

Supplements to:

**Maximum Entropy Distribution of Rainfall Intensity and Duration –
MEDRID: a method for precipitation temporal downscaling for sediment
delivery assessment.**

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1 INTRODUCTION

In Figure S1 we present the map of pluviometric stations with daily and sub-daily data in the Brazilian Northeastern Region. As discussed in the main text, there are few stations monitoring sub-daily precipitations in the region. Additionally, most stations in the left of the plot have a short time series and/or with gaps.

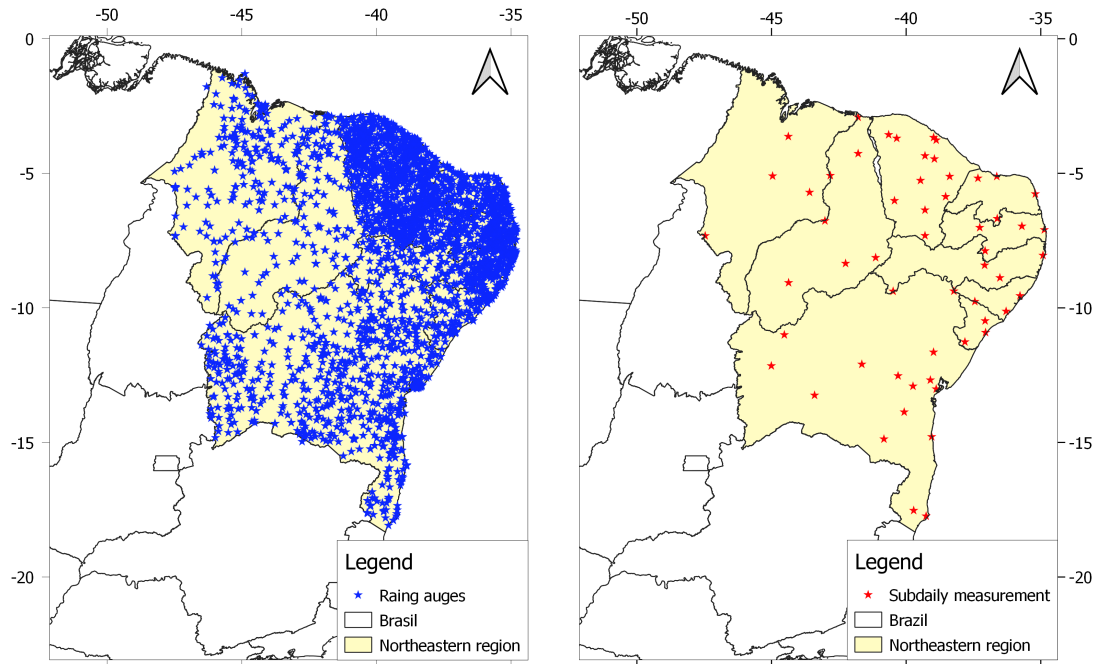


Figure S1: Map of Ville de Paris and Automatic stations in the Brazilian Semiarid Managed by the Brazilian National Water Agency (ANA, 2019).

2 MATERIALS AND METHODS

2.1 The Principle of Maximum Entropy

The Principle of Maximum Entropy (PoME) is grounded on the concept of entropy as a measure of uncertainty or information, as proposed by (Shannon, 1948). Based on abstraction, Jaynes (1957a,b) proposed the PoME to obtain the least-biased probability function on the basis of known information represented as constrains. The Shannon entropy equation is expressed as (Eq. S1):

$$h_x = - \int f(x) \ln f(x) dx \quad (S1)$$

h_x is the total entropy for the variable x . The function $f(x)$ that maximises h_x is the one that does not consider any non-proved hypothesis. To maximize Eq. S1, subjected to the constrains, we can formulate the Lagrangian function \mathcal{L} (Eq. S2) and differentiate in respect to f and equals the derivative to zero (Eq. S3).

$$\mathcal{L} = - \int_{x_0}^{x_1} f(x) \ln f(x) dx - \sum_{r=0}^n \lambda_r \left[\int_{x_0}^{x_1} f(x) g_r(x) dx - C_r \right] \quad (S2)$$

$$\frac{\partial \mathcal{L}}{\partial f} = 0 \rightarrow \frac{\partial \mathcal{L}}{\partial f} = -1 - \ln f(x) - \sum_{r=0}^n \lambda_r g_r(x) = 0 \quad (S3)$$

$\lambda_0, \lambda_1, \dots, \lambda_n$ are the Lagrange multipliers. $g_r(x)$ are functions of x related to the constraints. n is the number of restrictions besides the trivial ($r = 0 \rightarrow \int f(x) dx = 1$). Solving Equation S3 for $f(x)$ one finds the probability distribution in terms of the Lagrange multipliers as in Eq S4.

$$f(x) = \exp \left[- \sum_{r=0}^n \lambda_r g_r(x) \right] \quad (S4)$$

2.2 The SYPoME Model

Proposed by de Araújo (2007), the SYPoME (Sediment Yield Model based on the Principle of Maximum Entropy) allows the user to assess the hillslope sediment production of each event and is given by Equation S5:

$$Q_s = \bar{\varepsilon} A SDR = \bar{\varepsilon} A \frac{e^{\lambda L_m} (L_0 - x_0) \lambda - (e^{\lambda(L_0 - x_0)} - 1)}{\lambda L_0 (e^{\lambda(x_0 + L_m)} - 1)} \quad (S5)$$

$\bar{\varepsilon}$ ($\text{Mg ha}^{-1} \text{ yr}^{-1}$) is the gross erosion obtained, for example, by using the Universal Soil Loss Equation (USLE Wischmeier and Smith, 1978), A (ha) the hillslope contribution area, L_0 the hill slope length (m), L_m the maximum sediment travel distance (m), x_0 is the initial position of erosion in the hillslope and λ is a Lagrange multiplier. The ratio of the sediment portion

that reaches rivers and promotes siltation (Q_s) and all mobilised sediment ($\bar{\varepsilon} A$). The SDR is restricted to a closed interval ($SDR \in [0, 1]$).

The parameters λ and L_m can be obtained by solving the systems of equations derived with the PoME (Eq. S6)

$$\begin{cases} \frac{1}{L_m} = \frac{e^{\lambda(x_0+L_0)/2}}{e^{\lambda(x_0+L_m)} - 1} \\ \frac{e^{\lambda(x_0+L_m)} [\lambda(L_m+x_0) - 1] - e^{\lambda x_0} (\lambda x_0 - 1)}{\lambda (e^{\lambda(x_0+L_m)} - 1)} = K_v \left(\frac{\rho_s}{\rho_s - \rho} \right) \frac{\Omega L_0}{g \bar{\varepsilon} v_s} \end{cases} \quad (S6)$$

g (m s^{-2}) is the gravity, ρ (kg m^{-3}) is the density of water, ρ_s (kg m^{-3}) is sediment density, Ω ($\text{J s}^{-1} \text{m}^{-2}$) the stream power (Eq. S7) according to Bagnold (1977), v_s (m s^{-1}) is the sediment settling velocity and K_v is the delivery parameter related to surface conditions, which be calibrated or obtained as function of the parameters CP of the USLE. The system of Equations S6 allows us to obtain the two parameters necessary to calculate the SDR .

$$\Omega = \rho g S_0 R_H U \quad (S7)$$

S_0 (m m^{-1}) is the slope; R_H (m) the hydraulic radius that can be approximated to the flow depth for wide hills; and U (m s^{-1}) is the flow velocity. In his original work, de Araújo (2007) achieved good results (average absolute error 20%) with the model by using the average velocity for each event, given by Equation S8.

$$\bar{U} = \left(\frac{D}{H_e} \right)^{-1} \quad (S8)$$

H_e (mm) is the effective precipitation or total runoff and D (s) the total duration of the event. Hence, instead of requiring the knowledge of the complete hydrograph, we only need the information on the effective precipitation initiation and on its end, usually unavailable.

2.3 Gross Erosion Assessment

The Universal Soil Loss Equation (Wischmeier and Smith, 1978) is an empirical equation with simple implementation as expressed by the product below (Eq. S9):

$$\bar{\varepsilon} = R K L S C P \quad (S9)$$

R (rainfall and runoff factor or erosivity factor) represents the total energy of an event or a series of events which may produce erosion; K (erodibility factor) indicates how much the soil in the studied area is prone to be mobilised by the rain energy; LS (topographic factor) is the length factor and S the slope factor, directly connected to the topography; C (cover and management factor) is a measure of the effect of all cover and management variables, such as type and condition of vegetation and tillage practices; and P (management practice factor) accounts for good practices to reduce erosion, as contouring and terracing.

2.3.1 Erosivity Factor (R)

In order to calculate the gross erosion by employing the USLE we need to assess the erosivity value (R MJ ha⁻¹ h⁻¹). We used two approaches:

- i. Probabilistic approach

Based on measured data concerning sub-daily precipitation, we studied the best probabilistic distribution (uniform, gaussian, two-parameter gamma and beta distributions were tested) for the variable I_{30}/H . Using an estimated I_{30} (mm h⁻¹) we calculated the event erodibility using Equation S10

$$R = E I_{30} \quad (S10)$$

$$E = \begin{cases} 11.9 + 8.73 \log_{10} \bar{I} & \forall H < 76.2mm \\ 28.3 & \forall H \geq 76.2mm \end{cases} \quad (S11)$$

where E is a storm's kinetic energy, given by the Equation S10. In Eq. S11 above, H (mm) is the total precipitation and \bar{I} (mm h_{.1}) the average intensity. Note that we obtain \bar{I} as the ratio H/D .

- ii. Regional approach

Using measured data of rainfall intensities in a semiarid region (de Figueiredo et al., 2016), an equation for the monthly erosivity was calibrated. Events erosivity was obtained by distributing the months erosivity proportionally to the events total precipitation within the month (Eq. S12).

$$\begin{cases} R_m = \alpha \left(\frac{H_m^2}{H_a} \right)^\beta \\ R_{i,m} = \frac{R_m H_{i,m}}{H_m} \end{cases} \quad (\text{S12})$$

R_m is the months total erosivity, H_m the months total precipitation, H_a the average annual precipitation, and $R_{i,m}$ the erosivity of the i – th event of the month m , and $H_{i,m}$ the precipitation of the i – th event of the month m ; α and β are regional calibrated parameters equalling 565 and 0.42 respectively.

2.3.2 Erodibility factor (K)

Soil erodibility was estimated using the Soil Classification Maps of Brazil (IPECE, 2007) and the correspondent erodibility factor as obtained experimentally by Silva (1978).

2.3.3 Topography factor (LS)

The topography factor was calculated applying equation S13.

$$LS = 0.00984 L_r^{0.63} S^{1.18} \quad (\text{S13})$$

$$L_r = \frac{A_q}{4 \sum L_{den}} \quad (\text{S14})$$

where S is the slope in percentage and L_r is the average slope length, given by equation S14. A_q is the area of the pixel, sub-basin, or landscape unity and $\sum L_{den}$ the sum of all water paths within A_q .

2.3.4 Cover and management practice factor (CP)

We used satellite images (LandSat 8) and field surveys in order to identify the land use. From land use maps the parameter C was mapped using the values of table 8.8 of Haan et al. (1994,

p. 266). The practice factor P was assumed equals the unity, since no management practices were identified in the areas.

2.4 Runoff

To estimate the total runoff per event we used the Soil Conservation Service (1972) Curve Number method (Eq. S15). The CN value was estimated on the basis of land use, soil properties and antecedent moisture (Mishra and Singh, 2003). I_a accounts for all initial abstractions and S for the potential maximum retention of the catchment, all in millimetres. I_a is often represented as a fraction ϕ of S . In this study, ϕ was assumed equals 0.20 for all study areas. S is a function of CN (Eq. S16).

$$H_e = \frac{(H - I_a)^2}{(H - I_a + S)} \quad (\text{S15})$$

$$S = 25.4 \left(\frac{1000}{CN} - 10 \right) \quad (\text{S16})$$

The duration of the runoff was assumed to be equal to the duration of rainfall for the small catchments (< 10 hectares). For the medium, such as Aiuaba and Canabrava, field measurements suggest a duration, on average, 2.5 times longer than the rainfall (de Figueiredo et al., 2016) and for the larger catchments we used the Snyder (1938) Unit Hydrograph.

2.5 USLE Data

In Table S1 we present the values of the USLE parameters obtained accordingly to Wischmeier and Smith (1978). The parameter P was assumed equal to one, for no management practices were identified in the regions.

Table S1: Average characteristics of the study areas - LULC, area and USLE parameters

Name	Land Use	Area (km ²)	Slope (%)	K ^a	L (-)	S (-)	C (-)
Canabrava	Agriculture and open range cattle raising	2.9	6.6%	0.032	3.252	0.606	0.01
Aiuaba	Conservation area with native vegetation (Caatinga)	11.53	18.0%	0.015	3.16	1.944	0.0005
Várzea Volta	da Agriculture and open range cattle raising	155	22.1%	0.028	3.766	2.364	0.028
Acarape	Agriculture and open range cattle raising	208	10.1%	0.037	2.766	1.115	0.015
Sumé 2	Experimental area - Preserved vegetation (Caatinga)	0.0107	6.1%	0.021	1.126	0.523	0.008
Sumé 4	Experimental area - Degraded land without vegetation	0.0048	6.8%	0.021	0.848	0.64	1.000
Gilbués	Abandoned land under desertification process without vegetation	0.0004	15.6%	0.007	1.083	1.698	0.771

^a K in (Mg h MJ⁻¹ mm⁻¹)

3 Code - SYPoME

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1  PROGRAM SYPoME

!  PROGRAM TO SIMULATE SEDIMENT YIELD USING POME-EQUATION
!  1. VARIABLES DECLARATION

6  INTEGER nprec , iprec , ncell , icell , nev , iev , irep , i
   CHARACTER archivo1*20,archivo2*20
   CHARACTER*8, DIMENSION(10,3000) :: dia
   INTEGER, DIMENSION(10,3000) :: id
   REAL, DIMENSION(10,3000) :: D,dur ,R
11  COMMON /EVENTOS/ id ,D,dur ,R
   INTEGER, DIMENSION(100) :: igauge
   REAL ds , vs , A,K,CP,S0,S,w0,fL,L0,Kv
   COMMON /CELULAS/ ds , vs , A,K,CP,S0,S,w0,fL,L0,Kv,igauge

16 !  2. MAIN PROGRAM

   CALL ABERTURA(archivo1 ,archivo2 ,nprec ,ncell ,nev ,irep )

!  read rainfall-related data of the events
21  iprec = 0
   DO WHILE ( iprec .lt. nprec )
       iprec=iprec+1
       READ(20,*) i
       IF ( i.ne. iprec ) THEN
26         WRITE(*,*) ' Incompatibility between indexes of gauge stations !!!'
           WRITE(21,*) ' Incompatibility between indexes of gauge stations !!!'
       ENDIF
       WRITE(21,201) ' Precipitation gauge number ..... ',iprec
       WRITE(21,*) '-----'
31       WRITE(21,*) '   i   id   date   D(mm)   Dur(min)   R(MJ.mm/ha/h)   '
       WRITE(21,*) '-----'
       WRITE(*,201) ' Precipitation gauge number ....1..... ',iprec
       WRITE(*,*) '-----'
36       WRITE(*,*) '   i   id   date   D(mm)   Dur(min)   R(MJ.mm/ha/h)   '
       WRITE(*,*) '-----'
       iev = 0
       DO WHILE ( iev .lt. nev )
           iev=iev+1
           READ(20,*) id(iprec , iev), dia(iprec , iev),D(iprec , iev), dur(iprec , iev),R(iprec , iev)
41           WRITE(21,202) iev , id(iprec , iev), dia(iprec , iev),D(iprec , iev), +
               ENDDO
           WRITE(21,*) '-----'
           WRITE(*,*) '-----'
           ENDDO
46
!  read physiographic-related data of the cells and compute sediment yield

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SSY = 0
SGEr = 0
icell = 0
51 DO WHILE ( icell.lt.ncell)
    icell = icell+1
    READ (20,*) icell ,ds ,vs ,A,K,CP,S0,w0,Kv,igauge(icell)
    CALL CALCSY(icell ,nev ,SY ,GEr ,irep)
    SSY = SSY + SY
56    SGEr = SGEr + GEr
ENDDO

! close program
WRITE(21,203) ' Watershed gross erosion (kg) .....',SGEr
61 WRITE(21,203) ' Watershed sediment yield (kg) .....',SSY
WRITE(21,204) ' Watershed average delivery ratio .....',SSY/SGEr
WRITE(21,*)
WRITE(21,*) ' Program concluded successfully.'
WRITE(*,203) ' Watershed gross erosion (kg) .....',SGEr
66 WRITE(*,203) ' Watershed sediment yield (kg) .....',SSY
WRITE(*,204) ' Watershed average delivery ratio .....',SSY/SGEr
WRITE(*,*)
WRITE(*,*) ' Program concluded successfully.'
CLOSE(20)
71 CLOSE(21)
201 FORMAT (a50,i4)
202 FORMAT (i5,2x,i5,2x,a8,2x,f6.2,5x,f8.1,5x,f7.1)
203 FORMAT (a44,e10.4)
204 FORMAT (a44,f5.3)
76 END

! 3. SUBROUTINE THAT OPENS PROGRAM

SUBROUTINE ABERTURA(arquivo1 ,arquivo2 ,nprec ,ncell ,nev ,irep)
81
CHARACTER arquivo1*20,arquivo2*20,title*20
INTEGER nprec ,ncell ,nev ,irep

WRITE(*,*) ' SEDIMENT-YIELD ESTIMATION - SYPOME3'
86 WRITE(*,*)
WRITE(*,*) ' * Version 3'
WRITE(*,*) ' * SY equation based on the principle of maximum entropy'
WRITE(*,*) ' * Program can only compute up to 3000 events'
WRITE(*,*) ' '
91 WRITE(*,*) ' Universidade Federal do Ceara'
WRITE(*,*) ' Jose Carlos de Araujo'
WRITE(*,*) ' Technische Universitat Berlin'
WRITE(*,*) ' Pedro Alencar'
WRITE(*,*) ' 2019'
96 WRITE(*,*)

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WRITE(*,*) '-----'

WRITE(*,*) 'Type the name of the input file:'
READ(*,302) arquivo1
101 OPEN(20, file=arquivo1, status='old')
READ(20,*) title
! OPEN(20, file='in.txt', status='old')
WRITE(*,*)
WRITE(*,*) 'Type the name of the output file:'
106 READ(*,302) arquivo2
OPEN(21, file=arquivo2, status='new')
WRITE(*,*)
! OPEN(21, file='out.txt', status='new')
WRITE(*,*) 'Do you need a complete (1) or a simplified (2) report?'
111 READ(*,*) irep
IF(irep.ne.1.and.irep.ne.2) THEN
    WRITE(*,*) 'The number is not an option. Default (complete) report will be provided'
    irep = 1
ENDIF
116 ! irep = 2

WRITE(21,*) ' SEDIMENT-YIELD ESTIMATION - SYPOME3'
WRITE(21,*)
WRITE(21,*) ' * Version 3'
121 WRITE(21,*) ' * SY equation based on the principle of maximum entropy'
WRITE(21,*) ' * Program can only compute up to 3000 events'
WRITE(21,*) '
WRITE(21,*) ' Universidade Federal do Ceara'
WRITE(21,*) ' Technische Unibversitat Berlin'
126 WRITE(21,*) ' Jose Carlos de Araujo'
WRITE(21,*) ' Pedro Alencar'
WRITE(21,*) ' 2019'
WRITE(21,*)
WRITE(21,*) '-----'
131 WRITE(21,*) 'Title: ', title
WRITE(*,*) 'Title: ', title
WRITE(21,*) '-----'
WRITE(21,301) ' Input file ..... ', "default"
WRITE(21,301) ' Output file ..... ', "default"
136 WRITE(*,*) '-----'
WRITE(*,301) ' Input file ..... ', "default"
WRITE(*,301) ' Output file ..... ', "default"

READ(20,*) nprec
141 READ(20,*) ncell
READ(20,*) nev
WRITE(21,303) ' Number of precipitation gauges ..... ', nprec
WRITE(21,303) ' Number of cells ..... ', ncell
WRITE(21,303) ' Number of events ..... ', nev

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146 WRITE(21,*) '-----'
WRITE(*,303) ' Number of precipitation gauges ..... ',nprec
WRITE(*,303) ' Number of cells ..... ',ncell
WRITE(*,303) ' Number of events ..... ',nev
WRITE(*,*) '-----'
151
301 FORMAT (a50,a20)
302 FORMAT (a20)
303 FORMAT (a50,i4)
END
156
! 4. SUBROUTINE THAT COMPUTES SEDIMENT YIELD

SUBROUTINE CALCSY( icell ,nev ,SY,GEr, irep)

161 INTEGER icell ,nev ,iev ,irep
REAL SY,SYi,GEr,GEri ,beta
INTEGER, DIMENSION(100) :: igauge
REAL ds ,vs ,A,K,CP,S0,S,w0,fL,L0,Kv
COMMON /CELULAS/ ds ,vs ,A,K,CP,S0,S,w0,fL,L0,Kv,igauge
166
L0 = 10000*A/(2*w0)
IF (S0.lt.0.090) THEN
S = 10.8*SIN(ATAN(S0))+0.03
ELSE
171 S = 16.8*SIN(ATAN(S0))-0.50
ENDIF
beta = 11.16*SIN(ATAN(S0))/(3*(SIN(ATAN(S0))*0.8)+0.56)
fL = (L0/22.1)**(beta/(beta+1))

176 WRITE(*,400) ' Cell number ..... ',icell
WRITE(*,401) ' Area (ha) ..... ',A
WRITE(*,401) ' Soil density ( -) ..... ',ds
WRITE(*,401) ' Sedimentation velocity (m/s) ..... ',vs
WRITE(*,403) ' Drainage length w0 (m) ..... ',w0
181 WRITE(*,403) ' Slope length L0 (m) ..... ',L0
WRITE(*,401) ' Soil erodibility (ton.h/MJ/mm) ..... ',K
WRITE(*,402) ' Land-use factor CP ( -) ..... ',CP
WRITE(*,402) ' Average slope S0 ( -) ..... ',S0
WRITE(*,401) ' Slope factor S ( -) ..... ',S
186 WRITE(*,401) ' Slope length factor L ( -) ..... ',fL
WRITE(*,401) ' Vegetation parameter Kv ..... ',Kv

WRITE(21,400) ' Cell number ..... ',icell
WRITE(21,401) ' Area (ha) ..... ',A
191 WRITE(21,401) ' Soil density ( -) ..... ',ds
WRITE(21,401) ' Sedimentation velocity (m/s) ..... ',vs
WRITE(21,403) ' Drainage length w0 (m) ..... ',w0
WRITE(21,403) ' Slope length L0 (m) ..... ',L0

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196 WRITE(21,401) ' Soil erodibility (ton.h/MJ/mm).....',K
WRITE(21,402) ' Land-use factor CP (-).....',CP
WRITE(21,402) ' Average slope S0 (-) .....',S0
WRITE(21,401) ' Slope factor S (-).....',S
WRITE(21,401) ' Slope length factor L (-).....',fL
WRITE(21,401) ' Vegetation parameter Kv .....',Kv
201 WRITE(21,400) ' Number of rainfall station .....',igauge(icell)
IF (irep.eq.1) THEN
WRITE(21,*) '-----'
WRITE(21,*) ' id gross-er(kg) Stream-pw(J/s/m2) Lambda(1/m) Lm(m) SDR SY(kg/ha) '
WRITE(21,*) '-----'
206 ENDIF
SY = 0
GEr = 0
iev = 0
DO WHILE (iev.lt.nev)
211 iev=iev+1
CALL EVENT(icell,iev,GEr,SYi,irep)
GEr = GEr + GErI
SY = SY + SYi
216 ENDDO
WRITE(*,*) '-----'
WRITE(*,404) ' Total gross erosion (kg) in this cell ....',GEr
WRITE(*,404) ' Total sediment yield (kg) .....',SY
WRITE(*,405) ' Global sediment delivery ratio .....',SY/GEr
WRITE(*,*) '-----'
221 WRITE(21,*) '-----'
WRITE(21,404) ' Total gross erosion (kg) in this cell ....',GEr
WRITE(21,404) ' Total sediment yield (kg) .....',SY
WRITE(21,405) ' Global sediment delivery ratio .....',SY/GEr
WRITE(21,*) '-----'
226
400 FORMAT (a44,i6)
401 FORMAT (a44,f9.3)
402 FORMAT (a44,f9.4)
403 FORMAT (a44,f9.2)
231 404 FORMAT (a44,e10.4)
405 FORMAT (a44,f5.3)
END
! 5. SUBROUTINE THAT PROCESSES DATA FROM EACH EVENT
236
SUBROUTINE EVENT(icell,iev,GEr,SYi,irep)
INTEGER iev,irep,icell
REAL Lm,SDR,eps,erosion,streamp,f2,L2
241 REAL GEr,SYi
INTEGER, DIMENSION(100) :: igauge
REAL ds,vs,A,K,CP,S0,S,w0,fL,L0,Kv

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COMMON /CELULAS/ ds , vs , A, K, CP, S0 , S, w0, fL , L0, Kv, igauge
INTEGER, DIMENSION(10,3000) :: id
246 REAL, DIMENSION(10,3000) :: D, dur ,R
COMMON /EVENTOS/ id ,D, dur ,R

! id = event identity; D = runoff (mm/dur);
! dur = event duration (min); R = erosivity (MJ.mm/ha/h)
251

eps = R(igauge(icell),iev)*K*CP*S*fL/10
erosion = 10000*A*eps
GEri = erosion
streamp = 9807*L0*S0*(D(igauge(icell),iev)/1000)/(60*dur(igauge(icell),iev))
256 f2 = Kv*(ds/(ds-1))*streamp*L0/(9.807*eps*vs)

CALL PARAM(L0,Lm,L2,SDR,f2)
SYi = erosion*SDR
IF (irep.eq.1) THEN
261 WRITE(21,501) id(igauge(icell),iev),erosion,streamp,L2,Lm,SDR,SYi/A
ENDIF
501 FORMAT(i5,2x,e9.3,5x,e8.3,8x,e8.2,4x,f9.2,2x,f5.3,3x,f10.4)

END

266
! 6. SUBROUTINE TO COMPUTE VARIABLE SDR AND PARAMETERS Lm & L2

SUBROUTINE PARAM(L0,Lm,L2,SDR,f2)

271 INTEGER i1
LOGICAL run1
REAL L0,Lm,L2,SDR,f2
REAL Lm1,Lm2,Lm3,tol1,err1,nmax1
REAL*8 h1,h2,h3,a,b,aux_log

276

Lm1 = L0/100.
x0 = L0-Lm1
CALL Lambda(L0,f2,x0,Lm1,L2)
a = L2*(Lm1+x0)
281 b = L2*x0
h1 = log(a - 1. - (b - 1.)*exp(-L2*Lm1)) - log(f2*L2) - log(1. - exp(-a))

!print*,L2, f2, f2*L2, log(f2*L2)

286

Lm2 = 50*L0
x0 = 0.
CALL Lambda(L0,f2,x0,Lm2,L2)
a = L2*(Lm2+x0)
b = L2*x0
291 alfa = a/b
h2 = log(a - 1. - (b - 1.)*exp(-L2*Lm2)) - log(f2*L2) - log(1. - exp(-a))

```

```

i1 = 0
296  tol1 = 0.001
nmax1 = 100.
run1 = .TRUE.
DO WHILE (run1)
    i1 = i1+1
301
    Lm3 = (ABS(h1)*Lm2+ABS(h2)*Lm1)/(ABS(h1)+ABS(h2))
    x0 = MAX(0., L0-Lm3)
    CALL Lambda(L0, f2, x0, Lm3, L2)
    a = L2*(Lm3+x0)
306  b = L2*x0

    aux_log = (b-1)*exp(-L2*Lm3)
    aux_log = (a-1) - aux_log
    aux_log = abs(aux_log)
311

    h3 = log(aux_log) - log(f2*L2) - log(1. - exp(-a))
    IF(h3*h2 .le. 0.) THEN
        Lm1 = Lm3
        h1 = h3
316  ELSE
        IF(h3*h1 .le. 0.) THEN
            Lm2 = Lm3
            h2 = h3
        ELSE
321  IF (ABS(h1) .le. ABS(h2)) THEN
            Lm2 = Lm3
            h2 = h3
        ELSE
326  Lm1 = Lm3
            h1 = h3
        ENDIF
    ENDIF
    ENDIF
    err1 = ABS(h3)
331  IF (err1 .le. tol1 .or. i1 .ge. nmax1) THEN
        run1 = .FALSE.
    ENDIF
ENDDO
Lm = Lm3
336  x0 = max(0., L0-Lm)
    CALL Lambda(L0, f2, x0, Lm, L2)

    SDR = (L0-x0)/L0
    SDR = SDR*(fexp(L2*Lm)-L2*(L0-x0)/2.)
341  SDR = SDR/fexp(L2*(x0+Lm))

```

END

! 7. SUBROUTINE TO COMPUTE PARAMETER LAMBDA-2, GIVEN L0, f2 AND Lm

346

SUBROUTINE Lambda(L0, f2, x0, Lm, L2)

INTEGER i2

LOGICAL run2

351

REAL L0, f2, x0, Lm, L2

REAL xm, L21, L22, L23, tol2, err2, nmax2

REAL*8 g1, g2, g3, c1, c2, c3

i2 = 0.

356

nmax2 = 100.

tol2 = 0.001

xm = (x0+L0)/2.

361

L21 = (5E-8)/Lm

c1 = L21*(0.5*(L0-x0) + Lm)

g1 = log(L21*Lm) + c1 - log(1. - exp(-L21*(x0+Lm)))

L22 = 0.01

366

c2 = L22*(0.5*(L0-x0) + Lm)

g2 = log(L22*Lm) + c2 - log(1. - exp(-L22*(x0+Lm)))

i2 = 0.

run2 = .TRUE.

371

DO WHILE (run2)

i2 = i2+1.

L23 = (ABS(g1)*L22+ABS(g2)*L21)/(ABS(g1)+ABS(g2))

L23 = MAX(L23, (5E-8)/Lm)

c3 = L23*(0.5*(L0-x0) + Lm)

376

g3 = log(L23*Lm) + c3 - log(1. - exp(-L23*(x0+Lm)))

IF(g3*g2.1e.0.) THEN

L21 = L23

g1 = g3

381

ELSE

IF(g3*g1.1e.0.) THEN

L22 = L23

g2 = g3

ELSE

386

IF(ABS(g1).1e.ABS(g2)) THEN

L22 = L23

g2 = g3

ELSE

L21 = L23


```

391         g1 = g3
           ENDIF
       ENDIF
   ENDIF
   err2 = ABS(g3)
396   IF (err2 .le. tol2 .or. i2 .ge. nmax2) THEN
       run2 = .FALSE.
   ENDIF
ENDDO
!     requirement due to numerical stability
401   IF (L23*Lm .lt. 5E-8) THEN
       L23 = (5E-8)/Lm
   ELSE
       IF (L23*Lm .gt. 1.) THEN
406         L23 = 1./Lm
       ENDIF
   ENDIF
       L2 = L23
END
411
!     Function that computes approximation of exp(x) - 1 using McLaurin series
REAL FUNCTION fexp(x)
REAL x
416   fexp = x+(x**2)/2+(x**3)/6+(x**4)/24+(x**5)/120
END

```

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