

1        **Estimation of rainfall erosivity based on WRF-derived raindrop size distributions**

2        Qiang Dai<sup>1,2</sup>, Jingxuan Zhu<sup>1</sup>, Shuliang Zhang<sup>1</sup>, Shaonan Zhu<sup>3</sup>, Dawei Han<sup>2</sup> and Guonian Lv<sup>1</sup>

3        <sup>1</sup>Key Laboratory of VGE of Ministry of Education, Nanjing Normal University, Nanjing, China.

4        <sup>2</sup>Department of Civil Engineering, University of Bristol, Bristol, UK.

5        <sup>3</sup>College of Geographical and Biological Information, Nanjing University of Posts and  
6        Telecommunications, Nanjing, China

7        Corresponding author: Qiang Dai (qd\_gis@163.com)

8        **Key Points:**

- 9        • Rainfall kinetic energy derived from the Weather Research and Forecasting model offers  
10       a novel way to estimate large-scale soil erosion.
- 11       • Annual rainfall and erosivity are not always positively correlated.
- 12       • Highest rainfall erosivity of UK occurs in the west coast area during 2013–2017.

13

## 14 **Abstract**

15 Soil erosion can cause various ecological problems, such as land degradation, soil fertility loss,  
16 and river siltation. Rainfall is the primary water-driving force for soil erosion, and its potential  
17 effect on soil erosion is reflected by rainfall erosivity that relates to the raindrop kinetic energy.  
18 As it is difficult to observe large-scale dynamic characteristics of raindrops, all the current  
19 rainfall erosivity models use the function based on rainfall amount to represent the raindrops  
20 kinetic energy. With the development of global atmospheric re-analysis data, numerical weather  
21 prediction techniques become a promising way to estimate rainfall kinetic energy directly at  
22 regional and global scales with high spatial and temporal resolutions. This study proposed a  
23 novel method for large-scale and long-term rainfall erosivity investigations based on the Weather  
24 Research and Forecasting (WRF) model, avoiding errors caused by inappropriate rainfall–energy  
25 relationships and large-scale interpolation. We adopted three microphysical parameterizations  
26 schemes (Morrison, WDM6, and Thompson aerosol-aware) to obtain raindrop size distributions,  
27 rainfall kinetic energy and rainfall erosivity, with validation by two disdrometers and 304 rain  
28 gauges around the United Kingdom. Among the three WRF schemes, Thompson aerosol-aware  
29 had the best performance compared with the disdrometers at a monthly scale. The results  
30 revealed that high rainfall erosivity occurred in the west coast area at the whole country scale  
31 during 2013–2017. The proposed methodology makes a significant contribution to improving  
32 large-scale soil erosion estimation and for better understanding microphysical rainfall–soil  
33 interactions to support the rational formulation of soil and water conservation planning.

34

## 35 **1 Introduction**

36 Soil erosion plays a pivotal role in shaping the Earth’s physical landscape; however, it  
37 can threaten both ecosystems and human societies (Alewell et al., 2015). Accurate quantification  
38 of soil loss impact at large spatial scales is therefore important for developing land-use planning  
39 and sustainable conservation practices (Bilotta et al., 2012). The soil erosion rate is driven by a  
40 combination of factors, including rainfall, topography, soil characteristics, land cover, and land  
41 management applications (Wischmeier and Smith, 1958; Panagos et al., 2015b). Among these,  
42 rainfall is a driving force that accounts for a large proportion of soil loss throughout most of the  
43 world (Panagos et al., 2015b). The erosive force of rainfall with consequent runoff is represented

44 as erosivity of rainfall. This is a crucial factor for estimating soil loss in large-scale soil erosion  
45 models; for instance, the Universal Soil Loss Equation (USLE (Wischmeier and Smith, 1978) or  
46 RUSLE (Renard et al., 1997)), Limburg Soil Erosion Model (LISEM) (De Roo et al., 1996), and  
47 USLE-M (Kinnell and Risse, 1998).

48         Rainfall erosivity estimation involves the microphysical properties of rainfall and  
49 rainfall–soil interactions on different time steps (Petan et al., 2010). Impact of rainfall, the main  
50 mechanism driving the splashing of soil particles from the soil mass, which leads to soil erosion  
51 through soil disintegration and mobilization, relies on the kinetic energy (KE) of raindrop  
52 motions (Wischmeier and Smith, 1958; Wang et al., 2014). Robust measurement of raindrop size  
53 and terminal velocity is vital for estimating and predicting rainfall erosivity. Many measurements  
54 can be used to obtain these two parameters, including the stained paper or flour pellet methods  
55 (Marshall and Palmer 1948; Wischmeier and Smith, 1958), high speed cameras (Jones, 1959;  
56 Kinnell, 1981; McIsaac, 1990), and disdrometers (Petan et al., 2010; Angulo-Martinez et al.,  
57 2012). Accurate measurements of raindrop size can be provided in all their methods, and  
58 terminal velocity of raindrops can be further measured by video cameras and disdrometers.  
59 Velocity can also be estimated as the function of raindrop diameter from the empirical  
60 relationship (Beard, 1976; Atlas and Ulbrich, 1977; Uplinger, 1981; Van Dijk et al., 2002).  
61 When using ground observations, rainfall KE can be estimated at a given site.

62         However, direct measurement of rainfall KE in a large area is difficult because it requires  
63 considerable effort, as well as a dense network of expensive instruments that provide accurate  
64 outputs (Fornis et al., 2005; Mikoš et al., 2006; Meshesha et al., 2016; Dai et al., 2017). Previous  
65 studies have, therefore, mainly employed more readily accessible records like rainfall intensity,  
66 and attempted to estimate rainfall KE from the empirical relationship of unit KE ( $ke$ ) with  
67 intensity ( $ke-I$ ). Since Marshall and Palmer (1948) first observed a two-parameter exponential  
68 relationship between drop size and intensity, several forms of  $ke-I$  mathematical expressions for  
69 specific locations and climatic conditions have been proposed, including power-law (Park et al.,  
70 1982; Meshesha et al., 2016), linear (Sempere-Torres et al., 1998; Nyssen et al., 2005),  
71 polynomial (Carter et al., 1974), logarithmic (Wischmeier and Smith, 1978; Davison et al., 2005;  
72 Meshesha et al., 2014), and exponential (Kinnell, 1981; Brown and Foster, 1987) relationships.  
73 Among these, the exponential function has been preferentially used currently (Van Dijk et al.,  
74 2002; Fornis et al., 2005; Petan et al., 2010; Sanchez-Moreno et al., 2012; Lim et al., 2015).

75 Accurate raindrop size distribution (DSD) measured by disdrometers is widely used to derive  $ke$ -  
76  $I$  relationships (Angulo-Martínez et al., 2016; Meshesha et al., 2016). However, such empirically  
77 derived formulas indicate that rainfall  $ke$  will increase infinitely with increasing intensity,  
78 whereas studies (Rosewell, 1986; Angulo-Martínez et al., 2016; Meshesha et al., 2019) have  
79 found that rainfall  $ke$  reaches an top value when intensity is around  $70 \text{ mm h}^{-1}$  (Hudson, 1963;  
80 Wischmeier and Smith, 1978). More importantly, such a  $ke$ - $I$  relationship only represents local  
81 climate and precipitation microphysics and is valid for such regions. There is great uncertainty  
82 associated with rainfall erosivity estimation using this  $ke$ - $I$  relationship in a large domain  
83 (Angulo-Martínez and Barros, 2015), especially due to the poor spatial and temporal  
84 predictability of the  $ke$ - $I$  relationship. This has motivated researchers to directly calculate KE  
85 based on large-scale DSD measurements.

86 Ground- and space-based radar can be used to obtain DSD parameters (Atlas et al., 1973;  
87 Doelling et al., 1998). For example, the space-borne Dual-frequency Precipitation Radar (DPR)  
88 radar containing Ku- and Ka-bands in the Global Precipitation Measurement (GPM) satellite  
89 allows researchers to estimate the global three-dimensional spatial distribution of hydrometeors.  
90 Unfortunately, ground dual-polarization radars are available in limited areas (Prigent, 2010) with  
91 large uncertainties (Dai et al., 2019), and the GPM DPR instrument, which measures DSD with  
92 daily or longer temporal resolutions, fail to capture a full storm and meet the requirement for  
93 rainfall kinetic estimation. Mesoscale numerical weather prediction models, for instance, the  
94 WRF model, can simulate microphysical cloud processes and predict the evolution of particle  
95 size distribution through computationally feasible parametrization schemes (Dai et al., 2014;  
96 Brown et al., 2016). DSD on the ground can be derived from the WRF model through  
97 consideration of various physical processes, types of hydrometeor, and free degrees of size  
98 distributions in hydrometeor. As such, a number of recent researches have investigated the  
99 retrieval and uncertainty of DSD parameters by WRF (Gilmore et al., 2004; Ćurić et al., 2009;  
100 Brown et al., 2016; Yang et al., 2019).

101 The WRF model runs with initial and boundary conditions using global reanalysis  
102 datasets, such as those of the European Centre for Medium-range Weather Forecasts (ECMWF)  
103 and National Centers for Environmental Prediction (NCEP). In other words, WRF-derived DSD  
104 can be obtained for any given area with fine spatial and temporal resolutions rather than  
105 traditional course linear interpolations. We therefore attempted to estimate rainfall erosivity for

106 the entirety of the United Kingdom (UK) domain using WRF-derived DSD. For comparison, we  
 107 also calculated interpolated traditional disdrometer-derived rainfall erosivity. To our knowledge,  
 108 this work is the first attempt to take advantage of a numerical weather prediction model for  
 109 estimating rainfall erosivity anywhere around the world. The current study contributes to the  
 110 development of large-scale soil erosion estimation and provides a better comprehension of  
 111 microphysical rainfall–soil interactions.

## 112 **2 Methodology**

### 113 2.1 Disdrometer-based rainfall KE estimation

114 KE dominates the ability of raindrops to separate soil particles. The KE ( $e$ , unit: J) of a  
 115 raindrop with mass  $m$  (g) and terminal velocity  $v$  ( $\text{m s}^{-1}$ ) is defined by:

$$e = \frac{1}{2} mv^2 \quad (1)$$

116 Assuming a spherical volume for every raindrop shape, the mass of a drop can be  
 117 calculated from the cube of the diameter  $D$  (mm). Because instruments (e.g., disdrometers)  
 118 generally sample drop size, the mean radius and falling velocity of the corresponding sampling  
 119 drop-size class are used to represent  $D$  and  $v$ , expressed as  $D_i$  and  $v_i$ , respectively. In such cases,  
 120 the  $e_i$  with any drop of a given class is given as:

$$e_i = \frac{1}{12} 10^{-6} \pi \rho v_i^2 D_i^3 \quad (2)$$

121 where  $\rho$  is the water density ( $\text{g cm}^{-3}$ ). The sum of the KE of each individual raindrop within a  
 122 given rain depth that hits a given area defines the total KE. The unit rainfall KE  $ke_t$  in the  $t^{\text{th}}$   
 123 minute ( $\text{MJ ha}^{-1} \text{mm}^{-1}$ ) can be calculated as the sum of each drop KE in each size set, as follows:

$$ke_t = \frac{e_{sum}}{AP_t} = \frac{1}{AP_t} \sum_{i=1}^{ni} N_i e_i \quad (3)$$

124 where  $A$  represents the sample area of the sensor,  $P_t$  is rainfall depth at time  $t$ , and  $N_i$  is the drops  
 125 number in class  $i$ . The instrument sums up the number of raindrops in each sampling class and  
 126 produces the raindrop spectra for a time step. Here, we use the term  $ke$  to represent the  
 127 disdrometer-based KE estimated by DSD directly measured every minute. The terminal velocity

128 of a raindrop can be estimated from its power law empirical relationship with raindrop diameter  
 129 (Atlas and Ulbrich, 1977), with this considered more suitable for Chilbolton in the UK (Islam et  
 130 al., 2012):

$$v_{Atl} = 3.78D_i^{0.67} \quad (4)$$

131 Thus, unit rainfall KE estimates per minute are obtained by replacing  $v_i$  in Eq. (2) with  $v_{Atl}$ .

132 The other form of rainfall KE is expressed at an event scale and represents the sum of the  
 133 storm energy covering all time steps covering an event. The individual event energy ( $\text{MJ ha}^{-1}$ ) is  
 134 calculated as follows:

$$E = \sum_{t=1}^{nt} ke_t P_t \quad (5)$$

135 where  $P_t$  is the rainfall amount (mm) in the  $t^{\text{th}}$  minute and  $nt$  is the time steps number. Historical  
 136 rainfall data are divided into wet and dry periods. A string of erosive rainfall storms is first  
 137 extracted through the predefined rules. A continuous 6-h dry period interval was used to divide  
 138 rainfall events (Hanel et al., 2016), following the “minimum dry-period duration” definition of a  
 139 rainfall event (Bonta, 2004). Moreover, a rainfall amount of 12.7 mm was set as the threshold to  
 140 filter effective rainfall events (Renard et al., 1997).

141 Rainfall KE is obtained for a given site based on size and velocity of raindrops. When  
 142 disdrometer data are absent, energy can be estimated from empirical relationships using rainfall  
 143 intensity  $I$  (mm). Five commonly used functions (including exponential, logarithmic, power law,  
 144 and inverse proportion) have been mentioned in Section 1. Taking the exponential form as an  
 145 example, the rainfall KE at any location can be estimated as:

$$E_{\max} = e_{\max}(1 - ae^{-bI}) \quad (6)$$

146 where  $e_{\max}$  is the mean maximal value of energy measured under high rainfall intensity, and  $a$   
 147 and  $b$  are coefficients modeling the equation curve. Here, minimum KE can be determined by  
 148 parameters  $a$  and  $e_{\max}$  together, while the overall shape of the curve is modeled by parameter  $b$ .

149 2.2 WRF-based rainfall KE estimation

150 Differing from disdrometer measurements, the complete DSD cannot be obtained from  
 151 the WRF model. Instead, the DSD of the microphysical parameterization (MP) scheme is  
 152 handled with a constrained-gamma distribution model, which is defined as:

$$N(D) = N_0 D^\mu e^{-\lambda D} \quad (7)$$

153 where  $N_0$ ,  $\mu$ , and  $\lambda$  are the intercept, shape, and slope parameters of the DSD. In terms of  
 154 double-moment bulk schemes,  $N_0$  and  $\lambda$  can be abstracted from the number concentration  $N$  and  
 155 predicted mixing ratio  $q$ , as shown below:

$$N_0 = \frac{N \mathcal{M}^{\mu+1}}{\Gamma(\mu + 1)} \quad (8)$$

$$\lambda = \left[ \frac{cM(\mu + d + 1)}{q\Gamma(\mu + 1)} \right]^{\frac{1}{d}} \quad (9)$$

156  $c$  and  $d$  are the assumed power-law coefficients between diameter and mass ( $m = cD^d$ ), and  $\Gamma$   
 157 represents the function in gamma form (Morrison et al., 2009). The value of the shape parameter  
 158  $\mu$  ( $\mu = 0$ ) in double-moment schemes is fixed, except for the WRF double-moment 6-class  
 159 (WDM6) schemes, following gamma distribution, which defined  $\mu = 1$  (Jung et al., 2010;  
 160 Johnson et al., 2016).

161 Because DSD retrieval is sensitive to MPs (Cintineo et al., 2014; Morrison et al., 2015),  
 162 the WRF model this study adopted completely or partially three types of double-moment cloud  
 163 MP schemes. The Morrison double-moment scheme involves the number concentrations and  
 164 mixing ratios of multiple hydrometeors (Morrison et al., 2009). Moreover, the WDM6 scheme  
 165 further considers a prognostic factor to estimate and predict the cloud condensation nuclei (CCN)  
 166 number concentration (Hong et al., 2010; Lim and Hong, 2010). Finally, the Thompson aerosol-  
 167 aware (TAA) scheme can predict both ice nuclei (IN) and CCN number concentrations  
 168 (Thompson and Eidhammer, 2014).

169 The DSD parameters were thus obtained under the three WRF MPs. For theoretical DSD,  
 170  $ke$  estimates per minute were obtained by integration of the full raindrop size spectrum using:

$$ke'_t = \frac{1}{AR_t} \int_0^\infty N(D) \frac{1}{12} 10^{-6} \pi \rho v_i^2 D_i^3 dD \quad (10)$$

171 For the WRF-derived DSD covering the whole study area, there was no need to construct  
 172 a  $ke$ - $I$  relationship to interpolate KE in ungauged areas. The WRF-based rainfall KE under storm  
 173 event scale is thus given as:

$$E_w = \sum_{t=1}^{nt} ke'_t P_t \quad (11)$$

### 174 2.3 Rainfall erosivity estimation

175 Most storm events have relatively low intensities and KEs with occasional peaks, based  
 176 on the disdrometer DSD data used to evaluate the rainfall  $ke$ - $I$  function. Proper estimation of  
 177 rainfall erosivity potential should consider total KE over a long period. The rainfall erosivity  
 178 factor (or R-factor) is calculated by a multi-annual average of the total storm erosivity index  
 179 (Wischmeier and Smith, 1958; Van Dijk et al., 2002), while annual rainfall erosivity  $R$  can be  
 180 obtained using:

$$R = \sum_{m=1}^M (EI_{30})_m \quad (12)$$

181 where  $M$  is the total number of erosive events within a year.  $(EI_{30})_m$  are total rainfall kinetic  
 182 energy and maximum 30-min rainfall intensity recorded within 30 consecutive minutes (unit:  
 183  $\text{mm h}^{-1}$ ), respectively, for the  $m^{\text{th}}$  event.

184 Wischmeier and Smith (1958) first proposed the use of  $EI_{30}$ , as the rainfall erosivity for  
 185 each event, based on research data from many sources.  $I_{30}$  was calculated to have higher  
 186 relevance to soil erosion than maximum 5-min, 15-min, or 60-min rainfall intensities  
 187 (Wischmeier and Smith, 1958). The calculation of  $EI_{30}$  initially uses recording-rain gauge data to  
 188 divide continuous rainfall into time periods with equal rainfall intensity. Though rainfall  
 189 measurements with high temporal resolutions are required, it is difficult to obtain them from  
 190 general rainfall measurements. Therefore, short time equal-interval rainfall data with higher  
 191 accuracy over multiple years are preferred for estimating  $EI_{30}$ . For example, Xie et al. (2016)  
 192 used 1-min rainfall data instead of recording-rain gauge records. For coarse-resolution, equally



193 spaced data, researchers have proposed a conversion factor to reduce bias error (Weiss, 1964;  
 194 Williams and Sheridan, 1991).

195 The rainfall erosivity can be derived from rainfall KE. It plays a main dynamic role in  
 196 USLE/RUSLE, representing the potential for soil erosion caused by rainfall. To distinguish the  
 197 disdrometer- and WRF-derived rainfall erosivity in this study, we use the terms  $R_D$  and  $R_W$ ,  
 198 respectively.

## 199 2.4 Evaluation methods

200 Because there is no direct way to measure rainfall erosivity across a large area, it is  
 201 difficult to validate outcomes using observations. However,  $R_D$  is considered to be relatively  
 202 accurate due to its specific measurement of raindrops. We therefore assumed that  $R_W$  values were  
 203 accurate if it closely matched  $R_D$  of a given location. A long-term comparison of  $R_W$  and  $R_D$  at  
 204 disdrometer stations was thus conducted to evaluate the validity of  $R_W$ .

205 Three indicators were introduced for the evaluation: Pearson's correlation coefficient,  
 206 mean absolute error (MAE), and coefficient of determination ( $R^2$ ) (Borrelli et al., 2017). Pearson  
 207 correlation coefficient is an index used to evaluate the linear correlation between two variables,  
 208 and is defined as follows:

$$209 \text{ Pearson} = \frac{n \sum R_{D_i} \sum R_{W_i} - \sum R_{D_i} \sum R_{W_i}}{\sqrt{n \sum R_{D_i}^2 - (\sum R_{D_i})^2} \sqrt{n \sum R_{W_i}^2 - (\sum R_{W_i})^2}} \quad (13)$$

209 where  $n$  is the number of variable samples. Because this correlation cannot reveal the absolute  
 210 bias of rainfall erosivity values, the MAE was also used; this is defined as:

$$211 \text{ MAE} = \frac{\sum |R_{W_i} - R_{D_i}|}{n} \quad (14)$$

211  $R^2$  is an indicator to assess the fit of the trend line, expressed as the ratio of the variance  
 212 in the dependent variable predicted from the independent variable. It measures the extent to  
 213 which the model replicates observations based on the proportion of the results interpreted by the  
 214 model to the total change, written as:

$$R^2 = 1 - \frac{SS_{res}}{SS_{tot}} \quad (15)$$

215 where  $SS_{res}$  is the sum of squares of residuals between two variables, and  $SS_{tot}$  is the total sum of  
216 squares.

### 217 **3 Study area and data sources**

218 The whole of the UK was set as the experimental area for investigating rainfall erosivity  
219 estimation. The UK consists of mostly lowland terrain, with a maximum elevation of 1345 m.  
220 Water and wind are the most significant forces of soil erosion in the UK. Together, they cause  
221 approximately 2.2 million tons of topsoil to be eroded annually, seriously affecting soil  
222 productivity, water quality, and aquatic ecosystems through siltation of watercourses (EA, 2004).  
223 According to the Environmental Agency, the total cost of soil erosion in the UK is approximately  
224 \$88 million each year, including an agricultural production loss of \$17.6 million (O'Neill, 2007).  
225 More importantly, the changing climate may exacerbate the degree of erosion. For example,  
226 hotter, drier climates make soils more susceptible to wind erosion, and intense storms increase  
227 rainfall erosivity (Defra, 2009). Studies of water erosion in England and Wales (Morgan, 1985;  
228 Evans, 1990) have found that loose soils (especially sand), such as the soils found in Shropshire  
229 and Herefordshire in Wales, are more susceptible to water erosion. In a study of rainfall erosion  
230 in Europe, Panagos et al. (2015a) found that the humid Atlantic climate results in highly variable  
231 rainfall erosivity, such as higher R-factor values in western England and lower values in the  
232 eastern UK.

233 The gauge datasets used are from the land surface and marine surface measurements  
234 datasets (data availability: 1853–present) provide by the UK Met Office. A network of rain  
235 gauges covering 304 stations across the whole UK observes continuous rainfall data in hours  
236 (Figure 1). The base data of most stations comprises the times of each tip (0.2 mm per tip),  
237 converted into 1-h rain accumulations. The rainfall observations are not always valid for each  
238 hour at each station. The hourly grid-based rainfall maps are then calculated based on ordinary  
239 kriging interpolation of rain gauge network data to obtain the spatial distribution of rainfall for  
240 each time step, as inputs for rainfall erosivity estimation. This wide-range-use geostatistical  
241 approach can account for both the distance and pairwise spatial relationship between points

242 through variograms. The precipitation interpolation method uses sample gauge points taken at  
243 different locations and creates a continuous surface to achieve an accurate spatial variation  
244 estimation of rainfall patterns.

245 We used data from two disdrometers in southern England. The first was Chilbolton  
246 station (51°08'N, 1°26'W), with an impact-type Joss–Waldvogel disdrometer (JWD) mainly  
247 used to compute rainfall erosivity. It can measure drop sizes from 0.3 to 5.0 mm in 127 bins. The  
248 sampling period and collector area were 10 s and 50 cm<sup>2</sup>, respectively. Data were available for  
249 April 2003 to July 2018. The second was the University of Bristol station (51°27'N, 2°36'W),  
250 with an OTT Parsivel<sup>2</sup> disdrometer (OPD). Data were available for November 2015 to December  
251 2018. This disdrometer subdivides particles into appropriate classes and has a nominal cross-  
252 sectional area of 54 cm<sup>2</sup>. The 10-s period measurement data from the two disdrometers were  
253 averaged into a 1-min period to filter out time variations (Montopoli et al., 2008; Islam et al.,  
254 2012; Song et al., 2017).

255 Meteorological data comes from the ERA-Interim dataset, a global atmosphere re-  
256 analysis product, generated by the ECMWF. For the scientific community, ERA-Interim is  
257 considered to be one of the most important atmospheric datasets, with its data-rich period  
258 available since 1979 and updated in current time (Dee et al., 2011). The Integrated Forecasting  
259 System released in 2006 contains a 12-h analysis window derived 4-D variational analysis,  
260 driving the data assimilation system to generate ERA-Interim. The dataset covers 60 vertical  
261 classes of approximately 80 km from the ground to 0.1 hPa. The Gridded Binary format is used  
262 to store data for three months in a separate file. A data processing scheme was established to  
263 collect and retrieve ERA-Interim data of each rainfall event.

264 The rain gauge and Chilbolton disdrometer datasets can be obtained from British  
265 Atmospheric Data Centre in National Centre for Atmospheric Science research center (MO,  
266 2012). ERA-Interim data can be obtained from the ECMWF Public Dataset website  
267 (<https://apps.ecmwf.int/>). Considering the availability of the above datasets and model  
268 requirements, we mainly used data covering the period 2004–2017.

## 269 4 Results

### 270 4.1 Empirically derived rainfall erosivity estimation

271 To evaluate the  $R_w$ , the raindrop spectrum collected by the Chilbolton station disdrometer  
272 is used to estimate rainfall KE first. The key in estimating rainfall KE by disdrometer lies in  
273 building an empirical relationship between rainfall amount and KE. We used DSD measurements  
274 from 2004 to 2013 to establish five empirical relationships between unit rainfall kinetic energy  
275 ( $ke$ ) and intensity ( $I$ ) (Table 1) and used 2014–2017 data for the cross-validation. It can be seen  
276 from Table 1 that the inverse proportional relationship (Equation III) had the worst performance,  
277 in that both the calibration and validation  $R^2$  values were  $< 0.3$ . The values of the other equations  
278 were  $> 0.48$ , among which the exponential formula (Equation I) had the highest calibration  $R^2$   
279 (0.50) and validation  $R^2$  (0.45), respectively. In addition, the power law formula (Equation V)  
280 showed a similar performance to the exponential formula at rainfall intensities  $< 5 \text{ mm h}^{-1}$ .  
281 However, the power law formula also had a continuously increasing trend, which may not be  
282 suitable for high-intensities. Figure 2 shows the  $ke$ – $I$  relationship and five fitted curves at  
283 Chilbolton station. It can be seen that the two logarithmic curves (Equation II and IV) invariably  
284 overlap. The logarithmic form has been used for a long time in USLE (Wischemier and Smith,  
285 1978). It describes  $ke$  well at both low and high  $I$ , but does not have an upper limit. The power  
286 law curve (Equation V) can predict  $ke$  well at lower  $I$  but overestimates  $ke$  at high  $I$ . The  
287 exponent-based relationship (Equation I) is widely used in the literature and in forecast models  
288 such as RUSLE (Renard et al., 1997), which fits the data particularly well in Figure 2. Even  
289 though  $ke$  in exponential curve has a minimum value at very low  $I$ , it also should be noted that  
290 higher rainfall intensities are much more important in determining overall storm energy than  
291 lower intensities. Therefore, we adopted it here as the empirical formula to estimate rainfall  
292 erosivity in the UK.

293 Based on rainfall KE, the point  $R_D$  can be obtained at a disdrometer location. In the  
294 current study, we established a method to estimate the  $R$  using 60-min rainfall data.  $EI_{30}$  obtained  
295 from 1-min DSD data was considered as the standard  $R$  at Chilbolton Station. Hourly rain gauge  
296 data at the same location were used to calculate  $(EI_{30})_{60}$ , which refers to  $EI_{30}$  calculated from 60-  
297 min data. The regression relationship between  $EI_{30}$  and  $(EI_{30})_{60}$  was then established. The  $(EI_{30})_{60}$   
298 of each month, obtained from the 60-min rainfall data of the Chilbolton Station rain gauge in

299 2004–2013, was calculated. The regression relationship between the monthly sum of  $(EI_{30})_{60}$  and  
300 the standard monthly  $EI_{30}$  from DSD was calculated to obtain a coefficient of 1.836. Rainfall  
301 erosivity can subsequently be calculated by multiplying  $(EI_{30})_{60}$  by the coefficient.

302 Beyond assuming that the disdrometer-derived  $ke-I$  relationship can be applied to a  
303 whole study area; point rainfall measurements must be interpolated to obtain areal rainfall values  
304 in traditional rainfall erosivity estimation. We obtained 60-min rainfall data from 304 rain gauges  
305 around the UK from 2004 to 2017. Note that not all rain gauges were available for the whole  
306 period (available gauges each year are indicated in Figure 3). We used the ordinary kriging  
307 interpolation method to obtain the spatial distribution of rainfall for each time step. This wide-  
308 range-use geostatistical approach can account for both the distance and pairwise spatial  
309 relationship between points through variograms. Figure 3 shows the results of annual rainfall  
310 ( $Rain$ ), annual rainfall kinetic energy ( $E$ ), and annual rainfall erosivity ( $R$ ) for different years.  
311 The distribution trends of  $Rain$ ,  $E$ , and  $R$  were similar, and positively correlated except for  
312 certain locations or periods. For instance, in 2013,  $Rain$  in the northwestern UK decreased from  
313 west to east, while  $E$  and  $R$  decreased from south to north; furthermore, areas with large  $E$  and  $R$   
314 values in southeastern UK could not be directly observed from the rain map.

315 The key concern in traditional rainfall erosivity estimation is the spatial predictability of  
316 the  $ke-I$  relationship. To verify the regional reliability of this relationship, we used data from a  
317 newer disdrometer located at the University of Bristol, approximately 87 km from Chilbolton  
318 Station. The validation data at Bristol Station discontinuously covered the period 2016–2019.  
319 Figure 4 shows the exponential relationship of  $ke-I$  at Bristol station, which differed  
320 substantially from that based on data from Chilbolton station. A comparison of the modeled and  
321 observed event rainfall erosivity is shown in Figure 5. The modeled erosivity of rainfall event  
322 was not consistent with the observed event rainfall erosivity. The linear regression coefficient  
323 between these values was  $> 1.2$ , which was the result of the low  $ke$  for Bristol Station, and  $R^2$   
324 was  $< 0.85$ , indicating considerable uncertainty associated with disdrometer-based rainfall  
325 erosivity estimation.

326 In summary, the point rainfall erosivity estimated by disdrometer is considered to be  
327 accurate compared to other methods. However, a large-scale rainfall erosivity through a simple  
328 interpolation of rainfall KE is subjected to a significant uncertainty. In the following analysis, the

329 point  $R_D$  is used to appraise the performance of the proposed WRF-based estimated method, and  
 330 the  $R_D$  in the whole UK is only be used for a general comparison of spatial and temporal  
 331 distribution of rainfall erosivity.

#### 332 4.2 Rainfall and DSD estimation by WRF

333 We used the WRF model ver. 3.8, which has an Advanced Research WRF dynamical  
 334 core, to downscale the ERA-Interim reanalysis data. The double-nested domain configuration  
 335 used in the WRF model was centered at 55°19'N, 2°21'W and applied at a downscaling ratio of  
 336 1:5, a finest grid of 5 km, and a temporal resolution of 1 h. Table 2 lists the detailed parameters  
 337 used in this domain configuration. With the top pressure level set at 50 hPa in each, both  
 338 domains include 28 vertical levels. To obtain favorable initial weather conditions, the model ran  
 339 continuously to obtain five years of WRF simulation results.

340 Simulations were performed using three different bulk double moment MPs: the  
 341 Morrison (Morrison et al., 2009), WDM6 (Hong et al., 2010; Lim and Hong, 2010) and TAA  
 342 (Thompson and Eidhammer, 2014) schemes. All three can predict the number concentration and  
 343 hydrometeors mixing ratio for each time step. The WDM6 scheme also predicts the number  
 344 concentration of CCN (Hong et al., 2010; Lim and Hong, 2010), while the TAA scheme are able  
 345 to predict both IN and CCN number concentrations (Thompson and Eidhammer, 2014).  
 346 Additionally, other physical parameterizations include the Dudhia shortwave radiation scheme  
 347 (Dudhia, 1989), Mellor–Yamada–Janjic planetary boundary layer scheme (Janjić, 1994), RRTM  
 348 longwave radiation scheme (Mlawer et al., 1997), the Noah land-surface model (Ek et al., 2003),  
 349 and the Kain–Fritsch cumulus scheme (Kain, 2004),.

350 The median volume diameter parameter ( $D_0$ ) and generalized intercept parameter ( $N_w$ )  
 351 are generally used in the DSD model of WRF (Islam et al., 2012).

$$N_w = \frac{N_0 D_m^\mu}{f(\mu)} \quad (16)$$

$$f(\mu) = \frac{6(4 + \mu)^{\mu+4}}{4^4 \Gamma(\mu + 4)} \quad (17)$$

352 where  $D_m$  is the mass-weighted mean diameter. The  $f(\mu)$  is a function of the shape parameter  $\mu$ .  
 353 The parameter  $\mu$  is assumed as zero or one (based on microphysical scheme configuration) in

354 WRF. Figure 6 displays the spatial distribution of  $D_0$  and generalized intercept parameter  $N_w$  for  
355 a given day with rainfall countrywide (January 10, 2013).  $D_0$  and  $N_w$  had similar patterns and  
356 were mainly distributed across the southwestern and northeastern UK. The white strip in the  
357 middle of Figure 6 represents an area that received no rain. However, the three MPs yielded large  
358 differences;  $D_0$  of MP-TAA was the highest among three MPs, whereas  $N_w$  of MP-WDM6 was  
359 significant larger than the others. In addition,  $D_0$  and  $N_w$  did not consistently show a positive  
360 correlation. The different MP estimation results underscore the complexity of the rainfall process,  
361 which is the reason we estimated rainfall KE using WRF schemes instead of traditional formulas.

#### 362 4.3 Comparison of WRF- and disdrometer-derived rainfall erosivity at Chilbolton station

363 With the WRF-based rainfall intensity and DSD estimations, rainfall erosivity was  
364 derived using Equations (10)–(12). Hereafter, this is referred to as  $R_w$ , which is further  
365 distinguished based on the three MP schemes used:  $R_{w-Morrison}$ ,  $R_{w-WDM6}$ , and  $R_{w-TAA}$ . Figure 7  
366 compares disdrometer- and WRF-derived monthly rainfall erosivity estimations at Chilbolton  
367 station for the period 2014–2017. The general patterns of the four rainfall erosivity values were  
368 similar.  $R_{w-Morrison}$  tended to be larger than  $R_D$  in some months, whereas  $R_{w-TAA}$  matched the  $R_D$   
369 value relatively well for smaller values. Because WRF data were taken from a  $2 \times 2$ -km grid  
370 around Chilbolton station, there was a spatial error in addition to the systematic error of  
371 estimating rainfall erosivity. Based on the four-year data, the study area is rainy throughout the  
372 year with little  $R$  monthly, or seasonal patterns change (Figure 8), influenced by the temperate  
373 oceanic climate. Figure 8 also indicated that through the perspective of monthly average results,  
374  $R_{w-WDM6}$  values are low,  $R_{w-TAA}$  has a good similarity with low  $R_D$ , and  $R_{w-Morrison}$  is the closest to  
375  $R_D$  in value.

376 Table 3 shows the correlation indicator results between monthly  $R_D$  and the three types of  
377  $R_w$  at Chilbolton station. The Pearson correlation coefficients generally exceeded 0.7, supporting  
378 the potential utility of WRF-based estimation. In terms of MAE,  $R_{w-TAA}$  had the best performance  
379 (6.51), whereas  $R_{w-Morrison}$  and  $R_{w-WDM6}$  showed slightly worse performance (approximately 8).  
380 Among the three schemes,  $R_{w-TAA}$  had the best fit with  $R_D$ . The indicators and comparison results  
381 suggest that the deviations in results need to be considered; therefore, a method of bias  
382 elimination is described in Section 4.4.

#### 4.4 $R_W$ estimation for the whole UK

The  $R_W$  at Chilbolton station showed obvious systematic deviations compared with the disdrometer-derived results (see Section 4.2 and 4.3). Simple bias correction was therefore applied to adjust the individual storm KE estimations of  $R_W$ . The biases from dividing average  $R_{W-Morrison}$ ,  $R_{W-WDM6}$ , and  $R_{W-TAA}$  by average  $R_D$  during 2014-2017 were 0.55, 0.20, and 0.36, respectively.

The rainfall erosivity distribution for the whole UK was then obtained. Figure 9 shows the distribution of  $R_W$  at the annual scale covering the period 2013–2017. The pattern of the rainfall erosivity maps showed a general regional-dominant characteristic. For example, it always decreased from west to east, predominantly shaped by orography. Affected by the prevailing westerly winds, there was abundant rainfall in the western and northern mountains, as indicated by high rainfall KE values in these regions. In addition, among the study years, 2014 and 2015 showed higher national rainfall erosivity, with a large range in the west coast area.

Figure 10 shows the average  $R$  distribution for 2013–2017 estimated by rain gauges and WRF MPs. WRF grids could cover all regions in the UK evenly, offering more detailed erosivity results, especially in the mountainous northwestern region. Here, values of average  $R$  map calculated by rain gauges were much higher than three types of  $R_W$ , although they all have  $R$  decreased from west to east. Noted that  $ke-I$  empirical equation at Chilbolton station used in the whole UK, will not always be accurate in regions with different rainfall characteristics. In terms of  $R_W$  results, the three MPs obtained the same spatial pattern in rainfall erosivity, where  $R_{W-WDM6}$  yielded the greatest geographical difference. It is clear that the proposed WRF-based estimated method can capture more details of the spatial change of rainfall erosivity compared with the traditional disdrometer-based method.

The highest rainfall erosivity regions in the UK are concentrated in the mountainous areas along the western coast, related to their rainfall system. The moist air brought by the prevailing westerly wind from the Atlantic Ocean moves from west to east across the UK and rises when it encounters the mountains of western England. Therefore, the mountainous regions along the UK western coast have the highest rainfall amount and rainfall erosivity in the UK. In addition, western Scotland is under the subpolar oceanic climate, which enhances its humidity.



412 On the contrary, eastern Scotland and northeastern England are more likely to expose continental  
413 polar air mass, which brings dry and cold air and lower rainfall erosivity.

414 To evaluate the change in rainfall erosivity with time in the UK, the average value of all  
415 the WRF grids covering the whole UK was calculated over 2013–2017 (Figure 11). The average  
416  $R_W$  trends of  $R_{W-Morrison}$  and  $R_{W-TAA}$  were similar, both increasing from a minimum in 2013 to a  
417 maximum in 2014, and then gradually decreasing from 2014 to 2017. The red line in Figure 11  
418 indicates a series of mean values of the three MPs results, which varied from 36,782 to 51,600  
419  $\text{MJ mm ha}^{-1} \text{h}^{-1} \text{y}^{-1}$  (mean: 43,216  $\text{MJ mm ha}^{-1} \text{h}^{-1} \text{y}^{-1}$ ).

420 The maximum values for  $R_{W-Morrison}$  and  $R_{W-TAA}$  occurred in 2014, whereas that of  $R_{W-WDM6}$   
421 occurred in 2015. A sequence of extreme weather events occurred in the UK in 2014, including  
422 major winter storms in late January to mid-February, which caused widespread flooding and  
423 other economic losses, and greatly increased rainfall erosivity that year. However, the gauge-  
424 based interpolation map shows the average annual rainfall amount for the years 2013–2017 were  
425 884.9, 1014.0, 1008.5, 894.9, and 937.3 mm, respectively. The large rainfall erosivity difference  
426 between 2014 and 2015, and the two years with similar rainfall amount, indicates that much  
427 rainfall erosion occurs during the rainfall events of high intensity instead of simply high rainfall  
428 amount. A more notable variation pattern of rainfall erosivity may be found with longer  
429 simulation. The strength of the proposed method lies on its ability to estimate large covering and  
430 long-term rainfall erosivity.

## 431 **5 Discussion and conclusions**

432 This study presented a novel method for large-scale rainfall KE and erosivity estimation  
433 based on high-resolution, WRF-derived DSDs. Three microphysical parameterizations schemes  
434 (Morrison, WDM6, and Thompson aerosol-aware [TAA]) were designed to obtain raindrop size  
435 distributions, rainfall KE and rainfall erosivity for the entire of the UK covering the period of  
436 2013–2017. With validation from the long-term observations of a disdrometer, the WRF-based  
437 rainfall erosivity exhibited an acceptable performance at Chilbolton station. Among the three  
438 WRF schemes, TAA exhibited the most superior performance and was recommended for future  
439 investigation. The results revealed that high rainfall erosivity occurred in the west coast area of  
440 the UK. Compared with the traditional empirical method, the proposed method can explain  
441 rainfall erosivity from a microphysical perspective and reflect more spatial variation because of

442 changes in rainfall KE at the whole-country scale. Therefore, the development of a numerical  
443 weather prediction model offers an opportunity to better understand rainfall erosivity directly  
444 from its true definition. More importantly, because the WRF model is able to be driven by the  
445 global reanalysis data to obtain large-scale rainfall kinetic information, the proposed scheme can  
446 be easily applied to other regions, especially in ungauged areas.

447         Although an acceptable rainfall erosivity estimation is obtained using the WRF model,  
448 some uncertainties associated with it cannot be ignored. For example, as the MPs of WRF were  
449 closely related to DSD, improper determination of MPs will introduce additional uncertainty.  
450 The marked discrepancy among the three schemes (especially between Morrison and the others)  
451 in this study underscored the possible uncertainty associated with  $R_w$ . The reliability of the WRF  
452 model is heavily dependent on the model-driving initial data provided by mesoscale or global  
453 models and complicated scheme setting and parameter adjustment (Liu et al., 2013; Thompson  
454 and Eidhammer, 2014; Kumar et al., 2017). However, numerous uncertainties are observed in the  
455 parameterization of the WRF simulation, and the choice of microphysical schemes has a  
456 significant influence on the inverted DSD (Ćurić et al., 2009; Yang et al., 2019). Therefore,  
457 combining the DSDs obtained by an increasing number of disdrometers and the WRF model is  
458 valuable. For example, the Disdrometer Verification Network (DiVeN) in the UK (Pickering et  
459 al., 2019) started in Feb 2017 can be introduced to support and improve our estimation in future  
460 studies. Moreover, the measurement error by disdrometer may also contaminate the evaluation  
461 process. For example, when comparing the observed raindrop velocities based on the  
462 disdrometer at Bristol station with their empirical values, we observed dispersion of raindrops,  
463 with a number of drops showing significant deviations. This velocity distribution resulted in  
464 uncertainty in  $ke$  estimation.

465         Soil erosion in the UK is dominated by water erosion ( $10\text{--}30\text{ t km}^{-2}\text{ yr}^{-1}$ ), especially in  
466 areas with abundant rainfall in Scotland, where the soil loss rate is approximately 5–10 times that  
467 of dry areas (Duck, 1996). Thus, it is significant to estimate rainfall erosivity to elucidate the  
468 microphysical characteristics of rainfall and rainfall–soil interactions. Benaud et al. (2020)  
469 collated empirical soil erosion observations from UK-based studies into a geodatabase. However,  
470 there is a limitation that this database does not cover the entirety of the UK, especially the  
471 limited records in northern Scotland. In our future work, we propose to compare the soil loss  
472 database with our estimated soil loss using WRF DSD based rainfall erosivity and a soil erosion

473 model (such as RUSLE). We believe that not only can we better analyze the impact of rainfall  
474 and rainfall erosivity on the UK soil loss, but also help to better understand microphysical  
475 rainfall–soil interactions to support the rational formulation of soil and water conservation  
476 planning.

477 In addition, other sources of uncertainty, such as temporal downscaling of rainfall and  
478 point-to-area representative error by WRF, may introduce further uncertainty. This should be put  
479 in perspective of future work. It is expected that further exploration of research areas with  
480 different climatic and geographical characteristics would help us to establish a greater degree of  
481 accuracy on this matter.

#### 482 **Author contributions**

483 QD and JZ carried out the experiments, analyzed the data, and prepared the manuscript  
484 with contributions from all the co-authors. SLZ modified the text and provided financial support.  
485 SNZ carried out quality checks of WRF. GL and DH principally conceived the idea and design  
486 of the study.

#### 487 **Competing interests**

488 The authors declare that they have no conflict of interest.

#### 489 **Acknowledgments**

490 This work was supported by the National Natural Science Foundation of China (Nos.  
491 41871299 and 41771424), and the National Key R & D Program of China (Nos.  
492 2018YFB0505500, 2018YFB0505502). The authors acknowledge the British Atmospheric Data  
493 Centre and the European Centre for Medium-range Weather Forecasts as the sources of data used  
494 in the study.

495 The rain gauge datasets and Chilbolton disdrometers were sourced from the Met Office  
496 Integrated Data Archive System (MIDAS). Both datasets are available from the NCAS British  
497 Atmospheric Data Centre (<http://archive.ceda.ac.uk/>). The ERA-Interim data driving the WRF  
498 model can be downloaded from the ECMWF Public Datasets web interface  
499 (<https://www.ecmwf.int/>).

500 **References**

501 Alewell, C., Egli, M. and Meusburger, K. (2015). An attempt to estimate tolerable soil erosion  
502 rates by matching soil formation with denudation in Alpine grasslands. *Journal of Soils and*  
503 *Sediments* 15(6): 1383-1399.

504 Angulo-Mart ínez, M. and Barros, A. (2015). Measurement uncertainty in rainfall kinetic energy  
505 and intensity relationships for soil erosion studies: An evaluation using PARSIVEL disdrometers  
506 in the Southern Appalachian Mountains. *Geomorphology* 228: 28-40.

507 Angulo-Mart ínez, M., Beguer á, S. and Kysel ý, J. (2016). Use of disdrometer data to evaluate the  
508 relationship of rainfall kinetic energy and intensity (KE-I). *Science of the Total Environment* 568:  
509 83-94.

510 Angulo-Martinez, M., Beguer á, S., Navas, A. and Machin, J. (2012). Splash erosion under  
511 natural rainfall on three soil types in NE Spain. *Geomorphology* 175: 38-44.

512 Atlas, D., Srivastava, R. and Sekhon, R. S. (1973). Doppler radar characteristics of precipitation  
513 at vertical incidence. *Reviews of Geophysics* 11(1): 1-35.

514 Atlas, D. and Ulbrich, C. W. (1977). Path-and area-integrated rainfall measurement by  
515 microwave attenuation in the 1–3 cm band. *Journal of Applied Meteorology* 16(12): 1322-1331.

516 Beard, K. V. (1976). Terminal velocity and shape of cloud and precipitation drops aloft. *Journal*  
517 *of the Atmospheric Sciences* 33(5): 851-864.

518 Benaud, P., Anderson, K., Evans, M., Farrow, L., Glendell, M., James, M. R., ... & Brazier, R. E.  
519 (2020). National-scale geodata describe widespread accelerated soil erosion. *Geoderma*, 371:  
520 114378.

521 Bilotta, G., Grove, M. and Mudd, S. (2012). Assessing the significance of soil erosion.  
522 *Transactions of the Institute of British Geographers* 37(3): 342-345.

523 Bonta, J. (2004). Development and utility of Huff curves for disaggregating precipitation  
524 amounts. *Applied Engineering in Agriculture* 20(5): 641.

525 Borrelli, P., Robinson, D. A., Fleischer, L. R., Lugato, E., Ballabio, C., Alewell, C., Meusburger,  
526 K., Modugno, S., Schütt, B. and Ferro, V. (2017). An assessment of the global impact of 21st  
527 century land use change on soil erosion. *Nature Communications* 8(1): 1-13.

528 Brown, B. R., Bell, M. M. and Frambach, A. J. (2016). Validation of simulated hurricane drop  
529 size distributions using polarimetric radar. *Geophysical Research Letters* 43(2): 910-917.

530 Brown, L. and Foster, G. (1987). Storm erosivity using idealized intensity distributions.  
531 *Transactions of the ASAE* 30(2): 379-386.

532 Carter, C. E., Greer, J., Braud, H. and Floyd, J. (1974). Raindrop characteristics in south central  
533 United States. *Transactions of the ASAE* 17(6): 1033-1037.

534 Cintineo, R., Otkin, J. A., Xue, M. and Kong, F. (2014). Evaluating the performance of planetary  
535 boundary layer and cloud microphysical parameterization schemes in convection-permitting  
536 ensemble forecasts using synthetic GOES-13 satellite observations. *Monthly Weather Review*  
537 142(1): 163-182.

538 Ćurić, M., Janc, D., Vučković, V. and Kovačević, N. (2009). The impact of the choice of the  
539 entire drop size distribution function on Cumulonimbus characteristics. *Meteorologische*  
540 *Zeitschrift* 18(2): 207-222.

541 Dai, Q. and Han, D. (2014). Exploration of discrepancy between radar and gauge rainfall  
542 estimates driven by wind fields. *Water Resources Research* 50(11): 8571-8588.

543 Dai, Q., Bray, M., Zhuo, L., Islam, T., and Han, D. (2017). A scheme for raingauge network  
544 design based on remotely-sensed rainfall measurements. *Journal of Hydrometeorology* 18: 363-  
545 379.

546 Dai, Q., Yang, Q., Han, D., Rico - Ramirez, M. A., and Zhang, S. (2019). Adjustment of radar -  
547 gauge rainfall discrepancy due to raindrop drift and evaporation using the Weather Research and  
548 Forecasting model and dual-polarization radar. *Water Resources Research* 55: 9211–9233.

549 Davison, P., Hutchins, M., Anthony, S., Betson, M., Johnson, C. and Lord, E. (2005). The  
550 relationship between potentially erosive storm energy and daily rainfall quantity in England and  
551 Wales. *Science of the Total Environment* 344(1-3): 15-25.

552 De Roo, A., Wesseling, C. and Ritsema, C. (1996). LISEM: a single - event physically based  
553 hydrological and soil erosion model for drainage basins. I: theory, input and output. *Hydrological*  
554 *Processes* 10(8): 1107-1117.

555 Dee, D. P., Uppala, S., Simmons, A., Berrisford, P., Poli, P., Kobayashi, S., Andrae, U.,  
556 Balmaseda, M., Balsamo, G. and Bauer, d. P. (2011). The ERA - Interim reanalysis:  
557 Configuration and performance of the data assimilation system. Quarterly Journal of the Royal  
558 Meteorological Society 137(656): 553-597.

559 Defra (2009). Safeguarding our soils–A strategy for England. Defra, UK.

560 Doelling, I. G., Joss, J. and Riedl, J. (1998). Systematic variations of Z–R-relationships from  
561 drop size distributions measured in northern Germany during seven years. Atmospheric Research  
562 47: 635-649.

563 Duck, R. W. (1996). Regional variations of fluvial sediment yield in eastern Scotland. Erosion  
564 and Sediment Yield: Global and Regional Perspectives 236:157-161.

565 Dudhia, J. (1989). Numerical study of convection observed during the winter monsoon  
566 experiment using a mesoscale two-dimensional model. Journal of the Atmospheric Sciences  
567 46(20): 3077-3107.

568 EA (2004). The state of soils in England and Wales. Environment Agency, UK.

569 Ek, M., Mitchell, K., Lin, Y., Rogers, E., Grunmann, P., Koren, V., Gayno, G. and Tarpley, J.  
570 (2003). Implementation of Noah land surface model advances in the National Centers for  
571 Environmental Prediction operational mesoscale Eta model. Journal of Geophysical Research:  
572 Atmospheres 108(22):8851.

573 Evans, R. (1990). Soils at risk of accelerated erosion in England and Wales. Soil use and  
574 Management 6(3): 125-131.

575 Fornis, R. L., Vermeulen, H. R. and Nieuwenhuis, J. D. (2005). Kinetic energy–rainfall intensity  
576 relationship for Central Cebu, Philippines for soil erosion studies. Journal of Hydrology 300(1-4):  
577 20-32.

578 Gilmore, M. S., Straka, J. M. and Rasmussen, E. N. (2004). Precipitation uncertainty due to  
579 variations in precipitation particle parameters within a simple microphysics scheme. Monthly  
580 Weather Review 132(11): 2610-2627.

581 Hanel, M., Máca, P., Bašta, P., Vlnas, R. and Pech, P. (2016). The rainfall erosivity factor in the  
582 Czech Republic and its uncertainty. Hydrology and Earth System Sciences 20(10): 4307-4322.

583 Hong, S.-Y., Lim, K.-S. S., Lee, Y.-H., Ha, J.-C., Kim, H.-W., Ham, S.-J. and Dudhia, J. (2010).  
584 Evaluation of the WRF double-moment 6-class microphysics scheme for precipitating  
585 convection. *Advances in Meteorology* 2010.

586 Hudson, N. (1963). Raindrop size distribution in high intensity storms. *Rhodesian Journal of*  
587 *Agricultural Research* 1(1): 6-11.

588 Islam, T., Rico-Ramirez, M. A., Thurai, M. and Han, D. (2012). Characteristics of raindrop  
589 spectra as normalized gamma distribution from a Joss–Waldvogel disdrometer. *Atmospheric*  
590 *Research* 108: 57-73.

591 Janjić, Z. I. (1994). The step-mountain eta coordinate model: Further developments of the  
592 convection, viscous sublayer, and turbulence closure schemes. *Monthly Weather Review* 122(5):  
593 927-945.

594 Johnson, M., Jung, Y., Dawson, D. T. and Xue, M. (2016). Comparison of simulated  
595 polarimetric signatures in idealized supercell storms using two-moment bulk microphysics  
596 schemes in WRF. *Monthly Weather Review* 144(3): 971-996.

597 Jones, D. M. A. (1959). The shape of raindrops. *Journal of the Atmospheric Sciences* 16(1): 511-  
598 515.

599 Jung, Y., Xue, M. and Zhang, G. (2010). Simulations of polarimetric radar signatures of a  
600 supercell storm using a two-moment bulk microphysics scheme. *Journal of Applied Meteorology*  
601 *and Climatology* 49(1): 146-163.

602 Kain, J. S. (2004). The Kain–Fritsch convective parameterization: an update. *Journal of Applied*  
603 *Meteorology* 43(1): 170-181.

604 Kinnell, P. (1981). Rainfall intensity-kinetic energy relationships for soil loss prediction. *Soil*  
605 *Science Society of America Journal* 45(1): 153-155.

606 Kinnell, P. and Risse, L. (1998). USLE-M: empirical modeling rainfall erosion through runoff  
607 and sediment concentration. *Soil Science Society of America Journal* 62(6): 1667-1672.

608 Lim, K.-S. S. and Hong, S.-Y. (2010). Development of an effective double-moment cloud  
609 microphysics scheme with prognostic cloud condensation nuclei (CCN) for weather and climate  
610 models. *Monthly Weather Review* 138(5): 1587-1612.

611 Lim, Y. S., Kim, J. K., Kim, J. W., Park, B. I. and Kim, M. S. (2015). Analysis of the  
612 relationship between the kinetic energy and intensity of rainfall in Daejeon, Korea. *Quaternary*  
613 *International* 384: 107-117.

614 Marshall, J. S. and Palmer, W. M. K. (1948). The distribution of raindrops with size. *Journal of*  
615 *Meteorology* 5(4): 165-166.

616 McIsaac, G. (1990). Apparent geographic and atmospheric influences on raindrop sizes and  
617 rainfall kinetic energy. *Journal of Soil and Water Conservation* 45(6): 663-666.

618 Meshesha, D. T., Tsunekawa, A. and Haregeweyn, N. (2019). Influence of raindrop size on  
619 rainfall intensity, kinetic energy, and erosivity in a sub-humid tropical area: a case study in the  
620 northern highlands of Ethiopia. *Theoretical and Applied Climatology* 136(3-4): 1221-1231.

621 Meshesha, D. T., Tsunekawa, A., Tsubo, M., Haregeweyn, N. and Adgo, E. (2014). Drop size  
622 distribution and kinetic energy load of rainfall events in the highlands of the Central Rift Valley,  
623 Ethiopia. *Hydrological Sciences Journal* 59(12): 2203-2215.

624 Meshesha, D. T., Tsunekawa, A., Tsubo, M., Haregeweyn, N. and Tegegne, F. (2016).  
625 Evaluation of kinetic energy and erosivity potential of simulated rainfall using Laser  
626 Precipitation Monitor. *Catena* 137: 237-243.

627 Mikoš, M., Jošt, D. and Petkovšek, G. (2006). Rainfall and runoff erosivity in the alpine climate  
628 of north Slovenia: a comparison of different estimation methods. *Hydrological sciences journal*  
629 51(1): 115-126.

630 Mlawer, E. J., Taubman, S. J., Brown, P. D., Iacono, M. J. and Clough, S. A. (1997). Radiative  
631 transfer for inhomogeneous atmospheres: RRTM, a validated correlated - k model for the  
632 longwave. *Journal of Geophysical Research: Atmospheres* 102(14): 16663-16682.

633 MO (2012). Met Office Integrated Data Archive System (MIDAS) land and marine surface  
634 stations data (1853 - current).

635 Montopoli, M., Marzano, F. S. and Vulpiani, G. (2008). Analysis and synthesis of raindrop size  
636 distribution time series from disdrometer data. *IEEE Transactions on Geoscience and Remote*  
637 *Sensing* 46(2): 466-478.



638 Morgan, R. (1985). Assessment of soil erosion risk in England and Wales. *Soil use and*  
639 *Management* 1(4): 127-131.

640 Morrison, H., Milbrandt, J. A., Bryan, G. H., Ikeda, K., Tessendorf, S. A. and Thompson, G.  
641 (2015). Parameterization of cloud microphysics based on the prediction of bulk ice particle  
642 properties. Part II: Case study comparisons with observations and other schemes. *Journal of the*  
643 *Atmospheric Sciences* 72(1): 312-339.

644 Morrison, H., Thompson, G. and Tatarskii, V. (2009). Impact of cloud microphysics on the  
645 development of trailing stratiform precipitation in a simulated squall line: Comparison of one-  
646 and two-moment schemes. *Monthly weather review* 137(3): 991-1007.

647 Nyssen, J., Vandenreyken, H., Poesen, J., Moeyersons, J., Deckers, J., Haile, M., Salles, C. and  
648 Govers, G. (2005). Rainfall erosivity and variability in the Northern Ethiopian Highlands.  
649 *Journal of Hydrology* 311(1-4): 172-187.

650 O'Neill, D. (2007). The total external environmental costs and benefits of agriculture in the UK.  
651 Environment Agency, UK.

652 Panagos, P., Ballabio, C., Borrelli, P., Meusburger, K., Klik, A., Rousseva, S., Tadić, M. P.,  
653 Michaelides, S., Hrabal ěov á M. and Olsen, P. (2015a). Rainfall erosivity in Europe. *Science of*  
654 *the Total Environment* 511: 801-814.

655 Panagos, P., Borrelli, P., Poesen, J., Ballabio, C., Lugato, E., Meusburger, K., Montanarella, L.  
656 and Alewell, C. (2015b). The new assessment of soil loss by water erosion in Europe.  
657 *Environmental Science & Policy* 54: 438-447.

658 Park, S., Mitchell, J. and Bubenzer, G. (1982). Splash erosion modeling: physical analysis.  
659 *Transactions of the ASAE* 25:357-361.

660 Petan, S., Rusjan, S., Vidmar, A. and Mikoš, M. (2010). The rainfall kinetic energy–intensity  
661 relationship for rainfall erosivity estimation in the mediterranean part of Slovenia. *Journal of*  
662 *Hydrology* 391(3-4): 314-321.

663 Pickering, B. S., Neely III, R. R., & Harrison, D. (2019). The Disdrometer Verification Network  
664 (DiVeN): a UK network of laser precipitation instruments. *Atmospheric Measurement*  
665 *Techniques* 12: 5845-5861.

666 Prigent, C. (2010). Precipitation retrieval from space: An overview. *Comptes Rendus Geoscience*  
667 342(4-5): 380-389.

668 Renard, K. G., Foster, G. R., Weesies, G., McCool, D. and Yoder, D. (1997). Predicting soil  
669 erosion by water: a guide to conservation planning with the Revised Universal Soil Loss  
670 Equation (RUSLE), United States Department of Agriculture Washington, DC.

671 Rosewell, C. J. (1986). Rainfall kinetic energy in eastern Australia. *Journal of Climate and*  
672 *Applied Meteorology* 25(11): 1695-1701.

673 Sanchez-Moreno, J. F., Mannaerts, C. M., Jetten, V. and Löffler-Mang, M. (2012). Rainfall  
674 kinetic energy–intensity and rainfall momentum–intensity relationships for Cape Verde. *Journal*  
675 *of Hydrology* 454: 131-140.

676 Sempere - Torres, D., Porrà, J. M. and Creutin, J. D. (1998). Experimental evidence of a general  
677 description for raindrop size distribution properties. *Journal of Geophysical Research:*  
678 *Atmospheres* 103(2): 1785-1797.

679 Song, Y., Han, D. and Rico-Ramirez, M. A. (2017). High temporal resolution rainfall rate  
680 estimation from rain gauge measurements. *Journal of Hydroinformatics* 19(6): 930-941.

681 Thompson, G. and Eidhammer, T. (2014). A study of aerosol impacts on clouds and precipitation  
682 development in a large winter cyclone. *Journal of the Atmospheric Sciences* 71(10): 3636-3658.

683 Uplinger, W. (1981). A new formula for raindrop terminal velocity. *Conference on Radar*  
684 *Meteorology*, 20 th, Boston, MA.

685 Van Dijk, A., Bruijnzeel, L. and Rosewell, C. (2002). Rainfall intensity–kinetic energy  
686 relationships: a critical literature appraisal. *Journal of Hydrology* 261(1-4): 1-23.

687 Wang, L., Shi, Z., Wang, J., Fang, N., Wu, G. and Zhang, H. (2014). Rainfall kinetic energy  
688 controlling erosion processes and sediment sorting on steep hillslopes: a case study of clay loam  
689 soil from the Loess Plateau, China. *Journal of Hydrology* 512: 168-176.

690 Weiss, L. L. (1964). Ratio of true to fixed-interval maximum rainfall. *Journal of the Hydraulics*  
691 *Division* 90(1): 77-82.

692 Williams, R. and Sheridan, J. (1991). Effect of rainfall measurement time and depth resolution  
693 on EI calculation. Transactions of the ASAE 34(2): 402-0406.

694 Wischmeier, W. H. and Smith, D. D. (1958). Rainfall energy and its relationship to soil loss. Eos,  
695 Transactions American Geophysical Union 39(2): 285-291.

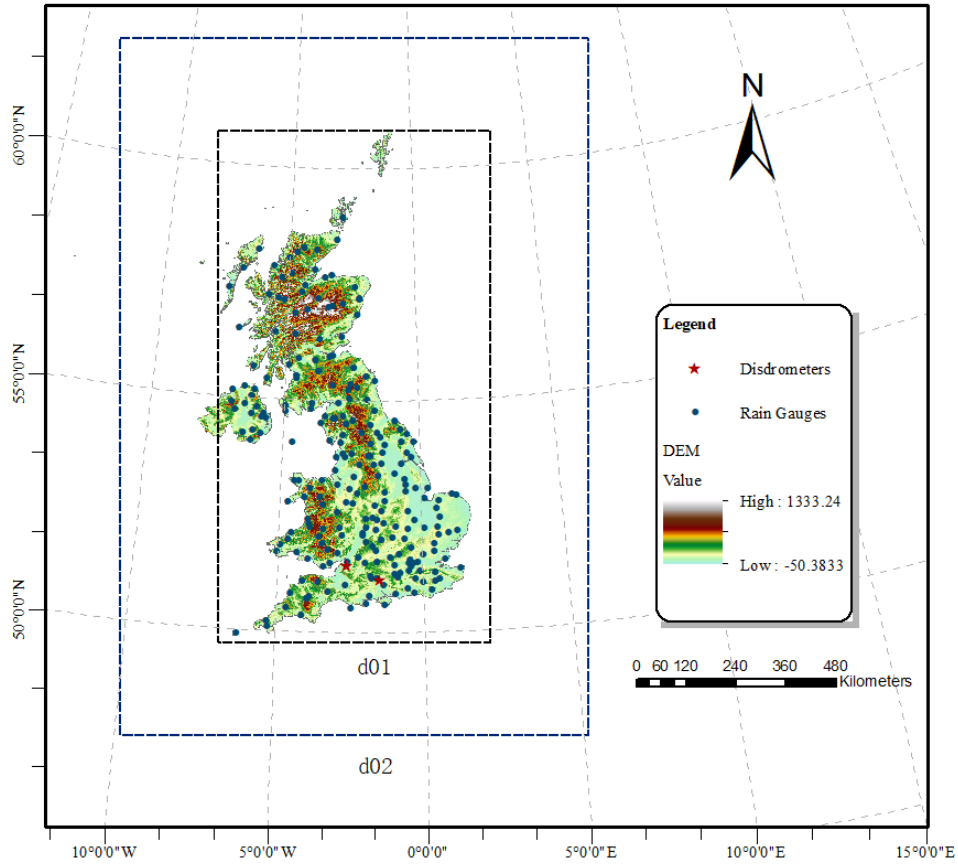
696 Wischmeier, W. H. and Smith, D. D. (1978). Predicting rainfall erosion losses-a guide to  
697 conservation planning. Department of Agriculture, Science and Education Administration, US.

698 Xie, Y., Yin, S., Liu, B., Nearing, M. A. and Zhao, Y. (2016). Models for estimating daily  
699 rainfall erosivity in China. Journal of Hydrology 535: 547-558.

700 Yang, Q., Dai, Q., Han, D., Chen, Y., and Zhang, S. (2019). Sensitivity analysis of raindrop size  
701 distribution parameterizations in weather research and forecasting rainfall simulation.  
702 Atmospheric Research 228:1-13.

703

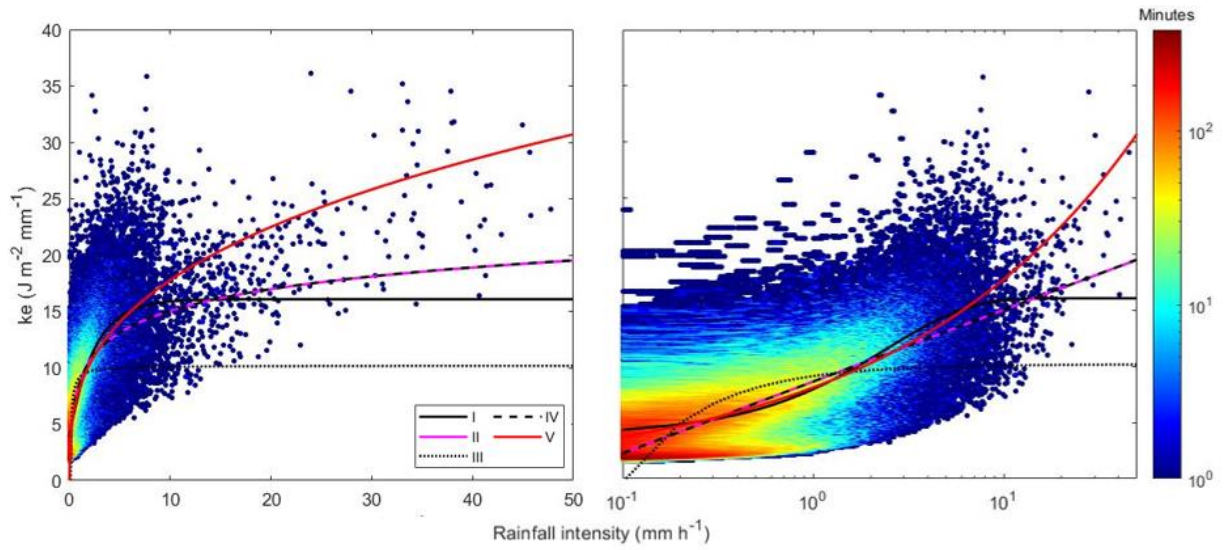
704



705

706 **Figure 1.** Location of rain gauges, Joss–Waldvogel disdrometer (JWD) at Chilbolton  
 707 Observatory, OTT Parsivel<sup>2</sup> disdrometer (OPD) at Bristol Observatory and configurations of  
 708 domain setups in the WRF model.

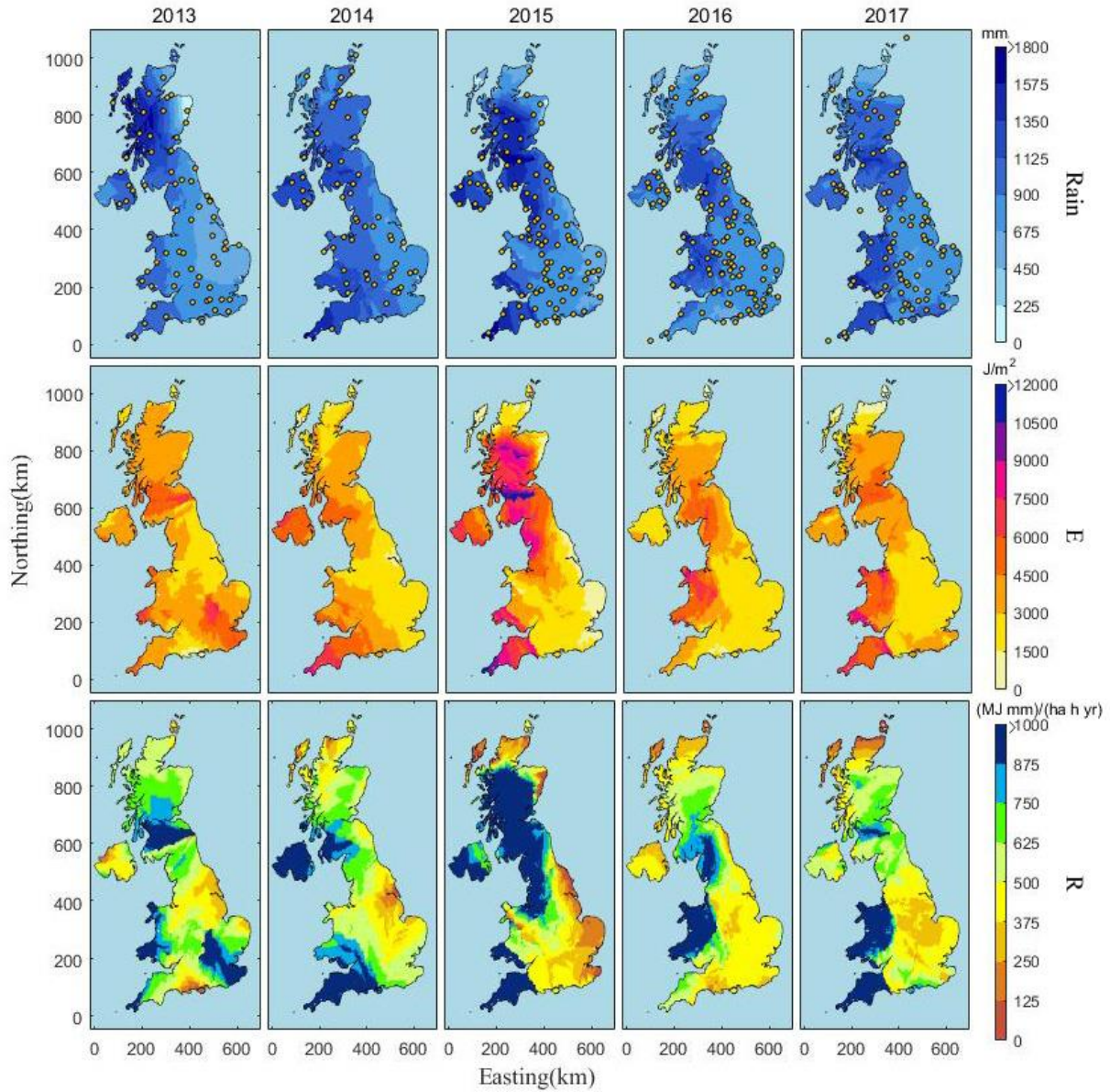
709



710

711 **Figure 2.** Minutes number per intensity class (x-axis) and  $ke$  class (y-axis) with five fitted  $ke-I$   
 712 curves at Chilbolton station (2004–2013), plotted on linear (left) and logarithmic (right) intensity  
 713 scales.

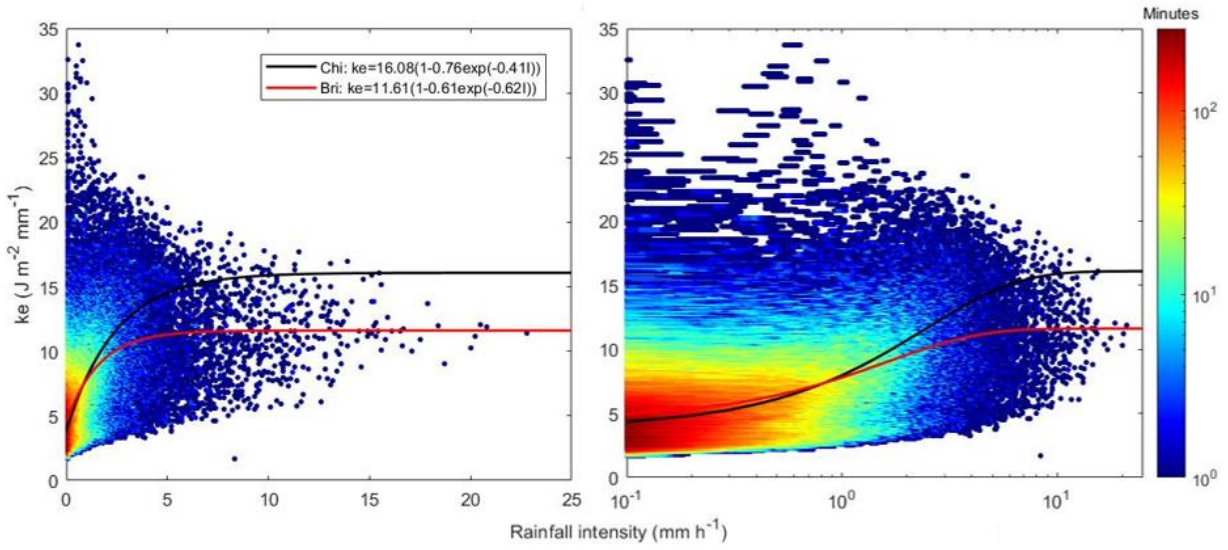
714



715

716 **Figure 3.** Gauge-based interpolation maps of annual rainfall amount (*Rain*), rainfall kinetic  
 717 energy (*E*) and rainfall erosivity (*R*) in 2013–2017.

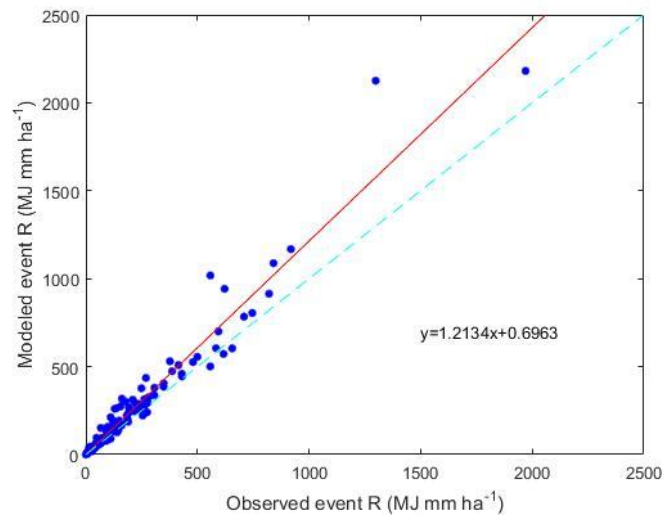
718



719

720 **Figure 4.** Minutes number per intensity class (x-axis) and ke class (y-axis) with fitted  $ke-I$   
 721 curves at Bristol station (2015–2018), plotted on linear (left) and logarithmic (right) intensity  
 722 scales.

723

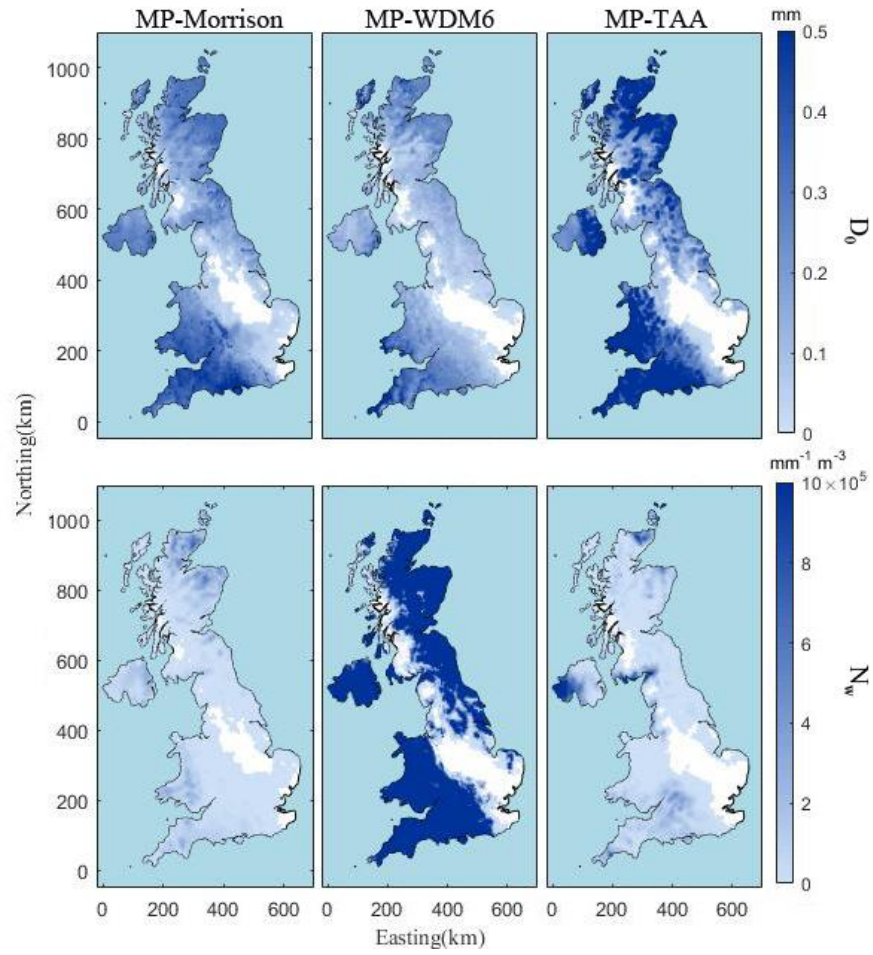


724

725 **Figure 5.** Comparison of observed and modeled event rainfall erosivity at Bristol Station,  
726 covering the period of 2016–2019.

727

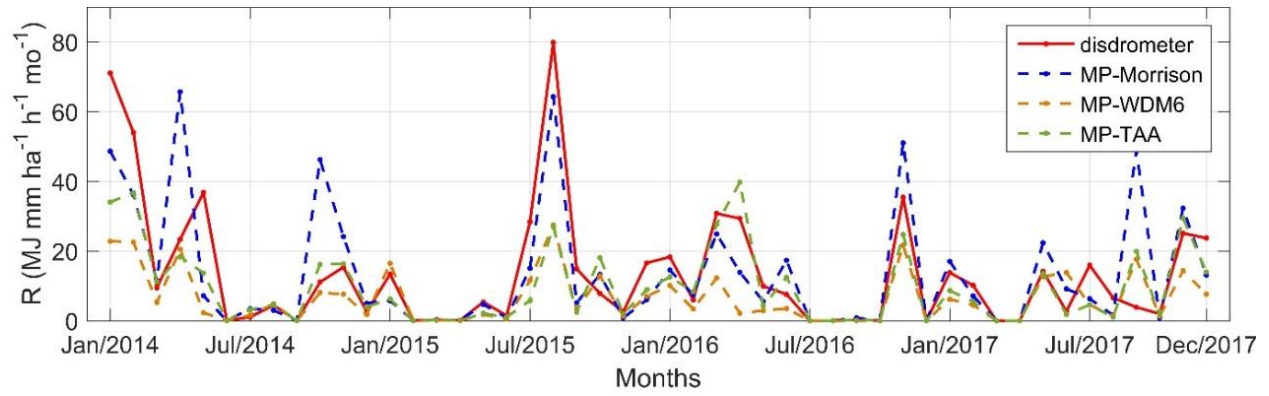




728

729 **Figure 6.** Map of average WRF DSD  $D_0$  and  $N_w$  (January 10, 2013).

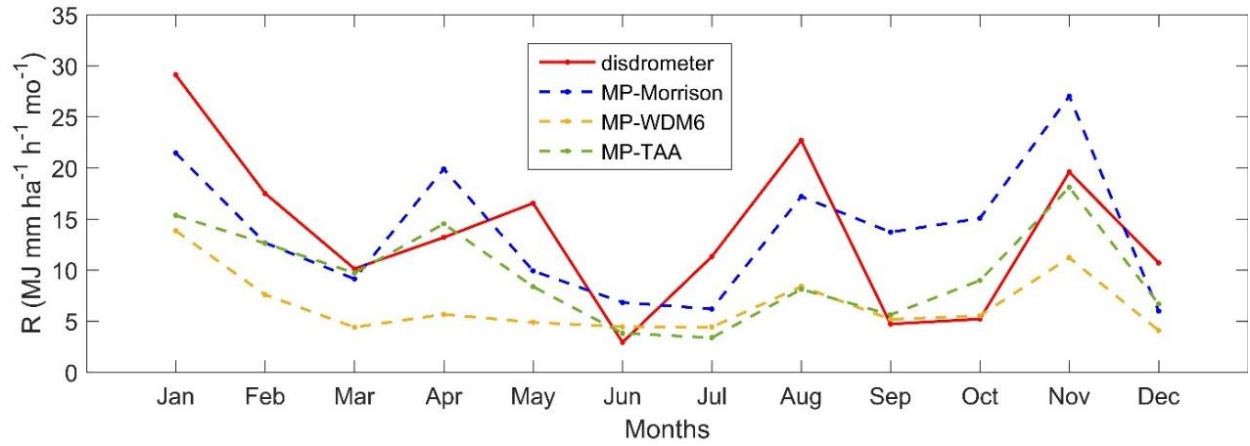
730



731

732 **Figure 7.** Comparison of disdrometer- and WRF-derived monthly rainfall erosivity estimations  
 733 at Chilbolton station (2014–2017).

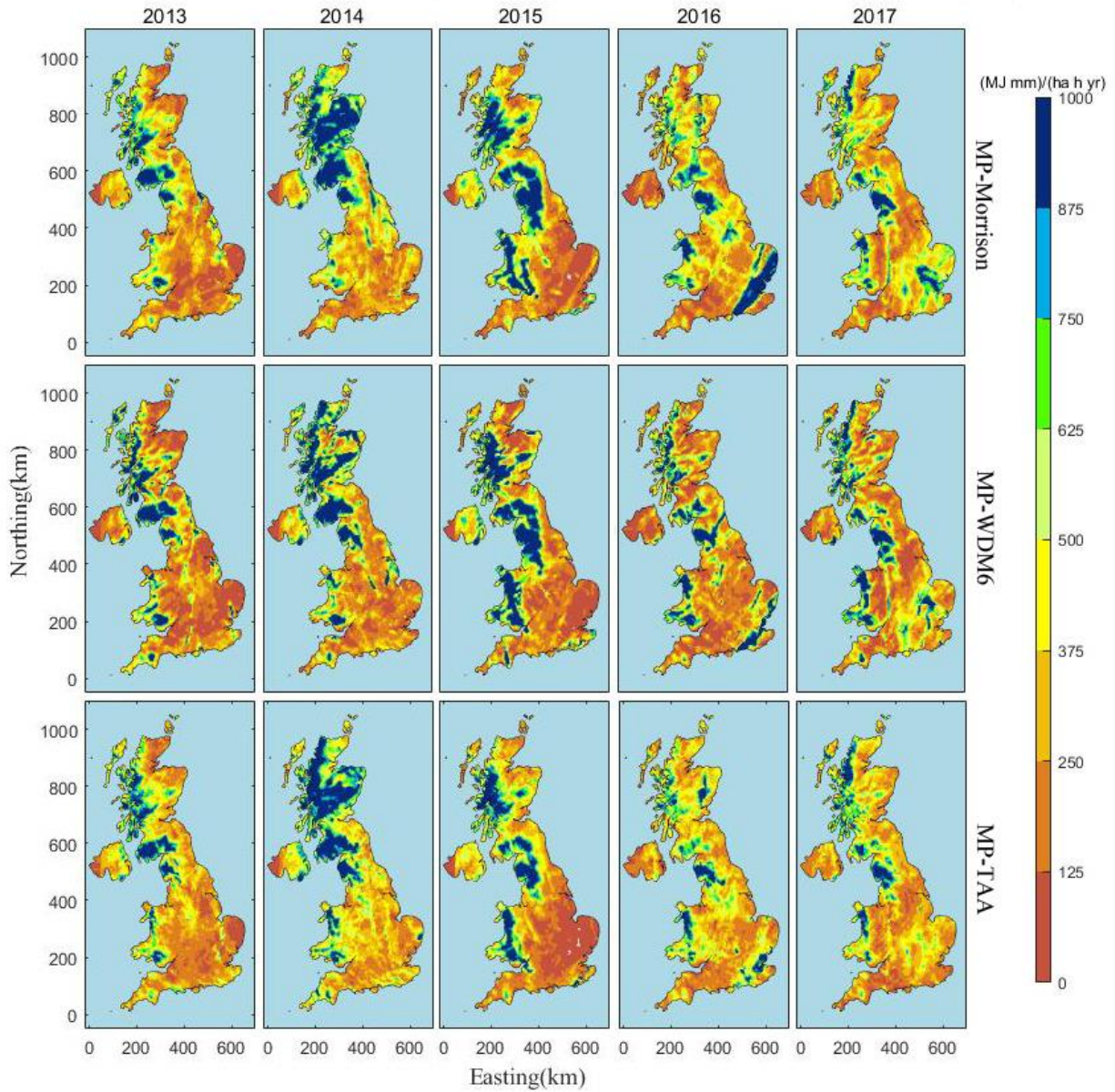
734



735

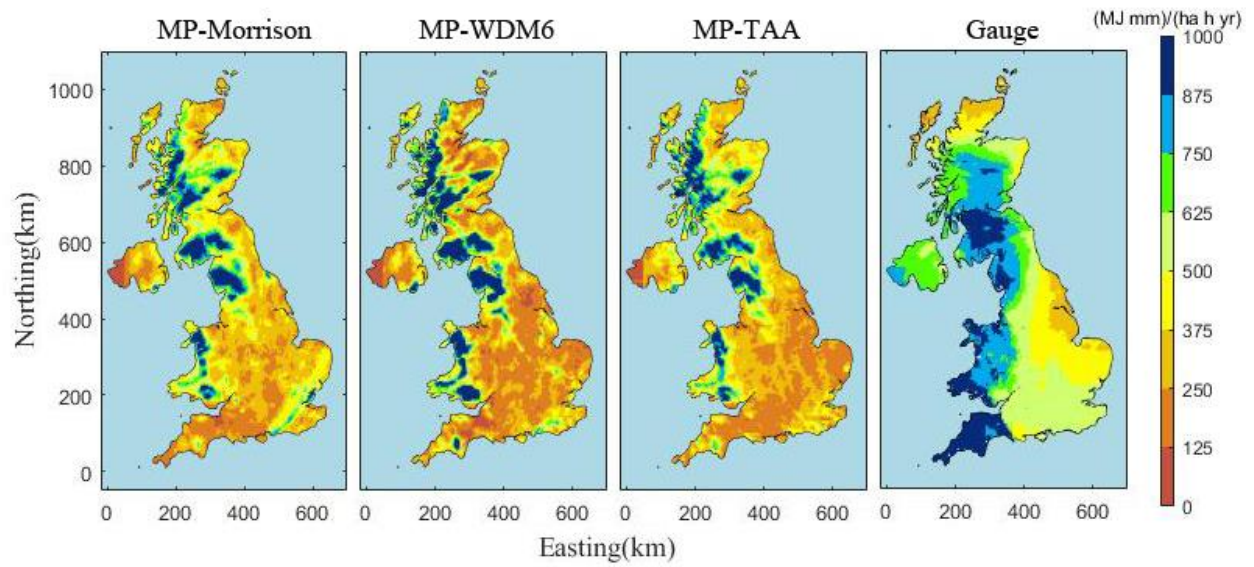
736 **Figure 8.** Comparison of disdrometer- and WRF-derived average monthly rainfall erosivity  
 737 estimations at Chilbolton station (2014–2017).

738



739 **Figure 9.** WRF-derived annual rainfall erosivity maps of the whole UK for different years.  
 740

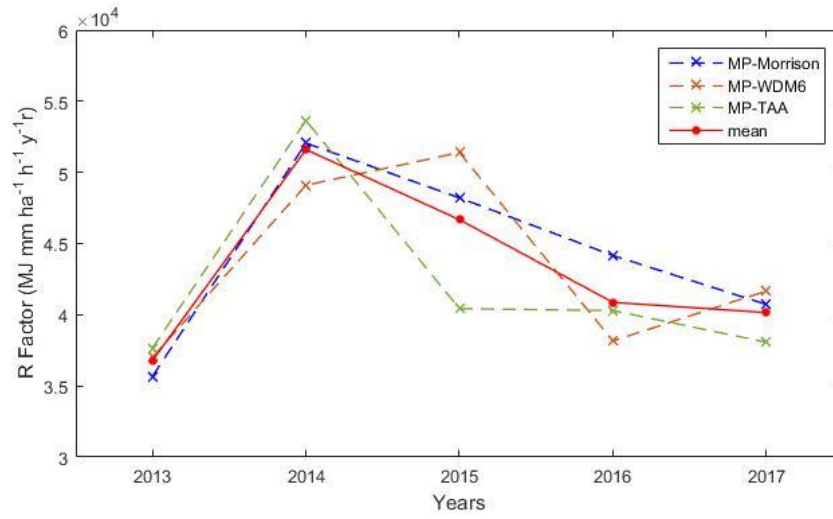
741



742

743 **Figure 10.** The 5-year (2013–2017) average annual rainfall erosivity maps based on WRF grids  
 744 and rain gauge interpolation.

745



746

747 **Figure 11.** WRF-derived average annual rainfall erosivity of all the WRF grids covering the  
 748 whole UK (2013–2017).

749

750 **Table 1.** Relationship of  $ke-I$  at Chilbolton Station (2004–2013).

<b>ID</b>	<b>Equation</b>	<b>Calibration R<sup>2</sup></b>	<b>Validation R<sup>2</sup></b>
<b>I</b>	$ke = 16.08(1 - 0.76e^{-0.41I})$	0.50	0.45
<b>II</b>	$ke = 8.65 + 6.39 \lg(I)$	0.48	0.43
<b>III</b>	$ke = 10.19 - 1.05/I$	0.29	0.25
<b>IV</b>	$ke = 8.65 + 2.78 \ln(I)$	0.48	0.43
<b>V</b>	$ke = 8.12I^{0.34}$	0.50	0.45

751

752

753 **Table 2.** The configurations of WRF model for two nested domains.

Domain	Domain size (km)	Grid Spacing (km)	Grid size	Downscaling ratio
d01	1,125 × 1,675	25	45 × 67	-
d02	655 × 1,230	5	131 × 246	1:5

754

755



756 **Table 3.** Indicators comparison between disdrometer-derived rainfall erosivity  $R_D$  and three  
757 types of WRF-derived rainfall erosivity at Chilbolton station on monthly scale (2014-2017).

Indicators	MP-Morrison	MP-WDM6	MP-TAA
Pearson	0.71	0.77	0.79
MAE	8.05	8.42	6.51
$R^2$	0.42	0.31	0.54

758