



1 **A reduced-order model for dual state-parameter geostatistical inversion**

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13 **0. Abstract**

14 To properly account the subsurface heterogeneity, geostatistical inverse models  
15 usually permit enormous amount of spatial correlated parameters to interpret the  
16 collected states. Several reduced-order techniques for the brick domain are  
17 investigated to leverage the memory burden of parameter covariance. Their capability  
18 to irregular domain is limited. Furthermore, due to the over fitting of states, the  
19 estimated parameters usually diverge to unreasonable values. Although some  
20 propriate tolerances can be used to eliminate this problem, they are presumed and  
21 heavily rely on the personal judgement. To address these two issues, we present a  
22 model reduction technique to the irregular domain by singular value decomposition  
23 (SVD). Afterward, the state errors and parameters are sequentially updated to leverage  
24 the over fitting. The computational advantages of the proposed reduced-order dual  
25 state-parameter inverse algorithm are demonstrated through two numerical  
26 experiments and one case study in a catchment scale field site. The investigations  
27 suggest that the stability of convergence dramatically improves. The estimated  
28 parameter values stabilize to reasonable order of magnitude. In addition, the memory  
29 requirement significantly reduces while the resolution of estimate preserves. The  
30 proposed method benefits multi-discipline scientific problems, especially useful and  
31 convenient for assimilating different types of measurements.

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## 34 1. Introduction

35 Groundwater is one of the necessary resources in many regions where the  
36 amount of rainfall and the capacity of reservoir is limited. To provide enough fresh  
37 water for the current and future uses in these areas, proper water resources  
38 management and contaminated site remediation strategies are required, which relies  
39 on the understanding of the site-specific spatial distribution of hydrological  
40 parameters (e.g., hydraulic conductivity and specific storage) in the prefer scale.

41 Many covariance based geostatistical approaches have been widely employed for  
42 aquifer characterization. Several previous studies suggested that the geostatistical  
43 inversion is superior than many other subsurface inverse modeling because it  
44 estimates the uncertainty and has ability to assimilate different type of observed data  
45 sequentially (Vesselinov et al., 2001). However, as pointed out by Illman et al. (2015),  
46 when the number of observations and unknown parameters are huge, the primary  
47 drawbacks of geostatistical inversion are the computational and memory burdens.

48 Several ensemble approaches have been proposed to handle the memory and  
49 large covariance matrices. For instance, Particle Filter or Sequential Monte Carlo  
50 method (SMC, Field et al., 2016; Zhang et al., 2017), iterative Ensemble Kalman  
51 Filter (EnKF, Schöniger et al., 2012; Ait-El-Fquih et al., 2016), iterative Ensemble  
52 Smoother (ES, Zhang et al., 2018), Extended Kalman Filter (EKF, Yeh and Huang  
53 2005; Leng and Yeh, 2003), and many other related methods construct the covariance  
54 between the parameter and state variable from a set of ensemble member. Since a  
55 bunch of realizations (usually several hundreds or thousands) are required to infer the  
56 population covariance from the sample covariance, the algorithm may not be  
57 computational affordable when the simulation time of single forward modeling is time  
58 consuming.

59 On the other hand, Quasi-Linear Geostatistical Approach (QLGA, Kitanidis,



60 1995) and Successive Linear Estimator (SLE, Yeh et al., 1996) avoid generating a  
61 large set of ensemble realizations. They construct the parameter covariance by some  
62 prior knowledge of unknown parameter field (e.g., covariance function, variance, and  
63 correlation length). Afterward, the covariance between the parameter and state  
64 variable is estimated through the sensitivity of state variable with respect to parameter.  
65 This approach requires significant amount of memory resource when the number of  
66 unknown parameter and state variable are huge. Furthermore, evaluating the  
67 sensitivity efficiently may be a difficult task for some scientific problems. As a result,  
68 considerable efforts are devoted to improving the capability of the algorithm. For  
69 instance, Sun and Yeh (1990) employed the adjoint approach to evaluate the  
70 sensitivity. It reduces the cost of running forward model from the order of number of  
71 unknown parameters to the number of state measurements. Saibaba and Kitanidis  
72 (2012) incorporates the hierarchical matrices technique with a matrix-free Krylov  
73 subspace approach to improve the computational efficiency. Liu et al. (2014) avoids  
74 the direct solution of sensitivity matrix by the Krylov subspace method. Li et al. (2015)  
75 and Zha et al. (2018) project the covariance matrix on the orthonormal basis and  
76 evaluate the cross product of sensitivity and squared root covariance directly using  
77 finite differencing approach. This method eliminates the sensitivity evaluation and  
78 reduces the computational cost of running forward model to the order of number of  
79 leading modes. Li et al. (2014) take the advantage of hierarchical nature of matrices to  
80 accelerate the computation of dense matrix vector products and rewrite the Kalman  
81 filtering equations into a computational efficient manner. Ghorbanidehno et al. (2015)  
82 extend their approach to the general case of non-linear dynamic systems. Similarly,  
83 Lin et al. (2016) reduces the computational complexity by projecting the parameters  
84 to different hierarchies of Krylov subspace. Pagh (2013) use fast Fourier transform to  
85 speed up the computation of covariance matrix multiplication. In addition, many



86 approaches reduce the computational cost and memory requirement. For example,  
87 Nowak and Litvinenko (2013) combine low rank approximations to the covariance  
88 matrices with fast Fourier transform; Kitanidis (2015) decomposes the covariance  
89 matrix by some orthonormal basis and shows that the choice of basis can be tailored  
90 to the problem of interest to improve estimation accuracy; Li et al. (2015) use discrete  
91 cosine transform to compress the data covariance matrix of a 1-D state variable series;  
92 Zha et al. (2018) use Karhunen-Loeve Expansion to compress the parameter  
93 covariance matrix of a 3-D parameter field. Other useful reduced order models are  
94 Galerkin projection (Liu et al., 2013), principal component (Kitanidis and Lee, 2014),  
95 randomized algorithm (Lin et al., 2017), Whittaker-Shannon interpolation (Horning et  
96 al., 2019), and Kronecker product decomposition (Zunino and Mosegaard, 2019).

97 In addition to reformulate the covariance matrix, the temporal moments  
98 eliminate the temporal derivative term in the governing equation. Thus, it is another  
99 potential method to reduce the data size and computational cost (Cirpka and Kitanidis,  
100 2000; Nowak and Cirpka, 2006; Yin and Illman, 2009).

101 There are several limitations exist in the previous geostatistical inverse  
102 algorithms. The first issue is over calibration or over fitting. During the inverse  
103 process, the calibration terminates when the difference between the observed and  
104 simulated states reduces to the value smaller than the given tolerance, an arbitrary  
105 value based on user's personal judgement. In practical, the tolerance is determined by  
106 the expected numeric and measurement errors. Since its true order of magnitude is  
107 unknow, the estimated parameter field sometimes diverges if the tolerance is  
108 underestimated. To be specific, the estimated parameters will first converge to the best  
109 values accompanied with the successive assimilation of the information about the  
110 subsurface heterogeneity embedded in the observed state variables. The values of  
111 parameter then diverge to the unreasonable huge or small values to compensate the



112 numeric and measurement errors. This instability is not user friendly because the  
113 reasonable (i.e., converged) estimate needs to be selected manually. Furthermore,  
114 when different types of measurement (e.g., water level, flux, temperature, gravity, etc.)  
115 are available, it is suggested that assimilate these data sequentially is a more robust  
116 approach than the simultaneous assimilation (Tsai et al., 2017). Accordingly, the  
117 manually determination of convergence prohibits the automatic sequential  
118 assimilation.

119 Second, when dealing with a 2-D or 3-D parameter or state variable fields, a  
120 specific matrix structures are required to efficiently decompose the unconditional  
121 covariance matrix to the orthonormal basis. For instance, a regular grid spacing is  
122 required to efficiently perform the fast Fourier transform (Nowak and Litvinenko,  
123 2013) and discrete cosine transform (Li et al., 2015). Similarly, Karhunen-Loeve  
124 Expansion (Zha et al., 2018) requires a brick or rectangle shape domain and grid. This  
125 requirement comes from the derivation of analytic eigenvalue and eigenvector of a  
126 separable exponential function.

127 To overcome these two existing limitations, we first introduce an additional step  
128 to estimate the error of state variables based on the error covariance matrices. Next,  
129 we derive a reduced order model using singular value decomposition. Afterward, we  
130 present a matrix manipulation method to eliminate the requirement of brick or  
131 rectangle domain during constructing the eigenvalue and eigenvector of unconditional  
132 covariance matrix.

133 This paper is arranged as follows. We first revisit the SLE that forms the  
134 geostatistical inversion approach (section 2.2). Thereafter, the algorithm is  
135 reformulated by collaborating with the data error, reduced order approach (i.e.  
136 singular value decomposition, SVD), and irregular domain (section 2.3). Furthermore,  
137 a perturbation method is proposed to improve the efficiency of covariance evaluation



138 process (section 2.4). In section 3, we test the proposed dual state-parameter  
139 estimation algorithm with two synthetic examples and a tomographic survey at the  
140 field site to demonstrate the superiority of the proposed method. Lastly, summary and  
141 conclusions are presented.

142

### 143 **2.1. Groundwater Flow Model.**

144 The 2-D groundwater flow in heterogeneous confined aquifer can be described  
145 as

$$146 \quad \nabla \cdot [T(\mathbf{x}) \cdot \nabla h(\mathbf{x}, t)] = S(\mathbf{x}) \frac{\partial h(\mathbf{x}, t)}{\partial t} \quad (1)$$

147 where  $h$  is the head responses (m),  $T$  is hydraulic transmissivity ( $\text{m}^2/\text{day}$ ),  $S$  is storage  
148 coefficient (-),  $\mathbf{x}$  is the vector in  $x$  and  $y$  directions, and  $t$  represents time (day).

149

### 150 **2.2. Reduced order successive linear estimator**

151 The singular value decomposition (SVD) is employed to reduce the order of the  
152 parameter covariance, leading to less memory requirement and more computational  
153 efficiency inverse exercise. Afterward, the data error is considered to improve the  
154 stability of convergence.

#### 155 **(1) Hard Data**

156 When the hard data are available, kriging is used to estimate the conditional  
157 parameter field and the corresponding conditional covariance matrix from the  
158 measured parameters. It is expressed as

$$159 \quad \hat{\mathbf{f}}^{(1)} = \hat{\mathbf{f}}^{(0)} + \boldsymbol{\varepsilon}_{ff}^{(0)} \mathbf{C} \mathbf{R}_{f^* f^*}^{-1} [\mathbf{f}^* - \hat{\mathbf{f}}^{(0)}] \quad (3)$$

160 and

$$161 \quad \boldsymbol{\varepsilon}_{ff}^{(1)} = \boldsymbol{\varepsilon}_{ff}^{(0)} - \boldsymbol{\varepsilon}_{ff}^{(0)} \mathbf{C} \mathbf{R}_{f^* f^*}^{-1} \mathbf{C}^T \boldsymbol{\varepsilon}_{ff}^{(0)} \quad (4)$$



162 in which  $\mathbf{f}^*$  ( $n_m \times 1$ ) is the measured parameters,  $\hat{\mathbf{f}}^{(0)}$  ( $n_f \times 1$ ) is the unconditional  
163 parameter field,  $\hat{\mathbf{f}}^{(1)}$  ( $n_f \times 1$ ) is the conditional parameter field.  $n_f$  represents the  
164 number of unknown parameters and  $n_m$  represents the number of measured parameters.  
165  $\boldsymbol{\varepsilon}_{ff}^{(0)} \mathbf{C}$  and  $\mathbf{C}^T \boldsymbol{\varepsilon}_{ff}^{(0)}$  ( $n_m \times n_f$ ) are the unconditional parameter covariance matrices  
166 depicting the spatial correlation between the measured parameters and all parameters.  
167  $\boldsymbol{\varepsilon}_{ff}^{(0)}$  ( $n_f \times n_f$ ) is the unconditional parameter covariance matrix depicting the spatial  
168 correlation between all parameters ( $\hat{\mathbf{f}}$ ).  $\mathbf{C}$  ( $n_f \times n_m$ ) is a matrix eliminating the column  
169 in  $\boldsymbol{\varepsilon}_{ff}^{(0)}$  when the corresponding measured parameter is absent.  $\boldsymbol{\varepsilon}_{ff}^{(1)}$  ( $n_f \times n_f$ ) is the  
170 conditional covariance matrix of all parameters. The diagonal term of the matrix (i.e.,  
171 residual variance) represents the remaining uncertainty of the estimated parameter  
172 after the information (measurements) is included. A small residual variance indicates  
173 the spatial trend of estimated parameter is close to the true, while a large value  
174 indicates the estimate is close to the initial guessed value (i.e. heterogeneity is not  
175 resolved).  $\mathbf{R}_{f^* f^*}$  ( $n_m \times n_m$ ) is the covariance matrix depicting the correlation between  
176 measured parameters. Notice that Cholesky and QR decompositions are utilized to  
177 solve the matrix multiplication of inverse  $\mathbf{R}_{f^* f^*}$  when it is and is not a positive  
178 definite matrix.

179 Since  $n_f$  is usually huge, storage demand of  $\boldsymbol{\varepsilon}_{ff}^{(0)}$  and  $\boldsymbol{\varepsilon}_{ff}^{(1)}$  may not be always  
180 affordable. Thus, singular value decomposition (SVD) is utilized to relieve this  
181 memory burden by keeping the leading eigenvalues and eigenvectors. The SVD of  
182  $\boldsymbol{\varepsilon}_{ff}$  is expressed as

$$183 \quad \boldsymbol{\varepsilon}_{ff} = \mathbf{g} \boldsymbol{\lambda} \mathbf{g}^T \quad (5)$$

184 where  $\boldsymbol{\lambda}$  ( $n_{svd} \times n_{svd}$ ) is eigenvalues,  $\mathbf{g}$  ( $n_f \times n_{svd}$ ) is eigenvectors, and  $n_{svd}$  is number



185 of leading eigenvalues. Substitute eq. (5) into eqs. (3) and (4), we have

$$186 \quad \hat{\mathbf{f}}^{(1)} = \hat{\mathbf{f}}^{(0)} + \mathbf{g}^{(0)} \boldsymbol{\lambda}^{(0)} \mathbf{g}^{(0)T} \mathbf{C} \mathbf{R}_{ff}^{-1} [\mathbf{f}^* - \hat{\mathbf{f}}^{(0)}] \quad (6)$$

187 and

$$188 \quad \mathbf{g}^{(1)} \boldsymbol{\lambda}^{(1)} \mathbf{g}^{(1)T} = \mathbf{g}^{(0)} \boldsymbol{\lambda}^{(0)} \mathbf{g}^{(0)T} - \mathbf{g}^{(0)} \boldsymbol{\lambda}^{(0)} \mathbf{g}^{(0)T} \mathbf{C} \mathbf{R}_{ff}^{-1} \mathbf{C}^T \mathbf{g}^{(0)} \boldsymbol{\lambda}^{(0)} \mathbf{g}^{(0)T} \quad (7)$$

189 Since  $\mathbf{g}^{(1)}$  is always a function of  $\mathbf{g}^{(0)}$ , it can be expressed as

$$190 \quad \mathbf{g}^{(1)} = \mathbf{g}^{(0)} \mathbf{u}^{(0)} \quad (8)$$

191 where is  $\mathbf{u}^{(0)}$  ( $n_{svd} \times n_{svd}$ ) is the matrix transferring the information of spatial

192 correlation of parameters to the next iteration. Accordingly, eq. (7) can reduce to

$$193 \quad \mathbf{u}^{(0)} \boldsymbol{\lambda}^{(1)} \mathbf{u}^{(0)T} = \sqrt{\boldsymbol{\lambda}^{(0)}} (\mathbf{I} - \sqrt{\boldsymbol{\lambda}^{(0)}} \mathbf{g}^{(0)T} \mathbf{C} \mathbf{R}_{ff}^{-1} \mathbf{C}^T \mathbf{g}^{(0)} \sqrt{\boldsymbol{\lambda}^{(0)}}) \sqrt{\boldsymbol{\lambda}^{(0)}} \quad (9)$$

194 in which  $\mathbf{I}$  is an identity matrix. By decomposing eq. (9) with SVD, we obtain the

195 updated eigenvalue  $\boldsymbol{\lambda}^{(1)}$  and  $\mathbf{u}^{(0)}$ . The updated eigenvector  $\mathbf{g}^{(1)}$  can be evaluated

196 by eq. (8).

## 197 (2) Error of Soft Data

198 After considering the hard data, the inherently presented data errors (e.g.,

199 measurement, numeric, round-off, truncation errors, etc.) are included prior to the

200 parameter estimation. The estimated data error and the corresponding covariance

201 matrix are expressed as

$$202 \quad \hat{\boldsymbol{\epsilon}}^{(r+1)} = \hat{\boldsymbol{\epsilon}}^{(r)} + \boldsymbol{\epsilon}_{hh}^{(r)} [\mathbf{J}_{fh}^{(r)T} \boldsymbol{\epsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)} + \boldsymbol{\epsilon}_{hh}^{(r)}]^{-1} [\mathbf{h}^{(r)} - (\mathbf{h}^* + \hat{\boldsymbol{\epsilon}}^{(r)})] \quad (10)$$

203 and

$$204 \quad \boldsymbol{\epsilon}_{hh}^{(r+1)} = \boldsymbol{\epsilon}_{hh}^{(r)} - \boldsymbol{\epsilon}_{hh}^{(r)} [\mathbf{J}_{fh}^{(r)T} \boldsymbol{\epsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)} + \boldsymbol{\epsilon}_{hh}^{(r)}]^{-1} \boldsymbol{\epsilon}_{hh}^{(r)} \quad (11)$$

205 in which  $\mathbf{h}^*$  ( $n_d \times 1$ ) is the observed head and  $\mathbf{h}^{(r)}$  ( $n_d \times 1$ ) is the simulated head

206 based on the estimated parameters from the  $r^{\text{th}}$  iteration.  $n_d$  represents the number of

207 measured state variables. The superscript  $r$  is the iteration index starting from one.



208  $\boldsymbol{\epsilon}_{hh}^{(1)}$  ( $n_d \times n_d$ ) is the unconditional covariance matrix of the observed head. The  
 209 diagonal terms represent the uncertainty of the measurement and the off diagonal  
 210 terms represent the correlation between errors.  $\boldsymbol{\epsilon}_{hh}^{(r)}$  and  $\boldsymbol{\epsilon}_{hh}^{(r+1)}$  ( $n_d \times n_d$ ) are the  
 211 conditional covariance matrices.  $\hat{\boldsymbol{e}}^{(1)}$  ( $n_d \times 1$ ) is the initial data error.  $\hat{\boldsymbol{e}}^{(r)}$  and  $\hat{\boldsymbol{e}}^{(r+1)}$   
 212 ( $n_d \times 1$ ) are the estimated data error.  $\mathbf{J}_{fh}^{(r)}$  ( $n_f \times n_d$ ) is the sensitivity of observed head  
 213 with respect to the estimated parameters during the  $r^{\text{th}}$  iteration.

214 The weight (i.e.,  $\mathbf{W}^{(r)} = \boldsymbol{\epsilon}_{hh}^{(r)} [\mathbf{J}_{fh}^{(r)T} \boldsymbol{\epsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)} + \boldsymbol{\epsilon}_{hh}^{(r)}]^{-1}$ ) is a combination of observed  
 215 head covariance matrix ( $\boldsymbol{\epsilon}_{hh}^{(r)}$ ) and simulated head covariance matrix  
 216 ( $\mathbf{R}_{hh}^{(r)} = \mathbf{J}_{fh}^{(r)T} \boldsymbol{\epsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)}$ ). It represents the ratio of data error ( $\boldsymbol{\epsilon}_{hh}^{(r)}$ , including numeric and  
 217 measurement errors) to the total error ( $\mathbf{R}_{hh}^{(r)} + \boldsymbol{\epsilon}_{hh}^{(r)}$ , including model structure,  
 218 parameter, numeric, and measurement errors). When the model is poorly calibrated,  
 219 the simulated head based on the current model structure and parameter values is much  
 220 uncertain than that of observed head (i.e.  $\mathbf{R}_{hh}^{(r)} \gg \boldsymbol{\epsilon}_{hh}^{(r)}$ ). Thus, the weight ( $\mathbf{W}^{(r)}$ ) is  
 221 small and the algorithm trusts the observation ( $\mathbf{h}^*$ ) more than the prediction ( $\mathbf{h}^{(r)}$ ).  
 222 After assimilating the subsurface characteristic casted in the observation, the  
 223 uncertainty of simulated head ( $\mathbf{R}_{hh}^{(r)}$ ) reduces and the algorithm trusts the observation  
 224 ( $\mathbf{h}^*$ ) less than the prediction ( $\mathbf{h}^{(r)}$ ). Therefore, the difference between  $\mathbf{h}^*$  and  $\mathbf{h}^{(r)}$  are  
 225 reflected into  $\hat{\boldsymbol{e}}^{(r)}$ . This data error calibration step is similar to the Kalman filter, but  
 226 instead of using the observation from previous time step only, we consider all of the  
 227 available observation simultaneously.

228 Again, substitute eigenvalue  $\lambda$  and eigenvector  $\mathbf{g}$  of  $\boldsymbol{\epsilon}_{ff}^{(r)}$  expressed in eq.  
 229 (5), the reduced order formulations of eqs. (10) and (11) are



$$230 \quad \hat{\mathbf{e}}^{(r+1)} = \hat{\mathbf{e}}^{(r)} + \boldsymbol{\varepsilon}_{hh}^{(r)} [\mathbf{H}_{fh}^{(r)} \mathbf{H}_{fh}^{(r)T} + \boldsymbol{\varepsilon}_{hh}^{(r)}]^{-1} [\mathbf{h}^{(r)} - (\mathbf{h}^* + \hat{\mathbf{e}}^{(r)})] \quad (12)$$

231 and

$$232 \quad \boldsymbol{\varepsilon}_{hh}^{(r+1)} = \boldsymbol{\varepsilon}_{hh}^{(r)} - \boldsymbol{\varepsilon}_{hh}^{(r)} [\mathbf{H}_{fh}^{(r)} \mathbf{H}_{fh}^{(r)T} + \boldsymbol{\varepsilon}_{hh}^{(r)}]^{-1} \boldsymbol{\varepsilon}_{hh}^{(r)} \quad (13)$$

233 where  $\mathbf{H}_{fh}^{(r)}$  ( $n_d \times n_{svd}$ ) is

$$234 \quad \mathbf{H}_{fh}^{(r)} = \mathbf{J}_{fh}^{(r)T} \mathbf{g}^{(r)} \sqrt{\boldsymbol{\lambda}^{(r)}} \quad (14)$$

235 Notice that if the number of state ( $n_d$ ) is huge, SVD can potentially be used to

236 decompose  $\boldsymbol{\varepsilon}_{hh}^{(r)}$  (eq. 5) and reduce the storage requirement.

### 237 (3) Soft Data.

238 After estimating the data error, the measured state variables and data errors are  
 239 substituted into successive linear estimator (SLE) (Yeh et al., 1996) to estimate the  
 240 conditional parameter fields and the corresponding residual covariance matrix:

$$241 \quad \hat{\mathbf{f}}^{(r+1)} = \hat{\mathbf{f}}^{(r)} + \boldsymbol{\varepsilon}_{ff}^{(r)} \mathbf{J}_{ff}^{(r)} [\mathbf{J}_{fh}^{(r)T} \boldsymbol{\varepsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)} + \boldsymbol{\varepsilon}_{hh}^{(r+1)}]^{-1} [(\mathbf{h}^* + \hat{\mathbf{e}}^{(r+1)}) - \mathbf{h}^{(r)}] \quad (15)$$

242 and

$$243 \quad \boldsymbol{\varepsilon}_{ff}^{(r+1)} = \boldsymbol{\varepsilon}_{ff}^{(r)} - \boldsymbol{\varepsilon}_{ff}^{(r)} \mathbf{J}_{ff}^{(r)} [\mathbf{J}_{fh}^{(r)T} \boldsymbol{\varepsilon}_{ff}^{(r)} \mathbf{J}_{fh}^{(r)} + \boldsymbol{\varepsilon}_{hh}^{(r+1)}]^{-1} \mathbf{J}_{ff}^{(r)T} \boldsymbol{\varepsilon}_{ff}^{(r)} \quad (16)$$

244 The reduced order version of SLE can be derived by substitute eq. (5) into eqs.

245 (15) and (16). That is,

$$246 \quad \hat{\mathbf{f}}^{(r+1)} = \hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)} \sqrt{\boldsymbol{\lambda}^{(r)}} \mathbf{H}_{fh}^{(r)T} [\mathbf{H}_{fh}^{(r)} \mathbf{H}_{fh}^{(r)T} + \boldsymbol{\varepsilon}_{hh}^{(r+1)}]^{-1} [(\mathbf{h}^* + \hat{\mathbf{e}}^{(r+1)}) - \mathbf{h}^{(r)}] \quad (17)$$

247 and

$$248 \quad \mathbf{g}^{(r+1)} \boldsymbol{\lambda}^{(r+1)} \mathbf{g}^{(r+1)T} = \mathbf{g}^{(r)} \boldsymbol{\lambda}^{(r)} \mathbf{g}^{(r)T} - \mathbf{g}^{(r)} \sqrt{\boldsymbol{\lambda}^{(r)}} \mathbf{H}_{fh}^{(r)T} [\mathbf{H}_{fh}^{(r)} \mathbf{H}_{fh}^{(r)T} + \boldsymbol{\varepsilon}_{hh}^{(r+1)}]^{-1} \mathbf{H}_{fh}^{(r)} \sqrt{\boldsymbol{\lambda}^{(r)}} \mathbf{g}^{(r)T} \quad (18)$$

249 Using eq. (8), eq. (18) further reduces to

$$250 \quad \mathbf{u}^{(r)} \boldsymbol{\lambda}^{(r+1)} \mathbf{u}^{(r)T} = \sqrt{\boldsymbol{\lambda}^{(r)}} (\mathbf{I} - \mathbf{H}_{fh}^{(r)T} [\mathbf{H}_{fh}^{(r)} \mathbf{H}_{fh}^{(r)T} + \boldsymbol{\varepsilon}_{hh}^{(r+1)}]^{-1} \mathbf{H}_{fh}^{(r)}) \sqrt{\boldsymbol{\lambda}^{(r)}} \quad (19)$$

251 By decomposing eq. (19) with SVD, we can evaluate the updated eigenvalue  $\boldsymbol{\lambda}^{(r+1)}$



252 and  $\mathbf{u}^{(r)}$ . The updated eigenvector  $\mathbf{g}^{(r+1)}$  then can be calculated by eq. (8).

#### 253 (4) Convergence Criterion

254 The estimated field is considered as the converge one when the spatial variance  
255 of the estimated parameter during several iterations are steady. The tolerance using  
256 mean squared error between the observed and simulated states is no longer necessary.

257

#### 258 2.3. Required Inputs

259 To initiate the algorithm, the initial guess of parameter field  $\hat{\mathbf{f}}^{(0)}$  and data error  
260  $\hat{\mathbf{e}}^{(0)}$ , as well as the unconditional covariance matrix of the parameters  $\boldsymbol{\varepsilon}_{ff}^{(0)}$  and  
261 observed data  $\boldsymbol{\varepsilon}_{hh}^{(0)}$  are required. The details are explained as followings:

262 **Parameter Field:** The initial parameter field  $\hat{\mathbf{f}}^{(0)}$  can be any reasonable values  
263 based on the prior knowledge.

264 **Parameter Covariance:** We assume the unconditional parameter covariance  
265 matrix is defined by an exponential covariance function

$$266 \quad \boldsymbol{\varepsilon}_{ff}^{(0)} = Var \cdot \exp\left(\frac{-|\mathbf{d}_x|}{\lambda_x} + \frac{-|\mathbf{d}_y|}{\lambda_y}\right) \quad (20)$$

267 where  $Var$  represents the unconditional spatial variance of the parameter;  $\mathbf{d}_x$  ( $n_f \times 1$ )

268 and  $\mathbf{d}_y$  ( $n_f \times 1$ ) are the distance between two parameters in  $x$  and  $y$  directions;  $\lambda_x$

269 and  $\lambda_y$  are the correlation lengths (m) in  $x$  and  $y$  directions.

270 The reduced order algorithm requires the evaluation of unconditional parameter  
271 covariance matrix  $\boldsymbol{\varepsilon}_{ff}^{(0)}$  in terms of eigenvalue  $\boldsymbol{\lambda}^{(0)}$  and eigenvector  $\mathbf{g}^{(0)}$ . In the  
272 real-world problem, the number of parameters  $n_f$  is usually in the order of  $10^3$  to  $10^5$ ,  
273 and the computational cost of conducting full SVD is  $n_f^3$  ( $O(n_f^3)$ ). Alternately,



274 truncated SVD with the complexity in  $O(n_f^2 n_f)$  can be used to approximate the  
 275 original eigenvalue and eigenvector.  $n_{fi}$  is the number of randomly chose column in  
 276  $\mathbf{\epsilon}_{ff}^{(0)}$ .

277 In addition to the numeric approach, the analytical solution of eigenvalues  $\lambda_n$   
 278 and eigenvectors  $\mathbf{g}_n$  with brick grid and domain (Ghanem and Spanos, 2003; Zhang  
 279 and Lu, 2004) is also available. In 2-D domain, they are analytically express as

$$280 \quad \lambda_n = \text{Var} \frac{2\lambda_x}{\lambda_x^2 w_{n,x}^2 + 1} \frac{2\lambda_y}{\lambda_y^2 w_{n,y}^2 + 1} \quad (21)$$

$$281 \quad \mathbf{g}_n = \frac{\lambda_x w_{n,x} \cos(w_{n,x} x) + \sin(w_{n,x} x)}{\sqrt{\frac{(\lambda_x^2 w_{n,x}^2 + 1)L_x}{2} + \lambda_x}} \frac{\lambda_y w_{n,y} \cos(w_{n,y} y) + \sin(w_{n,y} y)}{\sqrt{\frac{(\lambda_y^2 w_{n,y}^2 + 1)L_y}{2} + \lambda_y}} \quad (22)$$

282 where  $w_{n,x}$  and  $w_{n,y}$  are the positive roots of the characteristic equations

$$283 \quad (\lambda_x^2 w_{n,x}^2 - 1) \sin(w_{n,x} L_x) = 2\lambda_x w_{n,x} \cos(w_{n,x} L_x) \quad (23)$$

284 and

$$285 \quad (\lambda_y^2 w_{n,y}^2 - 1) \sin(w_{n,y} L_y) = 2\lambda_y w_{n,y} \cos(w_{n,y} L_y) \quad (24)$$

286 where  $L_x$  and  $L_y$  are the width of model domain in  $x$  and  $y$  directions.

287 Notice that if the model domain is irregular (i.e., not a line, squared, or brick  
 288 shape), one can first construct the eigenvalue and eigenvector for a regular domain  
 289 whose size is greater than the irregular one. Afterward, the eigenvector of the irregular  
 290 domain can be evaluated by

$$291 \quad \mathbf{g}_{irreg} = \mathbf{C}_2 \mathbf{g}_{reg} \quad (25)$$

292 in which  $\mathbf{C}_2$  ( $n_{f,irreg} \times n_{f,reg}$ ) is a matrix to eliminate the rows of  $\mathbf{g}_{reg}$  if the  
 293 corresponding grids are outside the model domain;  $n_{f,reg}$  is the number of parameter of



294 the regular line, squared, or brick domain;  $n_{f,irreg}$  is the number of parameter of the  
295 irregular domain.  $\mathbf{g}_{reg}$  and  $\mathbf{g}_{irreg}$  are the eigenvectors of regular and irregular  
296 domains.

297 **Data Error:** The initial data error  $\hat{\mathbf{e}}^{(0)}$  can set as zero.

298 **Data Covariance:** The unconditional covariance matrix of the observed data  
299  $\boldsymbol{\varepsilon}_{hh}^{(0)}$  is a diagonal matrix if the data error are mutually independent. Otherwise, a  
300 covariance function (e.g., eq. (20)) can be utilized to describe the unconditional  
301 correlation.

302

#### 303 2.4. Evaluation of Covariance

304 The algorithm also requires the evaluation of squared root of cross-covariance  
305  $\mathbf{H}_{jh}^{(r)}$ . One can evaluate the sensitivity by adjoint approach (e.g., Sykes et al., 1985;  
306 Sun and Yeh, 1990) first and substitute it into eq. (14) to derive  $\mathbf{H}_{jh}^{(r)}$ . The  
307 computational cost of the adjoint approach is to run the linear adjoint forward model  
308  $n_w$  (number of observation wells) to  $n_d$  (number of states) times, depending on the  
309 model configurations (e.g., confined, unconfined, saturated, unsaturated, and the types  
310 of boundary condition, etc.).

311 On the other hand, a perturbation approach (e.g., forward, backward, central  
312 differences, etc.) can be utilized to directly evaluate  $\mathbf{H}_{jh}^{(r)}$  so that the computation of  
313 sensitivity is eliminated. Let  $G(\cdot)$  represent the groundwater flow governing  
314 equation and its Taylor expansion evaluated on  $\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta$  is

$$315 G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) = G(\hat{\mathbf{f}}^{(r)}) + G'(\hat{\mathbf{f}}^{(r)})\mathbf{g}^{(r)}\delta + G''(\hat{\mathbf{f}}^{(r)})\frac{(\mathbf{g}^{(r)}\delta)^2}{2} + G'''(\hat{\mathbf{f}}^{(r)})\frac{(\mathbf{g}^{(r)}\delta)^3}{3!} + \dots \quad (26)$$

316  $\delta$  is an arbitrary value controlling the accuracy of approximation. Manipulating eq.



317 (26) yields

$$318 \quad G'(\hat{\mathbf{f}}^{(r)})\mathbf{g}^{(r)} = \mathbf{J}_{f_h}^{(r)T} \mathbf{g}^{(r)} = \frac{G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) - G(\hat{\mathbf{f}}^{(r)})}{\delta} - G''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^2 \delta}{2} - G'''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^3 \delta^2}{3!} - \dots$$

319 (27)

320 Multiplying both sides with  $\sqrt{\lambda^{(r)}}$ , eq. (27) becomes

$$321 \quad \mathbf{H}_{f_h}^{(r)} = \left[ \frac{G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) - G(\hat{\mathbf{f}}^{(r)})}{\delta} - G''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^2 \delta}{2} - G'''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^3 \delta^2}{3!} - \dots \right] \sqrt{\lambda^{(r)}} \quad (28)$$

322 Accordingly,  $\mathbf{H}_{f_h}^{(r)}$  can be approximated by

$$323 \quad \mathbf{H}_{f_h}^{(r)} \approx \frac{G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) - G(\hat{\mathbf{f}}^{(r)})}{\delta} \sqrt{\lambda^{(r)}} \quad (29)$$

324 and the corresponding error is

$$325 \quad err = \sqrt{\lambda^{(r)}} G''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^2 \delta}{2} + \dots \quad (30)$$

326 To evaluate  $\mathbf{H}_{f_h}^{(r)}$ , we need to run the forward model  $n_{svd}$  (number of kept eigens)  $\times$

327  $n_{event}$  (number of pumping or injection events) times.

328 If we further evaluate  $G(\cdot)$  on  $\hat{\mathbf{f}}^{(r)} - \mathbf{g}^{(r)}\delta$  and combine it with  $G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta)$ ,

329 we have

$$330 \quad G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) - G(\hat{\mathbf{f}}^{(r)} - \mathbf{g}^{(r)}\delta) = 2 \left[ G'(\hat{\mathbf{f}}^{(r)})\mathbf{g}^{(r)}\delta + G'''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)}\delta)^3}{3!} + \dots \right] \quad (31)$$

331 Multiplying both sides with  $\sqrt{\lambda^{(r)}}$  and  $\mathbf{H}_{f_h}^{(r)}$  can be approximated by

$$332 \quad \mathbf{H}_{f_h}^{(r)} \approx \frac{G(\hat{\mathbf{f}}^{(r)} + \mathbf{g}^{(r)}\delta) - G(\hat{\mathbf{f}}^{(r)} - \mathbf{g}^{(r)}\delta)}{2\delta} \sqrt{\lambda^{(r)}} \quad (32)$$

333 The corresponding error is

$$334 \quad err = \sqrt{\lambda^{(r)}} G'''(\hat{\mathbf{f}}^{(r)}) \frac{(\mathbf{g}^{(r)})^3 \delta^2}{3!} + \dots \quad (33)$$

335 The evaluation of more accurate  $\mathbf{H}_{f_h}^{(r)}$  requires the exercise of forward model  $2n_{svd} \times$

336  $n_{event}$  times.



337

## 338 **2.5. Computational Advantages**

339       The proposed reduced-order dual state-parameter inverse algorithm is efficient  
340 when the number of kept leading eigens ( $n_{svd}$ ) is less than 1500. If the ratio of domain  
341 size and correlation length is huge, large  $n_{svd}$  value increase the computational cost of  
342 SVD ( $O(n_{kl}^3)$ ). Furthermore, evaluating  $\mathbf{H}_{fn}^{(r)}$  through the forward or backward finite  
343 difference approach is efficient for many types of forward models (e.g., variable  
344 saturated diffusion equation, advection diffusion equation). It only requires executing  
345 the forward model for  $n_{svd} \times n_{event}$  (number of pumping events) times. On the contrary,  
346 when the forward model is elegant (e.g., fully saturated diffusion equation), it is  
347 cost-effective to evaluate the sensitivity of state with respect to unknown parameter  
348 (eq. 14,  $\mathbf{J}_{fn}^{(r)}$ ) through the adjoint method. Only  $n_w$  (number of observation wells)  
349 forward runs is required. In addition, updating state variable errors is efficient when  
350  $n_d$  (number of state variable) is less than 10000. The most expensive additional  
351 computational cost is to solve the inverse  $n_d \times n_d$  matrix (eqs. 12 and 13) through either  
352 Cholesky or QR decompositions (matrix multiplication is an easy task under the  
353 parallel computing scheme).

354

## 355 **3. Algorithm Verification**

356       In this section, three cases are used to examine the robustness of the proposed  
357 algorithm. The first and second cases involve hydraulic tomographic surveys in a  
358 synthetic aquifer without and with observation error, respectively. The third case is a  
359 2-D application of tomography experiment in the field site.

360       The coefficient of determination ( $R^2$ ) and the mean squared error (i.e.,  $L_2$  norm),  
361 defined as



362 
$$R^2 = \left[ \frac{(\mathbf{f}^* - \bar{\mathbf{f}}^*)^T (\hat{\mathbf{f}}^{(r)} - \bar{\hat{\mathbf{f}}}^{(r)})}{n_f \text{std}(\mathbf{f}^*) \text{std}(\hat{\mathbf{f}}^{(r)})} \right]^2 \quad (34)$$

363 and

364 
$$L_2 = \frac{(\mathbf{f}^* - \hat{\mathbf{f}}^{(0)})^T (\mathbf{f}^* - \hat{\mathbf{f}}^{(0)})}{n_f} \quad (35)$$

365 are utilized to evaluate the similarity between the reference and estimated parameter  
366 fields. Overbar represents the average.  $\text{std}(\cdot)$  stands for the standard deviation.

367

### 368 **3.1. Observation-Error Free Synthetic Case**

369 The observation-error free synthetic case considers transient state HT in a  
370 two-dimensional horizontal confined aquifer of 30×30 square elements (figure 1).  
371 Each element is 1 (m)×1 (m). The aquifer is bounded by the constant head boundary  
372 (30 m). The initial head is uniform (30 m) everywhere.

#### 373 **(a) Forward Model**

374 The reference field (figure 1) is generated using a spectral method (Gutjahr, 1989;  
375 Robin et al., 1993) with mean geometric  $T$  of one ( $\text{m}^2/\text{day}$ ), variance of  $\ln T$  of one (-),  
376 and correlation scales of 10 (m) at both x and y directions. Eight wells (white dots)  
377 are evenly installed in the aquifer to collect the aquifer responses induced by three  
378 sequential pumping tests from early time till the system reaches steady state. The  
379 pumping wells are labeled with squares. The noise free observed heads only contain  
380 the numerical error (e.g., round-off and truncation errors), and its value is smaller than  
381  $10^{-7}$  (m). The  $S$  is a constant value of 0.001 (-). The initial time step is 0.001 (day) and  
382 the maximum time step is 1 (day).

#### 383 **(b) Inverse Model**

384 Assume  $S$  is known and we would like to estimate the spatial  $T$  distribution. The



385 initial mean  $T$  ( $\hat{\mathbf{T}}^{(0)}$ ) is one ( $\text{m}^2/\text{day}$ ), variance of  $\ln T$  ( $\boldsymbol{\epsilon}_{ff}^{(0)}$ ) is one (-), variance of  
386 observed head ( $\boldsymbol{\epsilon}_{hh}^{(0)}$ ) is  $10^{-4}$  ( $\text{m}^2$ ), and the correlation lengths  $\lambda_x$  and  $\lambda_y$  are 10 (m).

### 387 (c) Results of Estimate

388 Figure 2 shows the performances of the estimated  $T$  value using old algorithm  
389 (SLE) and figure 3 presents the performances using the new algorithm. Figure 2a  
390 presents the evolutions of mean squared error between the observed and simulated  
391 heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var } \ln T$ ) during the calibration  
392 process. Figure 2b is the calibrated head at the final iteration. Figures 2c and 2d are  
393 the final and best estimated  $T$  field, respectively. Figure 2e and f are the scatter plots  
394 of the estimated  $T$  versus reference  $T$  corresponding to the final (figure 2c) and best  
395 (figure 2d) estimated  $T$  fields. As displayed in figure 2a, after  $L_2$  norm approaches  
396 steady, the spatial variance of estimated  $T$  (pink line) still increases with a constant  
397 rate. The gaining of spatial variation of estimated  $T$  values comes from the over  
398 calibrated observed head. Due to the natural of least squared algorithm (e.g.,  
399 minimizing the mean squared error of state variables), the algorithm compensates the  
400 numeric errors by adjusting the estimated  $T$  to unreasonably high and low values,  
401 although the general spatial trend of the estimated  $T$  fields remains similar. As the  
402 result, compare to the best estimate of  $T$  field (figure 2d and f), the final estimate  
403 diverges (figure 2c and e).

404 On the contrary, estimate using the new algorithm does not encounter the  
405 divergence issue. As shown in the calibration process (figure 3a), the spatial variance  
406 of estimated  $T$  (pink line) reaches steady after  $L_2$  decays to the value of  $10^{-10}$  (i.e.,  
407 magnitude of numeric error). The final estimated field (figure 3c) converges and the  
408 performances in terms of the statistical indices (figure 3d), namely  $L_2$ ,  $R^2$   
409 (determination coefficient), or the slope and intercept of the fitted linear relationship



410 between the estimates and the true values, are equally good as the best estimate by the  
411 previous algorithm (figure 2c). In other word, the new algorithm eliminates the over  
412 fitting issue.

413

### 414 **3.2. Noisy Synthetic Case**

415 This example aims to reveal the advantages of the algorithm when the  
416 measurement errors are presented. To accomplish this goal, the Gaussian noises with  
417 standard deviation of  $10^{-3}$  (m) are superimposed on the observed heads discussed in  
418 section 3.1. The design of inverse model is identical with those explained in section  
419 3.1.

420 Figure 4 shows the performances (evolution of calibration process, head fitting,  
421 contour of the estimate field, and the scatter plot between the estimate and reference  
422 fields) of the estimated  $T$  value using original algorithm, and figure 5 presents the  
423 performances using the new one. By comparing the final estimate with the manually  
424 selected best estimate of original SLE (figure 4d and f), the final estimated  $T$  field  
425 diverges as indicated by the increase in variance of  $\ln T$  (pink line in figure 4a),  
426 unreasonable high and low values (red and blue spots in figure 4c) of the final  
427 estimated  $T$  fields, and the uncorrelated estimate and reference  $\ln T$  values (figure 4e).  
428 On the contrary, the final estimate using the proposed algorithm shows that the  
429 estimated field converges to the reasonable spatial pattern and values. The variance of  
430  $\ln T$  (pink line in figure 5a) approaches stable and the simulated heads reproduce the  
431 adjusted observed heads (sum of observed heads and estimated head errors, figure 5b).  
432 Furthermore, the contour map and scatterplot of the final estimate (figure 5c and d)  
433 suggest the estimated field is close to the manually selected best estimate of original  
434 SLE (figure 4d and f) and the reference (figure 1). This means the new method no  
435 longer overestimate the parameter fields and can automatically converge to an optimal



436 estimate under the given constrains.

437

### 438 **3.3. Field Data**

439 The proposed algorithm is applied to a river stage tomographic survey conducted  
440 in Pingtung Plain, Taiwan. It is a 1200 km<sup>2</sup> catchment with three major rivers  
441 penetrating from the north to south (figure 6). The plain is bound by foothills and  
442 river valleys at the north, faults at the west and east, and the shoreline at the south. As  
443 illustrated in figure 6b, the geology inferred from well logs shows that the upstream  
444 subsurface is consist of gravel. Follows by the layered sand and clay structure at  
445 middle and down streams. The regions with unconsolidated coarse sediments (gravel  
446 and sand) are aquifer and with fine sediments (silt and clay) are aquitard. The aquitard  
447 is characterized as marine deposition because abundant fossils such as shells and  
448 foraminifera live in the shallow marine and lagoon are discovered. The aquifer is  
449 characterized as non-marine deposition. Figure 6c presents the stream stage and  
450 groundwater level variations during 2006. The average annual rainfall is 2500 mm,  
451 with most of the precipitation happen between May and September.

452 We focus on characterizing the heterogeneity of shallow aquifer because it is the  
453 major water source of agriculture, industrial, and municipal water supply. The average  
454 aquifer thickness is 40 m. This catchment is discretized into a two-dimensional  
455 horizontal confined aquifer with 5619 elements. Each element is 0.5 (km)×0.5 (km).  
456 There are 36 monitoring wells evenly placed across the catchment and measuring the  
457 hourly groundwater level variation of the aquifer since 1998. The aquifer is bounded  
458 by the time varying head boundary. The time varying heads along the boundary are  
459 extrapolated by kriging using the observed head collected from all of the monitoring  
460 wells. Water levels collected from stream gauges are incorporated into the diffusion  
461 wave equation to estimate the stream stages along the river. These estimated stages



462 are then treated as the prescribed head in the groundwater model. The initial  
463 groundwater level is estimated by spinning up the model for 6 years prior to June  
464 2006 utilizing the effective  $T$  ( $1 \text{ (m}^2\text{/day)}$ ), effective  $S$  ( $10^{-5}$  (-)), time varying head  
465 boundary, and stream stage variations.

466 The denoised groundwater levels from June to September 2006 are selected  
467 using the strategy (i.e., wavelet) discussed in Wang et al. (2017). There is a total of  
468 1440 measured heads selected for river stage tomographic survey. The initial mean  $T$   
469 ( $\hat{\mathbf{f}}^{(0)}$ ) is  $1 \text{ (m}^2\text{/day)}$ , variance of  $\ln T$  ( $\boldsymbol{\varepsilon}_{ff}^{(0)}$ ) is one (-), variance of observed head ( $\boldsymbol{\varepsilon}_{hh}^{(0)}$ )  
470 is  $10^{-4} \text{ (m}^2\text{)}$ , and the correlation lengths  $\lambda_x$  and  $\lambda_y$  are 15 (km). For simplicity, we  
471 assume  $S$  is uniform and focus on estimating the spatial  $T$  distribution. The patterns of  
472 estimated  $T$  fields should be consistent with the hydraulic diffusivity field.

473 Figure 7 presents the calibration using the original SLE algorithm. The  
474 increasing of variance of  $\ln T$  (figure 7a) near the end of iteration (iteration 100)  
475 suggests the estimate diverges, although the parameter field reproduces the observed  
476 drawdowns (figure 7b). The unreasonable huge spatial  $T$  variation corresponds to the  
477 significantly low and high values on the contour map of the final estimate field (figure  
478 7c). The contour map of manually selected best estimate is shown in figure 7d and the  
479 calibrated heads are similar with those in figure 7b.

480 Figure 8 shows the estimate using the new algorithm. The performance clearly  
481 demonstrates the robustness and usefulness of the new algorithm on characterizing the  
482 subsurface heterogeneity. Compared with the variance of  $\ln T$  in figure 7a, it stabilizes  
483 at the end of iteration (figure 8a) while still reproduces the adjusted observed heads  
484 (figure 8b). The estimated field (figure 8c) shares the similar spatial patterns with the  
485 manually selected one (figure 7d).

486 To further examine the reliability of the estimate, the estimated  $T$  field is



487 compared with the map of geological sensitivity regions (figure 9) delineated by the  
488 Department of Central Geology Survey, Taiwan. The geological sensitivity regions  
489 represent the major areas water recharges the aquifer. They are categorized by core  
490 samples, geophysics (e.g., electric resistivity), and geochemical survey. In general, the  
491 deposition of geological sensitivity region is gravel and the aquifer thickness is  
492 greater than 100 m (blue areas in figure 6b). Compared figure 9 with figure 7d and 8c,  
493 the high  $T$  regions located near the upper streams (red areas) are in parallel with the  
494 geological sensitivity regions.

495

#### 496 **4. Conclusion**

497 In this paper, a reduced order geostatistical model is developed to account for the  
498 subsurface heterogeneity. This method includes the evaluation of the errors of state  
499 variables and unknown parameters to improve the robustness of convergence. The  
500 over fitting problem (i.e., diverged estimated parameter fields) is leveraged by  
501 considering these errors into the calibration process. The memory burden (i.e. high  
502 dimensional parameter covariance) and requirement of domain shape (e.g., brick or  
503 rectangle) are also relieved by approximating the parameter covariance matrix  
504 through limited number of leading eigenvalues and eigenvectors using SVD.  
505 Meanwhile, the computation of sensitivity is replaced by the direct evaluation of  
506 cross-covariance through the finite differencing method. The modification relaxes  
507 barrier of implementing this inverse algorithm to different disciplines because the  
508 derivation of adjoint state method is no longer necessary. Lastly, as the stability of  
509 convergence is robust and the evaluation of cross-covariance (sensitivity) is efficient,  
510 the proposed algorithm is valuable and attractive for multi-discipline scientific  
511 problems, especially useful and convenient for assimilating different types of  
512 measurements.



513

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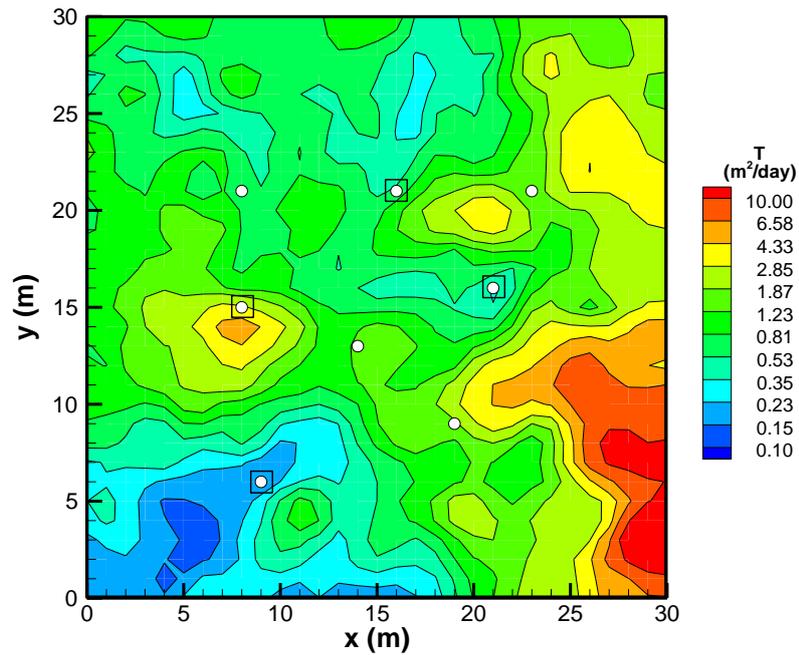
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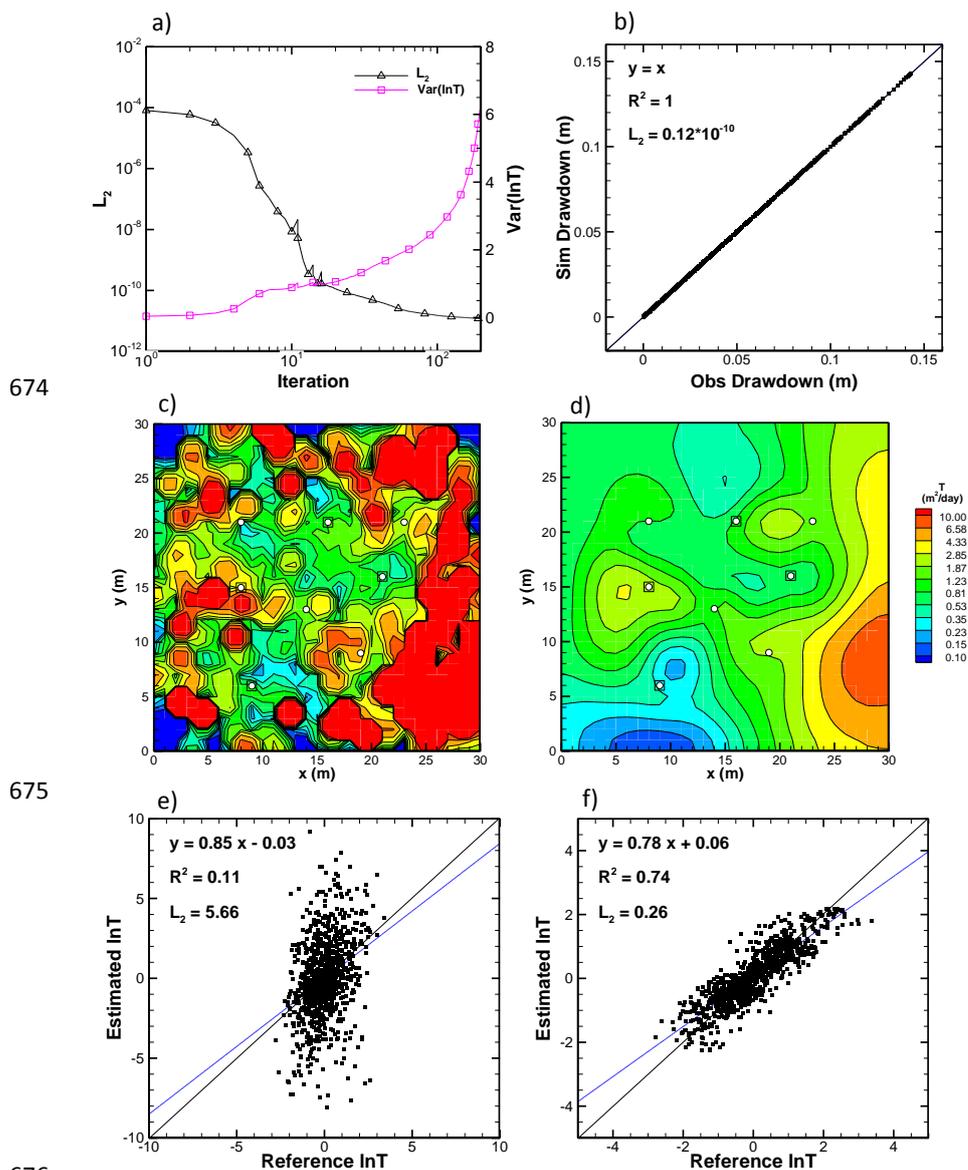
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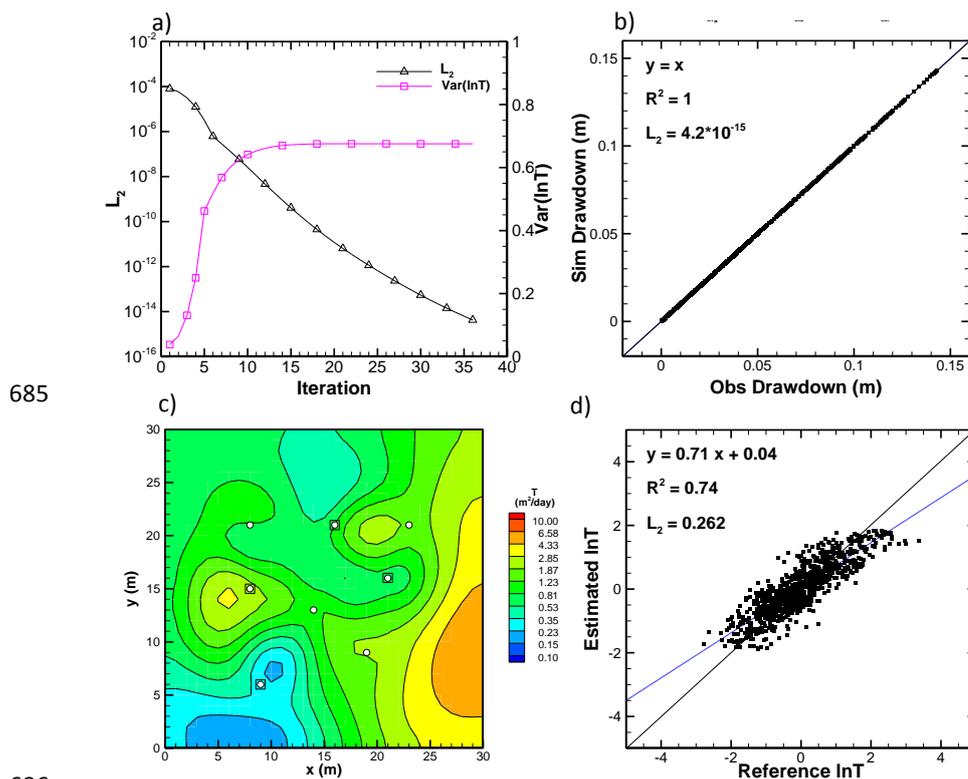


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670 Figure 1. Reference hydraulic transmissivity  $T$  (m<sup>2</sup>/day) field. The white dots  
671 represent monitoring wells and the squared are pumping wells. Four boundaries are  
672 the constant head.  
673



677 Figure 2. The estimated hydraulic transmissivity  $T$  ( $\text{m}^2/\text{day}$ ) field using noise free  
 678 observed head and old algorithm. a) The evolutions of mean squared error between  
 679 the observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var}(\ln T)$ )  
 680 during the calibration process. b) The calibrated head of the final iteration. c) The  
 681 final estimated  $T$  field. d) The best estimated  $T$  field. e) The scatter plots of final  
 682 estimated verses reference  $\ln T$ . f) The scatter plots of best estimated verses reference  
 683  $\ln T$ .

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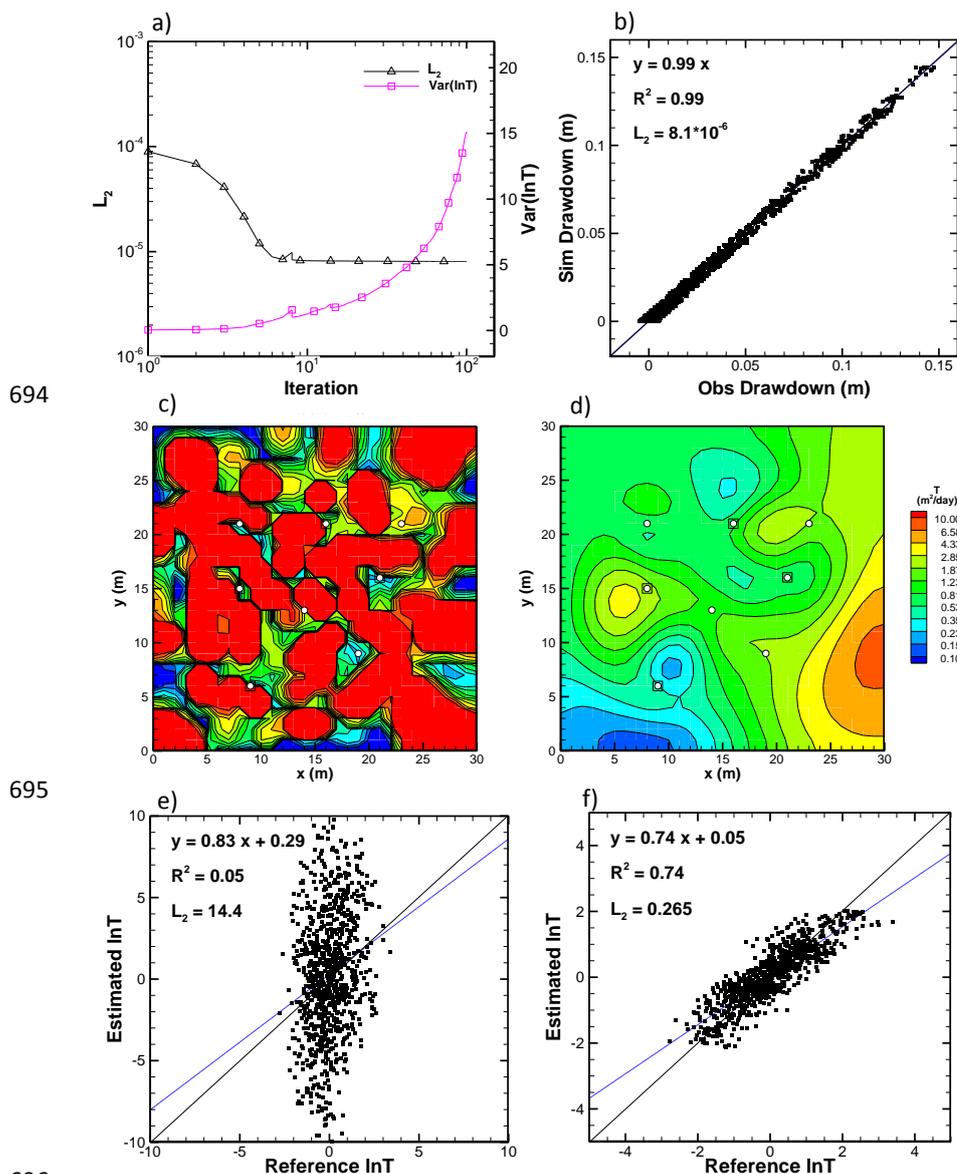
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687 Figure 3. The estimated hydraulic transmissivity  $T$  (m<sup>2</sup>/day) field using noise free  
 688 observed head and new algorithm. a) The evolutions of mean squared error between  
 689 the observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  (Var  $\ln T$ )  
 690 during the calibration process. b) The calibrated head of the final iteration. c) The  
 691 final estimated  $T$  field. d) The scatter plots of final estimated versus reference  $\ln T$ .

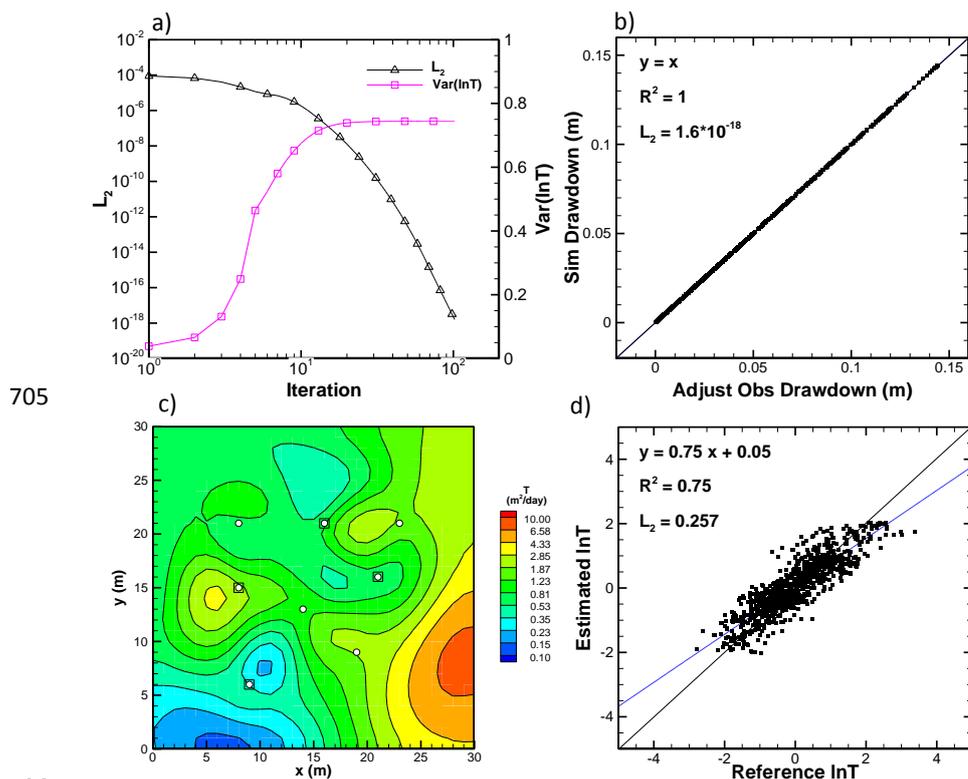
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 697 Figure 4. The estimated hydraulic transmissivity  $T$  ( $\text{m}^2/\text{day}$ ) field using noisy  
 698 observed head and old algorithm. a) The evolutions of mean squared error between  
 699 the observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var}(\ln T)$ )  
 700 during the calibration process. b) The calibrated head of the final iteration. c) The  
 701 final estimated  $T$  field. d) The best estimated  $T$  field. e) The scatter plots of final  
 702 estimated versus reference  $\ln T$ . f) The scatter plots of best estimated versus reference  
 703  $\ln T$ .

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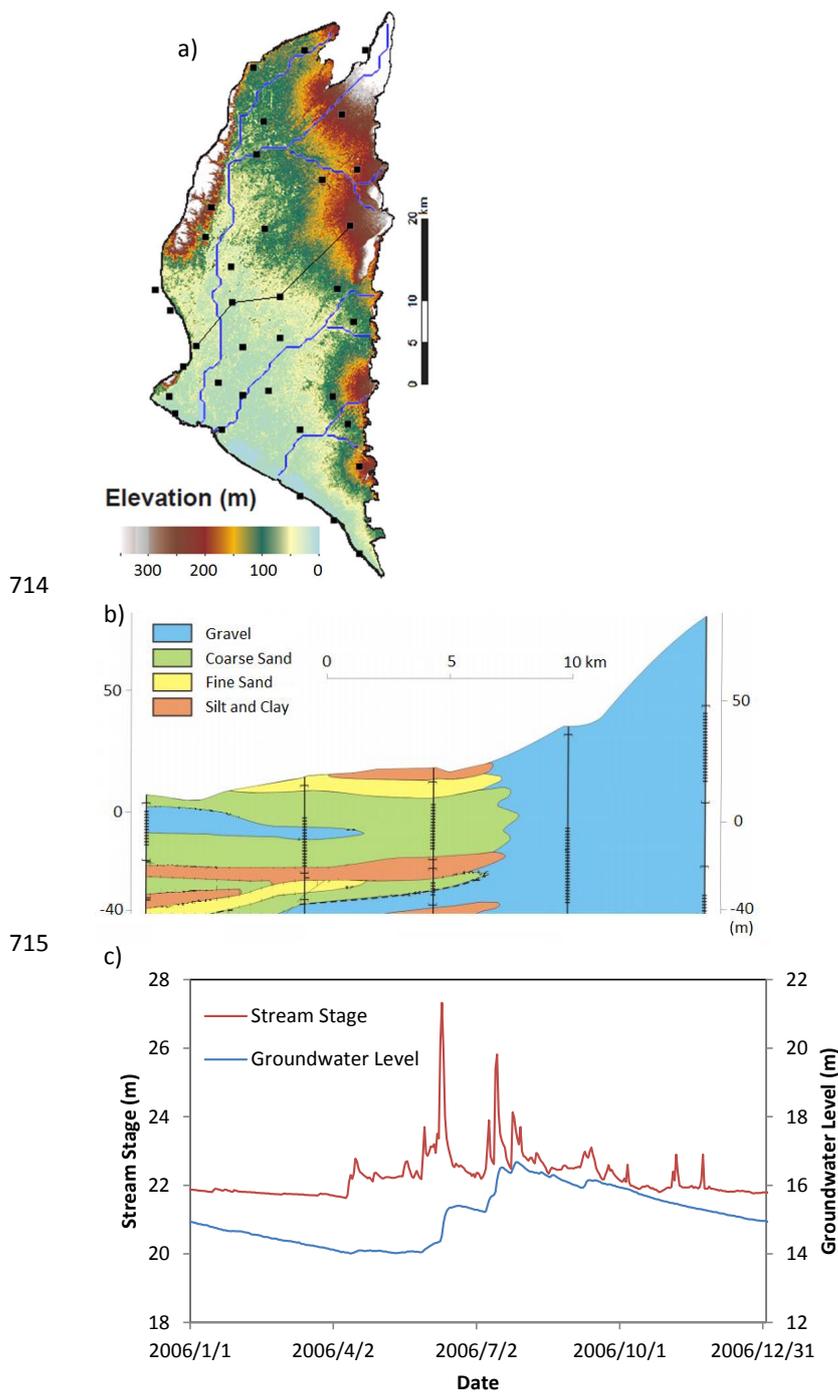


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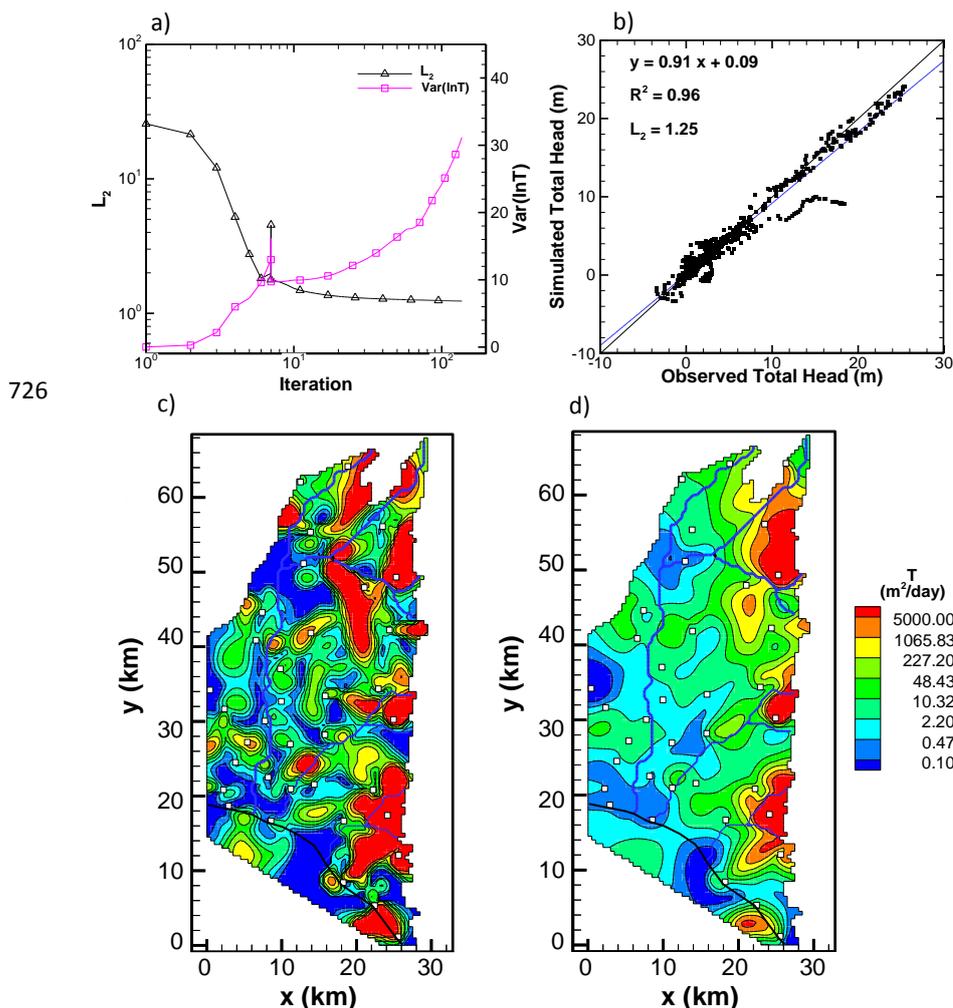
707 Figure 5. The estimated hydraulic transmissivity  $T$  ( $\text{m}^2/\text{day}$ ) field using noisy  
 708 observed head and new algorithm. a) The evolutions of mean squared error between  
 709 the observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var} \ln T$ )  
 710 during the calibration process. b) The calibrated heads verse adjusted observed heads  
 711 (observed head + estimated error) of the final iteration. c) The final estimated  $T$  field.  
 712 d) The scatter plots of final estimated verses reference  $\ln T$ .

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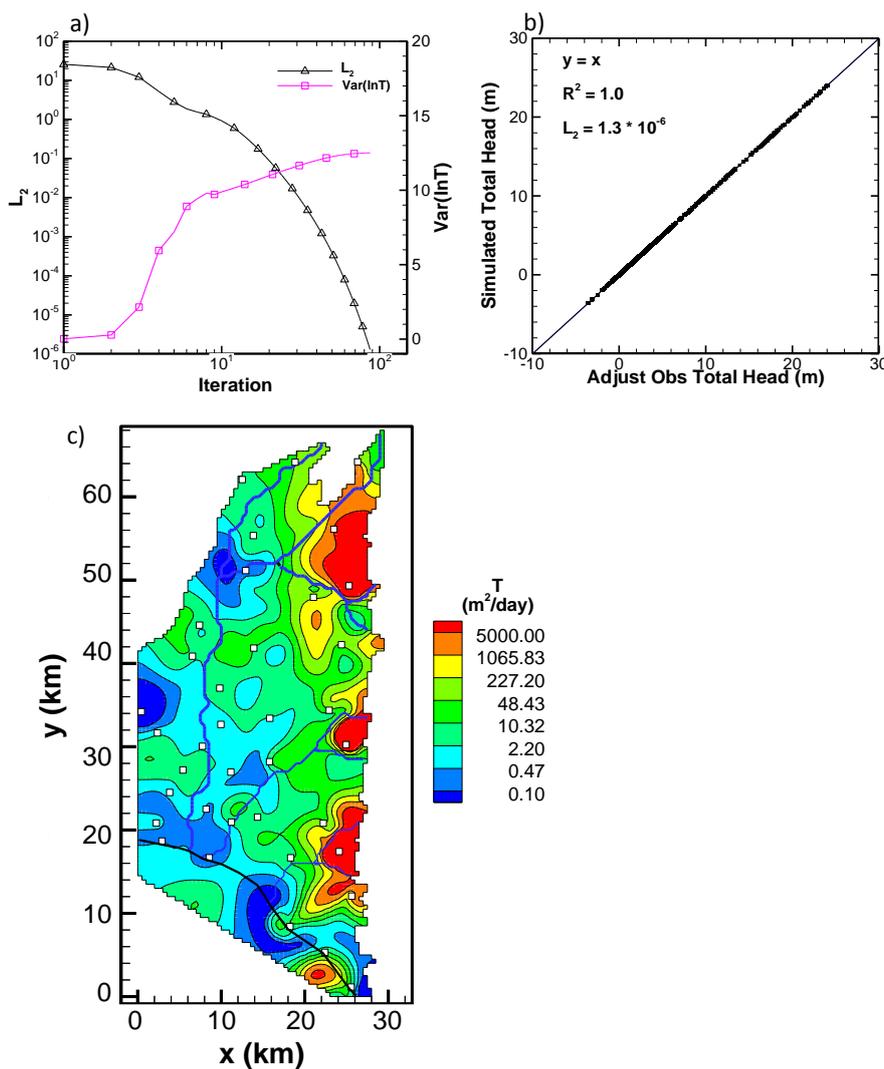




717 Figure 6. a) Topography of the study plain. The blue lines represent rivers and the  
718 black rectangles are groundwater monitoring wells. The black line is geological cross  
719 section. b) Geological cross section. c) Stream stage and groundwater level variations  
720 during 2006. a) and b) are modified from the website of Water Resources Agency, the  
721 administrative agency of the Ministry of Economic Affairs in Taiwan.  
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 728 Figure 7. The estimated hydraulic transmissivity  $T$  ( $\text{m}^2/\text{day}$ ) field using observed head  
 729 in the field and old algorithm. a) The evolutions of mean squared error between the  
 730 observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var} \ln T$ )  
 731 during the calibration process. b) The calibrated head of the final iteration. c) The  
 732 final estimated  $T$  field. d) The best estimated  $T$  field. The white squares represent  
 733 wells, the blue lines are rivers, and the black line is shoreline.

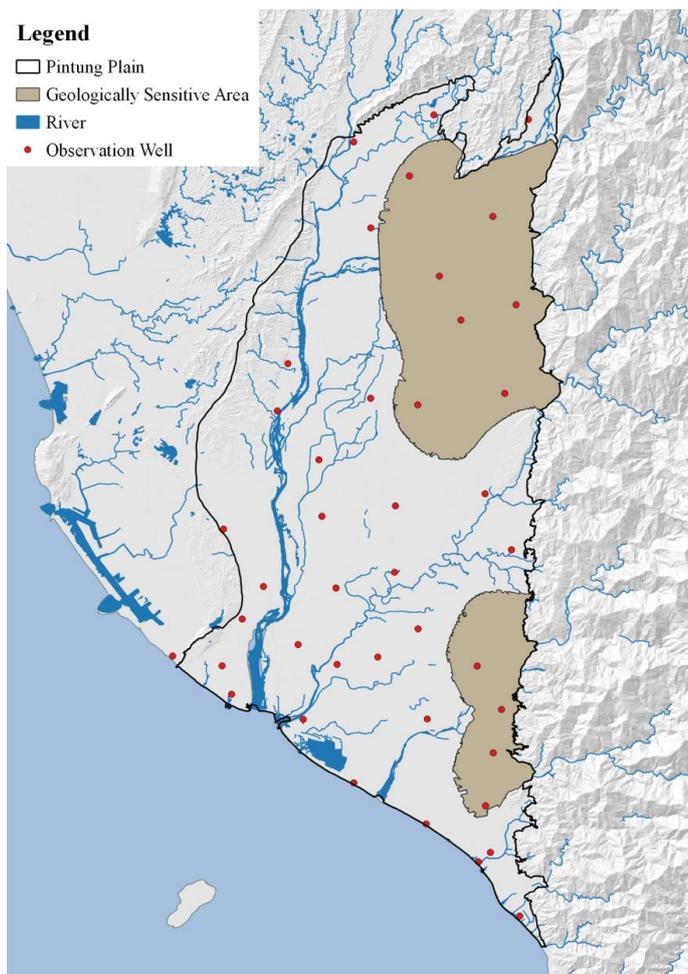


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738 Figure 8. The estimated hydraulic transmissivity  $T$  ( $\text{m}^2/\text{day}$ ) field using observed head  
 739 in the field and new algorithm. a) The evolutions of mean squared error between the  
 740 observed and simulated heads ( $L_2$  norm) and the spatial variance of  $\ln T$  ( $\text{Var} \ln T$ )  
 741 during the calibration process. b) The calibrated heads verse adjusted observed heads  
 742 (observed head + estimated error) of the final iteration. c) The final estimated  $T$  field.  
 743 The white squares represent wells, the blue lines are rivers, and the black line is  
 744 shoreline.

745



746  
747 Figure 9. Geological sensitivity regions delineated by the Department of Central  
748 Geology Survey, Taiwan.  
749



750 **Code/Data availability**

751 The code and data are available upon the request through corresponding author.

752

753 **Author contribution**

754 Y.-L. Wang designed the study, carried out the analysis, interpreted the data, and  
755 wrote the paper. T.-C. Jim Yeh and J.-P. Tsai provided the financial support and helped  
756 finalize the paper.

757

758 **Competing interests**

759 The authors declare that they have no conflict of interest.

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