooij et al. (2021), with  $h_d$  either fixed at  $-10^{6.8}$  cm  $H_2O$ , or its lower limit set at that value. These soils cover a wide range of textures (see Madi et al. (2018) and de Rooij et al. (2021) for details). At the time the data base was created, the the pressure plate apparatus was widely used in the dry range. Therefore, the standard deviation (SD) of the matric potential of any data point with  $h \leq -1000$  cm  $H_2O$  was set to half its value, thereby drastically reducing its weight in the objective function. The SD of  $h$  for  $0 > h > -1000$  cm  $H_2O$



210 was set to 1.0 cm, that for  $h = 0$  at 0.05 cm. The SD for the volumetric water content was set at 0.01 when  $h = 0$ , and to 0.02 otherwise. The sample height was set to zero for  $h \leq -1000$  cm and for  $h = 0$  cm. For the intermediate values of  $h$ , the sample height was set to the value specified in the UNSODA database. If a sample height was not reported, it was set to 3.0 cm.

### 3.2 Parameter fitting

215 The parameters were fitted using the SCE algorithm (Duan et al., 1992, 1993), implemented in Fortran in a code that accompanies this paper. The most important features of the code are summarized here. The code itself, further details of the code and the algorithm, as well as a user manual, can be downloaded (de Rooij, 2022). For each case, the code performs three optimization runs by minimizing the objective function: the root mean square error (RMSE) of the differences between fitted and observed values, weighted according to the error standard deviations of  
 220 the observed matric potentials and corresponding water contents provided on input, as detailed by de Rooij (2022).

Ten convergence criteria are evaluated. Criteria 1 and 2 take into account the results of the last few shuffles. The number of shuffles considered is twice the number of fitting parameters or an internally set number (5), whichever is larger.

1. In the best fits from the last set of shuffles, the range of a parameter exceeds neither the absolute nor the  
 225 relative user-specified tolerance.
2. In the best fits from the last set of shuffles, the range of the objective function does not exceed its absolute user-specified tolerance.
3. The parameter range in the final complexes does not exceed the maximum internally set permissible value.
4. The volume of the hypercube enveloping the final complexes does not exceed the maximum internally set  
 230 permissible value.
5. The parameter range in the most successful complex (minus the point with the highest RMSE) does not exceed the internally set maximum permissible value.
6. The volume of the hypercube enveloping the most successful complex (minus the point with the highest RMSE) does not exceed the internally set maximum permissible value.
- 235 7. A parameter does not exceed both the absolute and the relative user-specified tolerance in the final complexes.
8. A parameter does not exceed both the absolute and the relative user-specified tolerance in the most successful complex (without the point with the highest RMSE).
9. The change of the objective function between consecutive shuffles does not exceed the user-specified tolerance.
- 240 10. The Root Mean Square Error of the fit does not exceed a user-specified tolerance.



A relative improvement criterion similar to criterion 9 is often used as the sole criterion (e.g., in the R-package SoilHyp, Dettmann, 2021). Criteria 1, 3, 5, 7, and 8 are evaluated separately for each parameter. Convergence is achieved when no more than a user-prescribed number of these criteria failed for any of the parameters. The code keeps evolving and shuffling complexes until convergence is achieved or the user-specified maximum allowed number of evaluations of the objective function is exceeded. If not all criteria are considered relevant, the user can either set their thresholds unrealistically strict and increase the number of criteria that are allowed to fail, or set them excessively loose and decrease the number of criteria that are allowed to fail accordingly.

The algorithm generates large numbers of sets of fitted parameter values. A random sample of these is used to determine the correlation matrix of the parameters. The best fit, its RMSE and its correlation matrix are reported by the code for each of the three runs, and the run with the overall lowest RMSE is identified. The code returns a table of the fitted curve based on the best run, and reports the correction factor  $c$  used to compile this table. These tables are the basis for the plots shown below. If desired, the code also calculates the objective function on points of a regular grid covering the parameter space (map points) and writes a random sample of these to output. Even if this is not desired, a map is calculated based on a three-point grid along each principal axis of the parameter space. This resulting output is helpful if a user wishes to verify if the objective function is correctly calculated.

Normally, the first complexes of each run are filled with randomly selected points in the valid regions of the parameter space. Optionally, only the complexes of run 3 are filled with randomly selected points, while the first complexes of run 1 are filled with the map points with the lowest RMSE. The first complexes of run 2 then contain these map points perturbed by adding random noise to the parameter values.

For each fitting parameter, a maximum and minimum value need to be provided. If these values are equal, the parameter is treated as a fixed value, and the dimensionality of the parameter space is reduced accordingly. The number of complexes is two (for 8 or fewer fitting parameters) or four (see Duan et al. (1994)). If this leads to frequent convergence at local minima, the number of complexes can be set to twice the number of fitting parameters. The number of individuals in a complex and the number of evolution steps are twice the number of fitting parameters plus one. The number of individuals in the subcomplexes is the number of fitting parameter plus one. The number of offspring in each evolution step is one. These settings are all in accordance with Duan et al. (1994).

When the user chooses to use the map of regularly-spaced points in the parameter space to set the initial guesses of the first two runs, the code reduces the parameter ranges based on their ranges among the map points selected to fill the initial complexes.

No more than four convergence criteria were allowed to fail for convergence to be achieved. If convergence was not achieved, up to 20000 evaluations of the objective function evaluations would be performed. The actual number could be slightly higher because it was checked each time a shuffle had been completed. A map was not created,



275 and therefore, all three optimization runs started with random parameter combinations filling the complexes. The maximum allowed relative change of the RMSE between consecutive shuffles was  $10^{-6}$ . The maximum allowed value of the RMSE was 0.1. For the parameters, the absolute tolerances for  $\theta_s$ ,  $h_{ae}$ ,  $h_d$ ,  $\alpha$ , and  $n$  were 0.001, 0.1, 1000.0, 0.1, and 0.01, respectively. The relative tolerances were 0.1 for  $\alpha$  and 0.01 for the others. This choice reflects the limited sensitivity to  $\alpha$ .

280 The internally set relative tolerance for parameter variations for all complexes and for the most successful complex were both 0.01. The internally set required maximum size of the hypercube enveloping the range of fitted parameter values (again for all complexes as well as the most successful one), scaled by the volume of the hypercube defined by the minimum and maximum allowed parameter values, equals  $0.01^d$ , with  $d$  the number of fitting parameters that were not set at fixed values by the user.

## 285 4 Results and Discussion

Table 1 shows the fitted parameter values of the best fits, the resulting RMSE and the corresponding value of  $h_j$ . The value of  $\alpha$  for soil 1142 stands out. As explained above, high values of  $\alpha$  lead to a power-law type of SWRC between  $h_{ae}$  and  $h_j$ . An additional fit with  $\alpha$  capped at 1.0 confirmed that the shape of the SWRC is not very sensitive to large values of  $\alpha$ . The increase in the RMSE caused by limiting the range of  $\alpha$  was  $10^{-4}$ , and the changes in  $\theta_s$ ,  $h_{ae}$ , and  $n$  did not occur before the fourth significant digit. One can also switch from a sigmoidal model to a power-law model by invoking Eq. (9) if  $\alpha$  is very large, keeping the fitted values of the other parameters.

290 Fuentes et al. (1991) showed that for values of  $n$  smaller than 2, the asymptotic dry branch of the original parameterization of van Genuchten (1980) would lead to physically unacceptable behaviour. All soils in Table 1 have values of  $n$  in this range. This highlights the importance of avoiding a dry branch with an asymptote at a residual water content.

The range of values of  $h_j$  in Table 1 is only slightly beyond the range reported by Rossi and Nimmo (1994) for a smaller number of soils. This lends credibility to Eq. (8). In the few cases where  $h_d$  was fitted, the resulting values in Table 1 are close to the value proposed by Schneider and Goss (2012). Table 2 shows the the correction factor  $c$  of Eqs. (10) and (11), which ensures continuity of the SWRC. Seven of the 21 soils need a correction of  $h_d$  that exceeds 1%. The resulting shift of the dry-branch pF is also shown. For most soils, the shift is negligible. Only for soils 1122 and 1123 (both fine-textured soils with small values for both  $\alpha$  and  $n$ ), the shift exceeds 0.1 pF unit, but never more than 0.2 unit.

300 Only the optimizations for soils 1142 and 2104 converged, with convergence criteria 4, 6, 8, 9, and 10 satisfied for all parameters for soil 1142, and criteria 4 through 10 for soil 2104. None of the correlation coefficients of the parameter pairs for either soil exceeded 0.31. The other optimizations ran until the maximum number of objective function evaluations was exceeded. For soil 1120, criteria 9 and 10 were met for all parameters. For the remaining



soils, criteria 1, 2, and 9 were satisfied in all cases. For 14 soils, criterion 10 was met as well. For soil 3250, criterion 8 was also satisfied. The lack of convergence forced the code to keep exploring the parameter space, leading to a large proportion of randomly selected points because the reflection and contraction points determined by the SCE algorithm did not improve the fit. If the majority of points is randomly selected, there is no correlation between the parameters, and the correlation matrix does not provide any information.

Table 1. Fitted parameter values and the Root Mean Square Error (RMSE) of the best fits for 21 soils. The corresponding values of the derived parameter  $h_i$  are given as well. If parameter  $h_d$  was fixed during the fitting operation, its value is denoted in italic font.

Soil (UNSODA identifier and classification according to Twarakavi et al., 2010)	$\theta_s$	$h_{ae}$ (cm H <sub>2</sub> O)	$\log(-h_d)$ ( $h_d$ in cm H <sub>2</sub> O)	$\alpha$ (cm <sup>-1</sup> )	$n$	RMSE	$\log(-h_i)$ ( $h_i$ in cm H <sub>2</sub> O)
2126 A1	0.3808	-3.999	<i>6.8000</i>	0.1332	1.8319	0.1434	6.2779
1142 A2	0.2404	-25.90	6.5623	561.2	1.3882	0.0545	5.4435
2104 A2	0.3980	-2.990	<i>6.8000</i>	0.1156	1.4400	0.0715	5.8129
1120 A3	0.3076	-0.012	<i>6.8000</i>	0.02803	1.3016	0.0796	5.3601
1143 A3	0.2761	-5.017	<i>6.8000</i>	0.08308	1.2214	0.0589	4.8384
2110 A3	0.3634	-0.014	<i>6.8000</i>	0.03268	1.3431	0.0930	5.5343
2132 A3	0.3058	-0.004	<i>6.8000</i>	0.06055	1.1413	0.0417	3.7264
1121 A4	0.3441	-13.97	6.7811	0.04667	1.1560	0.0830	3.9970
1133 A4	0.3280	-240.5	<i>6.8000</i>	0.001366	1.1985	0.0477	4.6126
3260 B2	0.4740	-0.009	6.4711	0.02055	1.3234	0.0510	5.1281
3261 B2	0.4934	-0.015	<i>6.8000</i>	0.02379	1.3549	0.0731	5.5763
3263 B2	0.4628	-0.014	<i>6.8000</i>	0.01920	1.2925	0.0737	5.3151
3250 B4	0.5400	-3.796	<i>6.8000</i>	0.01236	1.2636	0.0611	5.1525
3251 B4	0.4980	-0.582	6.7479	0.01321	1.1576	0.0857	3.9918
4450 B4	0.3705	-0.548	<i>6.8000</i>	0.03784	1.1577	0.1150	4.0459
1135 C2	0.4147	-174.8	<i>6.8000</i>	0.001791	1.1763	0.0478	4.3361
1182 C2	0.5307	-8.131	<i>6.8000</i>	0.01349	1.1551	0.2484	3.9991
1122 C4	0.3571	-8.664	<i>6.8000</i>	0.001385	1.1550	0.0497	3.9976
1123 C4	0.3575	-67.17	<i>6.8000</i>	0.001008	1.1554	0.0663	4.0054
1180 C4	0.4885	-2.005	<i>6.8000</i>	0.1319	1.1549	0.2514	3.9962
1181 C4	0.4407	-7.282	<i>6.8000</i>	0.006671	1.1552	0.1593	4.0012

In all cases, the fitted parameter values for the runs with  $h_d$  fixed and  $h_d$  free as well as the three individual runs for each optimization were essentially in agreement, and the parameter values did not look suspect. Therefore, it was considered unnecessary to run the optimizations with modified convergence requirements in order to obtain more meaningful correlation matrices.



The reduced weights assigned to data points with  $pF > 3$  are reflected in the plots of Figs. 5 through 8, which show the fitted curves with  $h_d$  fixed and  $h_d$  fitted. In these plots, the fit with the lowest RMSE is plotted in red, and the corresponding curves for  $\theta_c$  and  $\theta_a$  are included. The other curve is shown in black. To illustrate how small the continuity correction  $c$  is, this curve is shown without this correction. The discontinuity at the junction point is only visible for soils 1133 (Fig. 6) and 1122 (Fig. 8).

Table 2. The continuity correction factor  $c$  (Eq.(11)) and the corresponding shift on the  $pF$  scale of the dry-branch correction for 21 soils.

Soil (UNSODA identifier and classification according to Twarakavi et al., 2010)	Correction factor $c$	$pF$ -shift dry branch
2126 A1	1.525E-10	6.62E-11
1142 A2	1.092E-11	4.74E-12
2104 A2	2.164E-07	9.40E-08
1120 A3	3.666E-05	1.59E-05
1143 A3	1.162E-04	5.04E-05
2110 A3	1.063E-05	4.62E-06
2132 A3	0.009750	0.00421
1121 A4	0.005323	0.00231
1133 A4	0.04130	0.0176
3260 B2	8.647E-05	3.76E-05
3261 B2	1.243E-05	5.40E-06
3263 B2	7.641E-05	3.32E-05
3250 B4	3.015E-04	1.31E-04
3251 B4	0.02300	0.00988
4450 B4	0.005833	0.00253
1135 C2	0.07969	0.0333
1182 C2	0.02266	0.00973
1122 C4	0.3664	0.136
1123 C4	0.5566	0.192
1180 C4	0.001627	7.06E-04
1181 C4	0.05147	0.0218

The fraction of adsorbed water increases when moving from sands (Figs. 5 and 6) through loams (Fig. 6 and 7) to clays (Fig. 8). Because the separation between capillary and adsorbed water is abrupt and binary at  $h_j$ , this should not be interpreted as representative for the more smooth transition in natural soils. Nevertheless, the direction of the trend is physically plausible.

Most soils (2126 and 1142 in Fig. 5; 1120, 1121, 1143, 2110, and 2132 in Fig. 6; 1142 and 2126 in Fig. 7; 1122, 1180, and 1182 in Fig. 8) have observed saturated water contents that seem to be too large compared to the other data



points. The causes (e.g., macropores or air inclusion) are not known. Data points at saturation were assumed to be very accurate and therefore had a high weight, which the plots reflect. It sometimes results in relatively low (more negative) air-entry values in coarse soils (Figs. 5 and 6 and Table 1, most notably soil 1142).

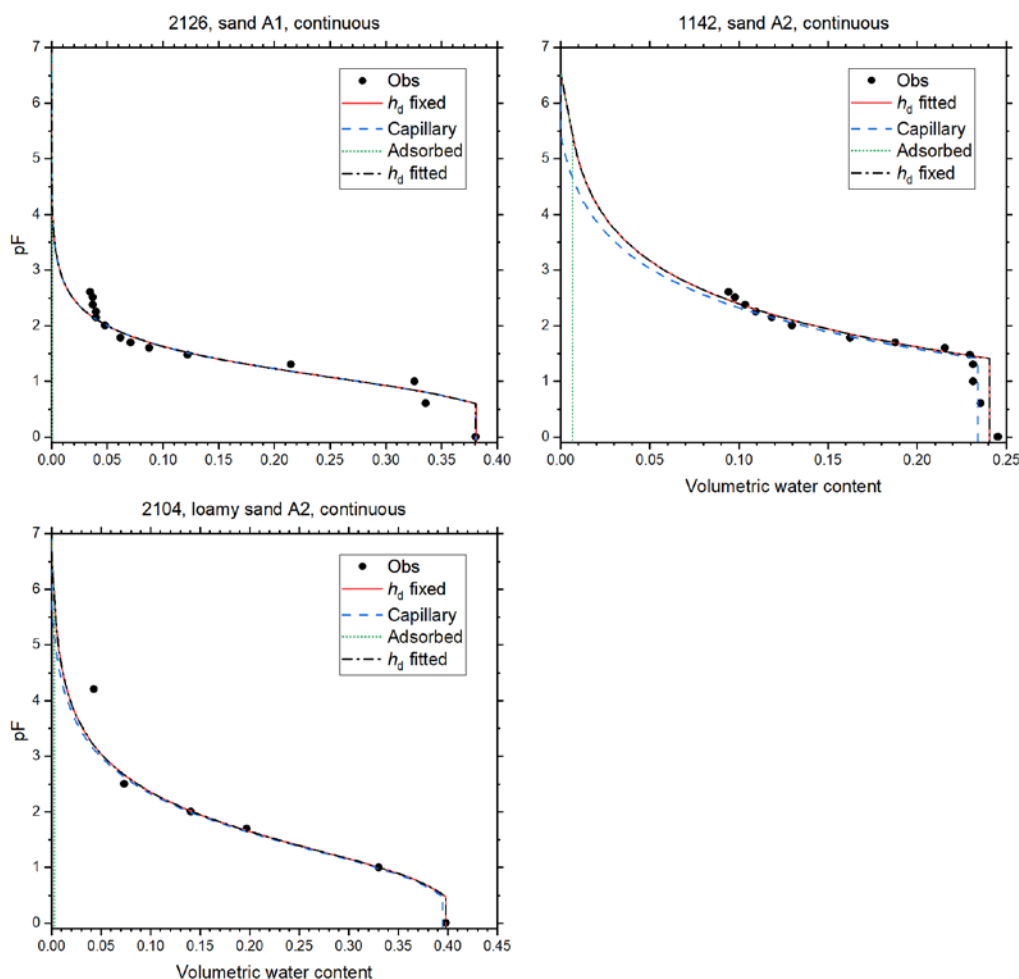


Figure 5: Soil water retention data and fitted curves for soils of classes A1 and A2 of Twarakavi et al. (2010). Curves fitted with  $h_d$  fixed at  $-10^{6.8}$  cm  $H_2O$ , and with  $h_d$  fitted with a cap at that value are shown. The one with the lowest Root Mean Square Error is shown in red. The volume fractions of capillary-bound water and water adsorbed in films is shown for this curve. The other curve is shown as black dash-dot line. This curve has not been corrected for continuity at the junction point. The vertical axes denote the logarithm (base 10) of the absolute value of the matric potential in cm  $H_2O$ .



All B2 soils (silt loams) and two out of three B4 soils (both silty clay loams) have high values of  $h_{ae}$ , indicating that the maximum pore size is large (Table 1). Although one would suspect that such fine-textured soils would have a low (more negative) air-entry value, the results are consistent with the data, as Fig. 7 shows.

Some of the C2 and C4 soils (1180-1182) have high RMSE values (Table 1). Their plots in Fig. 8 reveal that the  
345 shape of the curves was not captured well by Eq. (1).



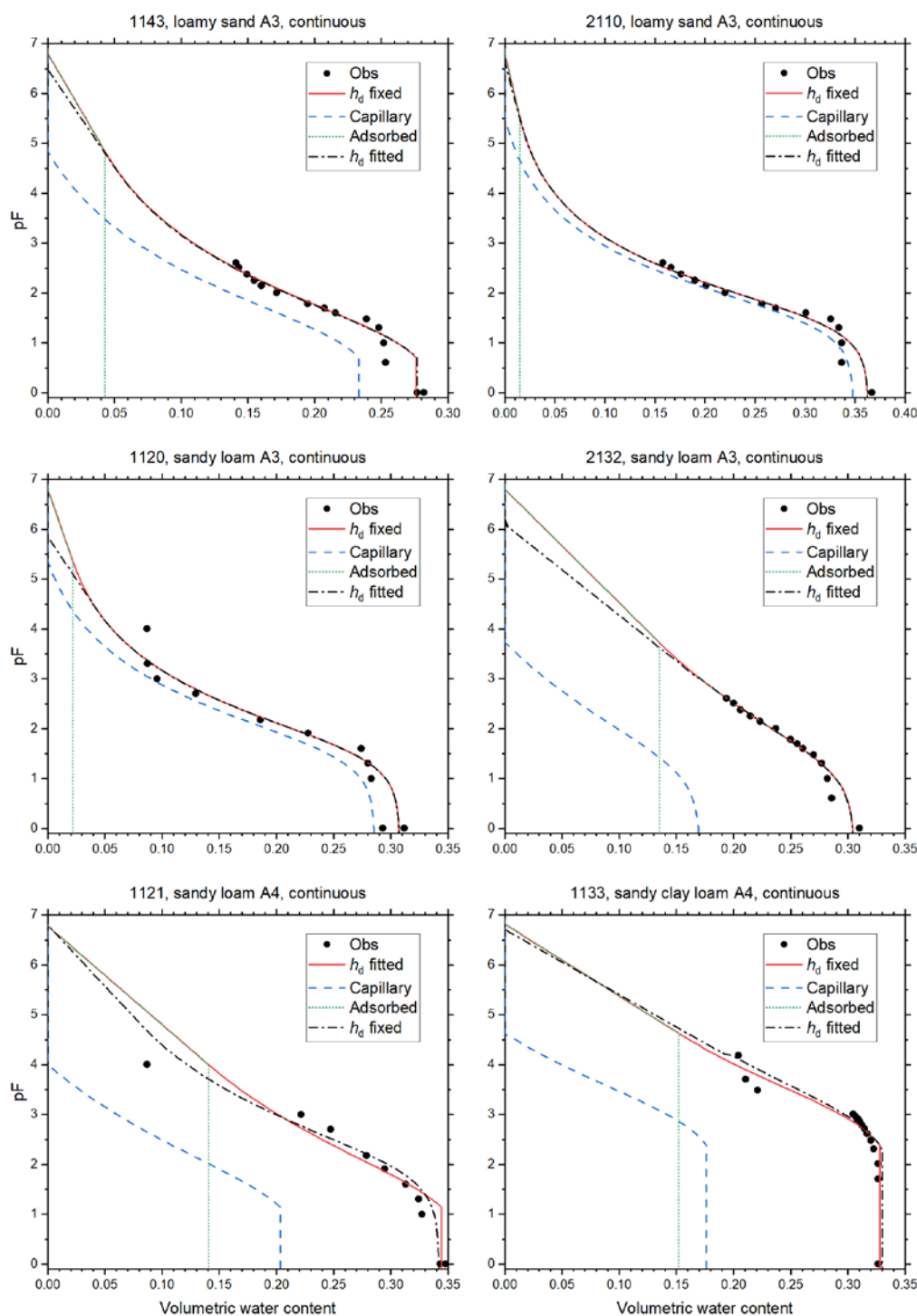


Figure 6: As Fig. 5, for soils of classes A3 and A4 of Twarakavi et al. (2010).

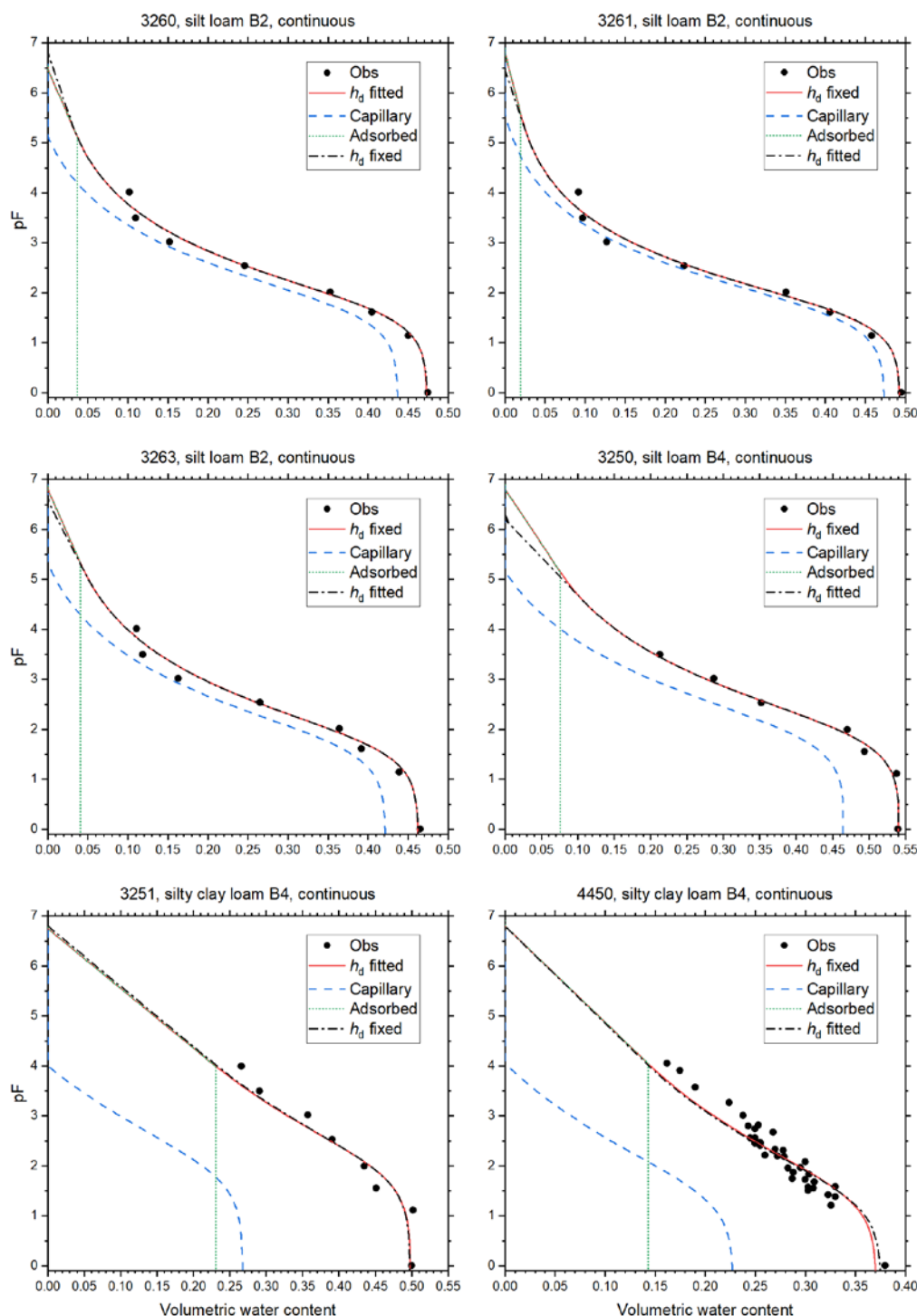


Figure 7: As Fig. 5, for soils of classes B2 and B4 of Twarakavi et al. (2010).

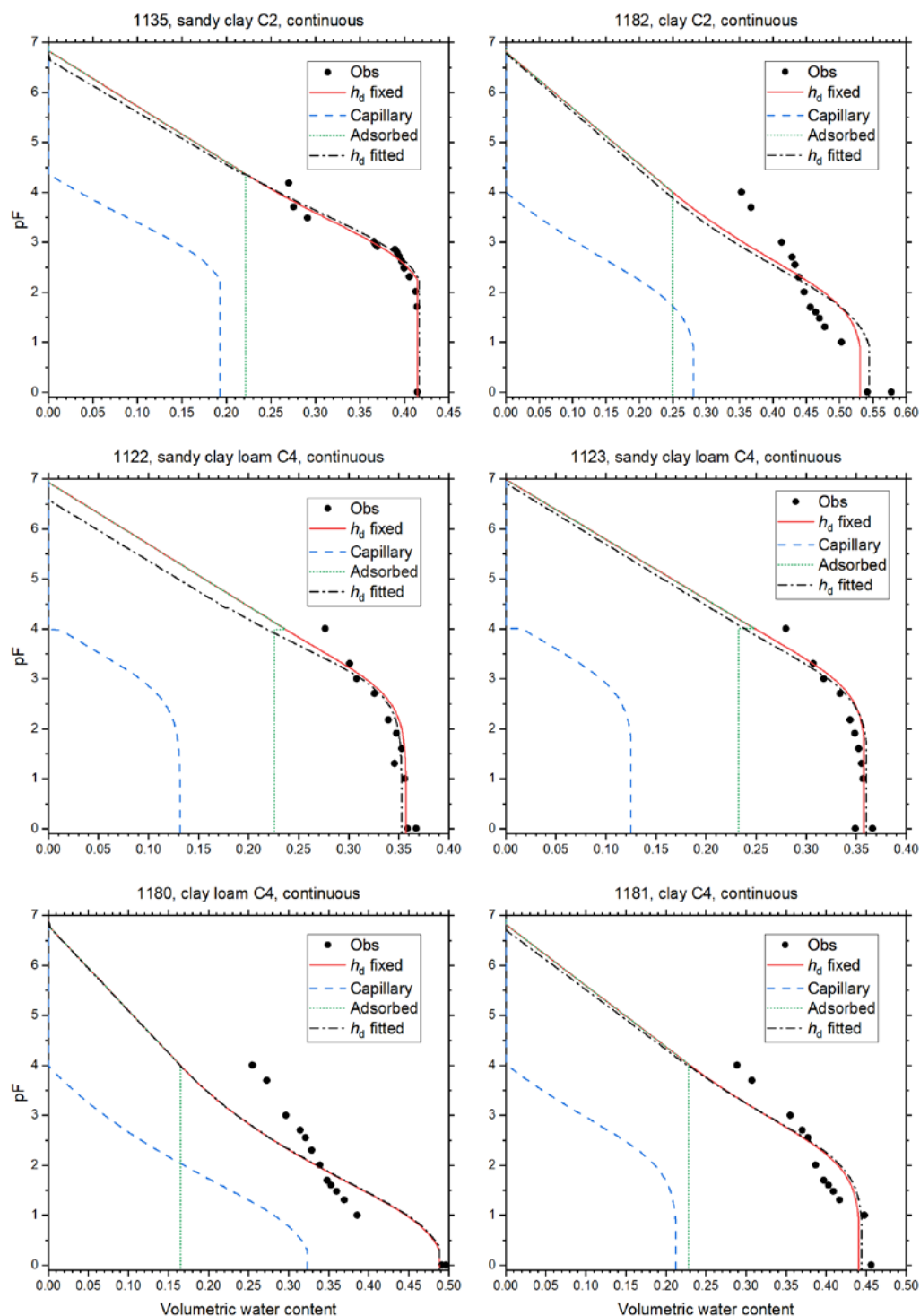


Figure 8: As Fig. 5, for soils of classes C2 and C4 of Twarakavi et al. (2010).



## 355 **Competing interests**

GdR is a member of the HESS Editorial Board. The peer-review process was guided by an independent editor, and the author has no other competing interests to declare.

## 360 **Data availability**

The UNSODA database with the soil data can be downloaded at <https://data.nal.usda.gov/dataset/unsoda-20-unsaturated-soil-hydraulic-database-database-and-program-indirect-methods-estimating-unsaturated-hydraulic-properties>. (National Agricultural Library, 2015)

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## **Code availability**

The Fortran code for fitting the SWRC parameters and post processing as well as its user manual are available from the Zenodo repository (de Rooij, 2022).

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