# Canopy temperature and heat stress are increased by compound high air temperature and water stress, and reduced by irrigation $-\mathbf{A}$ modeling analysis

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Abstract. Crop yield is reduced by heat and water stress, and even more when these conditionsy co-occur. Yet, compound effects of air temperature and water availability on crop heat stress are poorly quantified: existing crop models, by relying at least partially on empirical functions, cannot account for the feedbacks of plant traits and response to heat and water stress on canopy temperature. We developed a fully mechanistic model coupling crop energy and water balances, to determine canopy temperature as a function of plant traits, stochastic environmental conditions—and—their variability; and irrigation applications. While general, the model was parameterized for wheat. Canopy temperature largely followed air temperature under well-watered conditions; but when soil water potential was more negative than -0.14 MPa, further reductions in soil water availability led to a rapid rise in canopy temperature—up to 10 °C warmer than air at soil water potential of -0.62 MPa. More intermittent precipitation led to higher canopy temperatures and longer periods of potentially damaging crop canopy temperatures. Irrigation applications aimed at keeping crops under well-watered conditions could reduce canopy temperature, but in most cases were unable to maintain it below the threshold temperature for potential heat damage; the benefits of irrigation in terms of reduction of canopy temperature became smallerdecreased as average air temperature increased. Hence, irrigation is only a partial solution to adapt to warmer and drier climates.

**Keywords.** Canopy temperature; heat stress; water stress; compound events; wheat; irrigation; soil water balance; canopy energy balance

#### 1 Introduction

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High and stable crop yield requires suitable climatic conditions throughout the growing season. Abiotic stressors, like water scarcity and high temperatures, can adversely affect crop growth, development, and yield, as shown by controlled-condition and field experiments, large scale surveys, and crop model applications (e.g., Zampieri et al., 2017; Daryanto et al., 2017; Kimball et al., 2016; Ray et al., 2015; Asseng et al., 2015). Both water and heat stress impair photosynthesis (Way and Yamori, 2014; Lawlor and Tezara, 2009), undermine crop growth (Hsiao, 1973; Hatfield and Prueger, 2015) and reproduction (Prasad et al., 2011), and hasten crop development and leaf senescence (Lobell et al., 2012), although the

30 physiological mechanisms can differ (Fahad et al., 2017). Heat and water stress do not only act independently but have also have compound effects on plant phenology and physiology, so that heat stress is more detrimental if co-occurring with water stress (Mahrookashani et al., 2017; Prasad et al., 2011; Suzuki et al., 2014; Cohen et al., in press). Yet, these compound effects of heat and water stress are seldom considered, experimentally and via models (Rötter et al., 2018).

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Climate change is projected to increase <u>air</u> temperatures and, in many regions, decrease growing season precipitation or lengthen dry spells (IPCC, 2013). Hot and dry summers are becoming more common (Zscheischler and Seneviratne, 2017; Alizadeh et al., 2020) and changes in climate are already reducing and will likely further reduce crop yield and its stability, and ultimately global food security (e.g., Challinor et al., 2014; Masson-Delmotte et al., 2018; Moore and Lobell, 2015; Rosenzweig et al., 2014). The frequency and severity of crop heat and water stress <u>is-are</u> directly affected by <u>air highhigh-air</u> temperature and <u>low-soil</u> water availability, and <u>is are indirectly driven by enhanced-evapotranspiration, which is enhanced from by warm temperatures. Nevertheless, how air temperature and precipitation, and their variability, interact in defining the occurrence, extent, and duration of crop heat and water stress has not been investigated in detail.</u>

Canopy temperature allows more accurate estimates of the consequences of heat stress on the crop and its yield than air temperature (Gabaldón-Leal et al., 2016; Siebert et al., 2014; Rezaei et al., 2015). Indeed, eCanopy temperature can deviate from air temperature under field conditions, because of the interplay among plant traits, plant water availability, air temperature and humidity, solar radiation, wind velocity, and the ensuing canopy microclimate (Michaletz et al., 2016; Schymanski et al., 2013). Considering canopy instead of air temperature is particularly important when characterizing the effects of compound heat and water stress, and the mitigating potential of irrigation against heat stress, because canopy temperature can be substantially higher than air temperature under water stress (e.g., Siebert et al., 2014).

Heat stress and damage are the result of complex and interacting plant physiological processes, depending on the temperature reached by the specific organ and the duration of the stress. Crop response to temperature is nonlinear (Porter and Gawith, 1999; Sanchez et al., 2014). Exceeding crop- and phenological developmental stage-specific thresholds can lead to plant tissue damage and halted physiological processes, although the plant can still survive. Also, the duration of exposure to high temperatures affects the outcome. For example, the accumulation of high temperature days negatively affected yield in rainfed systems (Schlenker and Roberts, 2009). In the face of increasing variability in the climatic conditions, we need to determine how stochastic precipitation and air temperature combine in determining canopy temperature. Average canopy temperatures and duration of periods above the threshold for damage can provide indications on the exposure of crops to potential heat stress.

Irrigation can buffer some aspects of climatic variability and extremes imposed on crop production (Tack et al., 2017; Zhang et al., 2015; Li and Troy, 2018; Vogel et al., 2019). Irrigation directly alleviates water stress by supplementing precipitation. Further, by sustaining the plant's evaporative cooling, irrigation can reduce canopy temperature and hence the consequences of high air temperature (Vogel et al., 2019; Siebert et al., 2017). In other words, by removing water stress, irrigation can also diminish the occurrence of heat stress. Nevertheless, we lack a quantification of how much irrigation can reduce the effects of unfavorable air temperature and precipitation, and the occurrence of crop heat stress and compound heat and water stress.

Canopy temperature is difficult to measure directly, although it can be estimated indirectly based on thermal imagery (e.g., Still et al., 2019). Models are a powerful tool to explore how canopy temperature changes with growing conditions and plant traits, beyond what is feasible via direct observations in specific experiments. Existing crop canopy temperature models either link canopy to growing conditions via simple empirical relations (e.g., Shao et al., 2019; Neukam et al., 2016) or model explicitly the leaf or canopy energy balance (Webber et al., 2016; Fang et al., 2014; Webber et al., 2017). But, so far, the role of plant water availability has been included only via semi-empirical corrections even in mechanistic models. For example, actual canopy temperature was calculated based on canopy temperatures under maximum and zero stomatal conductances and a crop water stress index (for a review of approaches and their performance, see Webber et al., 2018; Webber et al., 2017). Mechanistic models fully representing plant physiology can estimate crop canopy temperature that better reflects soil water and weather dynamics, and how plants respond to environmental conditions. Such models are currently lacking, but are necessary to quantify the effects of joint changes in air temperature and precipitation patterns; and the benefits of irrigation.

We developed a mechanistic model to estimate crop canopy temperature as a function of crop physiology, soil features, and (stochastic) climatic conditions, coupling the canopy energy balance and the water transport through the soil-plant-atmosphere continuum (SPAC), with stomatal conductance based on an optimality principle. We used the model in a case study – wheat grown in a temperate climate – to answer the following questions:

- What are the compound effects of soil water availability and air temperature on crop canopy temperature?
- How does precipitation pattern influence canopy temperature and its variability, and the duration of potentially damaging canopy temperatures?
- How effective is irrigation in reducing canopy temperature and the duration of potentially damaging canopy temperatures, depending on the climatic regimes?

# 2 Methods

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#### 2.1 Model description

To quantify the compound effects of air temperature and precipitation regimes on canopy temperature, and the potential of irrigation to reduce the occurrence of <u>crop</u> heat stress, we developed a <u>mechanistic process-based</u> model describing the coupled canopy energy and water balances, and their interactions with the water balance of the rooting zone. See the model structure in Fig<sub>2</sub> 1 and the Supplementary Information – SI – for details and symbols. The model allows exploring how plant traits and physiological responses to growing conditions interact with air temperature and soil water availability in defining canopy temperature, while relying on parameters with clear physiological meanings (Table S2).

To limit parameter and computational requirements, a minimalist approach was used, lumping the canopy in a 'big leaf' (Amthor, 1994; Jarvis and McNaughton, 1986; Bonan, 2019) and the soil water dynamics in a 'bucket-filling' model, with

95 instantaneous losses via runoff and percolation below the rooting zone (e.g., Milly, 1994; Rodriguez-Iturbe et al., 1999).

These simplifications are expected to have minor repercussions on our conclusions (see SI, Section S5).

As detailed in the SI, combining the canopy water and energy balance, the canopy temperature,  $T_c$ , can be obtained as

$$T_c = T_a + \frac{Q^{\downarrow} + B_{n,ref}^{\downarrow} - \lambda g_{v,c} D}{c_p g_{H,c} + \lambda g_{v,c} s_s + 4 \varepsilon_c \sigma T_a^3 \left[ 1 - \exp\left( -K_{bl,d} \ L_{AI} \right) \right]}. \tag{1}$$

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where  $T_a$  is the air temperature;  $Q^{\downarrow}$  the net absorbed short-wave radiation;  $B_{n,ref}^{\downarrow}$  the net absorbed long-wave radiation at  $T_a$  (isothermal radiation); D the atmospheric vapor pressure deficit;  $g_{v,c}$  and  $g_{H,c}$  the total canopy conductances to water vapor and heat respectively, which include stomatal and aerodynamic conductances;  $\lambda$ ,  $c_p$ ,  $\varepsilon_c$ ,  $\sigma$ , and  $K_{bl,d}$  are constants (Table S1);  $s_s$  the slope of the vapor pressure vs. temperature curve, dependent on  $T_a$ ; and  $L_{AI}$  the leaf area index.

We explicitly included the dependence of stomatal conductance on environmental conditions and plant physiology exploiting an optimality principle: plants are assumed to maximize carbon uptake over a given period, subject to limited water availability (Mäkelä et al., 1996; SI, Eq. S9-S11). We chose this approach because it is simple yet based on an evolutionary principle; and has led to promising results (Buckley et al., 2017; Eller et al., 2020). Many Differently from other stomatal optimization models based on water use efficiency assume that photosynthesis is limited either by RuBisCO or electron transport rate. To avoid this a priori<sub>3</sub> assumption, we approximated the original Farquhar et al. (1980) model for the photosynthetic rate was approximated with a hyperbolic function that includes both links RuBisCO and electron transport rate limitations while retaining the same physiological parameters of Farquhar's model (Vico et al., 2013). This model was further developed here to account for the effects of the leaf boundary layer conductance and day respiration, and the key stomatal and non-stomatal effects of limited water availability on marginal water use efficiency and metabolic activity (Zhou et al., 2013; Manzoni et al., 2011; Vico and Porporato, 2008; see SI Section S1.2.1 for details). The results obtained with an alternative, empirical model of canopy conductance parameterized with eddy covariance data (SI, Eq. S30-S32; Novick et al., 2016) further support our mechanistic approach. But they Those result also highlighted the need to explicitly represent canopy gas exchanges to capture the dependence of canopy temperature on air temperature, unless site- and crop-specific data are available to determine the canopy conductance empirically (SI, Fig. S69). Finally, aerodynamic conductances to heat and vapor were determined based on wind velocity, U, and leaf width, via well-established semi-empirical relations describing heat and mass transport inside the leaf boundary layer and to the bulk atmosphere (SI, Sections S1.2.2 and S1.2.3).

The canopy conductances affect and are affected by the soil water balance and water transport along the SPAC. On the one hand, soil water potential influences leaf water potential and hence leaf physiological activities (stomatal conductance, metabolic rates, and marginal water use efficiency). On the other hand, stomatal conductance and atmospheric water demand drive the rate of canopy water losses and hence the decline of soil water content. We represented the soil water content as soil saturation, s (0 ≤ s ≤ 1; soil moisture hereafter), linked to soil water potential, ψ<sub>s</sub>, via texture-dependent soil water retention curves (SI, Eq. S24). A bucket-filling model was used to describe the soil moisture dynamics, with precipitation

and irrigation as input and evapotranspiration, deep percolation below the rooting zone and <u>superficial surface</u> runoff as losses, but neglecting the root structure, the time needed for the water to be redistributed within the soil, and lateral soil water movements (SI Section S1.3.1; Vico and Porporato, 2010). The soil water balance was coupled to a minimalist description of water transport through the SPAC, to determine the leaf water potential. The SPAC was modeled as a series of conductances, from the soil, through the plant, to the atmosphere (SI, Section S1.3.2; Manzoni et al., 2013).

These model components provide conductances and boundary conditions to apply Eq. (1) and quantify how canopy temperature,  $T_c$ , changes with environmental conditions and management: air temperature and humidity, wind velocity, incoming solar radiation, and precipitation; and irrigation applications, if any. The model needs to be solved iteratively (Fig. 1). At each time step (a day; see Section 2.23), the model considers the previous soil moisture and current atmospheric conditions; The previous canopy temperature and water potential are used as initial guesses for the numerical integration. First, the model determines the canopy boundary layer and aerodynamic bulk conductances and water supply and demand. Then, the canopy water potential  $\psi_c$  is determined iteratively by equating water supply and demand. After convergence is reached on  $\psi_c$ , the canopy energy balance is used to determine iteratively  $T_c$ . Finally, the soil water balance is updated with inputs and losses cumulated over the time step.

# 2.2 Metrics of potential heat stress damage

Based on  $T_c$ , we derived two metrics representing the potential for heat stress damage: i)  $T_{c,mean}$ , the mean canopy temperature during a specific period (anthesis; see Section 2.32); and ii)  $P_{CHS}$ , the fraction of days during such period when  $T_c$  exceeded the crop-specific threshold  $T_{th}$ , above which detrimental effects of crop heat stress are likely.  $P_{CHS}$  is thus a measure of the duration of the detrimental conditions, while  $T_{c,mean}$  quantifies the level of detrimental conditions.

# 2.23 Case study

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While the model is of general applicability, we focused on the case of wheat (*Triticum aestivum*) — a staple crop with relatively low tolerance to high temperatures when compared with other crops (Sanchez et al., 2014) — grown at 45 ° latitude N. All the model parameters are summarized in the SI, Table S2.

We restricted our analyses to anthesis, when wheat is most vulnerable to heat (Porter and Gawith, 1999) and water (Daryanto et al., 2017) stress. Anthesis was assumed to last 21 days (Mäkinen et al., 2018), starting at <a href="the-140th">the-140th</a> day of the year, i.e., <a href="mailto:May 20th">May 20th</a> (in line with observations and simulations at the latitude selected; Semenov et al., 2014; Bogard et al., 2011). For simplicity, the timing and length of anthesis <a href="was-were">was-were</a> kept constant under all <a href="mailto:air-temperatureclimatic">air-temperatureclimatic</a> scenarios <a href="mailto:and-negardless">and regardless of irrigation applications</a>.

The model is capable of simulating the diurnal course of the key variables, but, for simplicity, we focused on the central part of the day, when incoming short-wave radiation at the top of the canopy  $Q_0^{\downarrow}$  and air temperature  $T_a$  are at or near their daily

maxima, and  $T_c$  is expected to peak. Wind velocity U was assumed to be at the lowest end of its realistic range and  $Q_0^{\downarrow}$  that of clear sky conditions, thus providing the maximum expected  $T_c$  and a conservative estimate of the frequency of occurrence of potentially damaging temperatures.

While the model can be driven by mMeasured environmental conditions relative to a specific location could be used to force the model. Yet, here to systematically explore several climate scenarios, we employed synthetically generated environmental conditions, varying their parameters to systematically explore several climate scenarios. Daily precipitation was idealized as a marked Poisson process (Rodriguez-Iturbe et al., 1999), i.e., exponentially distributed interarrival times, with the average frequency λ<sub>p</sub>. Event depth was also assumed to be exponentially distributed, with average α<sub>p</sub> (SI, Section S1.4.2). The variability of T<sub>a</sub> around its long-term average μ<sub>Ta</sub> was described via an Ornstein-Uhlenbeck process (SI, Section S1.4.3; Benth and Benth, 2007). In line with the focus on the warmest part of the day, T<sub>a</sub> is to be interpreted as the maximum daily air temperature. Finally, U, Q<sub>0</sub><sup>1</sup>, and RH were assumed to be constant during the simulations (SI, Table S2), whereas air water vapor pressure, e<sub>a</sub>, and vapor pressure deficit, D, were calculated based on T<sub>a</sub> (Campbell and Norman, 1998).

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As baseline pedoclimatic conditions, we considered a sandy loam soil, average precipitation frequency  $\lambda_p$  of 0.2 d<sup>-1</sup>, average event depth  $\alpha_p$  of 8.2 mm (corresponding to an average annual precipitation total of 600 mm), long-term average air temperature  $\mu_{T_a}$  of 25 °C, air temperature standard deviation of 3.6 °C, air relative humidity *RH* of 40%, wind velocity *U* of 4 m s<sup>-1</sup>, and net incoming short-wave radiation  $Q_0^{\downarrow}$  of 800 W m<sup>-2</sup>. We also explored additional pedoclimatic conditions. Specifically, we considered more extreme precipitation scenarios, comprising increasing precipitation due to from increasing precipitation frequency; and a constant average annual precipitation total, but more intermittent precipitation, with reduced average precipitation frequency ( $\lambda_p$ =0.07 d<sup>-1</sup>) and increased average event depth ( $\alpha_p$ =23.5 mm). Long-term average air temperature  $\mu_{T_a}$  also of 20 and 30 °C were explored. Separate sensitivity analyses were run for the standard deviation of air temperature (SI, Fig. S36), soil texture (SI, Fig. S74), and *U*,  $Q_0^{\downarrow}$ , and *RH* (SI, Fig. S58).

For the irrigated case, a demand-based (water) stress-avoidance irrigation was considered, whereby an irrigation application is wais triggered whenever soil water potential reached the intervention point,  $\tilde{\psi}_s$  (Vico and Porporato, 2011). To ensure well-watered conditions,  $\tilde{\psi}_s$  was set to -0.07 MPa, i.e., just above the incipient water stress for wheat (-0.1 MPa; Kalapos et al., 1996). Each irrigation application restored a pre-set target soil water potential,  $\hat{\psi}_s$ , set at -0.01 MPa. The difference between the intervention point and the target soil water potential is large enough to allow the use of a traditional irrigation technology (e.g., sprinkler systems or surface irrigation; see Vico and Porporato, 2011 and references therein).

Finally, the crop- and phenological developmental-stage specific temperature threshold above which detrimental effects of crop heat stress are likely,  $T_{th}$ , was set equal to the maximum baseline temperature during anthesis.  $T_{th}$  is a large source of large uncertainty, when aiming at defining the occurrence of crop heat stress and its consequences on the crop and final yield (Siebert et al., 2017; Wanjura et al., 1992). Even within a specific developmental stage, there is a large variability of reported baseline and optimal temperatures, because of differences in variety, growing conditions, and experimental approach.

Further, crop's baseline and optimal temperatures are often defined based on air temperature, although plants respond to canopy or even organ temperature. As <u>discussed\_showed\_below</u>, the differences between air and canopy temperatures can be large, in particular under limited plant water availability. To make the comparison between  $T_c$  and  $T_{th}$  meaningful, <u>here\_we</u> considered a maximum baseline temperature obtained under well-watered conditions and low D; and set  $T_{th}$  equal to 30 °C (Saini and Aspinall, 1982). This value is <u>in agreement\_with\_similar to</u> those obtained in other experiments focusing on wheat (Porter and Gawith, 1999).

#### 2.43 Statistical tests

The simulated canopy temperatures were not normally distributed, according to the Anderson-Daring test (p<0.05). Hence, to test if median  $T_{c,mean}$  and  $P_{CHS}$  differed across scenarios, we employed the Mood<sup>2</sup>s test; and to test the difference in their variances, we used the Brown-Forsythe<sup>2</sup>s test. The test results are summarized in SI Tables S3-S8. Differences are commented on when p<0.05.

# 3 Results

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The stochasticity of air temperature,  $T_a$ , and precipitation occurrence was mirrored by the erratic variations of soil moisture, s, and canopy temperature,  $T_c$ , in the numerically simulated trajectories (exemplified in Fig. 2).  $T_c$  largely followed  $T_a$ , but s determined whether  $T_c$  was near or above  $T_a$ . Under well-watered conditions, when s ensured unconstrained transpiration,  $T_c$  was similar to or even occasionally lower than  $T_a$ ; whereas when s decreased,  $T_c$  became warmer than  $T_a$  (after approximately day 12 in Fig. 2). The evolution of  $T_c$  and other key physiological state variables, including stomatal conductance, photosynthesis and canopy water potential, during a dry down is reported in the SI, Fig. S1.

Despite the complex mechanisms linking  $T_a$  and plant water availability to  $T_c$ , the resulting temperature difference  $T_c - T_a$  followed a relatively simple pattern (Fig. 3). When s was above 0.34 (corresponding to  $\psi_s$ =-0.14 MPa for the soil chosen),  $T_c$  was within 1 to 2 °C of  $T_a$ , with  $T_c < T_a$  for  $T_a > 25$  °C. Conversely, for s < 0.34,  $T_c - T_a$  increased as s declined, with increasing slope, from 1 °C at s=0.34 to 10 °C at s=0.25 (corresponding to  $\psi_s$ =-0.62 MPa); and  $T_c - T_a$  was independent of  $T_a$  (i.e., under water stress  $T_c - T_a$  is driven by soil water availability for evaporative cooling). Hence, high  $T_c$  could be caused by high  $T_a$  or low s or their combination. The dependence of the plant's physiological state variable on s is reported in the SI, Fig. S2, for set  $T_a$ .

Temperature and precipitation patterns interacted in defining the mean\_canopy temperature during anthesis,  $T_{c,mean}$ . Increasing average precipitation totals decreased median  $T_{c,mean}$  (colors in Fig. 4, SI Table S3, S4), in particular at lower precipitation totals (red in Fig. 4) and higher long-term mean\_average air temperature  $\mu_{T_a}$  (right in Fig. 4).  $T_{c,mean}$  was less affected by annual average precipitation totals larger than 900 mm and  $\mu_{T_a}$  at 20 °C.  $T_{c,mean}$  variability increased with  $\mu_{T_a}$  and, to a lesser extent, with decreasing average precipitation totals (SI<sub>a</sub> Table S3, S4).

- Precipitation regimes affected median of  $T_{c,mean}$  and its variability even when considering the same precipitation total but different average precipitation frequencies,  $\lambda_p$  (and hence event depths,  $\alpha_p$ ; Fig. 5, top). When compared with the baseline precipitation scenario (red bars), larger but more intermitteentd events (i.e., lower  $\lambda_p$  and higher  $\alpha_p$ ; violet bars) resulted in higher  $T_{c.mean}$  median and variability in rainfed cropping (SI, Table S5). The median of  $T_{c.mean}$  increased with  $\mu_{T_a}$  regardless of rainfall pattern, whereas the variance increased in the baseline rainfed scenario, except under more intermittent precipitationwas not significantly affected (Table S6).
  - Irrigation reduced median and variance of  $T_c$  with respect to rainfed cropping under the same climatic scenario (red vs. blue hues in Fig. 5, top). Also, the dependence of  $T_c$  on precipitation pattern was reduced with irrigation (SI, Table S5). Yet, even despite the with-irrigation, median and variability of  $T_c$  increased with  $\mu_{T_a}$ , (SI, Table S6), although such the increase in median  $T_c$  was less marked than that under rainfed cropping (SI, Table S6).
- Irrigation applications reduced the fraction of days during which  $T_c$  was above the threshold temperature for potential heat damage,  $T_{th}$ , i.e., of likely crop heat stress ( $P_{CHS}$ ; Fig. 5 bottom). But it could not completely prevent this occurrence (i.e., median  $P_{CHS} > 0$ ), except for  $\mu_{T_a} = 20$  °C. Among the climatic scenarios considered, the largest mean\_median\_reduction in  $P_{CHS}$  (100%) occurred at  $\mu_{T_a} = 20$  °C, and the smallest (between\_503%\_ and 58%) in the more intermittent precipitation scenario at  $\mu_{T_a} = 30$  °C (Table 1).
- Increasing air temperature variability left median and variance of  $T_{c,mean}$  unaltered in rainfed cropping, but increased them in irrigated cropping (SI, Fig. S36 top and Table S7). There, the removal of water stress via irrigation madeked the resulting canopy temperature more sensitive to the air temperature regime. The median and variance of  $P_{CHS}$  increased with temperature variability, except the variance under the more intermittent rainfed scenario in the irrigated cropping (Fig. S63 bottom, Table S7). Finer soil texture did not affect  $T_{c,mean}$  and  $P_{CHS}$ , although the difference between rainfall scenarios remained (Fig. S4 and Table S8). Also incoming short-wave radiation  $Q_0^1$ , wind velocity U, and air relative humidity RH affected  $T_c$  (Fig. S58). An increase of  $Q_0^1$  increased  $T_c$ , in particular at S < 0.35. Decreasing U enhanced  $T_c$  for S < 0.35, but did not affect it when S > 0.35. In contrast,  $T_c$  slightly increased with RH for S > 0.35, but showed no response to it when S < 0.35. Finer soil texture did not affect  $T_{c,mean}$  and  $T_{c,mean}$  of reduced losses via deep percolation and runoff and stabilized soil moisture with deepening roots (Laio et al., 2001) are negligible (not shown).

#### 4 Discussion

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#### 4.1 Soil water availability and air temperature jointly affect canopy temperature

We quantified the compound effects on canopy temperature of environmental conditions: air temperature, soil water availability, incoming short-wave radiation, wind velocity, relative humidity, soil texture, and irrigation. Our model is an improvement with respect to existing approaches to simulate canopy temperature in agricultural systems, which rely on empirical corrections of values determined by means of the energy balance under extreme conditions (Fang et al., 2014; Webber et al., 2016). Lacking adequate modelling tools has limited our ability to effectively quantify the likelihood and extent of potential heat damage to crops; and the potential improvements by irrigation.

The role of environmental conditions is mediated by plant physiology and its response to conditions. Indeed losses via evapotranspiration dominated the soil water balance in all the climatic scenarios explored (see SI, Section S3.1). But, despite the complex mechanisms behind canopy temperature, the resulting pattern was relatively simple. Canopy temperature increased from cooler temperatures and wetter soils to warmer and drier conditions (Fig. 3). Under well-watered conditions, some thermoregulation occurred, cooling down or warming up the canopy depending on the air temperature, to ensure the canopy was near optimal temperature for photosynthesis (Michaletz et al., 2016).; †This thermoregulation capability was lost when low water availability limited evaporative cooling. The differences of canopy and air temperatures obtained with provided by the model are in line with experimental observations and other model results, thus lending support to our approach. In wheat, for example, daily maximum or mid-day canopy temperature was 2 to 10 °C higher warmer than air temperature under water stress, and from 1-to-2 °C warmer to up to 6\_°C cooler than air temperature under well-watered condition, among field observations - and model results (Pinter et al., 1990; Rashid et al., 1999; Jensen et al., 1990; Howell et al., 1986; Ehrler et al., 1978; Balota et al., 2008; Neukam et al., 2016; Webber et al., 2016; Schittenhelm et al., 2014; Webber et al., 2018; Mon et al., 2016). Our simulations led to canopies being 2 to 10 °C warmer than air under water stress, and to a cooling effect of 1 to 2 °C under warm but well-watered conditions. Differences between model results and observations can be ascribed to cultivar-specific traits, approach to measuring canopy temperature, measurement timing and position (within or just above the canopy), and environmental conditions (e.g., solar radiation, soil texture). Some of these aspects can be accounted for by the model, by adjusting the parameters to the specific crop and variety, and environmental conditions.

The difference between canopy and air temperature was higher than, and independent of, air temperature when soil water potential was below a critical value (Fig. 3). This threshold-like response mirrors that of stomatal closure and plant transpiration reduction with water stress (for wheat, e.g., Sadras and Milroy, 1996; Shen et al., 2002; Wang et al., 2008; Wu et al., 2011; Kalapos et al., 1996). Yet, no threshold for stomatal closure was imposed *a priori* in the model. The emerging threshold of soil water potential (-0.14 MPa) is comparable with the soil water potential corresponding to incipient stomatal closure in some experiments (-0.1 MPa; Kalapos et al., 1996), but lower-higher than those of others (between -0.27 and -0.35).

# 4.2 More intermittent precipitation and higher air temperature increase canopy temperature

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Climate change is expected to alter both air temperature and precipitation regimes, with further increases in average and extremely high air temperatures, and, in some regions, scarcer or more intermittent precipitation, i.e., longer dry spells (IPCC, 2013). Co-occurring dry and hot extremes are becoming increasingly frequent (Alizadeh et al., 2020; Zscheischler and Seneviratne, 2017). We showed that these compound changes can increase canopy temperature and its variability (Fig. 4 and 5).

For set air temperature conditions, even with same average precipitation totals, less frequent but larger precipitation events increased median and variance of canopy temperature, as well as the fraction of days during which the temperature threshold for potential heat damage was exceeded (Fig. 5). Larger, less frequent precipitation events result in enhanced losses via runoff and percolation below the rooting zone, thus reducing plant water availability; the ensuing (longer) dry down can thus lead to lower soil moisture levels, potentially enhancing canopy temperature. This result points to the importance of considering not only seasonal precipitation totals but also their timing. Indeed, reductions in the number of rainy days have already reduced crop yield, and could even override the benefits of increased total precipitation (Ram, 2016). For set precipitation regime,

Aan increase in the long-term average air temperature resulted not only in a\_higher mean canopy temperature during anthesis, as expected (Eq. 1), but also in a larger variability of such mean (Fig. 4 and 5). Even the extent of changes in mean canopy temperature during anthesis caused by alterations of the precipitation regimes depended on average air temperature (Fig. 5). Intermediate mean air temperature resulted in the largest response of mean canopy temperature to changes in precipitation frequency under constant average precipitation totals (Fig. 5). These complex, compound effects show that it is necessary to explicitly consider not just the means but also the timing and variability of air temperature and precipitation, and their joint effects, when quantifying the potential of climate change to cause crop heat stress. Hence, models accounting in full for the stochasticity of environmental conditions are needed.

Crops are also faced by increasing air carbon dioxide (CO<sub>2</sub>) concentration. While this further global change was not explored here, we speculate that an increase in air CO<sub>2</sub> concentration could reduce stomatal conductance and hence thus enhance canopy temperature, all the other conditions being the same. But reduced stomatal conductance can also reduce the rate of soil water storage depletion and hence thus the maximum canopy temperature reached during a dry down. The net results of an increase in air CO<sub>2</sub> concentration is are thus expected to be small. Indeed, air CO<sub>2</sub> concentration of 200 to 220 ppm above ambient increased canopy temperature only of up to 1 °C in Free Air CO<sub>2</sub> Enrichment experiments and in model simulations (Webber et al., 2018); and a weak reduction of yield loss to heat with enhanced CO<sub>2</sub> is expected (Schauberger et al., 2017).

#### 4.3 Irrigation reduces but does not cancel the risk of heat stress

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By reducing the occurrence and extent of water stress, irrigation could lower canopy temperature, and its variability, as well as the frequency of it exceeding the threshold for potential heat damage (Fig. 5). Irrigation can have positive effects on yields, not only by reducing water stress but also heat stress. Indeed, canopy-to-air temperature difference is well correlated with final yield (e.g., Blum, 1996; Reynolds et al., 1994; Thapa et al., 2018), except under extremely dry conditions (Schittenhelm et al., 2014); and often used for cultivar selection (Graß et al., 2020; Munns et al., 2010).

The extent of the reduction in canopy temperature and hence of the occurrence of potential heat stress even under stress-avoidance irrigation depended on precipitation regime and long-term average air temperature. Irrigation was particularly is reduction waseffective in reducing canopy temperature and the duration of potentially damaging conditions particularly marked at lower long-term average air temperature; for set long-term average air temperature, irrigation was slightly more effective and under more intermittent precipitation (Error! Reference source not found.(Table 1). Yet, irrigation aiming at maintaining the plants under well-watered conditions could not completely remove the possibility that canopy temperature exceeded the temperature threshold for potential heat damage, except under the coolest air temperature scenario. Further, the benefits of irrigation became smaller as air temperature increased. Irrigation could also have indirect effects on canopy temperature. At the regional scale, irrigation, by enhancing evaporation, can further reduce air temperature (e.g., Sacks et al., 2009; Lobell et al., 2008a) and canopy temperature, while lengthening developmental stages. These effects could be included by altering the air temperature regime (see Fig. 3 and 4 and Table 1 for the effects of average air temperature) and the duration of the anthesis.

The risk of canopy temperature exceeding the temperature threshold for potential heat damage under (water) stress avoidance irrigation can be interpreted as the potential heat stress attributable only to air temperature. This is because no limitation to evaporative cooling is expected under the imposed irrigation scenario, where the soil water potential triggering an irrigation application was less negative that the critical soil water potential emerging from Fig. 3. The reduction of the fraction of time when canopy temperature is above the threshold for potential heat damage obtained via irrigation (Table 1) is a measure of the relative role importance of air temperature and water stress in defining high canopy temperatures, thus disentangling their relative importance. In addition, for the most effective use of the available water resources against heat stress, the emerging threshold of soil water potential that limits water-stress induced high canopy temperatures (Fig. 3) could be used to define a crop-specific irrigation intervention point for irrigation. Maintaining the soil water potential above that threshold would require additional water resources while leading to marginal further cooling effects, i.e., little advantage in staving off heat stress.

Irrigation could not fully eliminate the negative effects of heatwaves and the warmer conditions expected in the future.-<u>But a wide-spread use of irrigation could directly or indirectly mitigate the effects of heatwaves (van der Velde et al., 2010).</u>

<u>Nevertheless, Eeven for air temperatures for which irrigation can reduce the potential for heat stress damage and considering temperatures.</u>

345 these regional effects, expanding irrigation to mitigate the effects of high canopy temperatures can be unadvisable or impossible, due to physical or economic water scarcity (Rosa et al., 2020), already unsustainable exploitation of water resources (Wada et al., 2010), or the negative impacts of irrigation on soil salt content and nearby water bodies (Daliakopoulos et al., 2016; Scanlon et al., 2007). Other management approaches are thus needed to limit the potential for crop heat stress, in particular under high average air temperatures (Deryng et al., 2011; Lobell et al., 2008b). Examples are shifting to more heat-tolerant cultivars and species (Tack et al., 2016); altering the sowing date (Lobell et al., 2014; Mourtzinis et al., 2019); or migrating crops (Sloat et al., 2020) so that anthesis occurs when air temperature is, on average, lower.

# **5 Conclusions**

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Longer dry spells and high <u>air</u> temperatures are expected to become even more frequent in the future, with potential negative and compound <u>ed</u> effects on crop development and yield. Exploring the occurrence and severity of crop heat stress requires quantifying canopy temperature and considering under which conditions it exceeds the temperature threshold known to create appreciable damage. We developed a mechanistic model to determine canopy temperature, based on the explicit coupling of the soil water dynamics with the canopy energy balance, and an optimality principle <u>for stomatal functioning</u>, mechanistically accounting for plant physiology and its response to (stochastic) environmental conditions.

Using wheat as a case study, we explored how canopy temperature and its variability changed with stochastic air temperatures and precipitation, in rainfed and irrigated cropping. When soil water potential-was less negative than -0.14 MPa, the additional benefit of an increase in soil water availability and hence potential evaporative cooling became marginal; and thermoregulation ensured semi-optimal leaf temperature. However, canopy temperature rose rapidly above air temperature when soil water potential was less than -0.14 MPa, due to lowered evaporative cooling.

Less frequent and more intense precipitation caused more variable soil water contents, leading to higher and more variable canopy temperatures, and a higher fraction of days when the temperature threshold for potential heat stress damage was exceeded. Larger precipitation totals and irrigation applications could reduce the occurrence of high canopy temperature and the potential for heat damage. Yet, irrigation could not completely remove the risk of crop heat stress when long-term mean average air temperature was 25 °C or higher, calling for alternative management solutions.

Accurate estimates of canopy temperature are necessary to assess the role of precipitation and air temperature patterns in defining the risk of <u>crop</u> heat stress, and evaluate the mitigation potential of irrigation. Mechanistic models explicitly linking plant physiology to environmental conditions also allow exploring the effects of plant traits on the occurrence and extent of water and heat stress. As such, these models can support management decisions, from irrigation applications to identifying crops able to avoid heat stress.

Code availability. The MATLAB code of the model will be made available through a public repository upon acceptance of this manuscriptThe code is available upon request, by contacting the corresponding author.

Data availability. Data for model parameterization are available in the cited literature.

*Author contributions*. GV conceived the idea. XL and GV developed the codes of the model. XL performed the analyses and created the figure. XL and GV wrote the manuscript. GV revised the manuscript.

Competing interest. The authors declare that they have no competing interests.

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Table 1: Reduction in the potential for heat stress by irrigation, as summarized by the  $\frac{\text{mean-}\underline{\text{median}}}{\text{reductions}}$  reductions of  $P_{CHS}$  from rainfed cropping to stress avoidance irrigation, using rainfed as reference.

	Baseline precipitation	More intermittent
	regime	precipitation
$\mu_{T_a}$	$(\alpha_p = 8.2 \text{ mm-};$	$(\alpha_p = 23.5 \text{ mm-};$
(°C)	$-\lambda_p = 0.2 \text{ d}^{-1}$	$-\lambda_p = -0.07 \text{ d}^{-1}$
20	100%	100%
25	78%	8 <u>0</u> 2%
30	53%	5 <u>8</u> 0%

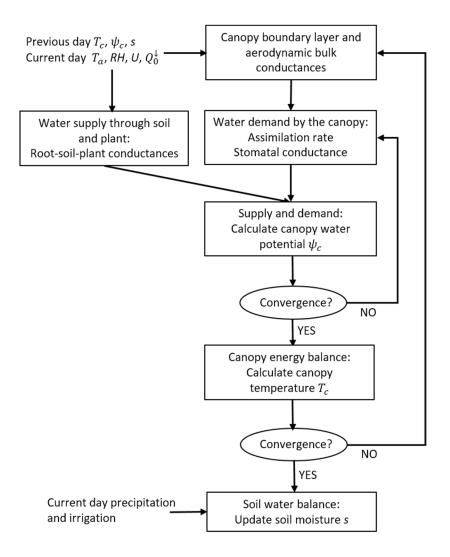


Figure 1: Flow diagram of the determination of canopy temperature and soil moisture dynamics.

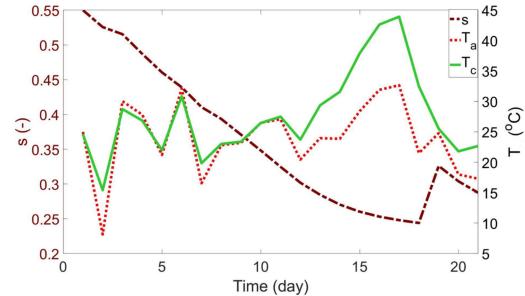


Figure 2: Example of numerically generated time series of soil moisture (s; dot-dashed burgundy line), air temperature ( $T_a$ ; dotted red line), and canopy temperature ( $T_c$ ; solid green line), for rainfed cropping. The left axis represents soil moisture, the right axis temperature. The model was run for 21 days with the baseline environmental conditions. Parameter values are listed in Table S2.

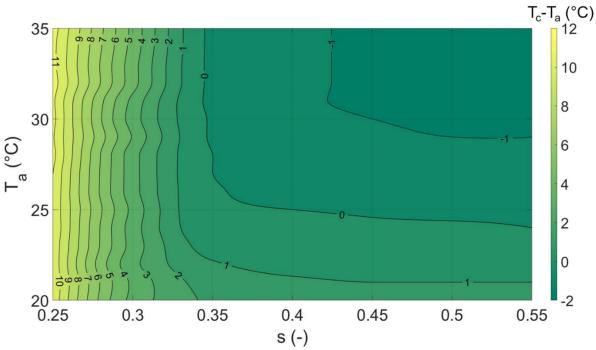


Figure 3: Canopy-air temperature difference,  $T_c - T_a$  (colors and contour lines), as a function of soil moisture (s; x-axis) and air temperature ( $T_a$ ; y-axis) for a sandy loam. All other parameters are summarized in Table S2.

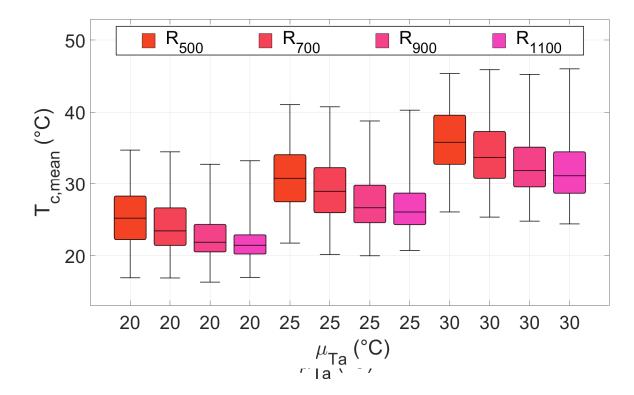
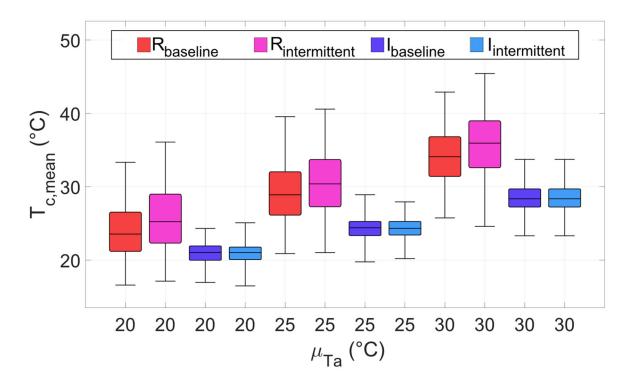
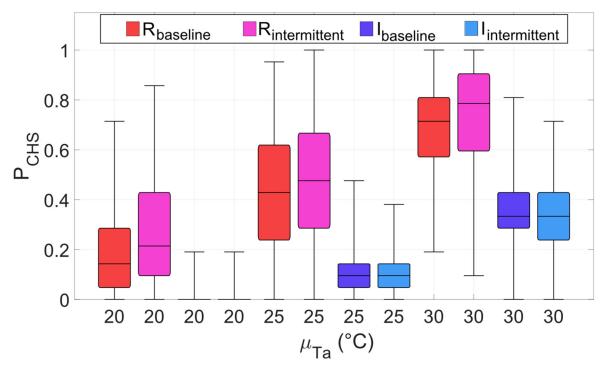
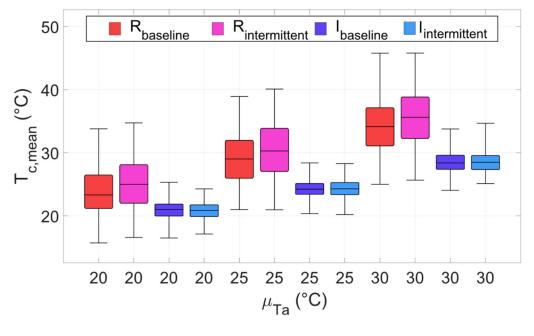


Figure 4: Distribution of mMean canopy temperatures during anthesis,  $T_{c,mean}$ , for four average annual precipitation totals (500, 700, 900, 110 mm; colors) and three long-term average air temperatures  $\mu_{T_a}$  (20, 25 and 30 °C; x-axis). Average precipitation depth  $\alpha_p$  was kept at 15 mm, while average precipitation frequency  $\lambda_p$  changed within each group of 4 boxes, from 0.091 to 0.137, 0.183, and 0.228 d<sup>-1</sup> (left to right), leading to increasing average annual precipitation totals (subscripts in the legend). For each climatic scenario, 500 21-day simulations were run. The horizontal black lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.







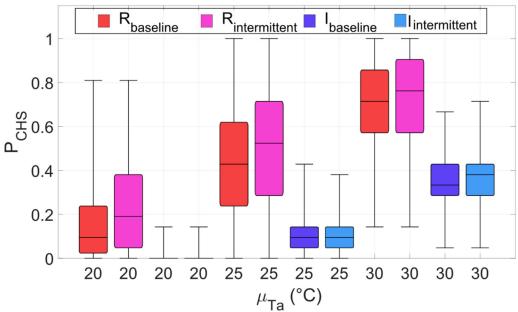


Figure 5: <u>MDistribution of mean canopy</u> temperature during anthesis ( $T_{c,mean}$ ; top) and percentage of days during which  $T_c$  is above the threshold temperature for potential heat damage,  $T_{th}$  ( $P_{CHS}$ ; bottom), under three long-term average air temperatures  $\mu_{T_a}$  (x-axis) and different precipitation and irrigation scenarios (colors). In each group of 4 boxes, from left to right, R<sub>baseline</sub> and R<sub>intermittent</sub> represent rainfed cropping, respectively under baseline precipitation ( $\alpha_p$ =8.2 mm;  $\lambda_p$ =0.2 d<sup>-1</sup>) and more intermittent precipitation ( $\alpha_p$ =23.5 mm-;  $\lambda_p$ =-0.07 d<sup>-1</sup>): I<sub>baseline</sub> and I<sub>intermittent</sub> refer to stress avoidance irrigation, under the same

precipitation regimes of the corresponding rainfed cases. For each climatic scenario, 500 21-day simulations were run. The horizontal black lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.

# **Supplementary Information to**

# Canopy temperature and heat stress are increased by compound high air temperature and water stress, and reduced by irrigation – A modeling analysis

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#### S1 Model description

To determine the canopy temperature, we developed a model considering the whole canopy as subject to the same conditions, with single exchange fluxes of energy and mass ('big-leaf model'; Tuzet et al., 2003; Bonan, 2019; Amthor, 1994; Jarvis and McNaughton, 1986), and uniform soil features and water content over the active rooting zone ('bucket filling model'; Rodriguez-Iturbe et al., 1999; Laio et al., 2001; Milly, 1994). For set conditions above the canopy (radiation, wind velocity, air temperature, and vapor pressure deficit), the model quantifies the canopy energy and water balances (Section S1.1-1.2), as a function of the canopy water potential. In turn, the canopy water potential was determined by the soil water balance and transport of water from the soil, inside the canopy to the atmosphere (Section S1.3). The whole system was forced by the conditions above the canopy and the precipitation input to the soil water balance, which were synthetically generated (Section S1.4). All the mathematical symbols are defined in Table S1. The model parameters are summarized in Table S2.

# 20 S1.1 Canopy conditions

# S1.1.1 Radiation

To determine the canopy energy balance, a simplified radiation model was used, accounting for visible, near-infrared, and long\_wave radiation separately (Goudriaan and Van Laar, 1994; Leuning et al., 1995). All fluxes were expressed on a per unit ground area basis.

Short\_wave radiation

25

The incoming short-wave radiation at the top of the canopy,  $Q_0^{\downarrow}$ , was partitioned into the <u>near-near-infrared</u> (NIR) and visible (PAR) components,  $Q_{0,NIR}^{\downarrow}$  and  $Q_{0,PAR}^{\downarrow}$ , based on the fractions  $f_{NIR}$  and  $f_{PAR}$  respectively.

By integrating the radiation absorbed by each canopy layer within a canopy, assuming constant leaf area density (Goudriaan and Van Laar, 1994; Bonan, 2019), the total radiation absorbed by the canopy for component *i* (with *i*=NIR, PAR) was determined as (Tuzet et al., 2003):

$$Q_i^{\downarrow} = Q_{0i}^{\downarrow} \left( 1 - \rho_i \right) \left[ 1 - exp\left( -K_{bl} \sqrt{1 - \sigma_i} L_{Al} \right) \right], \tag{S1}$$

where  $Q_{0,i}^{\downarrow}$  is the solar radiation above the canopy in the corresponding component,  $\rho_i$  is the canopy reflection coefficient,  $K_{bl}$  is the extinction coefficient for black leaves,  $\sigma_i$  is the leaf scattering coefficient (so that  $K_{bl}\sqrt{1-\sigma_i}$  represents the effective transmission coefficient), and  $L_{Al}$  is the canopy leaf area index.

The canopy extinction coefficient for black leaves depends on the direction of radiation and leaf orientation. Assuming an isotropic leaf angle distribution, it can be obtained as (Goudriaan and Van Laar, 1994)

$$K_{bl} = \frac{1}{2\cos\theta_{sun}},\tag{S2}$$

where  $\theta_{sun}$  is the solar zenith angle, determined based on the field location, day of the year, and time of the day (Dingman, 1994).

The canopy reflection coefficient for PAR (i=PAR) and NIR (i=NIR) was calculated as (Goudriaan and Van Laar, 1994)

$$\rho_i = 2K_{bl}(K_{bl} + K_{bl,d})^{-1} (1 - \sqrt{1 - \sigma_i}) (1 + \sqrt{1 - \sigma_i})^{-1}.$$
 (S3)

40 where  $K_{bl,d}$  is the extinction coefficient for diffuse radiation.

The total net short-wave radiation absorbed by the canopy is the us-sum of the PAR and NIR components,  $Q^{\downarrow} = Q_{PAR}^{\downarrow} + Q_{NIR}^{\downarrow}$ .

Thermal (long-wave) radiation

45 The net absorbed long\_wave radiation is the difference between the sky downward thermal radiation and the canopy upward emissivity (Leuning et al., 1995; Goudriaan and Van Laar, 1994):

$$B_n^{\downarrow} = (\varepsilon_a \sigma T_a^4 - \varepsilon_c \sigma T_c^4) \left[ 1 - exp(-K_{bl,d} \ L_{AI}) \right] \cong B_{n,ref}^{\downarrow} + \Delta B^{\downarrow}, \tag{S4}$$

where  $\varepsilon_a$  is the apparent emissivity for a hemisphere radiating at temperature  $T_a$  (Campbell and Norman, 1998),  $\varepsilon_c$  is the canopy emissivity,  $\sigma$  is the Stefan-Boltzmann constant,  $T_a$  and  $T_c$  are the air and canopy temperatures respectively (expressed in Kelvin). As in Eq. (S1), the term in square brackets is the result of integrating the fluxes over the whole canopy height (Bonan, 2019), although considering the black leaf transmissivity for thermal radiation  $K_{bl,a}$ . The simplifying assumption was made that the long-wave radiation exchange between the bottom of the canopy and the soil surface is negligible, because, under e-closed canopy, the soil temperature is similar to that of the canopy. The apparent emissivity depends on the cloud cover as  $\varepsilon_a = \varepsilon_{a,clear}(1 - 0.84 \, f_{cloud}) + 0.84 \, f_{cloud}$ , where  $\varepsilon_{a,clear}$  is the clear sky emissivity, proportional to  $T_a^2$ , and  $f_{cloud}$  the cloud cover fraction (Campbell and Norman, 1998).

The expansion on the far r.h.s. of Eq. (S4) is based on the linearization of the canopy emittance term, exploiting the binomial expansion. There,  $B_{n,ref}^{\downarrow}$  is the net isothermal long\_wave energy absorbed by the canopy (subscript *ref*) and  $\Delta B^{\downarrow}$  is the deviation from that. They were calculated as

$$B_{n,ref}^{\downarrow} = (\varepsilon_a \sigma T_a^4 - \varepsilon_c \sigma T_a^4) \left[ 1 - exp(-K_{bl,d} L_{AI}) \right]$$
  

$$\Delta B^{\downarrow} = 4 \varepsilon_c \sigma T_a^3 (T_a - T_c) \left[ 1 - exp(-K_{bl,d} L_{AI}) \right]$$
(S5)

# S1.1.2 Wind velocity

65

To determine the wind velocity at the <u>top of the canopy of</u>-height,  $h_c$ ,  $U(h_c)$ , we considered the atmospheric bulk wind velocity and assumed a logarithmic wind profile above the canopy, including the diabatic corrections, i.e.,

$$U(z) = \frac{u^*}{K_n} \left[ ln \left( \frac{z - d_0}{z_M} \right) + \Psi_M \right]$$
 (S6)

Here, z is the generic height above the ground (set to  $h_c$  to determine  $U(h_c)$ ),  $u^*$  the friction velocity,  $K_v$  the von Karman constant,  $d_0$  the zero plane displacement ( $d_0 \cong 2/3 h_c$ ),  $z_M$  the roughness length for the momentum, and  $\Psi_M$  the diabatic correction factor for momentum. The diabatic correction factor was determined based on the following empirical functions, for unstable ( $H \ge 0$ , with H being the sensible heat flux; Eq. S20 below) and stable (H < 0) conditions (Campbell and Norman, 1998):

$$\Psi_{M} = \begin{cases} -1.2 \ln \left[ \frac{1 + (1 - 16\zeta)^{1/2}}{2} \right] & H \ge 0 \\ 6 \ln(1 + \zeta) & H < 0 \end{cases}$$
 (S7)

 $\zeta$  is the atmospheric stability, accounting for the effects of buoyancy, measured as the ratio of the convective to mechanical production of turbulence (Bonan, 2019)

$$\zeta = -\frac{K_v g(z - d_0) H}{\hat{\rho}_a c_p T_a u^{*3}},\tag{S8}$$

where  $K_v$  is the von Karman constant, g the gravitational acceleration, z the height from the ground,  $\hat{\rho}_a$  the molar density of air,  $c_p$  the heat capacity of air,  $T_a$  the air temperature at height z (expressed in Kelvin), and  $u^*$  the friction velocity. The latter was obtained by rearranging the diabatic profile equation for wind velocity at height z, U(z), to yield  $u^* = K_v U(z) \left[ ln \left( \frac{z-d_0}{z_M} \right) + \Psi_M \right]^{-1}$ .

# S1.1.3 Vapor pressure deficit and air CO<sub>2</sub> concentration

It was assumed that turbulent transport is such that the relative humidity and the air carbon dioxide (CO<sub>2</sub>) concentration at the canopy level are the same as the reference ones, well above the canopy.

# S1.2 CO<sub>2</sub>, water vapor, and heat canopy exchanges

# S1.2.1 CO<sub>2</sub> assimilation and stomatal conductance

The stomatal conductance  $g_s$  was modeled based on the optimization principle, i.e., assuming that plants maximize cumulated net  $CO_2$  uptake over a given period, subject to limited water availability. The optimization principle and the optimal control theory provide the necessary condition for the stomatal conductance  $g_s$  to be optimal as  $\partial (A_{net} - \lambda_w E_l)/\partial g_s = 0$  (Mäkelä et al., 1996), where  $\lambda_w = \partial A_{net}/\partial E_l$  is the marginal water use efficiency,  $A_{net}$  is the net  $CO_2$  assimilation rate, and  $E_l$  is the transpiration rate (both expressed on a per unit leaf area basis).

In contrast to other optimization models based on water use efficiency (Katul et al., 2009; Medlyn et al., 2011), here no *a priori* assumption was made on whether photosynthesis is light- or RuBisCO- limited. Rather, the Farquhar model of photosynthesis (Farquhar et al., 1980) was approximated by a hyperbolic function, as (Vico et al., 2013)

$$A_{net} = k_1 \frac{c_i - \Gamma^*}{k_2 + c_i} - R_d, \tag{S9}$$

where  $c_i$  is the CO<sub>2</sub> concentration at the photosynthetic site (neglecting the mesophyll resistance),  $\Gamma^*$  is the CO<sub>2</sub> compensation point in the absence of dark respiration,  $R_d$  is the respiration rate in the light. The parameters  $k_1$  and  $k_2$  are related to the photosynthetic parameters as

$$k_1 = \frac{J}{4} k_2 = \frac{J}{4} \frac{a_2}{V_{c,max}}.$$
 (S10)

Here, J is the electron transport rate,  $V_{c,max}$  the maximum carboxylation rate; and  $a_2 = K_C(1 + c_{0a}/K_0)$ , with  $K_C$  and  $K_O$  being the Michelis-Menten constants for CO<sub>2</sub> fixation and oxygen inhibition, and  $c_{0a}$  the oxygen concentration in the air. The electron transport rate J depends on the light-saturated electron transport rate,  $J_{max}$ , and the available photosynthetically active radiation, expressed in  $\mu$ mol m<sup>-2</sup> s<sup>-1</sup> (obtained from  $Q_{PAR}^{\downarrow}$  = Eq. S1-S3, assuming a constant conversion factor of 4.6  $\mu$ mol J<sup>-1</sup>). The kinetic parameters ( $J_{max}$ ,  $V_{c,max}$ ,  $\Gamma^*$ ,  $K_C$  and  $K_O$ ) are a function of both canopy temperature (Bernacchi et al., 2001; Medlyn et al., 2002) and water availability (Vico and Porporato, 2008). The day respiration rate,  $R_d$ , was assumed to equal a fraction  $f_R$  of  $V_{c,max}$ , thus also depending on canopy temperature (and water availability).

The effects of water availability were considered directly on  $\lambda_w$ ,  $V_{c,max}$  and  $J_{max}$ . Following Zhou et al. (2013) and Manzoni et al. (2011),  $\lambda_w$  was assumed to be a function of the predawn canopy water potential  $\psi_{c,pd}$  (set equal to the predawn soil water potential). Considering the predawn canopy water potential as opposed to the instantaneous one was motivated by  $\lambda_w$  not responding instantaneously to canopy water potential. A monotonically-increasing dependence on water availability was used to minimize the data needed for a robust relationship (Manzoni et al., 2011):

$$\lambda_{w} = \lambda_{ww}^{*} \frac{c_{a}}{c_{c}^{*}} exp(\beta_{o} \psi_{c,pd}), \tag{S11}$$

where  $\lambda_{ww}^*$  is the marginal water use efficiency under well-watered conditions and at reference atmospheric CO<sub>2</sub> concentration ( $c_a^*$ ) and  $\beta_o$  is a fitting parameter describing the change in  $\lambda_w$  with water stress. More complex relationships have been suggested to match some observations, but they differ markedly only under extreme water stress (Manzoni et al., 2011) – conditions that are uncommon in most agricultural settings.

The effects of canopy water potential,  $\psi_c$ , on  $V_{c,max}$  and  $J_{max}$  were accounted for via a Weibull-type vulnerability curve, the parameters of which were determined by fitting <u>physiological\_leaf-level\_observations\_measurements</u> (Vico and Porporato, 2008). This approach allows accounting for non-stomatal limitations to photosynthesis under water stress – a mechanism necessary to reproduce observations (Zhou et al., 2013; Drake et al., 2017).

For simplicity, canopy water potential and temperature were not included in the optimization directly, but they did affect  $V_{c,max}$ ,  $J_{max}$  and  $\lambda_w$ . This is equivalent to assuming that the marginal effect of  $g_s$  on  $T_c$  and  $\psi_c$  is small with respect to that of  $g_s$  on  $A_{net}$  and  $E_l$ . It is important to emphasize that these assumptions apply only to the determination of stomatal conductance, i.e., all other modules include explicitly the roles of  $T_c$  and  $\psi_c$ .

This stomatal model represents a further development of that of Vico et al. (2013), because it explicitly includes the effects of water availability and day respiration, as well as the conductances to leaf boundary layer, and turbulent transport of vapor and heat, for more realistic estimates also under water stress and low wind velocity. The leaf boundary layer and turbulent transport in the atmosphere can act as further resistances to the vapor and  $CO_2$  exchanges with the surrounding atmosphere and decreases with wind velocity (see Eq. S13 below). Despite the additional feedbacks included in the model, a closed formula for the optimal stomatal conductance  $g_s$  can still be obtained, but it is cumbersome and hence not reported here.

#### S1.2.2 Minimum leaf conductance

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In parallel to the stomatal conductance, we considered a minimum conductance,  $g_{min}$ , that cannot be controlled by the plant (Kerstiens, 1996).  $g_{min}$  is known to change with water availability, although in ways that are complex, species-specific and not fully characterized yet (Duursma et al., 2019). And, while most of the experimental work has focused on the acclimation of  $g_{min}$  to low water availability as opposed to its instantaneous response, responses can occur even over few days (Bengtson et al., 1978). As a first approximation, it was assumed that  $g_{min}$  declines linearly with  $\psi_c$ , as

$$g_{min} = g_{min,ww} max \left( 1 - \frac{\psi_c}{\psi_{c,0}}, 0 \right)$$
 (S12)

where  $g_{min,ww}$  is the minimum conductance under well-watered conditions ( $\psi_c = 0$ ) and  $\psi_{c,0}$  is the leaf water potential at which the minimum conductance becomes negligible. Given the typically low value of  $g_{min,ww}$ , the exact functional dependence of  $g_{min}$  on  $\psi_c$  and its parameterization bears little consequences on the model outputs. Also, the role of  $g_{min}$  is negligible except under severe water stress, which, however, seldom occurs in most agricultural settings. Its inclusion was motivated to ensures that the model does not return unrealistic results should soil moisture reach an occasional low value during a prolonged dry down.

While  $g_{min}$  affects the amount of water lost by the leaves, it cannot be controlled by the plant and is independent of the stomatal conductance. So, considering in the optimization the total water losses at the leaf level,  $E_l$ , as opposed to the part stemming from the stomatal aperture only does not bear any consequence inaffect the resulting optimized stomatal conductance.

# S1.2.3 Canopy boundary layer conductances

The leaf boundary layer conductances to heat and vapor per unit leaf area ( $g_{H,bl}$  and  $g_{v,bl}$  respectively) were quantified as (Campbell and Norman, 1998):

$$g_{H,bl} = 1.4 \cdot 0.135 \sqrt{\frac{U(h_c)}{0.7 d_l}},$$

$$g_{v,bl} = 1.4 \cdot 0.147 \sqrt{\frac{U(h_c)}{0.7 d_l}},$$
(S13)

where  $d_l$  is the leaf width (in m; and the coefficient 0.7 transforms it in the leaf characteristic dimension) and  $U(h_c)$  is the wind velocity at canopy height (in m s<sup>-1</sup>; Eq. S6).

#### S1.2.4 Aerodynamic bulk conductance

140 A further conductance, the aerodynamic bulk conductance (per unit ground area),  $g_{H,a}$ , is needed to describe the turbulent transport of heat and mass from outside the leaf boundary layer to the bulk atmosphere. This conductance was determined as (Webber et al., 2016; Campbell and Norman, 1998)

$$g_{H,a} = \frac{\kappa_v^2 \hat{\rho}_a U(z)}{\left[ln\left(\frac{z-d_0}{z_M}\right) + \Psi_M\right] \left[ln\left(\frac{z-d_0}{z_H}\right) + \Psi_H\right]},\tag{S14}$$

where  $z_i$  is the roughness length for momentum (for i=M) and heat (for i=H), and  $\Psi_i$  is the <u>corresponding</u> diabatic correction factor for momentum (i=M) and heat (i=H). The diabatic correction factor for momentum (i=M) is given in Eq. (S7). From that, the diabatic correction factor for heat (i=H) can be determined as (Campbell and Norman, 1998)

$$\Psi_{H} = \begin{cases} \frac{\Psi_{M}}{0.6} & H \ge 0\\ \Psi_{M} & H < 0 \end{cases}$$
 (S15)

# S1.2.5 Total canopy conductances

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The total canopy conductance to water vapor (per unit ground area) was calculated as the series of stomatal and cuticular conductance, leaf boundary layer conductance, and aerodynamic bulk conductance. The minimum and stomatal conductances were assumed to operate in parallel, so that the net conductance is  $g_{sc} = g_{min} + g_s$  and it converges to  $g_{min}$ 

during drought (as suggested by Duursma et al., 2019). This net conductance occurs in series with the leaf boundary layer conductance. Assuming that both the abaxial and adaxial side of the leaf transpire at the same rate, the total leaf-level conductance to vapor per unit leaf area is

$$g_{v,l} = \frac{g_{sc} g_{v,bl}}{g_{sc} + g_{v,bl}}$$
 (S16)

The total conductance to water vapor (per unit ground area),  $g_{v,c}$ , is given by the series of the leaf-level conductance, and aerodynamic conductance,  $g_{H,a}$ ,

$$g_{v,c} = \frac{L_{AI}g_{v,l} g_{H,a}}{L_{AI}g_{v,l} + g_{H,a}}$$
(S17)

where the  $L_{AI}$  scales up the leaf-level conductances to the canopy, exploiting the big-leaf approximation.

The total canopy conductance to heat (per unit ground area),  $g_{H,c}$ , is instead the series of the leaf boundary layer and aerodynamic bulk conductances, i.e.,

$$g_{H,c} = \frac{L_{AI}g_{H,bl} g_{H,a}}{L_{AI}g_{H,bl} + g_{H,a}}$$
(S18)

#### S1.2.6 Canopy energy balance

The canopy energy balance can be written as (Campbell and Norman, 1998)

$$Q^{\downarrow} + B_n^{\downarrow} = H + \lambda ET, \tag{S19}$$

where  $Q^{\downarrow}$  and  $B_n^{\downarrow}$  are the net incoming shortwave- and long-wave radiations respectively, H is the sensible heat loss, and  $\lambda ET$  is the latent heat loss, with ET being the transpiration rate (per unit ground area) and  $\lambda$  the latent heat of vaporization for water. The sensible heat loss depends on the temperature difference between the canopy and the air as

$$H = c_p g_{H,c} \left( T_c - T_a \right), \tag{S20}$$

The canopy transpiration rate (per unit ground area), ET, is given by

$$ET = g_{v,c} \frac{e_s(T_c) - e_a(T_a)}{P_a} \cong g_{v,c} s_s(T_c - T_a) + g_{v,c} D$$
 (S21)

where  $e_s(T_c)$  is the saturated vapor pressure at canopy temperature,  $e_a(T_a)$  is the air vapor pressure,  $s_s = \Delta P_a^{-1}$ , with  $\Delta$  being the slope of the saturation vapor pressure versus temperature function and  $P_a$  (kPa) the atmospheric pressure (Campbell and Norman, 1998), and D is the air vapor pressure deficit. The expression on the far r.h.s. was obtained exploiting Penman's linearization of the saturated vapor pressure curve and it is line with the use of Penman Monteith equation for the calculation of canopy temperature.

Substituting Eq. (S4), (S20) and (S21) in Eq. (S19), the canopy energy balance reads

$$Q_{PAR}^{\downarrow} + Q_{NIR}^{\downarrow} + B_{n,ref}^{\downarrow} + \Delta B^{\downarrow} = c_p g_{H,c} (T_c - T_a) + \lambda g_{v,c} s_s (T_c - T_a) + \lambda g_{vc} D, \tag{S22}$$

where  $Q_{NIR}^{\downarrow}$  and  $Q_{NIR}^{\downarrow}$  were obtained via Eq. (S1). Rearranging the terms, the canopy temperature  $T_c$  was obtained explicitly as

$$T_{c} = T_{a} + \frac{Q_{PAR}^{\downarrow} + Q_{NIR}^{\downarrow} + B_{n,ref}^{\downarrow} - \lambda g_{v,c} D}{c_{p} g_{H,c} + \lambda g_{v,c} s_{s} + 4 \varepsilon_{c} \sigma T_{a}^{3} \left[ 1 - exp(-K_{bl,d} L_{AI}) \right]}.$$
 (S23)

#### S1.3 Soil water balance and water transport along the soil-plant-atmosphere continuum (SPAC)

#### S1.3.1 Soil water balance

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To limit parameter and computational requirements, we characterized plant available water by the soil water potential, averaged over the rooting depthzone,  $\psi_s$ , i.e., we neglected any potential inhomogeneity in root and soil water distribution in the soil volume where most of the plant roots are located. In turn,  $\psi_s$  is linked to the soil moisture, s (ranging from 0 for oven-oven-dry soils to 1 for saturated soils) as (Clapp and Hornberger, 1978)

$$\psi_s = \psi_{s,sat} \, s^{-b},\tag{S24}$$

where  $\psi_{s,sat}$  is the soil water potential at air entry and b is an empirical exponent. Both parameters depend on soil texture.

The most effective way to determine the dynamics of the soil moisture is via the soil water balance over the active rooting zone, of depth  $Z_r$  (Rodriguez-Iturbe et al., 1999; Vico and Porporato, 2011):

$$nZ_r \frac{ds}{dt} = P + I - ET_d - LQ, (S25)$$

where s is the soil moisture, P is the input via (effective) precipitation, I is the irrigation, if any,  $ET_d$  is the cumulated daily losses via evapotranspiration, and the term LQ combines losses via surface runoff and percolation below the rooting zone. This balance is to be interpreted at the daily time scale, so that inputs and outputs are idealized as occurring instantaneously in time. The dependence on time of the terms in Eq. (S25) is not explicitly indicated for notational clarity.

Irrigation, if any, was assumed to be demand-based, i.e., irrigation is applied when soil moisture reaches a pre-set level (the intervention point,  $\tilde{s}$ ). Each irrigation application provides a fixed amount of water, depending on the irrigation technology employed, equal to  $nZ_r(\hat{s}-\tilde{s})$ , where  $\hat{s}$  is the level of moisture restored by each irrigation application (target level) (Vico and Porporato, 2011). The soil moisture intervention point and target level were set to corresponds to specific soil water potentials (as per Eq. S24),  $\tilde{\psi}_s$  and  $\hat{\psi}_s$  respectively, thus considering the effect-role of soil texture. These parameters define the timing and amount of irrigation applications. A stress avoidance irrigation is performed when the intervention point  $\tilde{\psi}_s$  is equal or less negative than the soil water potential at which incipient stomatal closure occurs; whereas, more negative  $\tilde{\psi}_s$  correspond to deficit irrigation (English, 1990). The irrigation technology employed dictates the minimum water depth provided by each irrigation application, with more sophisticated approaches able to provide also smaller water depths, and

cheaper, more commonly employed technologies delivering larger water depths at each application (see, e.g., Vico and Porporato, 2011 and references therein). The target level  $\hat{\psi}_s$  thus depends on both the irrigation strategy, which sets  $\tilde{\psi}_s$ , and the irrigation technology, which sets the depth of each application.

The lossesses via evapotranspiration were assumed to be dominated by losses via transpiration, in line with the focus on the anthesis phase, when canopies are closed and soil water evaporation becomes negligible (Wei et al., 2017). The cumulated daily losses via evapotranspiration was were thus determined by cumulating the losses via canopy transpiration, ET (Eq. S21), during the day. The model was run only once per day, under the conditions likely resulting in the highest canopy temperatures (see Section 2.23 in the main text). To scale up the estimated losses via evapotranspiration at the daily scale, the dailywe assumed evapotranspiration rate was assumed to followed a parabolic diurnal evolution. Hence, the total daily losses via evapotranspiration wereas determined as

$$ET_d = \frac{2}{3}ET (t_{sunset} - t_{sunrise}), \tag{S26}$$

where  $t_{sunset} - t_{sunrise}$  is the day length, i.e., the time between sunrise and sunset.

Finally, in line with the daily interpretation of the water balance in Eq. (S25), losses via surface runoff and deep percolation below to the rooting zone, LQ, were assumed to occur instantaneously when soil moisture exceeds a threshold  $s_1$ , slightly above the soil field capacity. Hence, soil moisture dynamics is effectively upper-bounded by  $s_1$ .

## S1.3.2 Soil-plant-atmosphere continuum

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The soil water balance was coupled to a minimalist description of the soil-plant-atmosphere continuum (SPAC), to determine the leaf water potential. Water moves along the SPAC as driven by gradients of total water potential, from the soil to the leaf, and then to the atmosphere. Based on the electric analogy, the water flow was modulated by a series of resistances (or conductances): soil to root conductance; root to leaf (i.e., xylem) conductance; and leaf to the atmosphere (i.e., stomatal conductance). These conductances depend on soil features and plant traits, and decline with decreasing water potential. Details on these dependencies and parameter values are summarized in Manzoni et al. (2013).

### 215 S1.4 Environmental conditions above the canopy

The model requires solar radiation, air temperature and humidity in the bulk atmosphere, at height  $z > h_c$ , as well as the daily precipitation totals. To <u>systematically</u> explore different climatic scenarios, these environmental conditions were synthetically generated, as described next.

## S1.4.1 Solar radiation

The total incoming short\_wave solar radiation,  $Q_0^{\downarrow}$ , was set to a realistic and constant value. Clear sky conditions were assumed for the entire anthesis <u>period</u>, thus likely leading to an overestimate of  $T_c$  and a conservative estimate of the potential for heat damage.

#### S1.4.2 Precipitation

Daily precipitation was idealized as a marked Poisson process, i.e., with exponentially distributed interarrival times,  $\tau_n$  -(Rodriguez-Iturbe et al., 1999):

$$p_{\tau_n}(\tau_p) = \lambda_p \, e^{-\lambda_p \, \tau_p} \,, \quad \tau_p \ge 0, \tag{S27}$$

where  $\lambda_p$  is the average frequency of precipitation occurrence.

Each precipitation was assumed to occur instantaneously at the daily time scale (i.e., the temporal structure of precipitation is ignored). Each event provides a random amount  $h_p$ , assumed to be exponentially distributed

$$p_{h_p}(h_p) = \frac{1}{\alpha_n} e^{-\frac{1}{\alpha_p}h_p}, \quad h_p \ge 0,$$
 (S28)

with  $\alpha_p$  corresponding to the average precipitation depth.

With this model of precipitation, the average total annual precipitation is  $365\alpha_p\lambda_p$ .

## S1.4.3 Air temperature

Since the focus was on the warmest part of the day, we interpreted  $T_a$  as the daily maximum temperature. The day-to-day fluctuations of  $T_a$  were described as an Ornstein-Uhlenbeck process (Benth and Benth, 2007). The rate of air temperature change was thus expressed as

$$\frac{dT_a}{dt} = -\frac{1}{\tau_{T_a}} (T_a - \mu_{T_a}) + \sqrt{k_3} \eta_t$$
 (S29)

where  $\tau_{T_a}$  is the relaxation time (i.e.,  $\tau_{T_a}^{-1}$  is the mean-reversion rate of the process);  $\mu_{T_a}$  is the long-term mean of average maximum daily temperatures;  $k_3$  is the diffusion parameter, quantifying the noise 'size'; and  $\eta_t$  is a Gaussian white noise (with vanishing mean, unit variance and an autocorrelation with a sharp peak in zero and dropping to zero for any lag greater than 0; Ridolfi et al., 2011). With these assumptions,  $T_a$  has a Gaussian distribution, with mean  $\mu_{T_a}$  and standard deviation  $\left(\frac{\tau_{T_a}k_3}{2}\right)^{1/2}$ .

#### 240 S1.4.4 Wind velocity and relative humidity

Wind velocity and relative humidity above the canopy were assumed to be constant during the simulations.

### S1.5 Numerical simulations

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For each climate and irrigation scenario<sub>2</sub> and soil type, we <u>run ranran</u> 501 simulations, each lasting 21 days (the duration of the heading period under current climatic conditions; Mäkinen et al., 2018). The initial conditions for soil water content and air temperature for each 21-day simulation <u>correspond</u> were set equal to the final conditions for the previous 21-day simulation, i.e., the <u>simulations</u> were concatenated<sub>52</sub>. In such a way, the conditions at the beginning of each period are fully stochastic and <u>reflect a long period of operation of all the hydrological processes</u>, including the <u>reflect the effects of previously</u>—occurred conditions — an aspect particularly important for the soil water balance. For the first simulation, the initial soil water potential was set at  $\hat{\psi}_s$  and initial air temperature at  $\mu_{T_a}$ , but this simulation was excluded <u>from the analyses</u> to limit the influence of these arbitrary choices.

The model was solved via nested numerical iterations (Fig. 1 in the main text). For each day, air temperature and precipitation inputs were generated as detailed in Section S1.4. The  $T_c$  at the previous time step was used to determine the diabatic corrections and hence the aerodynamic conductance and the wind velocity, while  $\psi_c$  at the previous time step was used to estimate the aerodynamic and boundary layer conductances, the soil-to-leaf, and optimal stomatal conductances (Eq. S6-S8, S12-S18). Then, the resulting water demand (driven by  $g_s$ ,  $T_{c_s}$  and  $\psi_s$ , and D) was compared with the water supply through the soil, root, and plant (driven by the series of soil to root to plant conductances, and the difference in water potential between the soil and the canopy). The  $\psi_c$  for which supply equaled demand was calculated and used in the subsequent iteration, where when the values of conductances were updated. Once convergence on  $\psi_c$  was reached (i.e., when the absolute difference in  $\psi_c$  between two subsequent steps was smaller than  $\psi_{c,toler}$ ), the iterative loop on  $\psi_c$  was exited, and the  $g_s$  value corresponding to such  $\psi_c$  was used in the canopy energy balance, to obtain a new estimate of  $T_c$ . This whole eyele was repeated till convergence was reached also on  $T_c$  (with tolerance  $T_{c,toler}$ ), unless a pre-set maximum number of iterations  $Max_{iter}$  was reached.

Once  $T_c$  was determined, the mid-day losses via transpiration were calculated and scaled up to the daily level (Eq. S26), and the daily soil moisture balance was updated, including any input via precipitation or irrigation. The new soil moisture s was used as the basis to determine the soil water potential for the subsequent day.

Table 1: List of symbols.

Variable	Description	Units
$a_2$	Combination of the Michelis Menten constants for CO <sub>2</sub> fixation and	μmol mol <sup>-1</sup>
2	oxygen inhibition	,
$A_{net}$	Net CO <sub>2</sub> assimilation rate (per unit leaf area)	μmol m <sup>-2</sup> s <sup>-1</sup>
b	Exponent of soil water retention curve	-
$B_n^{\downarrow}$	Net incoming long_wave radiation	W m <sup>-2</sup>
$B_{n,ref}^{\downarrow}$	Net isothermal long_wave energy absorbed by the canopy	W m <sup>-2</sup>
$c_a^*$	Reference CO <sub>2</sub> concentration in the bulk atmosphere	μmol mol <sup>-1</sup>
$c_i$	CO <sub>2</sub> concentration at the photosynthetic site	μmol mol <sup>-1</sup>
$c_{Oa}$	Oxygen concentration in the bulk atmosphere	mmol mol <sup>-1</sup>
$c_p$	Heat capacity of air	J kg <sup>-1</sup> K <sup>-1</sup>
$d_0$	Zero plane displacement	m
$d_l$	Leaf width	m
D	Vapor pressure deficit	mol mol <sup>-1</sup>
$e_a(T_a)$	Air vapor pressure at air temperature $T_a$	mol m <sup>-2</sup> s <sup>-1</sup>
$e_s(T_c)$	Saturation vapor pressure at canopy temperature $T_c$	mol m <sup>-2</sup> s <sup>-1</sup>
ET	Instantaneous evapotranspiration rate (per unit ground area)	mol m <sup>-2</sup> s <sup>-1</sup>
$ET_d$	Daily evapotranspiration rate (per unit ground area)	m s <sup>-1</sup>
$ET_l$	Instantaneous evapotranspiration rate (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$f_{cloud}$	Cloud cover fraction	-
$f_{NIR}$	Fraction of total radiation in the NIR wavebands	-
$f_{PAR}$	Fraction of total radiation in the PAR wavebands	-
$f_R$	Ratio between $R_d$ and $V_{c,max}$	-
g	Gravitational acceleration	m s <sup>-2</sup>
<i>9</i> н,а	Aerodynamic bulk conductance (per unit ground area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{H,bl}$	Leaf boundary layer conductance to heat (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{H,c}$	Total canopy conductance to heat (per unit ground area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{min}$	Minimum conductance (i.e., conductance that cannot be controlled by the	mol m <sup>-2</sup> s <sup>-1</sup>

	plant; per unit leaf area)	
$g_{min,ww}$	Minimum conductance under well-water condition (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_s$	Stomatal conductance (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{sc}$	Sum of stomatal and minimum conductance (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{v,c}$	Total canopy conductance to water vapor (per unit ground area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{v,bl}$	Leaf boundary layer conductance to water vapor (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$g_{v,l}$	Leaf-level conductance to water vapor (per unit leaf area)	mol m <sup>-2</sup> s <sup>-1</sup>
$G_{S,ref}$	Reference surface canopy conductance (per unit ground area)rate	mmol⋅m <sup>-2</sup> ⋅s <sup>-1</sup>
$G_{s}$	Surface-Canopy conductance (per unit ground area)	mmol·m <sup>-2</sup> ·s <sup>-1</sup>
$h_c$	Canopy height	m
$h_p$	Precipitation event depth	m
Н	Sensible heat flux	W m <sup>-2</sup>
I	Irrigation application	m d <sup>-1</sup>
J	Electron transport rate	μmol m <sup>-2</sup> s <sup>-1</sup>
$J_{max}\left(J_{max,25}\right)$	Maximum electron transport rate (and reference value at 25 °C)	μmol m <sup>-2</sup> s <sup>-1</sup>
$k_1$	Parameter of the hyperbolic photosynthetic model (Eq. (S10))	μmol m <sup>-2</sup> s <sup>-1</sup>
$k_2$	Parameter of the hyperbolic photosynthetic model (Eq. (S10))	μmol mol <sup>-1</sup>
$k_3$	Diffusion parameter of air temperature (noise 'size')	$^{\circ}\text{C}^2 \text{ d}^{\text{-1}}$
$K_{bl}$	Extinction coefficient for black leaves	-
$K_{bl,d}$	Extinction coefficient for black leaves, under diffuse light and long_wave radiation	-
$K_C$	Michelis-Menten constants for CO <sub>2</sub> fixation	μmol mol <sup>-1</sup>
$K_O$	Michelis-Menten constants for oxygen inhibition	mmol mol <sup>-1</sup>
K <sub>sat</sub>	Soil hydraulic conductivity at saturation	m d <sup>-1</sup>
$K_v$	Von Karman constant	-
$L_{AI}$	Leaf area index	m <sup>2</sup> m <sup>-2</sup>
LQ	Surface runoff and deep percolation below the rooting depthzone	m d <sup>-1</sup>
m	Slope of surface conductance to water pressure deficit	[ln(kPa)] <sup>-1</sup>
$Max_{iter}$	Maximum iteration number	-

n	Soil porosity	-			
P	Daily total precipitation	m d <sup>-1</sup>			
$P_a$	Air pressure	kPa			
$P_{CHS}$	Fraction of days during which $T_c$ exceeded $T_{th}$	-			
$Q^{\downarrow}$	Total net short_wave radiation absorbed by the canopy	W m <sup>-2</sup>			
$Q_{0,i}^{\downarrow}$	Solar radiation above the canopy ( <i>i</i> = NIR, PAR)	W m <sup>-2</sup>			
$Q_i^{\downarrow}$	Total radiation of the component ( <i>i</i> = NIR, PAR)	W m <sup>-2</sup>			
$R_d$	Respiration rate in the light	μmol m <sup>-2</sup> s <sup>-1</sup>			
RH	Air relative Relative air humidity	-			
S	Soil moisture	-			
$S_S$	Slope of the vapor pressure vs. temperature curve	kPa K <sup>-1</sup>			
<i>s</i> <sub>1</sub>	Soil moisture above which runoff and percolation below the active rooting zone occur instantaneously				
t	Time	d			
$t_{sunrise}, t_{sunset}$	Time of sunrise, time of sunset	hr			
$T_a$	Air temperature	°C			
$T_c$	Canopy temperature	°C			
$T_{c,toler}$	Canopy temperature tolerance for the numerical simulations	°C			
$T_{th}$	Threshold above which crop heat stress occurs around during the anthesis period	°C			
$u^*$	Friction velocity	m s <sup>-1</sup>			
U(z)	Mean wind velocity at height z	m s <sup>-1</sup>			
$V_{c,max}$ $(V_{c,max,25})$	Maximum carboxylation rate (and reference value at 25 °C)	μmol·m <sup>-2</sup> ·s <sup>-1</sup>			
Z	Height from the ground	m			
$Z_M$	Roughness length for the momentum	m			
$Z_U$	Height of wind measurement	m			
$Z_r$	Active rooting depth	m			
$\alpha_p$	Average precipitation event depth	m			
$eta_o$	Fitting parameter of the marginal water use efficient response function to	-			

	water stress				
$\Gamma^*$	CO <sub>2</sub> compensation point in the absence of dark respiration	mol mol <sup>-1</sup>			
Δ	Slope of the vapor pressure vs. temperature curve	mol mol <sup>-1</sup> K <sup>-1</sup>			
$\Delta B^{\downarrow}$	Deviation of absorbed energy	W m <sup>-2</sup>			
$arepsilon_a$	Apparent long_wave emissivity for a hemisphere radiating at temperature $T_a$	-			
$arepsilon_{a,clear}$	Clear sky emissivity	-			
$arepsilon_c$	Long-wave canopy emissivity	-			
ζ	Atmospheric stability	-			
$ heta_{sun}$	Solar zenith angle	rad			
λ	Latent heat of vaporization for water	J kg <sup>-1</sup>			
$\lambda_p$	Average precipitation frequency	day <sup>-1</sup>			
$\lambda_w$	Marginal water use efficiency	mol mol <sup>-1</sup>			
$\lambda_{ww}^*$	$\lambda_{ww}^*$ Marginal water use efficiency under well-watered condition and reference air CO <sub>2</sub> concentration				
$\mu_{T_a}$	Long-term mean-average air temperature				
$\hat{ ho}_a$	Molar density of air	mol m <sup>-3</sup>			
$ ho_i$	Canopy reflection coefficient for PAR ( <i>i</i> =PAR) and NIR ( <i>i</i> =NIR)	-			
σ	Stefan-Boltzman constant	W m <sup>-2</sup> K <sup>-4</sup>			
$\sigma_i$	Leaf scattering coefficient for PAR ( <i>i</i> =PAR) and NIR ( <i>i</i> =NIR)	-			
$ au_p$	Precipitation interarrival time	d			
$ au_{T_a}$	Relaxation time (i.e., $\tau_{T_a}^{-1}$ is the mean-reversion rate of the Ornstein-Uhlenbeck process)	d			
$\psi_{c,0}$	Leaf water potential at which minimum conductance becomes negligible	MPa			
$\psi_c$	Canopy water potential	MPa			
$\psi_{c,pd}$	Predawn canopy water potential	MPa			
$\psi_{c,toler}$	Canopy water potential tolerance for the numerical simulations	MPa			
$\psi_s$	Soil water potential	MPa			
$ ilde{\psi}_{s}$	Irrigation intervention soil water potential	MPa			

$\hat{\psi}_s$		Target soil water potential for irrigation	MPa		
$\psi_{s,sat}$	$\psi_{s,sat}$ Soil water potential at saturation				
$\Psi_i$		Diabatic correction factor ( <i>i</i> = H for heat; <i>i</i> =M for momentum)	MPa		

# **Table S2: List of parameters.**

Symbol	Value	Unit	Source
Crop param	neters		I
$C_d$	0.3	-	(Katul et al., 2004; crop canopies)
$d_0$	$2/3 h_c$	m	(Jones, 1992)
$d_l$	0.04	m	
$f_R$	0.01	-	
$g_{min,ww}$	1.73×10 <sup>-2</sup>	mmol⋅m <sup>-2</sup> ⋅s <sup>-1</sup>	(Duursma et al., 2019; mean value for wheat)
$h_c$	0.6	m	
J <sub>max,25</sub>	132	$\mu$ mol·m <sup>-2</sup> ·s <sup>-1</sup>	(Wullschleger, 1993; wheat)
$K_c$	405	μmol mol <sup>-1</sup>	
$K_O$	278	mmol mol <sup>-1</sup>	
$L_{AI}$	2	$m_{leaf}^2 m_{ground}^{-2}$	(Vico and Porporato, 2008)
$T_{th}$	30	°C	(Saini and Aspinall, 1982)
$V_{c,max,25}$	83	μmol·m <sup>-2</sup> ·s <sup>-1</sup>	(Wullschleger, 1993; wheat)
$Z_r$	0.3	m	(Jackson et al., 1996)
$eta_o$	-1.26	MPa <sup>-1</sup>	(Manzoni et al., 2011; median value for forbs and grasses in mesic and we climates)
$\lambda_{ww}^*$	981	mol mol <sup>-1</sup>	(Manzoni et al., 2011; median value for forbs and grasses in mesic and we climates)
$\psi_{c,0}$	-3	MPa	

$c_a^*$	400	μmol mol <sup>-1</sup>	
$C_{Oa}$	210	mmol mol <sup>-1</sup>	
$k_3$	32.6	$^{\circ}\mathrm{C}^{2}\;\mathrm{d}^{\text{-1}}$	(Rigby and Porporato, 2008)
RH	40%	-	
$P_a$	101	kPa	
$Q_0^{\downarrow}$	800	W m <sup>-2</sup>	
$U(z_U)$	4	m s <sup>-1</sup>	
$Z_M$	$0.13 h_c$	m	(Jones, 1992)
$z_U$	2	m	
$\alpha_p$	8.2 (baseline scenario)	mm	Baseline scenario
$\lambda_p$	0.2 (baseline scenario)	d <sup>-1</sup>	Baseline scenario
$\mu_{T_a}$	25 (baseline scenario)	°C	Baseline scenario
$ au_{T_a}$	0.81	d	(Rigby and Porporato, 2008)
Soil parame	eters		
	4.38 (loamy sand)		
b	4.90 (sandy loam)	-	(Laio et al., 2001)
	5.39 (loam)		
	0.42 (loamy sand)		
n	0.43 (sandy loam)	-	(Laio et al., 2001)
	0.45 (loam)		
	1.0 (loamy sand)		
$K_{sat}$	0.8 (sandy loam)	m d <sup>-1</sup>	(Laio et al., 2001)
Suc	0.2 (loam)		
	0.57 (sandy loam),		
$s_1$	0.62 (loamy sand)	-	(Laio et al., 2001)
1	0.72 (loam)		
$ ilde{\psi}_s$	-0.07	MPa	
	-0.01	MPa	
$\hat{\psi}_s$		1911 4	
$\psi_{s,sat}$	-1.7×10 <sup>-4</sup> (loamy sand)	MPa	(Laio et al., 2001)
,	-7×10 <sup>-4</sup> (sandy loam)		

	-1.43×10 <sup>-3</sup> (loam)		
Energy bala	ance parameters		ı
$f_{cloud}$	0.1 (i.e., clear skiesy)	-	
$f_{NIR}$	0.55	-	(Campbell and Norman, 1998)
$f_{PAR}$	$1-f_{NIR}$	-	(Campbell and Norman, 1998)
$K_{bl,d}$	0.8	-	(Campbell and Norman, 1998)
$arepsilon_{a,clear}$	$9.2\ 10^{-6}T_a^2$	-	(Swinbank equation; Campbell and Norman, 1998)
$\varepsilon_c$	0.97	-	(Campbell and Norman, 1998)
$ ho_i$	0.057 ( <i>i</i> =PAR) 0.389 ( <i>i</i> =NIR)	-	(Leuning et al., 1995)
σ.	0.2 ( <i>i</i> =PAR)	_	(Leuning et al., 1995; Goudriaan and Van
$\sigma_i$	0.8 ( <i>i</i> =NIR)		Laar, 1994)
Numerical s	simulation parameters		
Max <sub>iter</sub>	15	-	
$T_{c,toler}$	0.1	°C	
$\psi_{c,toler}$	0.001	MPa	

#### S2 Model behaviour

The temporal evolution of key model variables during a soil moisture dry down, assuming constant air temperature at 25 °C, is presented in Fig. S1: and the dependences on soil moisture in Fig. S2. As soil moisture decreased, the canopy-to-air temperature difference  $T_c - T_a$  and the marginal water use efficiency  $\lambda_w$  increased; while maximum carboxylation rate  $V_{c,max}$ , net CO<sub>2</sub> assimilation rate  $A_{net}$ , total leaf-level conductance to water vapor  $g_{v,l}$  and the leaf, root and soil water potentials  $(\psi_l, \psi_r)$  and  $\psi_s$  rapidly became more negative. Conversely, all the variables were largely independent of soil moisture under well-watered conditions.

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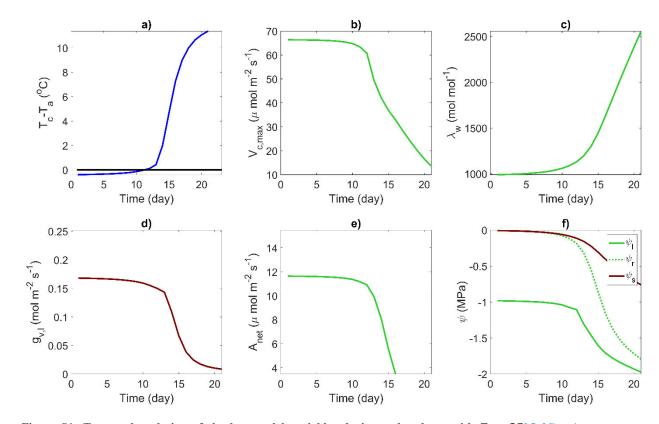


Figure S1: Temporal evolution of the key model variables during a dry down with  $T_a = 25^{\circ}C_{\circ}C_{\circ}C_{\circ}$ ; a) canopy temperature difference  $T_c - T_a$ , b) maximum carboxylation rate  $V_{c,max}$ , c) marginal water use efficiency  $\lambda_w$ , d) total leaf-level conductance to water vapor  $g_{v,l}$ , e) net CO<sub>2</sub> assimilation rate  $A_{net}$ , f) leaf, root, and soil water potentials,  $\psi_l$ ,  $\psi_r$  and  $\psi_s$ . The black horizontal line in a) corresponds to  $T_c - T_a = 0$ :

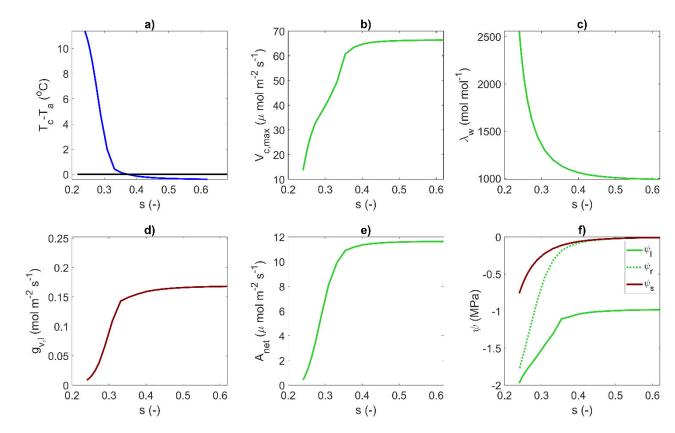


Figure S2: Dependence of the key variables on soil moisture s: a) canopy temperature difference  $T_c - T_a$ , b) maximum carboxylation rate  $V_{c,max}$ , c) marginal water use efficiency  $\lambda_w$ , d) total leaf-level conductance to water vapor  $g_{v,l}$ , e) net CO<sub>2</sub> assimilation rate  $A_{net}$ , f) leaf, root, and soil water potentials,  $\psi_l$ ,  $\psi_r$  and  $\psi_s$ . The black horizontal line in a) corresponds to  $T_c - T_c = 0$ .

#### S3 Additional results

#### S3.1 Water fluxes

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The dominant loss from the soil water balance occurred via evapotranspiration, with deep percolation and runoff playing a secondary role in all climatic and irrigation scenarios (Fig. S3, S4). Larger average precipitation totals (Fig. S3 far right), larger more intermittent precipitation events and irrigation applications (Fig. S4 pink and blue hues) increase the extent and variability of losses via runoff and deep percolation, although their quantitative role remains secondary when compared to cumulated evapotranspiration (compare panels in Fig. S3 and S4).

There was a large variability of the cumulated soil water fluxes relative to cumulated precipitation across the 500 simulated 21-day anthesis. The ratio of cumulated evapotranspiration and cumulated deep percolation and runoff over cumulated precipitation can exceed 1, when there was a net reduction in the soil water storage from the beginning to the end of the 21-day anthesis.

Irrigation exceeded the cumulated precipitation, in particular under larger but more intermittent precipitation (Fig. S5). This precipitation scenario also led to larger variability in cumulated irrigation inputs, in particular under higher long-term average air temperatures. Also the median number of irrigation applications per 21-day period increased from 1 at long-term air average temperature of 20 °C and for the baseline precipitation scenario at 25 °C, to 2 in the more intermittent precipitation at 25 °C and at 30 °C. Given the short duration of the period considered, it is not possible to discern smaller differences in number of irrigation applications and hence irrigation frequencies across climatic regimes.

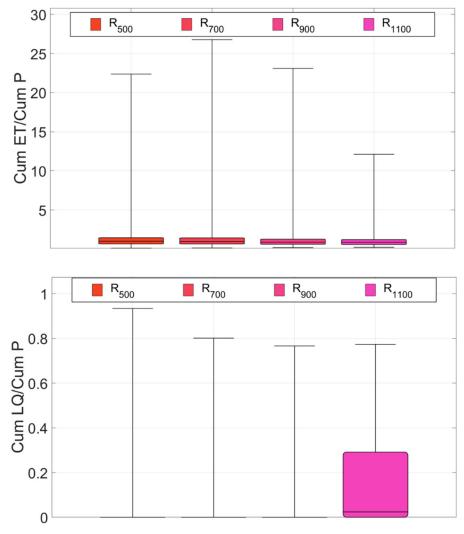
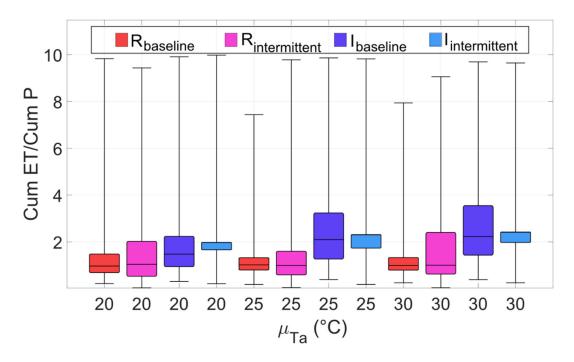


Figure S3: Distribution of the ratios of 21-day cumulated evapotranspiration (cum ET; top) and runoff and deep percolation (cum LQ; bottom) to cumulated precipitation (cum P), for four average annual precipitation totals (500, 700, 900, 1100 mm; colors), for long-term average air temperature  $\mu_{T_a} = 25$  °C. The precipitation scenarios are the same as those in Fig. 4 in the main text, i.e., average precipitation depth  $\alpha_p$  was kept at 15 mm, while average precipitation frequency  $\lambda_p$  changed within each group of 4 boxes from left to right, from 0.091 to 0.137, 0.183, and 0.228 d<sup>-1</sup>. While in all cases 500 21-day simulations were run, ratios were not defined (and hence not included) when no precipitation was recorded over the 21-day period (from left to right, in 18, 8, 2, and 1 % of the simulations). The horizontal dark lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.



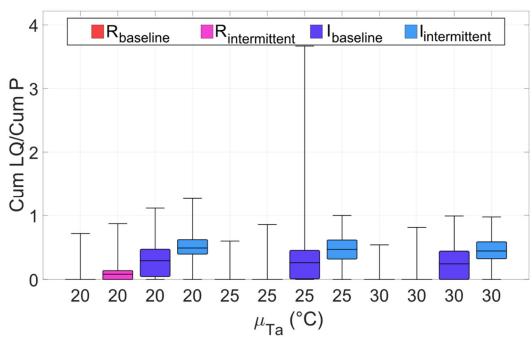


Figure S4: Distribution of the ratios of 21-day cumulated evapotranspiration (cum ET; top) and runoff and deep percolation (cum LQ; bottom) to cumulated precipitation (cum P), under three long-term average air temperatures  $\mu_{T_a}$  (x-axis) and different precipitation and irrigation scenarios (colors). The climatic and irrigation scenarios are as in Fig. 5 in the main text: in each group of 4 boxes, from left to right,  $R_{baseline}$  and  $R_{intermittent}$  represent rainfed

cropping, respectively under baseline precipitation ( $\alpha_p$ =8.2 mm;  $\lambda_p$ =0.2 d<sup>-1</sup>) and more intermittent precipitation ( $\alpha_p$ =23.5 mm;  $\lambda_p$ =0.07 d<sup>-1</sup>); I<sub>baseline</sub> and I<sub>intermittent</sub> refer to stress avoidance irrigation, under the same precipitation regimes of the corresponding rainfed cases. While in all cases 500 21-day simulations were run, ratios were not defined (and hence not included) when no precipitation was recorded over the 21-day period (between 1 and 2 % of the simulations for the baseline precipitation scenario; and between 21 and 25 % of the simulations for the more intermittent precipitation scenario). The horizontal dark lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.

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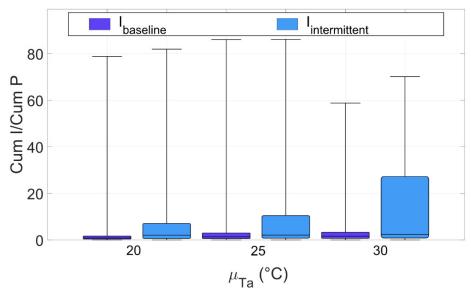


Figure S5: Distribution of the ratios of 21-day cumulated irrigation (cum I) to cumulated precipitation (cum P), under three long-term average air temperatures  $\mu_{T_a}$  (x-axis) and different precipitation scenarios (colors). The climatic and irrigation scenarios are as in Fig. 5 in the main text and Fig. S5: in each pair of 2 boxes, from left to right, I<sub>baseline</sub> and I<sub>intermittent</sub> represent stress avoidance irrigation, respectively under baseline precipitation ( $\alpha_p$ =8.2 mm;  $\lambda_p$ =0.2 d<sup>-1</sup>) and more intermittent precipitation ( $\alpha_p$ =23.5 mm;  $\lambda_p$ =0.07 d<sup>-1</sup>). The number of datapoints for each box is the same as Fig. S5. The horizontal dark lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.

## S3.12 Effects of air temperature variability

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We tested different air temperature variability by altering the diffusion parameter (noise 'size')  $k_3$ , to which the air temperature variance is proportional (Section S1.4.3). The patterns of  $T_c$  and  $P_{CHS}$  were independent of  $k_3$  for rainfed conditions, but their medians and variance increased with increasing  $k_3$  diffusion parameter under irrigation (Fig. S36, Table S7).

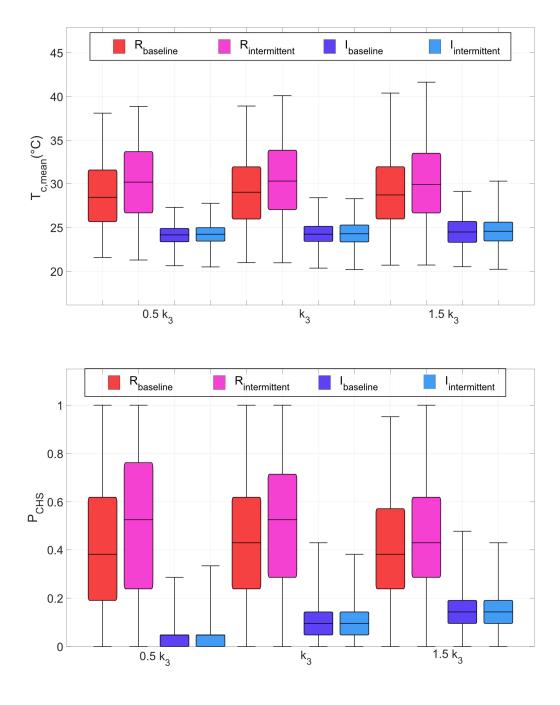


Figure S36: Distribution of the mMean canopy temperature during anthesis,  $T_{c,mean}$  (top) and percentage of days during which  $T_c > T_{th}$ ,  $P_{CHS}$  (bottom) under three noise 'sizes'  $k_3$ , corresponding to half of the baseline (left), baseline (center) and 1.5 times the baseline (right). Long-term mean\_average air temperature was kept at  $\mu_{T_a}$ =25 °C. precipitation and irrigation scenarios are as in

Fig 5 in the main text: in each group of 4 boxes, from left to right, R<sub>baseline</sub> and R<sub>intermittent</sub> represent rainfed cropping, under baseline precipitation ( $\alpha_p = 8.2 \text{ mm}$ ;  $\lambda_p = 0.2 \text{ d}^{-1}$ ) and more intermittent precipitation ( $\alpha_p = 23.5 \text{ mm}$ ;  $\lambda_p = 0.07 \text{ d}^{-1}$ ) respectively. Ibaseline and I<sub>intermittent</sub> refer to stress avoidance irrigation, under the same precipitation regimes as for the corresponding rainfed case. For each climatic scenario, 500 21-day simulations were run. The horizontal dark lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.

## S3.23 Effects of soil texture

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Soil texture determines the soil water storage capacity, the losses below the rooting zone, and the ability of the plant to take up water. Despite these potential roles of soil texture on soil and water plant dynamics, soil texture had no effect on median and variance of  $T_{c,mean}$  and  $P_{CHS}$ , although the differences induced by the precipitation regime remained (Fig. S47, Table S8).

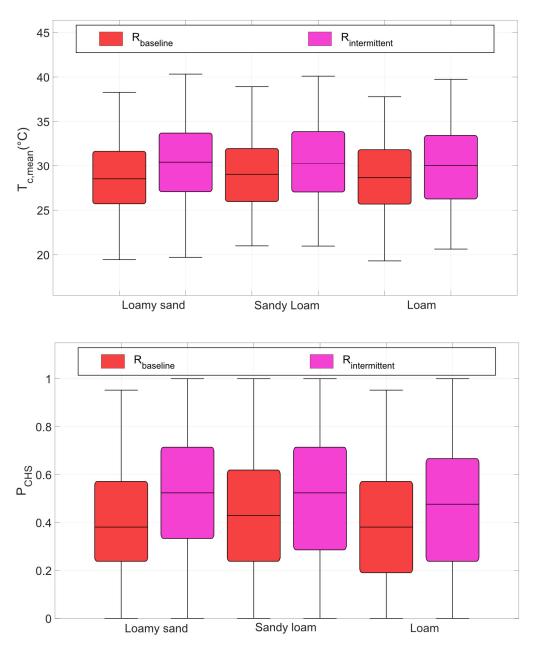


Figure S47: Distribution of mMean canopy temperature during anthesis,  $T_{c,mean}$  (top) and percentage of days during which  $T_c > T_{th}$ ,  $P_{CHS}$  (bottom) for three soil types: from left to right, loamy sand-(baseline), sandy loam (baseline), and loam. Rbaseline and Rintermittent represent rainfed cropping, under baseline precipitation ( $\alpha_p$  =8.2 mm;  $\lambda_p$  =0.2 d-1) and more intermittent precipitation ( $\alpha_p$  =23.5 mm;  $\lambda_p$  = 0.07 d-1) respectively. For each precipitation scenario and soil type, 500 21-day simulations were run. The horizontal dark lines are the median values; the boxes extend from the first to the third quartile; whiskers cover the whole range.

# S3.34 Effects of solar radiation, wind velocity, and air relative humidity

We tested the sensitivity of  $T_c$  to radiation  $Q_0^{\downarrow}$ , wind velocity U, and relative humidity RH, at different soil moistures (Fig. S§5). Higher  $Q_0^{\downarrow}$  led to higher  $T_c$ . Lower U enhanced canopy temperature at low soil moisture. High RH slightly increased  $T_c$  at high soil moisture.

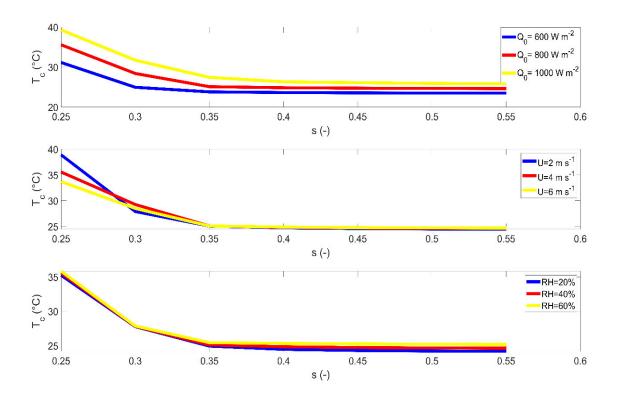


Figure S85: Canopy temperature,  $T_c$ , as a function of soil moisture, s, as obtained for three levels of short-wave radiations  $Q_0^{\downarrow}$  (top), wind velocity U (center), and relative humidity RH (bottom). All the other parameters are as in Table S2.

### **S4 Statistical tests**

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We tested whether medians and variance of  $T_{c,mean}$  and  $P_{CHS}$  differed between pedoclimatic scenarios, by means of Mood's median test and Brown-Forsythe's test of equal variance. Results are summarized in Table S3 to S8.

Table S3: Statistical tests of the effects of average annual precipitation totals amount at different long-term mean average air temperature,

 $\mu_{T_a}$  (columns), based on 500 simulations. For each test, the test statistics (top) and p value (bottom) are reported. The degrees of freedom (df) are specified for each type of test. Data are summarized in Fig. 4 in the main text.

	20 °C	25 °C	30 °C
Test on equal median df=3	232.02 <0.001	2 <u>13</u> 28.78 <0.001	177.49 <0.001
Test on equal variance df=[3, 1996]	42.36 <0.001	19.38 20.82 <0.001	7.97 <0.001

Table S4: Statistical tests of the effects long-term mean-average air temperatures for different average annual precipitation totals (from 500 to 1100 mm; columns), based on 500 simulations. For each test, the test statistics (top) and p value (bottom) are reported. The degrees of freedom (df) are specified for each type of test. Data are summarized in Fig. 4 in the main text.

	500 mm	700 mm	900 mm	1100 mm
median	56 <u>82</u> . <u>62</u> 80 <0.001	7	692. <u>3450</u> <0.001	785.34 825.14 <0.001
variance	_			4 <u>5</u> 7. <u>82</u> 43 <0.001

		20 °C			25 °C					30 °C			
		Effect o precipita pattern	ation	Effect o irrigatio		Effect o precipita pattern	ation	Effect o irrigatio	f	Effect o precipita pattern		Effect o irrigatio	
		Rainfed	Irrigated	Baseline precipita tion		Rainfed		Baseline precipita tion		Rainfed	Irrigated	Baseline precipita tion	More intermitt ent precipita tion
		R <sub>baseline</sub> vs R <sub>intermittent</sub>	I <sub>baseline</sub> VS I <sub>intermittent</sub>	R <sub>baseline</sub> vs I <sub>baseline</sub>	R <sub>intermittent</sub> vs I <sub>intermittent</sub>	R <sub>baseline</sub> vs R <sub>intermittent</sub>	I <sub>baseline</sub> vs I <sub>intermittent</sub>	R <sub>baseline</sub> vs I <sub>baseline</sub>	R <sub>intermittent</sub> vs I <sub>intermittent</sub>	R <sub>baseline</sub> vs R <sub>intermittent</sub>	I <sub>baseline</sub> VS I <sub>intermittent</sub>	R <sub>baseline</sub> vs I <sub>baseline</sub>	R <sub>intermittent</sub> vs I <sub>intermittent</sub>
$T_{c,mean}$	Test on equal median df=1	17.42 <u>32</u> .40 <0.001	0.02 3.14 0.08 <u>0.9</u> 0	138.38 <u>1</u> 53.66 <0.001	345.742 87.30 <0.001	12.54 < 0.001	0. <u>78</u> 14 0. <u>38</u> 7	360.00 <del>3</del> 45.74 <0.001	484.42 <0.001	16.38 <u>26</u> .90 <0.001	0.78 <u>0.0</u> 0 0.38 <u>1.0</u> 0	84.42	602.185 01.26 <0.001
	Test on equal variance df=[1,998]	13.32 <u>18</u> .49 <0.001	9		478.06 <u>5</u> 00.80 <0.001	<u>5</u>		68.75	83.39	4.11 <u>9.9</u> 3 <0.05	0. <u>00</u> <del>55</del> 1.00 <del>0.4</del> 6		417.16 <u>3</u> 27.12 <0.001
$P_{CHS}$	Test on equal median df=1	2 <u>3</u> 0. <u>11</u> 2 2 <0.001	1.34 <u>0.1</u> 32.32 20.1320	54.53	12.98	22.03 <u>13</u> .00 <0.001	0.71 0.40	490.96 <u>4</u> 78.33 <0.001	58.39	83	0. <u>79</u> 90 0.3 <u>7</u> 4	472.21 <u>4</u> 99.48< 0.001	
	Test on equal variance df=[1,998]	.06	2. <u>20</u> <del>08</del> 0.1 <u>4</u> 5		<u>82.66</u>	8	0. <u>0419</u> 0. <u>8467</u>		590.33 <u>5</u> 88.32 <0.001	4	3.60 <sub>0.0</sub> 4 0.84 <u>06</u>	116.85	131.57 <u>8</u> 2.91 <0.001

		Rainfed		Irrigated		
		Baseline precipitation	More intermittent precipitation	Baseline precipitation	More intermittent precipitation	
$T_{c,mean}$	Test on equal median df=2	6 <u>64</u> 40. <u>62</u> 19 <0.001	534. <u>93</u> 35 <0.001		980.21 <u>1000</u> <0.001	
	Test on equal variance df=[2,1497]	2.68 <del>7.19</del>	0.11 <mark>2.55</mark> 0. <u>89</u> 08	19.2 8.18 <0.001	5.39 <u>24.02</u> <0.01	
$P_{CHS}$	Test on equal median df=2	5 <u>83.2171.5</u> 4 <0.001	457.37 473.04 <0.001	9 <u>3</u> 24. <u>6</u> 70 <0.001	909.45 972.86 <0.001	
	Test on equal variance df=[2,1497]	36.57 <del>27.75</del> <0.001	19. <u>6692</u> <0.001	238.00 276.15 <0.001	336.63 292.53 <0.001	

Table S7: Statistical tests of the role of air temperature variance on median and variance of canopy temperatures, for different rainfall patterns and management combinations, based on 500 simulations. For each test, the test statistics (top) and p value (bottom) are reported. The degrees of freedom (df) are specified for each type of test. Data are summarized in Fig. S63.

		Rainfed		Irrigated	
		precipitation	More intermittent precipitation	Baseline precipitation	More intermittent precipitation
	Test on equal median df=2	3.38 <del>1.78</del>	2.13 <mark>1.78</mark> 0. <u>35</u> 41	12.74 <u>11.20</u> <0.01	7.98 8.26 <0.05
	variance	0. <del>09</del> 17	0.24 <u>81</u> 0. <u>4579</u>	33. <u>1461</u> <0.001	23.4 <u>8</u> 7 <0.001
$P_{CHS}$	Test on equal median df=2	4.52 <u>3.86</u> 0.1 <u>4</u> 0		327. <u>75</u> 84 <0.001	295. <u>7051</u> <0.001
	Test on equal variance df=[2,1497]	19. <u>22</u> <del>31</del> <0.001	2 <del>7.69</del> 28.83 <0.001	68.09 <u>64.26</u> <0.001	65.21 <u>64.82</u> <0.001

		precipitation	More intermittent precipitation
$T_{c,mean}$	Test on equal median df=2	<del>1.34</del> <u>2.50</u>	1.460.98 0.4861
	Test on equal variance df=[2,1497]	0. <u>33<del>20</del></u>	1.10 <del>0.46</del> 0. <u>36</u> 3
$P_{CHS}$	Test on equal median df=2	2. <u>1273</u> 0. <u>3526</u>	1.452.42 0.4930
	Test on equal variance df=[2,1497]	0.0 <u>7</u> 4 0.9 <u>46</u>	1. <u>90</u> 47 0. <u>1523</u>

## S5 Methodological considerations

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## S5.1 Modeling assumptions and their implications

420 The model developed does not explicitly take into account the vertical dimension, i.e., the canopy was approximated by a big leaf and the soil moisture balance was represented via a bucket-filling model.

The big-leaf approximation scales up the leaf-level carbon and water fluxes, assuming that the entire canopy is subject to the same conditions and behaves in the same way. Hence, sunlit and shaded leaves cannot be distinguished. This could underestimate the effects of solar radiation and the temperature of sunlit leaves. Indeed,  $T_c$  simulated by big-leaf model was around 1 °C higher than the simulated temperatures for shaded leaves but lower than those of sunlit leaves (Dai et al., 2004). Yet, we considered solar radiation at the top of the canopy, thus effectively representing sunlit leaves, i.e., providing an overestimate of the temperatures to which leaves are exposed. Further, the big-leaf approximation cannot capture the effects of the wind velocity profile within the canopy, leading to canopy layers nearer to the ground to be warmer than the higher ones. These are also the layers where solar radiation is lower, thus potentially balancing out the effects of the simplifications implicit in the big-leaf framework.

The bucket-filling model assumes uniform soil moisture conditions over the active rooting zone, thus potentially underestimating the soil water availability near the soil surface soon after rainfall events and deeper in the profile later in the dry down. Hydraulic redistribution and, in general, the plant's ability to take up water at different depths limit the effects of such simplification on the modeled soil moisture (Guswa et al., 2002) and hence on the model results. Neglecting lateral flows is generally adequate in most agricultural contexts, where fields are flat and horizontally homogeneous. We also assumed instantaneous (at the daily time scale) runoff and deep percolation when soil moisture reached the threshold  $s_1$ —just above soil field capacity. Because soil hydraulic conductivity is a highly non-linear function of soil moisture (Clapp and Hornberger, 1978), the soil drains quickly above  $s_1$ . Indeed, this simplified approach leads to soil moisture dynamics similar to those obtained including runoff as saturation excess and assuming deep percolation to be proportional to the soil hydraulic conductivity (e.g., Laio et al., 2001; not shown). The small quantitative contributions of losses via runoff and deep percolation to the soil water balance (Fig. S3 and S4) lend further support to the choice of a simplified description of these processes. The advantage of considering instantaneous losses above  $s_1$  is that the soil moisture balance can be integrated with a daily time step – in line with that of the canopy temperature model – without significant numerical errors (Clapp and Hornberger, 1978).

While the model is capable of simulating the diurnal cycle and the whole growing season, we limited the analyses to the warmest part of the day and the crop's most sensitive developmental stage, anthesis. Similarly, the model can accommodate the temporal evolution of environmental conditions beyond air temperature <u>fluctuations</u> and precipitation occurrence, but we set them constant and interpreted them as averages (for RH and U) and maximum (for  $Q_0^{\downarrow}$ ) during the simulation period. We also assumed clear skies, thus potentially overestimating canopy temperatures when compared with cloudy conditions. Taken together, these assumptions leaded to an overestimate of  $T_c$  and hence of the frequency of canopy temperature exceeding the threshold for potential damage.

#### S5.2 Alternative approach to estimating canopy conductance

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The soil moisture – canopy conductance relation emerging from the stomatal optimization model coupled with the SPAC (Eq. S9-S18) was compared with an empirical model of canopy-level conductance determined based on eddy covariance data. The dependence of canopy conductance to water vapor on DD was shown to be well approximated as (Oren et al., 1999):

$$G_s = G_{s,ref} \cdot [1 - m \cdot \ln(P_a D)], \tag{S30}$$

where  $P_a$  is the air pressure (in kPa); the intercept parameter  $G_{S,ref}$  is the reference surface conductance rate (mmol m<sup>-2</sup> s<sup>-1</sup>)<sub>2</sub> corresponding to the <u>canopy</u> conductance at  $D = 10^{-2}$  mol mol<sup>-1</sup>; and the slope parameter m ([ln(kPa)]<sup>-1-1</sup>) represents the sensitivity of <u>surface canopy</u> conductance to D. Both  $G_{S,ref}$  and m increase with soil water availability, as e.g. shown by a <u>synthesis of eddy covariance data</u> (Novick et al., 2016). For crops, a linear regression of the data presented by Novick et al. (2016) yielded

$$G_{s,ref} = 552 \theta + 259,$$
 (S31)

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$$m = 0.57 \theta + 0.13, \tag{S32}$$

where  $\theta$  is the volumetric soil water content, related to the soil moisture s as  $\theta = n$  s, with n being the soil porosity.

During a dry down, the predicted <u>surface canopy</u> conductance obtained with the empirical approach (Eq. S30-S32) and the mechanistic model used in this work (Eq. S9-S18) were similar at air temperature  $T_a = 20$  °C, but the empirical model provided a higher value of conductance at  $T_a = 15$  °C and a lower one at  $T_a = 25$  °C and 30 °C (Fig. S26). These discrepancies underline the importance of including mechanistically all the temperature dependences, unless site- and crop-specific data are available to correctly determine the canopy conductance empirically.

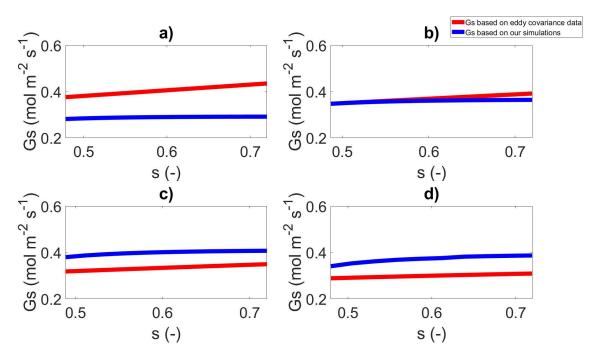


Figure S62: Comparison of two approaches to the determination of the canopy conductance for different air temperatures (a, b, e, d correspond to = 15, 20, 25, 30 °C respectively). Surface Canopy conductance  $G_s$  (mol m<sup>-2</sup> s<sup>-1</sup>) as a function of soil moisture s, based on the upscaling of the leaf-level optimal stomatal conductance (in blue) is compared with and the empirical model based on eddy covariance data (Eq. S30-S32; in red) for different air temperatures (a, b, c, d correspond to  $T_a$  = 15, 20, 25, 30 °C

475 respectively). To avoid extrapolations, the range of soil moisture considered corresponds to that for which data on  $G_s$  are available in Novick et al. (2016).

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