# Combining passive- and active-DTS measurements to locate and quantify groundwater discharge variability into a headwater stream

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**Abstract.** Exchanges between groundwater and surface water play a key role for ecosystem preservation, especially in headwater catchments where groundwater discharge into streams highly contributes to streamflow generation and maintenance. Despite several decades of research, investigating the spatial variability of groundwater discharge into streams still remains challenging mainly because groundwater/surface water interactions are controlled by multi-scale processes. In this context, we evaluated the potential of using FO-DTS (Fiber Optic Distributed Temperature Sensing) technology to locate and quantify groundwater discharge at high resolution. To do so, we propose to combine, for the first time, long-term passive-DTS measurements and active-DTS measurements by deploying FO cables in the streambed sediments of a first- and second-order stream in gaining conditions. The passive-DTS experiment provided eight-month monitoring of streambed temperature fluctuations along more than 530 m of cable, while the ~~punctual~~ active-DTS experiment, performed during few days, allowed a detailed and accurate investigation of groundwater discharge variability over a 60 m-length heated section. ~~Results show that L~~long-term passive-DTS measurements turn out to be an efficient method to detect and locate groundwater discharge along several hundreds of meters. The continuous eight-months monitoring allowed ~~and to investigate the temporal pattern~~ highlighting changes in the groundwater discharge dynamic in response to the hydrological dynamic of the headwater catchment.~~of exchanges over the annual hydrological cycle~~. However, the quantification of fluxes with this approach remains limited given the high uncertainties ~~associated to the~~ on estimates, due to uncertainties on thermal properties and boundary conditions.~~especially due to the assumptions made about thermal properties.~~ On the contrary, active-DTS measurements, which have seldom been performed in streambed sediments and never applied to quantify water fluxes, ~~never been in streambed sediments up to now,~~ allow estimating the spatial distribution of both thermal conductivities and the groundwater fluxes at high resolution all along the 60-m heated section of FO cable ~~with very low uncertainties all along the heated section of FO cable~~. The method allows describing the variability of streambed properties at an unprecedented scale and reveals the variability of groundwater inflows at small scale. In the end, this study shows the potential and the interest of the complementary use of passive- and active-DTS experiments to quantify groundwater discharge at different spatial and temporal scales. Thus, r~~R~~esults show that groundwater discharges are mainly concentrated in the upstream part of the watershed, where steepest slopes are observed, confirming the importance of the topography in

the stream generation in headwater catchments. However, t~~T~~hrough the high spatial resolution of measurements, it was also possible to highlight the presence of local and highly contributive groundwater inflows, probably driven by local ~~changes of hydraulic properties~~heterogeneities. ~~These results about groundwater discharge variability offer~~ The possibility to quantify groundwater discharge at high spatial resolution through active-DTS offers promising perspectives for the characterization of distributed responses times, but also for studying biogeochemical hotspots and hot moments.

## 1 Introduction

Understanding groundwater and stream water interactions as integral components of a stream catchment continuum is crucial for efficient development and management of water resources (Bencala, 1993; Brunke and Gonser, 1997; Sophocleous, 2002). Particularly essential for the preservation of groundwater dependent ecosystems and riparian habitats (Kalbus et al., 2006), these interactions play a major role on physical, geochemical and biological processes occurring in the stream or in the hyporheic zone (Frei et al., 2019; Jones and Mulholland, 2000). More specifically, these exchanges control water quality affecting river ecohydrology and hydrochemistry, particularly during dry periods when groundwater is the principal contribution to stream discharge (Brunke and Gonser, 1997). This is particularly true in headwater catchments where groundwater discharge highly contribute to streamflow generation (Winter, 2007). However, localizing and quantifying exchanges between groundwater and stream water is often difficult as these exchange are controlled by multi-scale processes and are therefore highly variable in time and in space (Brunke and Gonser, 1997; Fleckenstein et al., 2006; Flipo et al., 2014; Harvey and Bencala, 1993; Kalbus et al., 2009; Varli and Yilmaz, 2018; Woessner, 2000).

A wide range of methods exists to estimate water fluxes between stream and groundwater including solute tracer concentrations (Brandt et al., 2017; Liao et al., 2021), seepage meter measurements (Rosenberry et al., 2020) or the use of heat as a groundwater tracer (Anderson, 2005; Constantz, 2008), which is particularly efficient in identifying patterns of focused discharge. The approach relies on the detection of temperature anomalies observed at the sediment-water interface (Tyler et al., 2009; Sebok et al., 2013; Westhoff et al., 2011) or into the streambed (Krause et al., 2012; Lowry et al., 2007) when significant differences exist between groundwater and stream water temperatures. Then, the comparison of temperature variations monitored at different depths in the streambed provides information on groundwater discharge (Anderson, 2005; Constantz, 2008; Hatch et al., 2006; Keery et al., 2007; Lapham, 1989; Stallman, 1965; Webb et al., 2008; Winter et al., 1998). Indeed, the diurnal or seasonal water temperature variations propagates deeper for losing streams (downward conditions) than for gaining streams (upward conditions), since heat transfer is either attenuated or enhanced by groundwater discharge (Constantz, 2008; Goto et al., 2005). Thus, the use of Vertical Thermal Profiles (VTP) is widely applied for determining flow directions, quantifying groundwater discharge (Hatch et al., 2006; Lapham, 1989; Keery et al., 2007) and estimating hydraulic parameters (Constantz and Thomas, 1996). Nevertheless, only ~~punctual~~ point measurements of the stream-aquifer interactions are achievable with this approach. Considering the spatial variability and the complexity of flow

at the GW/stream interface, extensive information on spatial and temporal temperature patterns are required to gain a more complete understanding of flows at reach scale, and even more at watershed scale.

65       This was made possible by the development and the use of the Fiber Optic Distributed Temperature Sensing (FO-DTS) technology for environmental applications (Selker et al., 2006b, a; Shanafield et al., 2018; Tyler et al., 2009). FO-DTS provides continuous temperature data through space and time along fiber optic cables at high spatial resolution (Habel et al., 2009; SEAFOM, 2010; Ukil et al., 2012). By deploying FO cables at the bottom of the stream, the DTS technology allows temperature monitoring of the longitudinal linear stream/sediments interface allowing detecting thermal anomalies induced

70    by groundwater discharge into the stream (Briggs et al., 2012; Gilmore et al., 2019; Koruk et al., 2020; Moridnejad et al., 2020; Rosenberry et al., 2016; Selker et al., 2006b, a; Westhoff et al., 2007, 2011). This approach was also used to study seasonal and temporal fluctuations of groundwater discharge into streams (Matheswaran et al., 2014; Slater et al., 2010) and into a lake (Sebok et al., 2013). Energy balance models have been efficiently applied to interpret passive-DTS measurements and quantify groundwater/stream water exchanges (Selker et al., 2006b; Westhoff et al., 2011). However their use remains

75    limited because it requires monitoring significant temperature changes over time, limiting the application of the method to large groundwater inflows or small headwater streams. To overcome such limitations, some studies proposed to detect thermal anomalies in the streambed by burying the FO cable into the streambed sediments in the hyporheic zone (Krause et al., 2012; Le Lay et al., 2019b; Lowry et al., 2007), to improve the possibility of localizing groundwater inflows.

        Despite that, the quantification of fluxes from passive-DTS measurements remains challenging. In theory, the
80    implementation of three FO cables buried at different depths, as proposed by Mamer and Lowry (2013), would be ideal to measure the attenuation of the stream temperature variations into the sediments in order to get high-resolution fluxes estimates. Unfortunately, such approach is technically very difficult to apply in the field. Considering this difficulty, Le Lay et al. (2019a) proposed coupling FO-DTS data collected along a single fiber-optic cable at a given depth with ~~punctual~~ point temperature measurements from thermal lances. In the approach, it is assumed that temperature boundary conditions can be

85    characterized from the temperature measurements collected with the thermal lances and extrapolated all along the stream to be combined with FO-DTS measured at a given depth. Moreover, the question of sediments thermal properties and their spatial variability remained unexplored, even though thermal conductivity highly impacts flux estimates (Sebok and Müller, 2019). Based on these assumptions, they showed the temporal variability of exchanges associated to the annual hydrological cycle and the possibility of estimating diffuse groundwater inflows (Le Lay et al., 2019a).

90       Alternatively, active-DTS methods, consisting in heating the FO cable, have been recently developed to improve the capabilities of FO-DTS methods for estimating fluxes in different environmental conditions (Bense et al., 2016; Simon et al., 2021). In particular, it was demonstrated that the difference of temperature between an electrically heated and a non-heated FO cable is directly dependent on water fluxes, offering the possibility to estimate fluxes (Bense et al., 2016; Read et al., 2014; Sayde et al., 2015). Thus, active-DTS methods have been used to estimate wind speed in the low atmosphere

95    (Lapo et al., 2020; Sayde et al., 2015; van Ramshorst et al., 2020), in dam monitoring (Ghafoori et al., 2020; Perzlmaier et al., 2004; Su et al., 2017), for groundwater fluxes measurements in open (Banks et al., 2014; Klepikova et al., 2018; Read et

al., 2014, 2015) and sealed boreholes (Munn et al., 2020; Selker and Selker, 2018) or else in direct contact within sedimentary aquifers (del Val et al., 2021; des Tombe et al., 2019). Despite promising developments, active-DTS methods have been seldom used in hydrology to estimate groundwater/surface water interactions. Kurth et al. (2015) coupled passive- and active-DTS measurements and highlighted areas with lower and higher flow rates over the cable, but the quantification of fluxes remained unexplored. Briggs et al. (2016) developed a novel probe to quantify vertical fluxes at high resolution using active-DTS measurements, but the probe only permits a local-scale characterization of the stream-aquifer dynamic.

In this study, we propose to use for the first time active-DTS measurements to quantify groundwater discharge in the stream of a headwater catchment. The application of active-DTS methods in such context is particularly promising since the interpretation of active-DTS measurements in saturated porous media provides estimates of both sediments thermal conductivities and groundwater fluxes over a large range and with an excellent accuracy (Simon et al., 2021). This method should allow quantifying groundwater discharge and characterizing the streambed thermal properties at an ~~unprecedent~~unprecedented spatial scale. In complement of active-DTS measurements, which were limited in space and time, a ~~long term~~ eight-months passive-DTS experiment was conducted at the catchment scale in order to infer the temporal and spatial patterns of groundwater discharges over the investigating period ~~location and dynamics of groundwater discharge~~. Therefore, this study also investigates how these two experiments could be compared and combined to characterize both the spatial and the temporal dynamics of groundwater discharge. To do so, FO cables were deployed in the streambed sediments of a headwater stream within a small agricultural watershed. In the following, we first present the headwater catchment and the experimental setup before presenting the methods used to interpret both passive- and active-DTS measurements. Fluxes estimates obtained with both passive- and active-DTS measurements are then compared and the advantages and limitations of each method are finally discussed.

## 2 Materiel and methods

### 2.1 The experimental setup on the Kerrien watershed

#### 2.1.1 The Kerrien watershed

The experiment has been conducted in the Kerrien watershed located in South-western Brittany (4°7'24.87''O:47°56'26.97''N). It is part of the AgrHys Environmental Research Observatory, whose principal aim is to understand and characterize transit times in small agricultural catchments (https://www6.inra.fr/ore_agrhys). The site is a part of the French network of critical zone observatories (Gaillardet et al., 2018) and supports extensive hydrological and geochemical research. This site was selected because it presents the advantage of readily installed equipment and instruments (Fovet et al., 2018).

As shown in Fig. 1, the watershed is a headwater watershed with a second-order stream, subdivided in three first-order sub-watersheds namely the Kerrien, the Kerbernez and the Gerveur sub-watersheds. The Kerrien sub-watershed is a small agricultural watershed (9.5 ha) with steeper slopes in the upper parts (14% slopes) than in the bottom lands (5%

slopes), characterized by a large wetland (Ruiz et al., 2002). As pointed out in Fig. 1, downstream the wetland, the fields

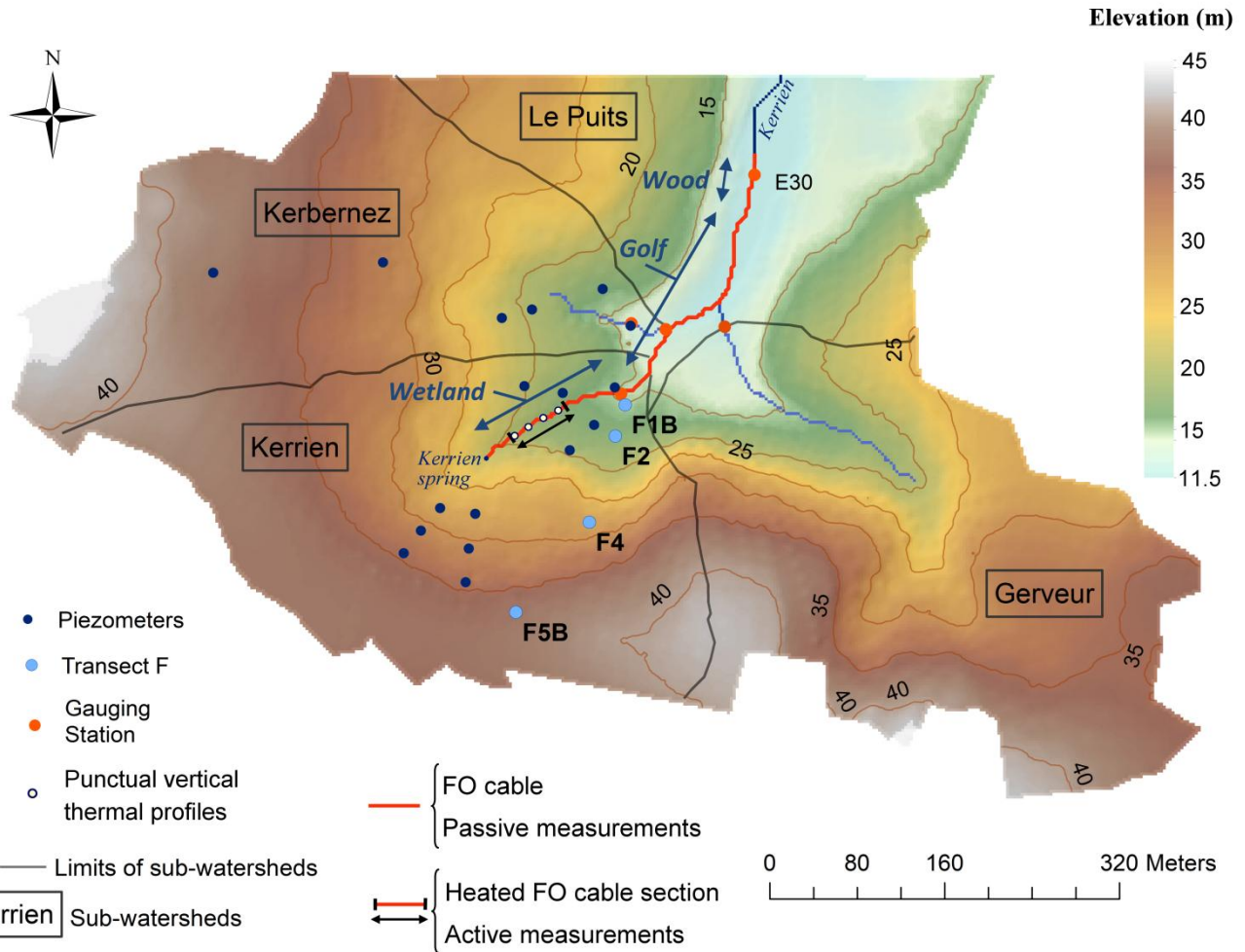
130 were converted into a golf course. In this man-made environment, the stream has been completely restored and dammed to facilitate maintenance. Drainage pipes contribute to drain precipitation from the watershed area directly into the stream, limiting the potential groundwater recharge by draining precipitation from the watershed area into the stream. Further downstream, the stream reaches a natural wood plain.

135

**Figure 1: Description of the watershed with the location of piezometers, gauging station and fiber optic cables.**

### 2.1.2 Hydrological dynamics of the study site

The Kerrien watershed has been particularly studied and instrumented for estimating transit times in a small agricultural watershed (Fovet et al., 2015a; Martin, 2003), as shown in Fig. 1. For this study, we are using the data from the

140 piezometer transfect F (Fig. 1) including the hillslope piezometer F5b (20 m depth) and the mid-slope piezometer F4 (15 m

depth) as markers for the deep groundwater storage dynamics and the riparian piezometers F2 (2 m depth) and F1b (5 m depth) as markers for the riparian groundwater storage dynamics. The gauging station E30 provides stream flow rate.

Runoff is insignificant, so that most of effective precipitation is infiltrating in this headwater watershed. The annual rainfall (1114 mm on average) is well-distributed over the year but recharge mainly occurs in autumn and winter. Therefore, the contribution of groundwater to the stream flow reaches 80-90% (Fovet et al., 2015b; Martin et al., 2006; Ruiz et al., 2002) with the stream discharge during high water periods being highly correlated with hillslope head gradient (Martin, 2003). As shown in Fig. 2a, piezometric levels show clear seasonal fluctuations with high levels during winter and spring and low levels during summer and autumn. The hydraulic gradient between the aquifer and the stream as well as the evolution of the stream discharge suggest that groundwater discharge into the stream should be particularly expected during the high water level period (From December to June).

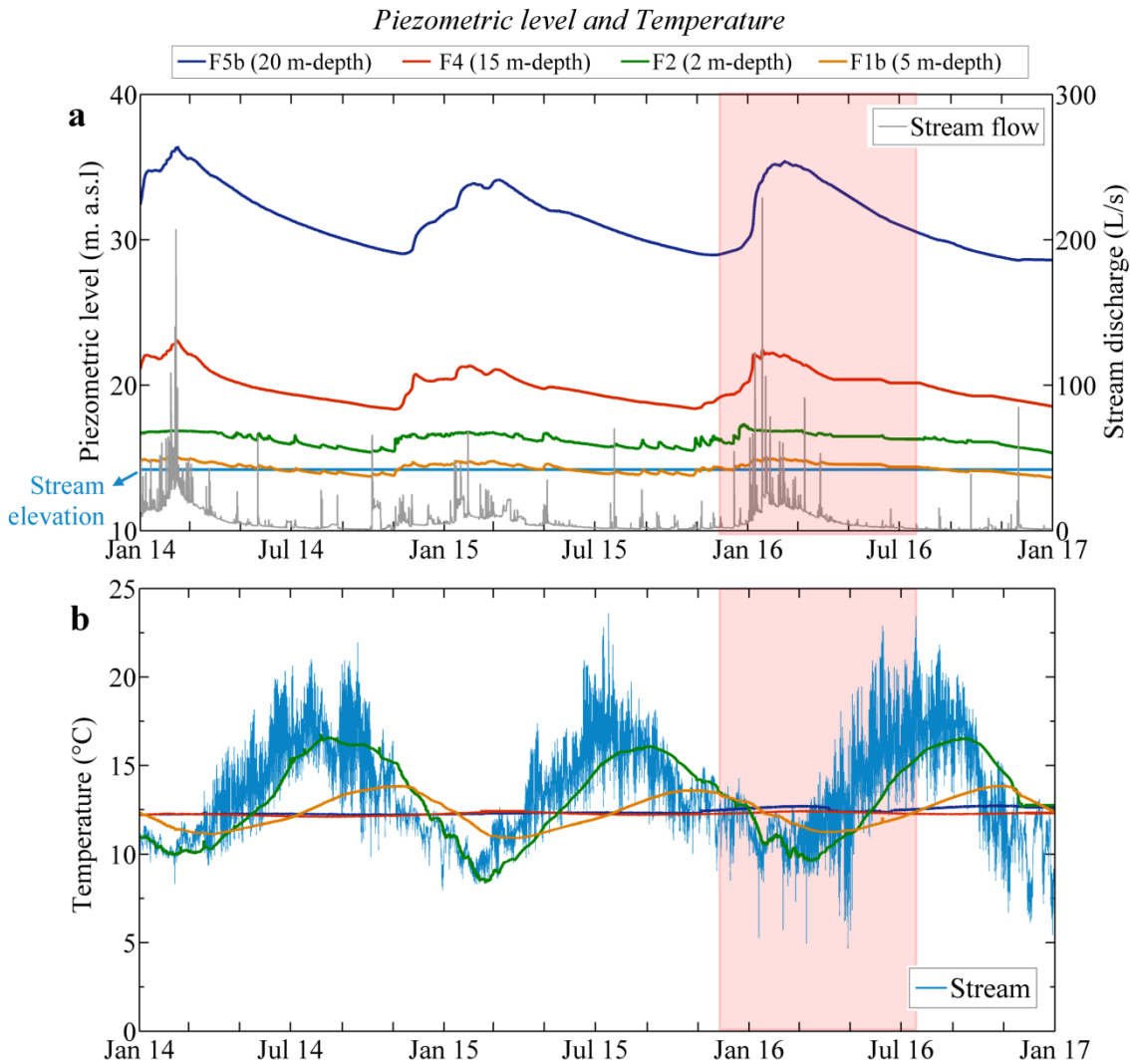



**Figure 2: a. Changes in stream flow and in piezometric levels along the transect F over three years. b. Stream and groundwater temperature fluctuations over time along the transect F. The red-colored area corresponds to the period of passive-DTS measurements, conducted from December 2015 to the July 15ᵗʰ, 2016.**

155     Figure 2b shows temperature fluctuations in the stream and in piezometers over a time period from July 2013 to May 2017. While the groundwater temperature is almost constant in the upslope domain (piezometers F5b and F4), temperature variations recorded in the stream and in the downslope domain (F2 and F1b) show larger variations following daily and seasonal temperature variations. It can easily be shown that temperature variations recorded in F2 and F1b result from the diffusion of air temperature variations through the water columns of piezometers. The detection in the stream of

160     thermal anomalies induced by groundwater discharge requires a significant contrast of temperature between stream and groundwater as well as a significant groundwater discharge compared to the stream flow. Here, considering the relatively small difference of temperature between groundwater and stream water and in order to detect potential diffusive inflows, the choice was made to bury the FO cable within the sediments, which should facilitate the detection of potential temperature anomalies as marker of groundwater discharge (Krause et al., 2012; Le Lay et al., 2019b; Lowry et al., 2007). Otherwise,

165     active-DTS measurements should highlight advective heat transfer, controlled by groundwater discharge.

## 2.2 Passive-DTS measurements and data interpretation

### 2.2.1 FO cable deployment and data acquisition

    To investigate the temporal and spatial dynamics of groundwater discharge, a FO cable has been deployed in the streambed sediments in the southern part of the study site, as shown in Fig. 1. Streambed temperature variations were

170     recorded along this cable using the DTS technology from December 2015 to July 2016. The FO cable has been deployed downstream from the Kerrien spring. In total, more than 530 m length of BruSens FO cable has been buried directly into the streambed. Due to some obstacles (coarse gravels, cobbles, gauging stations, etc.), it was not possible to bury the FO cable in few places. Everywhere else, the average burial depth was estimated to be 8 cm. The first 165 meters of the FO cable have been deployed in the Kerrien sub-watershed, where the stream is surrounded by a wetland. The streambed is formed by sand

175     and sludge whose thickness is low but large enough to bury properly the cable. Then, besides a harder substrate, the FO cable was deployed in the golf area. In few local places, the burying was not possible and FO cable was set on the streambed. The last 70 meters of the FO cable have been deployed in a wood plain, a natural environment, where a deeper sandy riverbed facilitates cable burying. As highlighted in Fig. 2a, the eight-month experiment insured the monitoring of streambed temperature during both high and low water tables. The highest levels were recorded from January to mid-April, period over

180     which the wetland is saturated up to the surface.

    The FO cable has been connected to a FO-DTS control unit, a Silixa XT-DTS instrument (5 km range). The DTS unit was configured in double-ended configuration (van de Giesen et al., 2012) to collect data at 25 cm and 10 minutes sampling interval. Two calibration baths (one at the ambient temperature and a fridge), as well as PT100 probes (0.1°C) and RBR SoloT probes (0.002°C accuracy) were used to calibrate the data. To assess the accuracy of temperature measurements,

a RBR SoloT probe was set up at the gauging station E30 located at the entrance of the wood. Comparison between DTS measurements and RBR SoloT probes validated the temperature measurements, with a relative uncertainty of measurements (standard error) estimated at 0.05°C and absolute uncertainty of measurement that can reach at maximum 0.2°C depending on the period of measurement.

In complement, 4 vertical temperature profiles (VTP) were installed in the streambed in the wetland area by deploying temperature sensors (HOBO U12-015-02 sensors - ±0.25°C precision) at 12.5 and 22 cm-depth in the streambed sediments. The position of these sensors in the stream is shown in Fig. 1 and was chosen at locations where groundwater discharge has been observed using preliminary results obtained from FO-DTS monitoring. From upstream to downstream, the VTP are numbered from 1 to 4. For each location, the evolution of temperature was recorded from April 07th, 2016 to May 03rd, 2017 using HOBO U12-015-02 sensors (±0.25°C precision). These VTP will be used to quantify local groundwater discharge and results will be compared with estimates from FO-DTS measurements.

### 2.2.2 Data interpretation

Groundwater inflows can be detected by localizing temperature anomalies. Those can be easily identified by plotting the evolution of the temperature over time and space, especially for long time series. Thermal anomalies can also be identified using an analysis of the standard deviation (SD) of temperature for a given period (Sebok et al., 2015), since the calculation of the standard deviation provides insights about amplitudes of temperature variations. In case of groundwater discharge, the value of the SD of streambed temperature is expected to be much lower than the value of the SD of the stream temperature. Therefore, relative variations of fluxes along the cable could be determined from relative variations of SD.

Then, to quantify vertical fluxes, we use the FLUX-BOT model, a code proposed by Munz and Schmidt (2017), using a numerical heat transport model to solve the 1D heat transport equation (Carslaw and Jaeger, 1959; Domenico and Schwartz, 1998). This 1D model allows calculating the specific discharge in the z direction (i.e. the vertical Darcy flux) by inversing measured time series observed at least at three different depths. Temperature variations are simulated according to the optimized fluxes. The quality criteria calculated between the simulated temperatures and the measured one (NSE, R² and RMSE) allow discussing the quality of flux estimates. Thus, the model estimates the direction and the intensity of the flow and may highlight the temporal variability of exchanges.

To apply the model, the stream temperature and the groundwater temperature were chosen as upper and lower boundary conditions respectively. The stream temperature was measured for the wetland area at the Kerrien spring with a temperature sensor and at the gauging station E30 (RBR SoloT) for the wood plain area. The temperature signal recorded at 15-m depth in the piezometer F4 (Fig. 2b) was used to set the groundwater temperature. The FLUX-BOT model was first used for interpreting the temperature measurements of the four VTP installed in the streambed. Considering the upper and lower boundary conditions previously defined, the numerical model reproduces the temperature evolution collected at 12.5- and 22-cm depth and provides an estimate of vertical fluxes for each profile. Details about the interpretation of VTP using the FLUX-BOT model are provided as supplement (Fig. S1 and S2). The results are compared in the section 3.3 with

estimated fluxes from passive- and active-DTS measurements. Identically, the FLUX-BOT model is used to reproduce and interpret passive-DTS measurements collected at various spots along the cable. A loop was added in the initial code allowing the interpretation of data collected for each measurement point. For both applications, the vertical mesh size of the model was set at 0.01 m, as recommended by Munz and Schmidt (2017). Concerning the thermal properties of the saturated sediments, the volumetric heat capacity was set at $3x10^6$ J.m$^{-3}$.K$^{-1}$. The streambed sediments being composed of saturated clay, silt, sand and gravel, the thermal conductivity may typically range between 0.9 and 4 W.m$^{-1}$.K$^{-1}$ (Stauffer et al., 2013). Thus, considering the importance of the sediment thermal conductivity on groundwater fluxes estimates (Sebok and Müller, 2019), the model was applied for 3 values of thermal conductivity (1, 2.5 and 4 W.m$^{-1}$.K$^{-1}$).

**2.3 Active-DTS measurements**

Active-DTS measurements were conducted in April 2016 concurrently with passive-DTS measurements by deploying an additional FO cable within the streambed in the wetland, as shown in Fig. 1. While the active-DTS experiment was conducted, passive-DTS measurements had already been collected for three months, which allowed highlighting clear and significant temperature anomalies along the cable deployed in the wetland area (See results section below). Assuming that these temperature anomalies could be associated to potential groundwater exfiltration zones, the choice was made to conduct the active-DTS experiment in this area.

Figure 3 presents the experimental setup of the active-experiment. A FO cable is electrically heated through its steel armouring and the elevation in temperature, associated to the heat injection, is continuously monitored all along the heated section using the FO inside the cable. Without any flow, heat transfers occur through the porous media only by conduction and a gradual and continuous increase of temperature is therefore expected (Simon et al., 2021). If water flows through the porous medium, advection partly controls the thermal response by dissipating a part of the heat produced by the heat source. The higher the water flow, the lower should be the temperature increase (Simon et al., 2021). Contrary to passive-DTS measurements, one of a main advantage of the method is the possibility of investigating groundwater fluxes in any conditions, independently of natural temperature gradients. However, similarly to most thermal-based methods (Constantz, 2008), it is assumed that groundwater flows are perpendicular to FO cables (Simon et al., 2021).

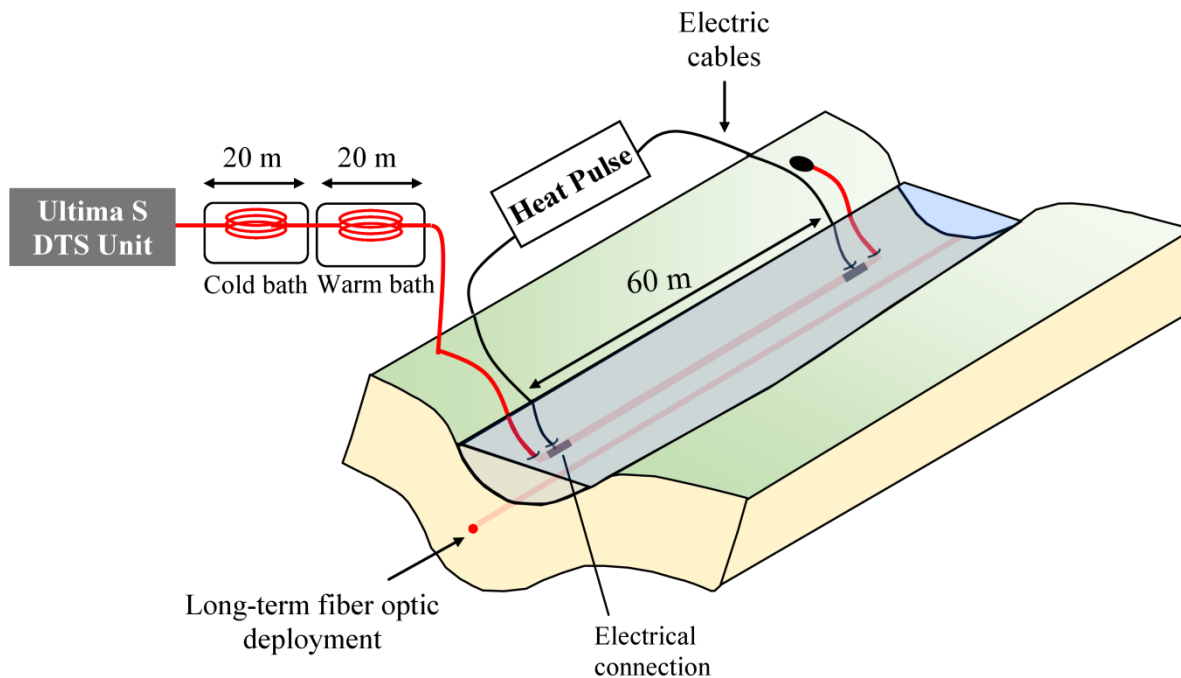



**Figure 3: Experimental setup of the active experiment: a 60 meter-section of a heatable cable has been electrically isolated, buried in the sediments and then heated by connecting to a power controller.**

245     For the active-DTS experiment, 150 meters of BruSens FO cable have been connected to a FO-DTS control unit, a Silixa Ultima S instrument. The unit was configured in double-ended configuration to collect data at 12.5 cm sampling and 60 seconds time interval. The effective spatial resolution of DTS measurements with this unit was estimated varying between 66 and 90 cm following the methodology proposed in Simon et al. (2020). The calibration process applied was almost similar to the one applied for calibrating passive-DTS measurements. The only difference is that a warm calibration bath was

250     used as reference section during the active-DTS experiment while a bath at ambient temperature was used for the passive-DTS experiment. To do so, heating resistors were set in the bath and air pumps were used to homogenize the temperature within. Considering the important temperature rise expected during the active experiment, using a warmed calibration bath is essential because the bath temperatures must preferably bracket the full range of temperatures expected to occur along the cable (van de Giesen et al., 2012).

255     Note that, while passive-DTS measurements have been monitored all along the stream, a much shorter section of FO cable has been used for the active-DTS experiment, due to the power limitations (3300 W) of the generator used for power supply. A 60-meters section of the 150 m FO cable has been buried in the streambed in parallel with the FO cable previously installed for the passive experiment. As the heating experiment induces a very localized thermal perturbation within the streambed, the non-heated cable was not affected by the heat injection. Thus, natural streambed temperature

260     fluctuations were monitored during the experiment using the non-heated cable. It should be noted that, during the FO cable

deployment in the streambed, local heterogeneities led to the impossibility to deploy the whole FO heating section in the streambed. Thanks to cable numbering, these non-buried sections were accurately located. For buried sections, the burial depth was measured in situ and estimated to be around 8 to 10 cm. This 60-m section has been electrically isolated and heated using a power controller (provided by CTEMP, https://ctemps.org/) supplying a constant and uniform heating rate

265 power of 35 $W.m^{-1}$ along the heated FO cable. The heated cable has been energized continuously during 4 hours and the recovery was also monitored for an additional 3 hours after turning off the power controller.

Before interpreting the data, data were processed to remove the measurement points corresponding to sections where the cable was not buried in the streambed but laid in the bottom of the stream. These sections were precisely marked during the cable installation. Moreover, since the temperature increase is mainly controlled by convection in the stream,

270 thermal responses measured during the heating phase in non-buried sections of cable are different from thermal responses observed in buried section and are easily identifiable with temperature rises reaching steady-state in one or two minutes (Read et al., 2014). Then, the data processing method developed in Simon et al. (2020) which consists in calculating the derivative of the temperature with respect to distance was applied. It allows highlighting areas where the temperature changes occur at a scale smaller than the spatial resolution of measurements, which leads to identify measurements that are

275 representative of the effective temperature.

Finally, among all the section used for active-DTS measurements, 172 measurements points are thought to be significant. Note that the raw data of active-DTS measurements, the data processing (sorting and quality check) and the definition of significant points are presented in detail in the supplement material. The data were further interpreted using the ADTS Toolbox proposed by Simon and Bour (~~Submitted~~2022) for automatically interpreting active-DTS measurements. The

280 ADTS Toolbox contains several MATLAB codes that allow estimating the thermal conductivities and the groundwater fluxes (specific discharge) and their respective spatial distribution all along the heated section. The method is based on an analytical approach proposed and validated by Simon et al. (2021), that consists in defining, for each measurement point along the heated section, the optimized values of thermal conductivity and flux that allow reproducing at best the associated temperature increase measured over the heating period. The use of the ADTS toolbox also provides an estimate of the

285 associated uncertainties (Simon and Bour, ~~Submitted~~2022).

## 3 Results

In the following, we first focus on the interpretation of passive-DTS measurements with the aim of locating groundwater discharges and characterizing its temporal dynamics. Then, we present and analyse results of the ~~punctual~~ active-DTS experiment, performed during few days. Both results are further compared.

## 3.1 Passive-DTS measurements

### 3.1.1 Spatial variability of temperature signals

Figure 4a synthesizes the results of the passive-DTS experiment and shows temperature signals monitored all along the FO cable deployed in the streambed sediments. The x-axis indicates the distance between the Kerrien spring (located at 0 m) and each measurement point in the streambed. Temperature variations are presented from December 2015 to July 2016 (y-axis). In June and July, despite very low flows, the stream never dried up. Two different behaviours are highlighted in the figure. On the one hand, vertical yellow lines can be observed near the Kerrien Spring in the first 150 meters of cable. These lines emphasize that the temperature recorded in these areas is relatively constant over time (few temperature variations are recorded). On the other hand, away from the spring, beyond 300 m, clear and large differences in temperature are observed between colder periods (from December to mid-April) and warmer periods (from mid-April to July).

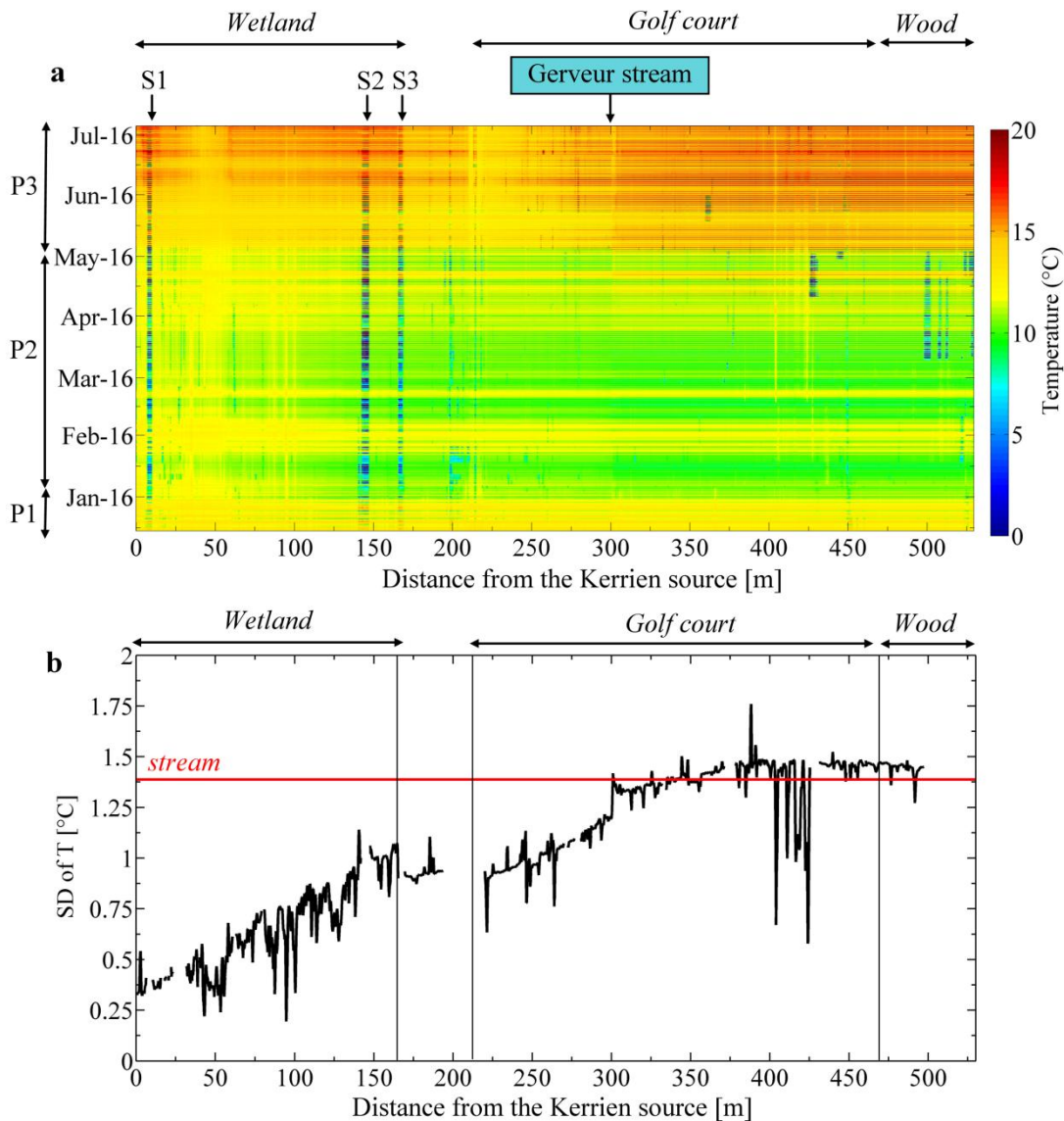



**Figure 4: a. Long-term monitoring of streambed temperature along the river using DTS. Sections S1, S2 and S3 match with spots where the cable lies on the bank because of obstacles in the stream (gauging stations). Temporary thermal anomalies located for instance in 425 m and around 500 m correspond to air-exposed periods during which the cable was not held at the sediment/water interface. b. Standard Deviation (SD) of the temperature calculated over the experiment duration for each measurement point along the FO cable. Sections where the cable was outside the stream or punctually unburied were removed. The red line represents the SD of the stream temperature (1.38°C) measured at the gauging station E30.**

To highlight the spatial variability of the temperature signal, the Standard Deviation (SD) of temperature was calculated for each measurement point over the whole duration of the experiment as presented in Fig. 4b. The value of the SD of stream temperature ($\approx 1.375$ °C) directly reflects the amplitude of daily temperature fluctuations. Concerning the SD of streambed temperature, its value is relatively stable and very low (around 0.37 °C) in the first 50-m of measurements, near

the spring. Then, it progressively increases from upstream to downstream and stabilizes around the value of the SD of the stream temperature at around 300 meters (in the middle of the golf area).

The lowest SD values are recorded in the upstream wetland (d < 160 m in Fig. 4b). In this area, as illustrated in Fig. 5a by the red curve (94.56 m, σ = 0.2 °C), the temperature is relatively stable over time (around 12.5°C) and the daily stream temperature fluctuations are widely attenuated (the SD varies between 0.19 and 0.93°C while the SD of the stream temperature is 1.38°C). However, significant differences are observed between temperature measurements from upstream to downstream, as highlighted by the progressive increase of SD measured from the spring to 160 m. This increase reflects the increase of the amplitudes of daily temperature fluctuations collected from upstream (orange line in Fig. 5b, σ = 0.36 °C) to downstream (grey line in Fig. 5b, σ = 0.95 °C). In addition, the profile of SD (Fig. 4b) also shows isolated "spikes" associated with very low SD values, in agreement with the yellow lines observed in Fig. 4a. These spikes can be associated with spots where the amplitude of temperature is low all over the period of measurements, as illustrated by blue curve in Fig. 5b (53.38 m), where the value of the SD is equal to 0.24 °C. As we shall see in the next sections, the relative temperature stability suggests that these spikes or "hotspots" may be associated to local groundwater discharges.

Further downstream (from 220 m up to 300 m in the first part of the golf area), while the value of the SD progressively increases (Fig. 4b), higher amplitudes of daily temperature variations are monitored as illustrated in the Fig. 5a by the blue curve (227.5 m, σ = 0.93 °C). In this area, SDs values are lower than the one calculated in the stream (1.3 °C, Fig. 4b) meaning that the daily temperature fluctuations are slightly attenuated. Once again, the progressive increase of the value of the SD highlights differences in temperature amplitude (the further, the higher the amplitudes of temperature). Finally, in the second part of the golf area and in the wood (starting from approximately 300 m), SDs values tend towards the value of the SD of the stream (1.3 °C, Fig. 4b). The associated streambed temperature variations are almost identical to the stream variations, as illustrated in the Fig. 5a by the yellow line (357.91 m, σ = 1.42 °C). Note here that the SD evolution shows a well-marked step at 300 m from 1.2 to 1.4°C, exactly at the confluence between the Kerrien and the Gerveur streams (see Fig. 1). Moreover, very isolated decreases of SDs can be observed between 402 and 425 m, where significant thermal anomalies are monitored from mid-February to mid-April.

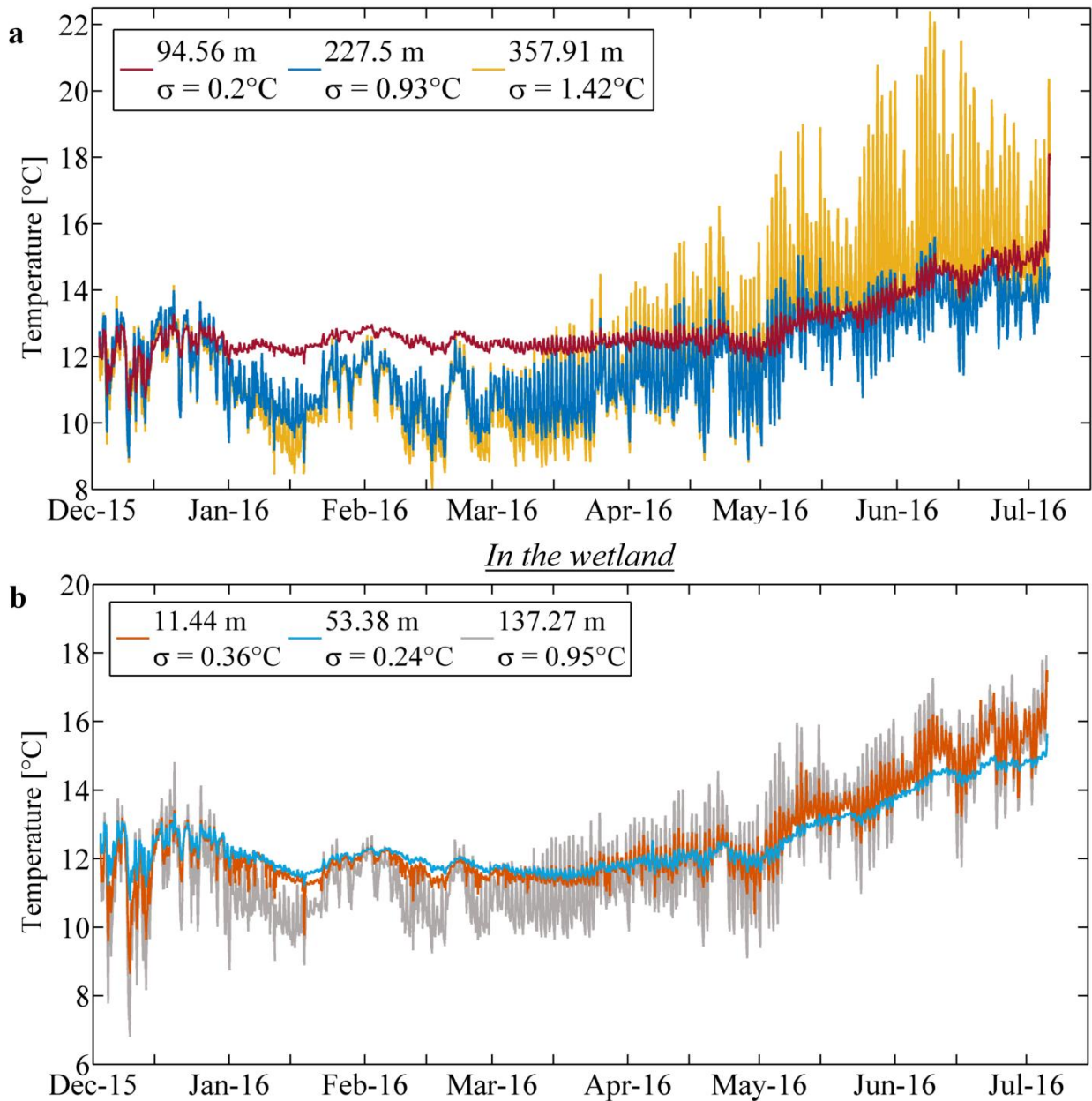



**Figure 5: a. Examples of streambed temperature variations measured with the FO-DTS a. at 94.56 m, 227.5 m and 357.91 m from upstream with respective SD values equals to 0.2 °C, 0.93 °C and 1.42 °C; b. in the wetland area at 11.44 m, 53.38 m and 137.27 m from upstream with respective SD values equals to 0.36 °C, 0.24 °C and 0.95 °C.**

Streambed temperature measurements clearly show a general trend with an increase of the amplitudes of temperature variations measured from upstream (the spring) to downstream, up to around 300 m. In the first 300 meters,

temperature fluctuations appear attenuated compared to the daily temperature fluctuations and the streambed temperature variations measured more downstream (beyond 300 m). Thus, lower temperature amplitude variations suggest groundwater inflows, especially for the measurement points where the lowest values of SD are recorded (minimal spikes of SD digressing from the general trend, as illustrated by the blue line in Fig. 5b). Indeed, for these "hotspots", thermal anomalies are clearly recorded and the temperature is relatively stable over time according to the stable groundwater temperature (around 12.5-13°C). The general increase of SD from the spring up to 300 m may be associated to a global decrease of groundwater inflows from upstream to downstream in the first 300 meters of the watershed. Higher and very localized inflows would be located in spots where the value of the SD is clearly lower than the general trend. Nevertheless, the gradual increase of the SD could also be alternatively explained by the fact that the stream water temperature, equal to the groundwater temperature at the spring, may progressively equilibrate with the air temperature when travelling along the stream.

To summarize, hotspots associated to minimal spikes of SD are certainly associated to local groundwater discharges, but the general evolution of temperature SD may be due to different factors.

### 3.1.2 Quantifying groundwater/ stream water exchanges

To go further in the interpretation of streambed temperature variations, the FLUX-BOT model was applied for each measurement point. A detailed example of the application of the FLUX-BOT model on a single measurement point (d = 5.08 m) including the quality criteria associated to the fluxes estimates is presented in Fig. S3. Although the model was applied for each measurement point, simulated temperature variations are consistent only with DTS measurements located in the first 150 meters of the temperature profile (SD < 1°C) with NSEs > 0.74, $R^2$ > 0.85 and RMSEs < 0.9°C. Beyond 150 m, the quality of the results considerably decreases with NSEs < 0.6, $R^2$ < 0.65 and RMSEs > 1.8°C. Thus, the uncertainties on fluxes estimates are too large in this lower part of the watershed (for d>150 m) to estimate groundwater discharge. Consequently, the model is found not applicable to interpret temperature measurements and results are not provided here.

Figure 6 shows the results of the application of the FLUX-BOT model on passive-DTS measurements collected along the cable deployed in streambed sediments in the wetland area, for d < 150m, where the model is applicable. The model predicts negative values of fluxes all along the interpreted section, indicating upward water flow, which strengthens the assumption of groundwater discharge into stream. However, as shown in Fig. 6b, groundwater fluxes estimates are strongly dependent on the value of thermal conductivity of the sediments used in the model. By varying the thermal conductivity from 1 $W.m^{-1}.K^{-1}$ (blue line) to 4 $W.m^{-1}.K^{-1}$ (green line), the estimated discharge is around 4 times higher. For instance, at d = 75 m, the mean flux is estimated $-3.43 \times 10^{-6}$ $m.s^{-1}$ for $\lambda$=1 $W.m^{-1}.K^{-1}$ against $-1.48 \times 10^{-5}$ $m.s^{-1}$ for $\lambda$ = 4 $W.m^{-1}.K^{-1}$. Note however that the results are more sensitive to the value of the thermal conductivity when groundwater inflows are higher (see Fig. S3 for more details).

Regardless of uncertainties, the model also predicts a general decrease of groundwater discharge from upstream to downstream. Higher groundwater inflows are estimated upstream, at the head of the catchment and close to the spring (Fig. 6b). The inflows are estimated twice higher near the spring than downstream. Hence, assuming a thermal conductivity of the

sediments $\lambda = 2.5$ W.m$^{-1}$.K$^{-1}$ (orange line in Fig. 6b), the mean flux is estimated $-1.24 \times 10^{-5}$ m.s$^{-1}$ near the spring (d = 0 m) while it only reaches $-6.55 \times 10^{-6}$ m.s$^{-1}$ for d = 150 m. The comparison with the SD profile (Fig. 6a) tends to confirm the correlation between the value of the SD of streambed temperature and the importance of groundwater discharge. Results also suggest that local spikes of SD (at 95 or 100 m for instance) can be associated to preferential pathways, where groundwater discharge is locally estimated four times higher than elsewhere.

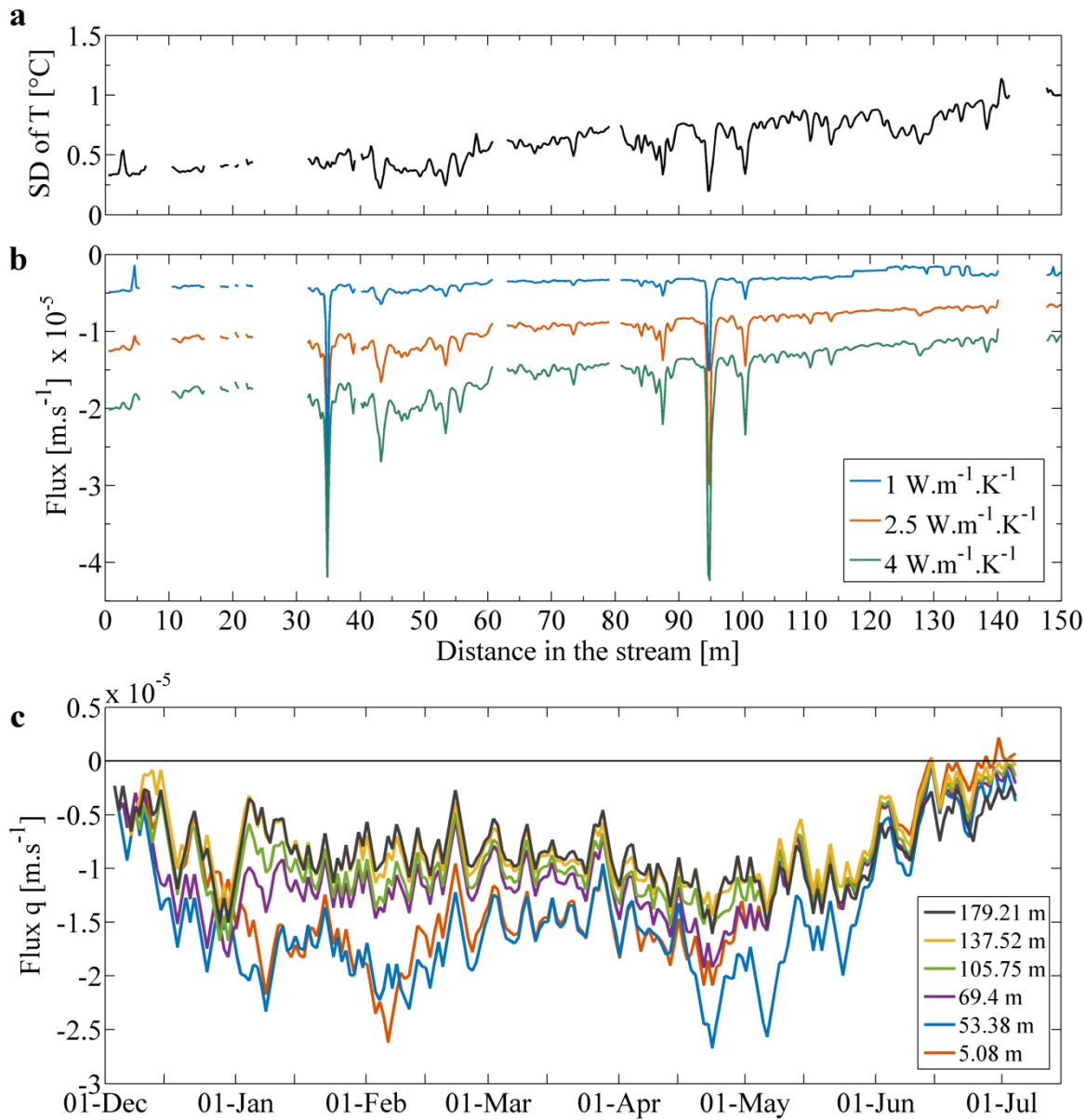
Finally, Figure 6c shows the evolution in time of groundwater discharges estimated for six different measurement points, assuming thermal conductivity $\lambda = 2.5$ W.m$^{-1}$.K$^{-1}$. The variability of fluxes is greater from January to May with groundwater inflows varying between $5 \times 10^{-6}$ and $2.5 \times 10^{-5}$ m.s$^{-1}$. Lower groundwater inflows are detected during the first month of the experiment ($<7.5 \times 10^{-6}$ m.s$^{-1}$) and at the end of the experiment ($<6 \times 10^{-6}$ m.s$^{-1}$), which seems consistent with stream gauging evolution. The same temporal dynamic is observed for all data collected in the wetland area.

385

**Figure 6: a. Profile of SD of the streambed temperature calculated over the experiment duration for each measurement point located along the FO cable and deployed in the wetland area; b. Profiles of mean fluxes estimated over the experiment duration using the FLUX-BOT model from DTS measurements collected in streambed sediments in the wetland area considering 3 values of thermal conductivity (Negative values indicate upward water flux); c. Temporal evolution of the estimated flow considering**

390  **λ=2.5 W.m⁻¹.K⁻¹.**

### 3.2 Active-DTS measurements

### 3.2.1 Data interpretation

As explained in section 2.3, some measurements points were excluded from the analysis either because the heated FO cable could not have been correctly buried or because temperature measurements were not representative of the effective temperature signal. The data interpretation was thus focused on the selected significant data points as shown in Fig 7a. This Figure presents the increase of temperature $\Delta T$ measured 3.45 hrs after the start of the heat experiment. We recall that the temperature rise $\Delta T(t)$ measured during active-DTS experiments depends on the thermal conductivity of the sediments which controls the rate of increase through time and on groundwater flow which limits the temperature rise (Simon et al., 2021). Despite some areas without data, the values of $\Delta T$ measured 3.45 hrs after the start of the heat experiment are distributed over less than 55 m offering a large view of the variability of thermal responses. The value of $\Delta T$ is particularly variable and ranges between 19.42 °C (at 11.2 m) and 36°C (at 132.5 m). However, despite the variability observed, adjacent points present in general a similar dynamic with similar values of $\Delta T$, suggesting similar behaviours over a certain range or scale.

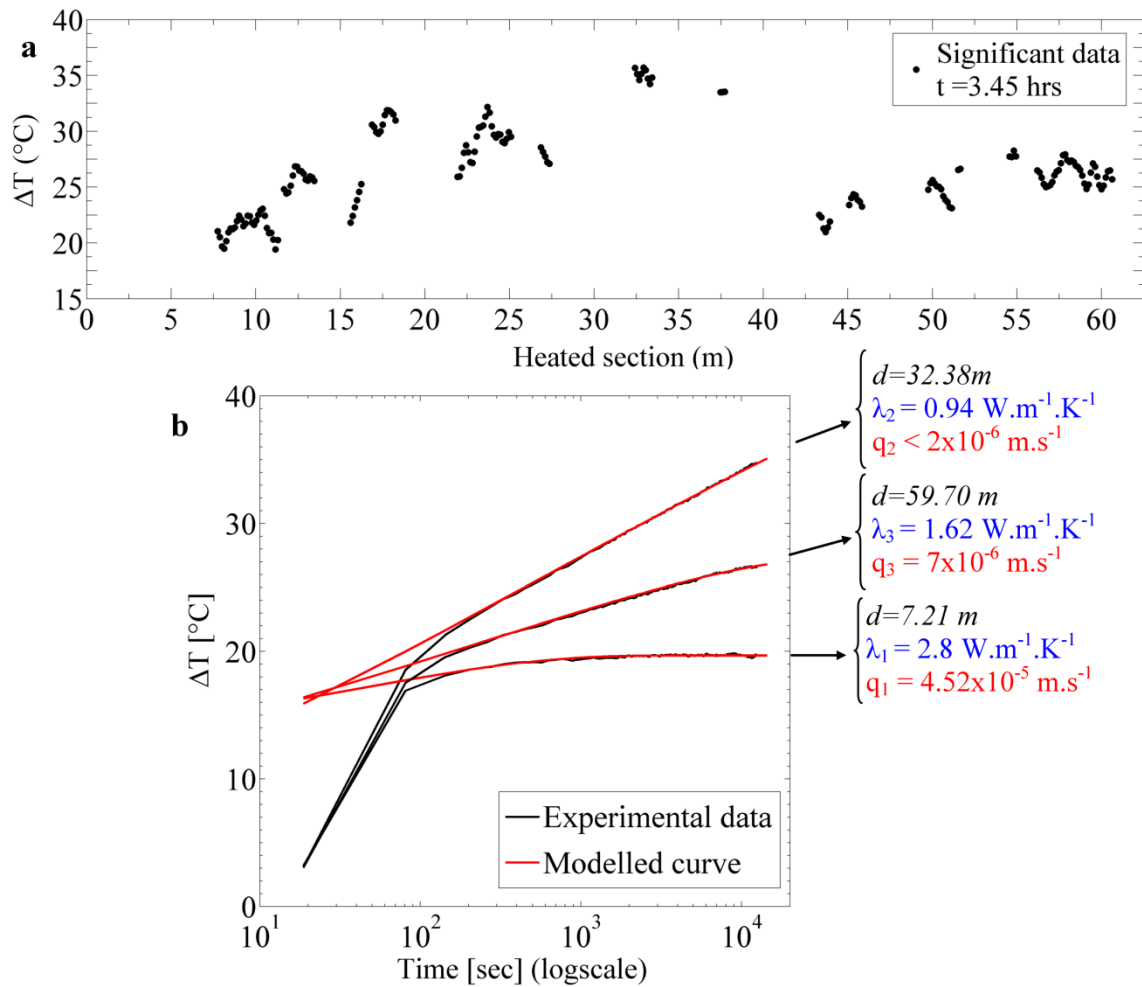



**Figure 7: a. Significant ΔT values measured 3.45hrs after the start of the heating period measured along the buried FO section. b. Examples of data interpretation on three thermal response curves observed in the data (black lines). The MILS model was used to reproduce the temperature increase during both the conduction- and advection-dominant periods (red lines).**

Each data point was interpreted using the ADTS Toolbox to estimate thermal conductivities and fluxes. Figure 7b shows three examples of thermal response curves observed in the data collected along the heated FO section (black lines) and their respective interpretation with the ADTS Toolbox (red lines). The data interpretation focuses on the interpretation of the second part of the temperature increase (for $t > 90$ sec) corresponding to the temperature increase controlled by heat conduction and advection in the sediments (Simon et al., 2021). As illustrated in Fig. 7b, the thermal conductivity highly controls the thermal response and the variability of $\Delta T$. For instance, at $d = 32.38$ m, the temperature rise reaches 34.7 °C after 3.45 hrs of heating, in concordance with the very low thermal conductivity estimated (0.94 W.m$^{-1}$.K$^{-1}$). On the contrary opposite, at $d = 7.21$ m, where the temperature rise is much lower and reaches only 19.7 °C, $\lambda$ is estimated at 2.8 W.m$^{-1}$.K$^{-1}$. The fluxes are then estimated using the temperature at later times, as the intensity of the flux controls

temperature stabilization (Simon et al., 2021). Thus, for instance, the following fluxes values of $7 \times 10^{-6}$ m.s$^{-1}$ and $4.52 \times 10^{-5}$ m.s$^{-1}$ are estimated at $d = 59.70$ m and $d = 7.21$ m respectively. However, for some points, as illustrated by the temperature evolution measured at $d = 32.38$ m, the temperature does not stabilize for later times and keeps increasing with no inflexion over the whole heating period. This implies either no-flow conditions ($q = 0$ m.s$^{-1}$) or very low-flow conditions which presume that the heat duration was not long enough to reach temperature stabilization (Simon et al., 2021). In these cases, only an estimate of $q_{lim}$ can be provided, which corresponds to the highest value of flow that would induce such temperature increase. For instance, at $d = 32.38$ m, the flux is estimated to be lower than $2 \times 10^{-6}$ m.s$^{-1}$.

### 3.2.2 Spatial variability of thermal conductivities and water fluxes estimates

Figure 8 shows the estimation of both the thermal conductivities (Fig. 8a) and the fluxes (Fig. 8b) obtained from active-DTS measurements using the ADTS Toolbox. It provides an estimate of their respective spatial distribution at very small scale. As shown in Fig. 8a, the thermal conductivities estimated along the heated section vary between 0.8 and 3.14 W.m$^{-1}$.K$^{-1}$, with a median value at 1.65 W.m$^{-1}$.K$^{-1}$. The RMSE calculated between observed data and the best-fit model was systematically lower than 0.05 °C. Seeing the data noise ($< 0.1$ °C), the maximal uncertainty of these estimates is estimated to be $\pm 0.2$ W.m$^{-1}$.K$^{-1}$.

As shown in Fig. 8b, estimated groundwater fluxes vary between $2 \times 10^{-6}$ and $4.74 \times 10^{-5}$ m.s$^{-1}$, with a mean value at $1.34 \times 10^{-5}$ m.s$^{-1}$ and a SD of $9.18 \times 10^{-6}$ m.s$^{-1}$. For 9 locations (blue points), only the value of $q_{lim}$ was evaluated since the departure of the conduction regime towards temperature stabilization was not reached at the end of the heating period. Note that the data interpretation does not provide the flow direction, the temperature increase being identical for upward and downward conditions. Although significant measurements are not available all along the sections, results show a decrease of the flux from upstream to downstream, particularly in the first twenty meters of measurements. At greater distances, fluxes are more diffuse in space, except at few locations, for instance at 43, 50 and 52 m from the start of the heated section where higher values are observed. Interestingly, very local and high fluxes values, spreading on less than 2 m, can be observed, as for instance at $d = 10$ m.

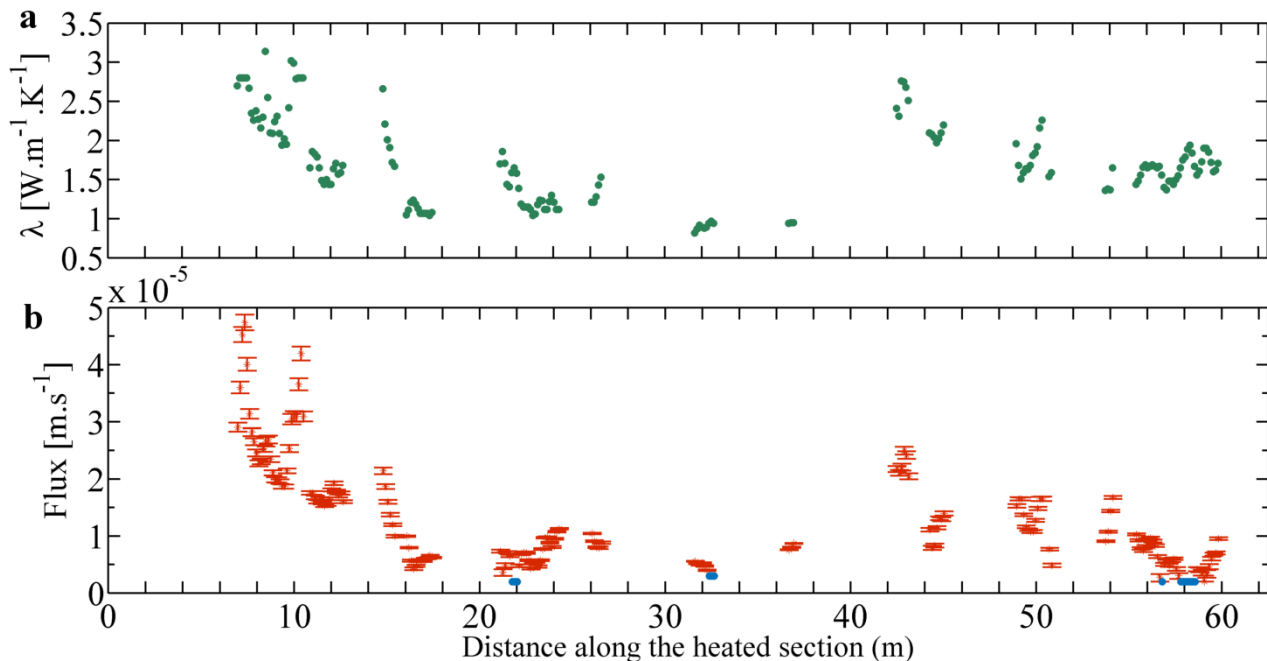



**Figure 8: The interpretation of active-DTS measurements along the heated section of FO cable leads to estimate the spatial distribution of both a. the thermal conductivity (uncertainty = ± 0.2 W.m⁻¹.K⁻¹) and b. the water fluxes and their associated errors (error bars). Blue points mark locations where the temperature stabilization is not reached and where an estimate of $q_{lim}$ is provided. Errors bars corresponding to uncertainties on flow estimates calculated with respect to data noise for each measurement points.**

### 3.3 Comparison between passive- and active-DTS measurements

Figure 9 compares estimated values of groundwater fluxes for the 7th April 2016. The flow direction is assumed upward in agreement with passive-DTS measurements (Fig. 6b).

For passive-DTS measurements, the two light grey curves correspond to fluxes estimates considering $\lambda = 1$ W.m⁻¹.K⁻¹ and $\lambda = 4$ W.m⁻¹.K⁻¹, assuming that the effective values of fluxes should range between these two estimates. The estimation of groundwater discharges clearly remains highly uncertain because of the lack of knowledge about thermal conductivity variations. Results show nevertheless a slight decrease of groundwater discharge from upstream to downstream but the high uncertainty probably blurs the actual trend.

On the contrary, flux estimates from active-DTS measurements (pink points) present a much smaller uncertainty (Fig 9), confirming the interest of using a heat source to improve fluxes measurements. Flux estimates from both passive- and active-DTS measurements roughly agree, but active-DTS measurements reveal a larger spatial variability regarding groundwater discharge. Interestingly, flux estimates from active-DTS measurements can be qualitatively compared with the evolution of the SD of temperature (green line). The lowest SD values are located in the first 55 m of the stream, which is in good agreement with active-DTS measurements that highlighted highest groundwater discharges between 47 and 53 m (between $1.7 \times 10^{-5}$ and $4.9 \times 10^{-5}$ m.s⁻¹). Between approximately 55 and 60 m, the value of SD increases rapidly (from 1.25 °C

460   at 54 m to 2°C at 60 m) while the fluxes estimated from active-DTS measurements decrease linearly (from $2.1 \times 10^{-5}$ at 56.8 m to $4.2 \times 10^{-6}$ m.s$^{-1}$ at 58.5 m). From 60 m, the SD increases and the associated values of fluxes estimated from active-DTS are particularly low, varying for instance between $2 \times 10^{-6}$ and $1.1 \times 10^{-5}$ m.s$^{-1}$. Interestingly, the locations of local increases of groundwater discharge detected with the active experiment at 87.5 m, 95 m and 100 m (black arrows) match well with isolated decreases of SD values. Note also that flux estimates from active-DTS measurements are in very good agreement

465   with the results of VTPs (blue line). The estimated flux based on passive-DTS measurements at 53.4 m is also in good agreement with active-DTS results despite the large uncertainty.

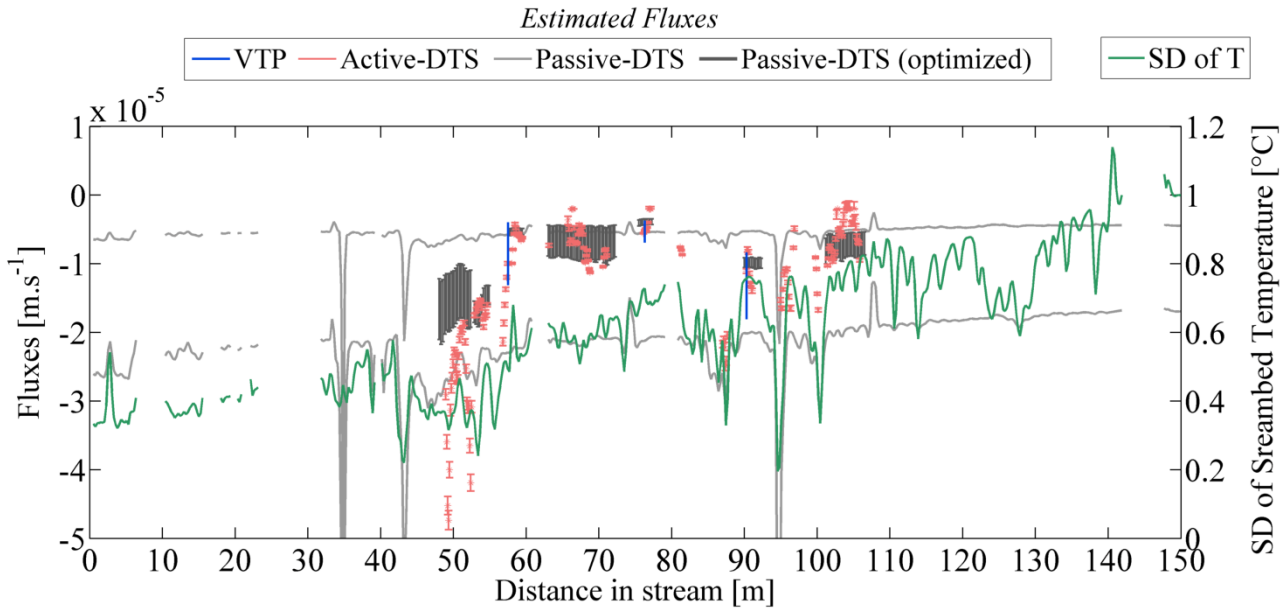



**Figure 9: Comparison of flow estimated the 7$^{th}$ April 2016 using the vertical temperature profiles (VTP), the passive-DTS measurements and the active-DTS measurements. Results are compared with the evolution of SD of the temperature calculated**
470   **from passive-DTS measurements. The black arrows highlight localized groundwater discharge.**

Theoretically, considering the effective value of thermal conductivity in the model, should highly improve the results obtained from passive-DTS measurements. Thus, the thermal conductivity estimates providing from active-DTS measurements were used to fully re-interpreted the passive-DTS measurements using the FLUX-BOT model. As a result, the estimated range of fluxes was highly reduced and was found in much better agreement with other estimates, as shown by

475   dark grey lines in Fig. 9. For instance, between 63 and 72 m, the thermal conductivity was evaluated from active-DTS measurements between 1 and 1.9 W.m$^{-1}$.K$^{-1}$ depending on measurement points (Fig. 8a). Using such values, the fluxes estimated from passive-DTS measurements in this area vary between $-9.5 \times 10^{-6}$ and $-4.3 \times 10^{-5}$ m.s$^{-1}$ (dark grey lines), whereas initially estimated between $-2.2 \times 10^{-5}$ and $-5.4 \times 10^{-6}$ m.s$^{-1}$ considering $\lambda$ between 1 and 4 W.m$^{-1}$.K$^{-1}$ (light grey lines). As shown in Fig. 9, except between 48 and 52 m where small discrepancies remain, this approach significantly reduces the

480   range of fluxes estimated and shows that passive-DTS results are in good agreement with active-DTS results when an independent and more precise estimate of the thermal conductivity is considered.

## 4 Discussion

In the following, we discuss the advantages and limitations of applying either passive- or active-DTS experiments depending on the objectives of the study and on technical limitations. Thus, we first focus on the possibilities of detecting and localizing groundwater inflows and their spatial and temporal dynamics before discussing the ability of quantify groundwater discharges. Besides comparing both approaches, we show the interest of combining both methods to infer the spatial and temporal variability of groundwater discharge at the catchment scale.

### 4.1 Detecting, localizing and monitoring groundwater discharge

Results show that long-term passive-DTS measurements turn out to be an efficient method to detect, locate and monitor thermal anomalies that can be further interpreted as marker of groundwater discharge. The approaches consisted in burying a FO cable in the streambed along several hundreds of meters, in order to record streambed temperature variations at high resolution during several months. The high spatial and temporal resolution of measurements is clearly the main advantage of the passive-DTS experiment since such achievement would not have been possible with individual temperature probes. Moreover, although the FO installation in the streambed can be difficult depending on the streambed nature, the long-term recording of temperature is relatively easy and autonomous.

Streambed temperature measurements recorded with the FO cable allow making first assumptions about the spatial and temporal dynamics occurring in the watershed if used over a several-month-long monitoring. To do so, the calculation of the Standard Deviation (SD) of streambed temperature over time appears a reliable proxy for locating inflows (Fig. 4 and 5), since lower SDs values reflect larger attenuation of daily temperature amplitudes. Here, the SD of temperature increases progressively from upstream to downstream up to reaching the SD of stream temperature around d = 300 m (Fig. 4b). Very localized and low values of SD, described previously as minimal spikes of SD digressing from the general trend, also appear along the profile. Theoretically, temperature variations recorded in the streambed depend on the stream temperature variations and on the intensity of stream water/groundwater exchanges (Constantz, 2008). Interpreting the data without measuring stream temperature variations along the stream requires assuming that the stream temperature is uniform along the investigated section. In this case, the value of SD of the stream temperature can be assumed uniform as well along the investigated section and any value of SD measured in the streambed lower to the SD of the stream temperature could actually be interpreted as the result of groundwater inflows. Here, this assumption seems reasonable since shade and lighting conditions as well as water depths are very similar along the investigated section. Moreover, the transit time from the spring to the gauging station is relatively rapid due to the short distances. The river slopes and the low water depths imply a fast balance between the air temperature and the stream temperature. This assumption is partly confirmed with the stream temperature recorded near the spring with the DTS, in an area where the FO cable is not buried but lies in the bottom of the stream. At this location, the SD of the temperature equals 1.03°C, which is a little less 1.375 °C, the value recorded in the stream at the gauging station E30, located at around 490 m of the spring. However, this suggests that the SD of the stream

temperature signal should be relatively high, greater than 1°C all along the stream and consequently much larger than the SD recorded within the streambed, especially in the upstream section of the stream (first 300 meters).

Consequently, results suggest a decrease of groundwater inflows from upstream to downstream in the first 300 meters of the watershed with higher and localized inflows in spots characterized by SDs values clearly lower than the general trend. This is strengthened by the fact that the lowest values of SD (minimal 'spikes' of SD illustrated by the blue line in Fig. 5b) correspond to clear thermal anomalies for which the temperature appears relatively stable over time. Beyond 300 m, the values of the SD are almost equal to the SD of the stream temperature and the recorded temperature variations are approximately similar to stream temperature variations. Concerning the second part of the golf area (from 300 to around 470 m), the data interpretation remains difficult because of the hard substrate that limited the burying of the FO cable. However, in the last 70 meters of the FO cable (wood plain), the cable was easily buried in a thick sandy riverbed. Thus, values of SDs in this area, equals to the one recorded in the stream, would suggest the absence of groundwater inflows, which would remain limited to the wetland and therefore to the upper part of the watershed with highest topographic changes, as we shall discuss below.

Active-DTS measurements could also be used for localizing inflows, since the approach allows the accurate quantification of groundwater fluxes. However, contrary to passive-DTS measurements that can be easily used to provide groundwater discharge areas, their identification from active-DTS measurements requires going through flux quantification, which can be more constraining. Moreover, this method requires more instrumentation and the length of the heated section is limited depending on the power supply available (Simon et al., 2021). Thus, flow investigation at the watershed scale is way more difficult to achieve unless multiplying the installation of heated sections in the streambed. Furthermore active-DTS measurements provide a punctual estimate of fluxes. To characterize the temporal dynamic of flow, these experiments must be often repeated, which is clearly more constraining than conducting long-term passive-DTS measurements, because active-DTS experiments require more instrumentation (heat-pulse system, electrical cables…). However, the repetition of active-DTS measurements offer very promising perspectives for environmental monitoring as recently shown by Abesser et al. (2020) who repeated surveys under different meteorological or hydrological conditions in order to monitor the evolution of thermal and hydraulic properties of the soil subsurface.

## 4.2 Quantification of groundwater discharge

### 4.2.1 About the large uncertainties associated to the interpretation of passive-DTS measurements

The inverse numerical FLUX-BOT model was used to quantify the vertical fluxes from passive-DTS measurements in the first 150 meters of the temperature profile which represents 545 measurements points. Although this approach provided fluxes estimates, their relevance can clearly be discussed. Indeed, the estimates are highly uncertain, which demonstrates the difficulty of quantifying groundwater fluxes using passive-DTS measurements recorded along a single FO cable. The large uncertainties on estimates are due to several sources of uncertainties. Firstly, the model relies on the

comparison of temperature variations recorded at 3 different depths. Ideally, the approach would require deploying at least 3 FO cables in the field (Mamer and Lowry, 2013) in order to continuously measure temperature conditions at high resolution at upper and lower boundaries, which was technically impossible in the field. Thus, as discussed above, the stream temperature variations were assumed uniform along the studied section, which seems consistent here. Moreover, the

550    temperature signal recorded in the piezometer F4 was used to set the lower boundary condition of the model. This piezometer seems to be a good proxy for groundwater temperature since the temperature signal measured at 20 m-depth in the piezometer F5b is similar to the one measured at 15 m-depth in the piezometer F4. This also suggests that the temperature of groundwater discharging into the stream is uniform along the investigated portion of the catchment. However, although the assumptions about stream and groundwater temperatures seem reasonable, it considerably increases the

555    uncertainties on fluxes estimates. Secondly, the model requires defining the burial depth of the cable to calculate vertical fluxes while results are very sensitive to this parameter. Complementary tests (not shown here), conducted by varying the depth of the FO cable in the model, suggest that varying the burial depth by ± 2 cm induces in average a difference of ± 50% on fluxes estimates, showing the high uncertainty associated to the uncertainty on burial depth. Last but not least, results showed that thermal conductivity values have a very strong impact on fluxes estimates, which is consistent with the results

560    of Briggs et al. (2014), Duque et al. (2016), Lapham (1989) and Sebok and Müller (2019). The lack of knowledge and assumptions on thermal conductivities values lead to high uncertainties on fluxes estimates using both VTP and passive-DTS measurements (Fig. 6b). *In-situ* estimates of thermal conductivities using thermal conductivity probes could considerably improve the fluxes estimates, as demonstrated by Duque et al. (2016), who reported up to 89% increase in flux estimates when using *in situ* measured sediment thermal conductivities. However, seeing the high spatial variability of the thermal

565    conductivity highlighted through the active-DTS experiment, it would certainly require a tremendous effort in the field to characterize such variability with single probes. Moreover, it will not remove others sources of uncertainties associated to the burial depth of the FO cable or to the lack of temperature measurements at different depths all along the section.

Consequently, uncertainties on fluxes estimates are so large that passive-DTS experiment does not appear as a reliable and accurate method for estimating seepage rates. However, in the first 150 m, the model allows determining the

570    flow direction (upwelling fluxes), demonstrating that thermal anomalies can definitely be associated to groundwater inflows confirming the spatial and temporal dynamics of exchanges occurring in the wetland. Note that the model was not even applicable in the lower part of the watershed (for d>150 m) to estimate flow direction. Thus, despite the values of the SD recorded between d=150 m and d=300 m suggesting potential groundwater inflows, groundwater inflows are probably too low or diffuse in this part of the watershed to apply the model and validate even the flow direction.

575    To summarize, fluxes quantification from passive-DTS measurements depends on several assumptions about thermal properties and boundary conditions, which induces high uncertainties on fluxes estimates. Burying a single FO cable in the streambed, although very promising and interesting, is limited to fully characterize and quantify groundwater/surface water interactions, even in a headwater watershed. For further applications, results suggest the necessity of deploying an additional FO cable at the bottom of the stream in order to measure also stream temperature variations at high resolution all

580 along the studied section. This seems the only way to fully and efficiently extend the thermal-based classical methods (Constantz, 2008; Hatch et al., 2006) at high spatial resolution. A third buried FO cable would be the optimal configuration to estimate distributed vertical fluxes (Mamer and Lowry, 2013) and reduce the uncertainties on fluxes estimations based on passive-DTS measurements.

### 4.2.2 AAccuracy of fluxes estimated with active-DTS measurements~~bout the ability of Active-DTS methods to provide accurate fluxes estimates~~

Contrary to passive-DTS measurements, the active-DTS measurements turn out to be an efficient method to estimate fluxes ~~at high resolution and with a very low uncertainty~~. From only 4 hrs of measurements, the approach provides an estimate of both the thermal conductivities and the fluxes along the heated cable confirming the high variability of these two parameters in space (Fig. 8). Despite some difficulties to install the heated FO cable, fluxes were even so estimated for 590 172 measurements points along a 60-meter section of cable, which is an excellent performance. This high resolution is particularly interesting to characterize spatial variabilities at small scale. Such results cannot be achieved with any other methods commonly used in this context. Note that the installation of the heated FO cable was entirely manual and rapid, which probably partly explains the relatively large number of measurement points removed from data processing. Nevertheless, the use of tools like ploughs should improve the burying of the cable, limit the alteration of the riverbed and 595 allow for a much better control of the burial depth.

Results show that streambed thermal conductivities are relatively variable in space, typically between 0.9 to 3.1 $W.m^{-1}.K^{-1}$ (Fig. 8a), which is consistent with streambed sediments, composed of saturated clay and silt, and saturated sand and gravel, whose thermal conductivity values commonly range respectively between 0.9 and 4 $W.m^{-1}.K^{-1}$ (Stauffer et al., 2013). The large range of thermal conductivities observed in this relatively small section of streambed (less than 60m) 600 demonstrates the interest of distributed measurements to ~~fully~~ characterize streambed heterogeneity. No other method could provide an estimate of the thermal properties at this spatial resolution.

Groundwater fluxes were estimated between $2x10^{-6}$ and $4.74x10^{-5}$ $m.s^{-1}$, in very good agreement with the results of the VTPs (Fig. 9). The results suggest a decrease of the groundwater discharge from upstream to downstream, with the most significant inflows located in the first 20-m of the heated section. Elsewhere, groundwater discharge is more diffuse in space 605 although significant groundwater discharge areas can be locally observed. These local increases of groundwater discharge match with isolated decreases of streambed temperature SD values, calculated from passive-DTS measurements (Fig. 9). This confirms the possibility of investigating very local groundwater inflows and the capability of investigating the spatial evolution of fluxes at very small scale.

The magnitude of groundwater flux is also in good agreement with the measured stream flow. Considering the 610 width and the length of the investigated stream where groundwater inflows have been estimated, contribution to the stream can be roughly evaluated around 4 $L.s^{-1}$. This means that 57% of the stream flow at the time of the experiment was

contributed by groundwater knowing that the average flow measured at the downstream gauging station was 7 L.s$^{-1}$ for this period.

615    It clearly appears that the main advantages of the approach are i) the low uncertainty on fluxes estimates and ii) the associated estimates of thermal conductivities. The use of the ADTS Toolbox that automatically interprets active-DTS measurements (Simon and Bour, 2022Submitted) highly facilitates data interpretation, which is finally much easier than the interpretation of passive-DTS measurements. Contrary to passive-DTS measurements, the interpretation of active-DTS measurements provides estimates of thermal conductivities with a very good accuracy. Thus, the approach does not require

620    assuming thermal conductivity values which considerably reduce the uncertainties of the fluxes estimates. However, the burial depth of the heated cable might potentially affect the thermal response, if the cable is too close to the stream. In this case, the stream temperature could limit the temperature elevation by dissipating the heat produced and further investigations should be done to quantify the effect of the near stream on estimates. However here, the active-DTS experiment was conducted straight after the installation of the cable, ensuring that the burial depth was sufficient to limit the effect of the

625    near stream (results from modelling showed that the heating is particularly localized around the heated cable). Finally, in gaining streams, active-DTS measurements are independent of temperature boundary conditions, as long as the groundwater temperature is constant over time. Indeed, in gaining conditions, with no groundwater temperature variations, the temperature evolution measured along the FO cable is exclusively due to heat injection, streambed sediment properties and groundwater flow intensity. Here, over the heating experiment, an average temperature of 12.1 °C with a standard deviation

630    of 0.12 °C has been recorded in sediments along non-heated buried sections of the cable demonstrating that the streambed temperature was not affected by potentials air/stream variations and that the temperature variations recorded along the heated section are exclusively due to the heat experiment. In losing conditions, since diurnal water temperature variations propagates deeper, it could be necessary to separate the temperature evolution induced by the heat injection and the one depending on stream temperature variations.

635    **4.2.3 About the complementary use of both approaches**

    Finally, the complementary of both approaches should be noted. First, the data interpretation of active-DTS measurements does not provide the flow direction contrary to the interpretation of passive-DTS measurements. Note that the temperature variations recorded before the heating period and after the end of the recovery can be used to determine the flow direction as soon as the stream temperature variations are assumed uniform along the heated section. Of course, results of

640    active-DTS measurements are useful to validate the general behaviour/trend highlighted through passive-DTS measurements, that is a baseline of groundwater discharge associated to local and important spikes of discharge. They do not fully allow validating the different hypothesis made to interpret passive-DTS measurements but they permit to check the consistency of the results obtained. Results also show (Fig. 9) that the interpretation of active-DTS measurements can be directly used to improve the interpretation of passive-DTS measurements. Indeed, the values of thermal conductivities,

645 estimated from active-DTS measurements, can be used to calibrate the inverse model and therefore to reduce the uncertainties on fluxes estimates from passive-DTS measurements. This is a very promising result since it highly facilitates the interpretation of passive-DTS measurements. Once thermal conductivity distribution is known along the section, passive-DTS-experiments could therefore be considered as an independent and full tool to quantify GW discharge at high resolution through long-term monitoring (although the assumption on the stream temperature remains an issue).

650 Moreover, note also that for the interpretation of both passive- and active-DTS measurements, the flow is assumed to be vertical and perpendicular to the FO cable. Although flow is generally assumed vertical when using heat as a tracer for studying groundwater/stream interactions (Constantz, 2008; Hatch et al., 2006; Lapham, 1989), nonvertical fluxes can affect natural temperature profiles and associated fluxes estimates (Bartolino and Niswonger, 1999; Cranswick et al., 2014; Cuthbert and Mackay, 2013; Lautz, 2010; Reeves and Hatch, 2016). Obviously, like for most thermal-based methods, this is
655 a main limitation when using passive-DTS measurements to detect and quantify groundwater discharge. Likewise, nonvertical fluxes could also affect the interpretation of active-DTS measurements. Thus, some studies suggest that the impact of the angle of the flow against the cable is significant as soon as it differs more than ±30° from being perpendicular (Aufleger et al., 2007; Chen et al., 2019; Perzlmaier et al., 2004).

## 4.3 Characterizing groundwater discharge dynamics

660 The complementary use of these two DTS approaches allows characterizing spatial and temporal patterns of groundwater discharge in this headwater catchment. Results and associated fluxes estimates are consistent with previous studies that predicted that 80-90% of the stream flow was induced by groundwater discharge (Fovet et al., 2015b; Martin, 2003). Interestingly, the two approaches allow characterizing the groundwater discharge dynamic at two different scales. This is a particularly promising and exciting achievement since groundwater/surface water interactions are generally
665 controlled by multi-scale processes, making their characterization particularly challenging in the field (Brunke and Gonser, 1997; Fleckenstein et al., 2006; Flipo et al., 2014; Harvey and Bencala, 1993; Kalbus et al., 2009).

First, conducting measurements over more than 530 m-linear allow describing groundwater discharge dynamic at the catchment scale. Thus, results suggest that the groundwater contribution is localized in the very head of the catchment, in the upstream near the spring where the steepest slopes can be observed. Further downstream, beyond 60 m from the spring,
670 the groundwater discharge decreases progressively and rapidly. This confirms the importance of the topography in the stream generation in headwater area (Harvey and Bencala, 1993; Sophocleous, 2002; Tóth, 1963; Winter, 2007) and the role of local topography variations on groundwater discharge (Baxter and Hauer, 2000; Flipo et al., 2014; Frei et al., 2010; Jencso et al., 2009; Stonedahl et al., 2010; Tonina and Buffington, 2011; Unland et al., 2013).

Secondly, the high resolution of DTS measurements allows studying groundwater discharge dynamic at very small
675 scale and thus highlighting local heterogeneities, which would not have been possible with more integrative methods. Therefore, beyond the role of topography which acts as the main driver of groundwater inflows, variations of hydraulic conductivity could also explain the presence of local hotspots with high groundwater inflows, highlighted with both methods

in the wetland area, upstream near the spring. Indeed, these hotspots spikes that would highly contribute to the stream flow may be driven by local changes in the hydraulic gradient, induced by the successive streambed topography changes, but are more likely due to hydraulic properties changes given the amplitude and scale of variations. Such hydraulic conductivity variations could come from uneven bedrock weathering or to the presence of fractures which is very common in such bedrock geology (Buss et al., 2008; Guihéneuf et al., 2014). Such heterogeneities may control flow in the subsurface but can also influence the nature of the streambed. This would also explain why the values of fluxes seem correlated, at least at some places, with the values of thermal conductivities (Fig. 8). Indeed, our results suggest that local hotspots with high groundwater inflows are also associated to higher values of thermal conductivities. This is consistent with a change of streambed properties. Indeed, clay and silt have much lower hydraulic conductivities than sand but also lower thermal conductivities (Stauffer et al., 2013). Although cross-correlation analysis would be useful to go further in the interpretation, such correlation would not be surprising since the nature of the streambed affects both its hydraulic conductivity and its thermal properties.

Concerning temporal variations, three different time periods were clearly identified from the passive-DTS measurements according to the behaviour of the streambed temperature evolution over time (Fig. 4 and 5). The increase in precipitations in winter certainly leads to increase gradually the hydraulic gradient, which induces groundwater exfiltration into the stream once the elevation of the groundwater table becomes higher than the elevation of the stream stage. In spring, the groundwater table decreases progressively and so do the groundwater contribution to stream flow. Since changes in piezometric levels are periodic with alternating periods of high and low water table levels, we can assume that exchanges have a similar temporal dynamic from year to year, which can help managing water resources. These results are consistent with the temporal dynamic of exchanges observed under temperate climate where the intensity of groundwater/surface water exchanges fluctuates according to seasonal patterns (Brunke and Gonser, 1997; Sophocleous, 2002). More important, these results highlight the interest of the long-term monitoring of streambed temperature with DTS. Here, with only eight months of measurements, the experiment allowed continuously monitoring hydrological conditions changes and clearly identifying "hot-moments" corresponding to groundwater discharge periods. In headwater catchments, these tools should allow in the near future investigating the distribution of response times of groundwater discharges to some specific events, which is very promising.

## 5 Conclusions

Passive- and active-DTS measurements were conducted concurrently in the same experimental site in order to characterize the spatial and temporal patterns of groundwater discharge into a first and second-order stream. Long-term passive-DTS monitoring can easily be used to assess the spatial and the temporal dynamics of groundwater discharge. The analysis of streambed temperature recordings allows identifying thermal anomalies that can be interpreted as markers of

710 groundwater inflows into the stream. Here, results suggest that groundwater discharge is localized in the upper part of the watershed where topographic gradients are the highest.

However, this study also demonstrates the limitations of passive-DTS measurements for quantifying groundwater discharges. When a single FO cable is buried in the streambed, the data interpretation requires making strong assumptions about the thermal conductivity of sediments and about the stream temperature. Uncertainties may be reduced if previous and

715 independent measurements of the variability of streambed thermal conductivities are conducted through active-DTS measurements.. Nevertheless, the interpretation of passive-DTS measurements would still rely on the assumption that the stream temperature is uniform along the studied section. In practice, the proper estimation of passive-DTS measurements conducted in streambeds would require measuring the stream temperature with the same spatial resolution and thus deploying a second FO cable at the bottom of the stream.

720 Active-DTS measurements allowed going way further in the characterization of groundwater inflows through the estimate of fluxes and their spatial distribution with a very low uncertainty in comparison with passive-DTS measurements and *in situ* thermal methods. The quantification of groundwater fluxes through the active-DTS measurements clearly shows the co-existence of both local hotspots, characterized by very localized and high groundwater inflows, and more diffuse groundwater inflows elsewhere along the heated section. This allowed confirming the role of topography on the large-scale

725 variations of groundwater discharge, but also the role of heterogeneities at small scales. Such small-scale variability of groundwater discharge is certainly associated to hydraulic conductivity variations. Moreover, the active-DTS experiment allowed describing the high variability of thermal conductivity in space

Finally, it should be noted that passive-DTS measurements permitted to locate the spatial and temporal patterns of groundwater inflows on relatively large distances, while active-DTS measurements allowed a much more precise and robust

730 estimate of both thermal conductivities and fluxes which can highly contribute to improve passive-DTS methods interpretation. Hence, the combination of active- and passive-DTS methods provided an imaging of the spatial variability of groundwater inflows. It allowed better inferring the role of topography, which acts as the main driver of groundwater inflows in the upper part of the watershed, and also the impact of hydraulic conductivity variations which may explain the presence of very localized and high groundwater inflows.

735 Thus, these methods and especially active-DTS measurements conducted in the streambed open very promising perspectives for novel characterization of the groundwater/stream interfaces, especially if surveys are repeated under different meteorological or hydrological conditions. Being able to continuously monitoring the temporal dynamic of exchanges is a very promising achievement that could be useful to understand the hydrological behaviour in the watershed but also for characterizing the distribution of response times of groundwater discharge. This can be particularly useful for

740 studying biogeochemical hotspots and hot moments (Krause et al., 2017; Singh et al., 2019; Trauth and Fleckenstein, 2017) or to couple this approach with natural tracers to assess the residence times in the hyporheic zone (Biehler et al., 2020; Liao et al., 2021).

**Data availability**

The data presented in this study are available online.

745 Link through data related to the active-DTS experiment:

http://geowww.agrocampus-ouest.fr/geonetwork/apps/georchestra/?uuid=535a3738-0ed7-4376-99f1-9a7a652b893d

Link through data related to the passive-DTS experiment:

http://geowww.agrocampus-ouest.fr/geonetwork/apps/georchestra/?uuid=a5f2a68f-bf63-469c-839b-1e1edf1f8624

**Supplement link:**

750 **Author contribution**

Conceptualization: NS, OB, LL, OF and ZT; Data curation: NS; Formal analysis: NS; Funding acquisition: OB; Investigation: NS, OB, NL, MF, OF, HLL and ZT; Methodology: NS; Project administration: OB, OF and ZT; Resources: NL and MF; Software: NS; Supervision: OB; Validation: NS and OB; Visualization: NS; Writing – original draft preparation: NS; Writing – review & editing: NS, OB, OF, ZT and LL.

755 **Competing interests**

The authors declare that they have no conflict of interest.

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