

1 **Identifying uncertainties in hydrologic fluxes and seasonality from**
2 **hydrologic model components for climate change impact**
3 **assessments**

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9 **Abstract:** Assessing impacts of climate change on hydrologic systems is critical for developing
10 adaptation and mitigation strategies for water resource management, risk control and ecosystem
11 conservation practices. Such assessments are commonly accomplished using outputs from a
12 hydrologic model forced with future precipitation and temperature projections. **The algorithms**
13 **used for the hydrologic model components (e.g., runoff generation) can introduce significant**
14 **uncertainties in the simulated hydrologic variables.** Here, a modeling framework was developed
15 that integrates multiple runoff generation algorithms with a routing model and associated
16 parameter optimizations. This framework is able to identify uncertainties from both hydrologic
17 model components and climate forcings as well as associated parameterization. Three
18 fundamentally different runoff generation approaches: runoff coefficient method (RCM,
19 conceptual), variable infiltration capacity (VIC, physically-based, infiltration excess) and simple-
20 TOPMODEL (STP, physically-based, saturation excess), were coupled with the Hillslope River
21 Routing model to simulate surface/subsurface runoff and streamflow. **A case study conducted in**
22 **Santa Barbara County, California, reveals increased surface runoff in February and March while**
23 **decreased runoff in other months, a delayed (3 days, median) and shortened (6 days, median) wet**
24 **season, and increased daily discharge especially for the extremes (e.g., 100-yr flood discharge,**
25 **Q₁₀₀). The Bayesian Model Averaging analysis indicates the probability of such increase can be**
26 **up to 85%. For projected changes in runoff and discharge, general circulation models (GCMs)**
27 **and emission scenarios are two major uncertainty sources, accounting for about half of the total**
28 **uncertainty. For the changes in seasonality, GCMs and hydrologic models are two major**
29 **uncertainty contributors (~35%). In contrast, the contribution of hydrologic model parameters to**
30 **the total uncertainty of changes in these hydrologic variables is relatively small (<6%), limiting**
31 **the impacts of hydrologic model parameter equifinality in climate change impact analysis. This**
32 **study provides useful information for practices associated with water resources, risk control and**
33 **ecosystems conservation and for studies related to hydrologic model evaluation and climate**
34 **change impact analysis for the study region as well as other Mediterranean regions.**

35 1. Introduction

36 Streamflow is essential to human and ecosystems, supporting human's life and economic
37 activities, providing habitat for aquatic creatures, and exporting sediment/nutrients to coastal
38 ecosystems (Feng et al., 2016; Barnett et al., 2005; Milly et al., 2005). Understanding streamflow
39 characteristics is important for water-resources management, civil infrastructure design and
40 making adaptation strategies for economic and ecological practices (Feng et al., 2019). With
41 economic development and population growth, the emission of greenhouse gas is likely to
42 increase during 21st century (IPCC, 2014). The increase in global surface temperature is
43 projected to exceed 2°C by the end of 21st century even under moderate emission scenarios (e.g.,
44 Representative Concentration Pathways, RCPs, 4.5 and 6.0) (IPCC, 2014). Intensified hydro-
45 meteorological processes, altered precipitation forms and patterns, and intensified atmospheric
46 river events and oceanic anomalies (e.g. El Nino events) are projected and likely to cause
47 substantial impacts on hydrologic fluxes (Barnett et al., 2005; Tao et al., 2011; Dai,
48 2013; Dettinger, 2011; Vicky et al., 2018; Cai et al., 2014; Feng et al., 2019).

49 The integration of climate projections and hydrologic models enables the investigation of
50 hydrologic dynamics under the future climate conditions. However, the simulated hydrologic
51 fluxes contain uncertainties from various sources. Due to the epistemic limitations (e.g., human's
52 lack of knowledge about hydrologic processes and boundary conditions) and the complexities in
53 nature (e.g., temporal and spatial heterogeneity), hydrologic models are simplified
54 representations of natural hydrologic processes (Beven and Cloke, 2012). **Generally, hydrologic**
55 **models have modules simulating water partitioning at land surface (named as runoff generation**
56 **process in this study), evapotranspiration (ET), and water transportation along terrestrial**
57 **hillslopes and channels (named as routing process here).** Each process can be represented in
58 different ways, which thus results in uncertainties in simulated variables. For the runoff
59 generation process, surface runoff is mainly represented as infiltration excess overland flow (or
60 Hortonian flow (Horton, 1933)) or saturation excess overland flow. Infiltration excess overland
61 flow occurs when water falls on the soil surface at a rate higher than that the soil can absorb.
62 Saturation excess overland flow occurs when precipitation falls on completely saturated soils.
63 Surface runoff can also be quantified conceptually, for example, a runoff coefficient can be used
64 to generate surface runoff as a proportion of precipitation rate. Subsurface runoff is generally

65 represented as functions of soil characteristics and topographic features. The complexity of these
66 functions varies significantly, from simple linear to combinations of multiple non-linear.
67 Parameterization can be another uncertainty source. Due to the nonlinearity of hydrologic
68 processes, different combinations of model parameters can achieve similar, if not identical,
69 model performance. **Model parameter selections based on calibration metrics can result in**
70 **different optimal parameter values (i.e., parameter equifinality).** When it comes to hydrologic
71 impact assessments, the climate forcings, which differ among General Circulation Models
72 (GCMs) due to the model discrepancy and the uncertainty of future emission scenarios, also
73 contribute to the uncertainties in hydrologic simulations. Without appropriate assessment of
74 these uncertainties, standalone studies on the climate change impacts can be difficult to interpret.
75 Systematic assessments of the relevant uncertainties associated with simulated hydrologic fluxes
76 are needed.

77 Some studies have been performed to investigate uncertainties mentioned above at both
78 variable scales (for example, (Wilby and Harris, 2006;Vetter et al., 2015;Valentina et al.,
79 2017;Kay et al., 2009;Eisner et al., 2017;Su et al., 2017;Schewe et al., 2014;Hagemann et al.,
80 2013;Asadih and Krakauer, 2017;Chegwidden et al., 2019;Hattermann et al., 2018;Addor et al.,
81 2014)). **Most previous studies treated hydrologic models as a whole package. However,**
82 **hydrologic models consist of multiple components (e.g., runoff generation, ET and routing).**
83 **These components can be significantly different among models. When considering the**
84 **hydrologic model as a whole, it is difficult to quantify relative uncertainty contributions from**
85 **different components.** Troin et al. (2018) tested the uncertainties from hydrologic model
86 components for snow and potential ET. In this study, a consistent hydrologic modeling
87 framework that integrates multiple runoff generation process models with surface, subsurface
88 and channel routing processes and associated parameter uncertainties was developed. This
89 framework enables uncertainties from different components representing hydrologic processes
90 and associated model parameters as well as model forcings (e.g., precipitation and temperature)
91 to be quantified and compared in a consistent manner. In this framework, three runoff generation
92 process models which represent three fundamentally different approaches mentioned above were
93 used. The conceptual frameworks were adapted from the variable infiltration capacity model
94 (Wood et al., 1992;Liang et al., 1996) (infiltration excess), simple-TOPMODEL (Niu et al.,
95 2005) (saturation excess), and the runoff coefficient method (Feng et al., 2019) (conceptual).

96 Each approach was coupled within one routing model (i.e., Hillslope River Routing model, HRR
97 (Beighley et al., 2009)) to simulate the terrestrial hydrological processes. This modeling
98 framework was also integrated with a Bayesian model averaging (BMA) analysis to assess the
99 performance of different model-forcing-parameter combinations and to provide actionable
100 information (e.g., probability of estimated changes) for associated practices, such as water
101 resource management and ecology conservation.

102 A case study was presented for Santa Barbara County (SBC), CA, a biodiverse region
103 under a Mediterranean climate with a mix of highly developed and natural watersheds. Previous
104 studies (e.g., Feng et al., 2019) showed that the intensified storm events concentrated in a shorter
105 and delayed wet season in SBC under future climate conditions will cause significant increase in
106 discharge, especially the extremes (e.g., 100-yr discharge). The climate change impacts on the
107 path and quantity of surface/subsurface runoff and discharge will impact the soil erosion,
108 sediment/nutrients transport and subsequently affect the coastal ecosystems (Myers et al., 2019)
109 Feng et al., 2019). The longer dry season may also contribute to the increased occurrence of
110 droughts and wildfires (Myers et al., 2019). Therefore, changes in these hydrologic variables
111 (e.g., runoff, discharge and seasonality) under future climate conditions and associated
112 uncertainties are essential to assess the vulnerability of coastal region in CA and make adaptation
113 strategies to accommodate climate change. In this study, we simulated future hydrologic
114 variables using three hydrologic models forced with climate outputs from 10 GCMs that were
115 selected for their good performance in representing historical meteorological characteristics in
116 the study region, under 2 emission scenarios (RCP 4.5 and RCP 8.5) (Feng et al., 2019). The
117 main objectives of this study were to: (1) evaluate and compare the performance of hydrologic
118 models with different approaches representing runoff generation process using a consistent
119 modeling framework; (2) quantify the relative contributions of different sources (including
120 hydrologic process models, parameterizations, GCM forcings and emission scenarios) to the total
121 uncertainty in simulated surface/subsurface runoff, streamflow, and seasonality; and (3) provide
122 actionable information and suggestions for studies and practices associated with hydrologic
123 impacts of climate change.

124 **2. Methods**

125 **2.1 Study region**

126 The study region is located in coastal Santa Barbara County (SBC), California, where
127 watersheds drain into the Santa Barbara Channel from just west of the Ventura River to just east
128 of Point Conception (Figure 1). The combined land area is roughly 750 km² with 135 watersheds
129 ranging from 0.1 to 123 km². The local climate is Mediterranean, with an average annual
130 precipitation of roughly 600 mm (Feng et al., 2019). Most of the annual precipitation occurs in
131 fall/winter with 85% of rainfall occurring in the November-March period. Thus, it is
132 characterized by the intense and flashy floods in winter time. More than 80% of annual discharge
133 occurs in only a few number of large events during January-March and a large fraction of annual
134 discharge happens within one day (Beighley et al., 2003). River channels are typically filled with
135 sediment during dry season (April-October) and are scoured with the initiation of wet season
136 floods (Scott and Williams, 1978; Keller and Capelli, 1992). River flow is the major source of
137 sediment exported to the coastal sandy beaches in SBC. Therefore, the timing of seasonality,
138 path of runoff, and magnitudes of flood events are critical to both local community and coastal
139 ecosystems.

140 **2.2 Data**

141 Daily precipitation and temperature with a spatial resolution of 0.0625° x 0.0625°
142 (roughly 6 by 6 km) (Livneh et al., 2015), and daily streamflow from 4 USGS gauges for the
143 period 1984-2013 were used to calibrate and validate the hydrologic models. The Global Soil
144 Dataset for use in Earth system models (GSDE) was used to estimate saturated hydraulic
145 conductivity and saturated moisture content. The 16-day composite albedo product (MCD43C3)
146 with a spatial resolution of 0.05° x 0.05° and the monthly aerosol optical depth product
147 (MOD08M3) with a spatial resolution of 1.0° x 1.0° both derived from NASA's Moderate
148 Resolution Imaging Spectroradiometer (MODIS) were used to determine net radiation for
149 evapotranspiration (PET) estimation. **The aerosol optical depth product was downscaled to 0.05°
150 x 0.05° (Raoufi and Beighley, 2017).**

151 For the historical (1986-2005) and future climate simulations (2081-2100), downscaled
152 precipitation and temperature from ten climate models (please refer to Pierce et al. (2014) and
153 Pierce et al. (2015) for model details) in Coupled Model Inter-Comparison Project, Phase 5,
154 (CMIP5) (Taylor et al. 2012) for two emission scenarios RCP 4.5 and RCP 8.5 (Moss et al.
155 2010) were used. These 10 GCMs were selected because they have the best performance in
156 representing historical climate dynamics at southwest U.S. and California state scales (Pierce et
157 al., 2018).

158 2.3 Hydrologic modeling framework

159 2.3.1 Hydrologic model development

160 This modeling framework was developed on the basis of the Hillslope River Routing
161 model (HRR) (Beighley et al., 2009). The watersheds were delineated using the Digital Elevation
162 Model (DEM) data. The sub-basins were irregular-shape catchments defined by the flow
163 accumulation area threshold. In this study, the threshold was 1 km², which means the sub-basins
164 (model units) were in size of roughly 1 km². The hydrogeological inputs of hydrologic models,
165 including surface roughness, saturated hydraulic conductivity, soil thickness, porosity, plane
166 slope, channel slope and channel roughness, were averaged over each sub-basin. **This indicates**
167 **these parameters were averaged for each model unit, the majority of which has an area of**
168 **roughly 1 km², with less than 1% having an area of <1 km².** The geometry of each sub-basin
169 (plane length and width) was calculated based on an “open-book” assumption, which assumes
170 each sub-basin is a rectangular divided by the river channel into two identical parts like an open
171 book. Please refer to Beighley et al. (2009) for more details. The grid-based potential ET (PET)
172 was estimated using the method of Raoufi and Beighley (2017). The precipitation and PET were
173 extracted for each sub-basin using an area-weighted average method. Then the water-balance
174 model (i.e., runoff generation method) was applied to each model unit to simulate runoff
175 generation processes. Here, three runoff generation methods: runoff coefficient (Feng et al.,
176 2019), and the methods used in Variable Infiltration Capacity (VIC) (Wood et al., 1992;Liang et
177 al., 1996) and simple-TOPMODEL model (Niu et al., 2005), were used to simulate the
178 generation of surface and subsurface runoff excess. The routing methods within the HRR model
179 (i.e., kinematic wave for surface and subsurface lateral routing and Muskingum-Cunge for
180 channel routing) were used to simulate the transport of runoff excess. To clarify, we denote the

181 three runoff generation algorithms: runoff coefficient, runoff generation method used in Variable
182 Infiltration Capacity and runoff generation method used in simple-TOPMODEL as RCM, VIC
183 and STP, respectively. Three hydrologic models which integrate one of these runoff generation
184 methods with HRR routing model are referenced as RCM-HRR, VIC-HRR and STP-HRR,
185 respectively. The differences between simulations from these three models were considered as
186 the uncertainty resulting from hydrologic models. The three runoff generation algorithms were
187 described in the Supplemental material.

188 The water movement between soil layers in the soil matrix was similar to that in the
189 modified VIC-2L model (Liang et al., 1996). The soil was divided into 2 layers: upper layer (0.6
190 m) and lower layer (1.2 m). **The soil thickness data was from the Soil Survey Geographic**
191 **(SSURGO) Data Base for Santa Barbara County (NRCS, 1995)**. After the surface runoff was
192 determined, the infiltrated water was added to the upper soil layer, and the soil moisture was
193 updated. If the upper soil was oversaturated, the excess water was returned to surface. **The**
194 **evapotranspiration was estimated using Eq. S15**. The interaction between upper and lower soil
195 layers was simulated using the Clapper-Hornberger equation (Eq. S16-S17). Subsurface runoff
196 was generated from the bottom of the lower soil layer. **After the water fluxes (runoff, ET and**
197 **water movement between soil layers) were determined, the soil moisture was updated which**
198 **would be used for the water balance calculation in the next time step**. After water excess for
199 surface and subsurface runoff was quantified, the kinematic wave approach was applied to
200 simulate the transport of runoff from the planes (surface and subsurface), and the Muskingum
201 Cunge method was used for channel routing following the conservation equations (Eq.S18-S20)
202 (Beighley et al., 2009). Two conceptual parameters K_{s_all} and K_{ss_all} were used in the routing
203 model, to account for spatial heterogeneity at the model unit scale and uncertainties in the hydro-
204 geologic inputs associated with the plane routing processes (e.g., surface roughness and saturated
205 hydraulic conductivity). A conceptual illustration of the hydrologic models is shown in Figure 2.

206 2.3.2 Model calibration

207 After the models were setup, a state-of-the-art optimization algorithm, Borg
208 Multiobjective Evolutionary Algorithm (Borg MOEA) (Hadka and Reed, 2013), was adopted to
209 optimize the model parameters (Table 1). The models spun up for one year to ensure the

210 equilibrium status. For each model, there were 4 parameters calibrated for runoff generation
211 processes and 2 parameters calibrated for routing processes. K_{s_all} and K_{ss_all} are conceptual
212 parameters, and they can be different for different model structures even for the same study
213 region. Therefore, they were calibrated for each model separately. The Nash–Sutcliffe model
214 efficiency coefficient (NSE) (Eq. (1)) was used to assess model performance, as it accounts for
215 model performance in terms of both timing and magnitudes of peak flow and base flow that are
216 particularly important in this study. The optimal parameter set was determined after the
217 improvement of error was minimized (here it was defined as $\Delta NSE < 0.005$).

$$NSE = 1 - \frac{\sum_{t=1}^T (Q_s^t - Q_o^t)^2}{\sum_{t=1}^T (Q_o^t - \overline{Q_o})^2} \quad (1)$$

218 where Q_s^t and Q_o^t are simulated and observed discharge at time t, respectively, ($m^3 s^{-1}$); and $\overline{Q_o}$ is
219 the mean observed discharge during the study period of length T, ($m^3 s^{-1}$).

220 To quantify the uncertainties from model parameters, we selected 10 parameter sets using
221 the following criteria: (1) select 4 parameter sets with highest NSE based on the calibration
222 results; (2) rank the rest parameter sets based on their performance (i.e., NSE), and randomly
223 select 6 sets from the top 20% candidates. This parameter selection process enabled us to take
224 both parameter dominance and variability into account, while maintaining the high model
225 performance, which is important for the uncertainty analysis. These 10 parameter sets were then
226 used for uncertainty analysis.

227 2.4 Uncertainty Analysis

228 The uncertainty was quantified by running each of the 30 hydrologic model-parameter
229 sets (i.e., 3 hydrologic models and 10 parameter sets, $3 \times 10 = 30$) with each of the 20 forcing sets
230 (i.e., 10 GCMs and 2 emission scenarios, $10 \times 2 = 20$) for a total of 600 simulations. Here, we used
231 GCM outputs as the forcings of hydrologic models for both historical (1986-2005) and future
232 (2081-2100) periods. For each simulation scenario (i.e., the combination of hydrologic model,
233 parameter set, GCM and RCP), the historical and future daily streamflow and runoff were
234 simulated, and the relative changes (%) were quantified. Note, there is no RCPs for historical
235 period, and we used the same historical simulation for RCP 4.5 and 8.5. To evaluate the
236 uncertainty sources and their relative significance in these simulated changes in runoff, discharge

237 and seasonality for the future period, the analysis of variance (ANOVA) (Vetter et al.,
 238 2015;Addor et al., 2014;Hattermann et al., 2018;Chegwidden et al., 2019) was used. The
 239 contribution of each uncertainty source for a variable of interest (e.g., monthly runoff, 100-yr
 240 flood discharge or the duration of wet season) was defined as the fraction of its variance to the
 241 total variance. The total variance was quantified as the total sum of squares (SS_{total}) of
 242 differences between the simulations and the mean of all simulations (Eq. (2)):

$$SS_{Total} = \sum_{i=1}^{N_{Hyd}} \sum_{j=1}^{N_{para}} \sum_{k=1}^{N_{GCM}} \sum_{l=1}^{N_{RCP}} (q_{ijkl} - q_{oooo})^2 \quad (2)$$

243 where q_{ijkl} is the simulated value of the variable of interest by i^{th} hydrologic model with j^{th}
 244 parameter set, forced by k^{th} GCM projection under l^{th} RCP scenario; q_{oooo} is the overall average
 245 of the simulated variable. Next, the SS_{Total} can be divided into 15 parts representing the 4 main
 246 effects (or first-order effects), 6 second-order, 4 third-order and 1 fourth-order interaction effects.
 247 For clarity, the third and fourth orders of interaction effects were combined and represented as
 248 $SS_{3,4}$ in Eq. (3).

$$\begin{aligned} SS_{Total} = & SS_{Hyd} + SS_{para} + SS_{GCM} + SS_{RCP} + SS_{Hyd.para} + SS_{Hyd.GCM} \\ & + SS_{Hyd.RCP} + SS_{para.GCM} + SS_{para.RCP} + SS_{GCM.RCP} \\ & + SS_{3,4} \end{aligned} \quad (3)$$

249 where SS_{Hyd} , SS_{para} , SS_{GCM} and SS_{RCP} are the main effects (i.e., uncertainties or variance) from
 250 hydrologic models, hydrologic model parameters, GCMs and RCPs, respectively;
 251 $SS_{Hyd.para}$, $SS_{Hyd.GCM}$, $SS_{Hyd.RCP}$, $SS_{para.GCM}$, $SS_{para.RCP}$ and $SS_{GCM.RCP}$ are uncertainties
 252 from interactions between the hydrologic models and parameterization, hydrologic models and
 253 GCMs, hydrologic models and RCPs, parameterization and GCMs, parametrization and RCPs,
 254 and GCMs and RCPs, respectively. The calculation of each order is illustrated in Eq. S21-S23.

255 To avoid bias from the difference in sample sizes of uncertainty sources (i.e., 3
 256 hydrologic models, 3 parameter sets, 10 GCMs and 2 RCPs), a subsampling step was performed
 257 by following Vetter et al. (2015). In the subsampling step, 2 samples (i.e., the minimum number
 258 of uncertainty source, here it is RCPs) from each source were randomly selected, that is, 2

259 hydrologic models, 2 parameter sets, 2 GCMs and 2 RCPs, which indicates N_{Hyd} , N_{para} , N_{GCM}
260 and N_{RCP} in Eq. (2), (S21)-(S23) are all equal to 2. This generated $C_3^2 \times C_{10}^2 \times C_{10}^2 \times C_2^2=6075$
261 subsamples. For each subsample, the fractional sum of squares was calculated for each effect
262 using Eq. S21-S23, and then the average of variance fractions of each source is used as the
263 uncertainty contribution from that source using Eq. S24.

264 2.5 Probability of estimated changes

265 In addition to quantifying uncertainties and associated contributions from different
266 sources, an evaluation on the probability of uncertain changes in discharge can be useful to
267 provide actionable information for the stakeholders such as water resource managers. In this
268 study, the Bayesian model averaging (BMA) (Duan et al., 2007) was used to evaluate the model
269 performance in reproducing historical hydrologic conditions, and then weights were assigned to
270 each of them based on their performance. A model with better performance was assigned a
271 higher weight, assuming it has a higher probability to represent the truth. Note, there is no RCPs
272 for historical period, so only combinations of hydrologic models, parameter sets and GCMs
273 ($3 \times 10 \times 10=300$) were evaluated. Here the models' performance in representing annual mean
274 discharge (Q_m) and annual maximum daily discharge (Q_p) is evaluated. **Here, the annual mean**
275 **discharge was defined as the average of daily streamflow in a year.** The details of this procedure
276 can be found in the Supplemental material. After the weights of model ensemble were obtained
277 using the BMA method, the statistics of posterior probability distribution (here it was assumed to
278 be normal distribution) of estimated changes in Q_m , Q_p and Q_{100} in the future (2081-2100)
279 relative to historical period 1986-2005 were calculated using Eq. S29-S34.

280 2.6 Definition of hydrologic seasonality

281 To quantify the onset and duration of hydrologic seasons, we calculated the accumulative
282 discharge in the whole basin for each water year. Then the day showing the 10% of accumulative
283 annual discharge was defined as the onset of the wet season, and the number of days between the
284 10 and 90% of the accumulated discharge series was defined as the duration of the wet season.

285 **3. Results and Discussion**

286 **3.1 Hydrologic model performance**

287 The three hydrologic models performed well in representing streamflow dynamics in the study
288 region. The NSE varies within 0.56-0.67 and 0.53-0.62 for calibration and validation periods,
289 respectively, in Mission Creek (USGS gauge NO. 11119750) (Figure 3). At other calibrated
290 watersheds, the models perform similarly well with NSE varying between 0.45-0.60 for
291 calibration period and 0.42-0.62 for validation period (Figures S1-S3). Simulated streamflow
292 from the three models matches the in-situ measurements in both magnitudes and timing of
293 hydrographs at event scales (Figure 3b). At annual scale, simulated annual peak flows are
294 comparable to the observations in most years. However, in some years with extreme events, for
295 example in January 1995, February 1998 and January 2005 (highlighted in Figure 3c), the
296 simulated peaks are much lower than the gauge records. This disparity can be attributed to the
297 input bias (e.g., precipitation or streamflow measurements). This was identified using an
298 ‘extreme scenario’ simulation, which assumed 100% precipitation is transformed to surface
299 runoff (i.e., without any loss due to, for example, infiltration or evapotranspiration) and
300 transported immediately to river channels and represents the maximum streamflow considering
301 groundwater is minimal in the study region (Beighley et al., 2003). Even in this extreme
302 scenario, the simulated peaks were still lower (events highlighted in red in Figure 3c) or slightly
303 higher (event highlighted in blue in Figure 3c) than the gauge observations. This is likely
304 because that model forcings are biased low for these events. One possible source of this bias can
305 be the grid-based precipitation dataset which averages the precipitation rates over the grid
306 masking spatial heterogeneity and thus reducing precipitation rates at some locations. The
307 uncertainties in gauge measurements can also be a bias source. For example, in typical
308 conditions the uncertainty in streamflow measurements ranges between 6%-19% in small
309 watersheds, but it can be higher during large storm events when accurate stage measurements are
310 more difficult (Harmel et al., 2006). Beighley et al. (2003) also identified the overestimation of
311 gauge records for the 1995 January event at Gauge 11119940. As for mean annual discharge, all
312 three models tend to overestimate it for the study period, mainly due to the overestimation of
313 subsurface flow during dry seasons (Figure 3d). This highlights challenges of simulating
314 hydrologic processes in semiarid regions under a Mediterranean climate.

315 Among the three hydrologic models, STP-HRR has the best overall performance (i.e.,
316 highest average NSE), mainly due to its better ability for capturing flood peaks than the other
317 two models (Figures 3, S1-S3). The peak performance is likely a result of the STP-HRR
318 representing the runoff generation process as an exponential relationship between soil moisture
319 and runoff rates, which makes runoff generation more sensitive to soil moisture dynamics as
320 compared to the other two models. This algorithm is well suited to represent the significant
321 nonlinearity of hydrologic response to rainfall in the study region. RCM-HRR and VIC-HRR
322 have similar overall performance (i.e., similar average NSE), however, they represent hydrologic
323 dynamics differently. VIC-HRR tends to perform better in representing small peak flows than
324 RCM-HRR while worse in simulating mean flow (or total discharge volume) (Figures 3, S1-S3).
325 This is because as the wet season proceeds, the lower soil layer is close to saturation (i.e.,
326 relative soil moisture is higher than the threshold W_s for VIC-HRR) which initiate the quadratic
327 relationship between soil moisture and subsurface runoff in VIC-HRR. This quadratic response
328 to soil moisture conditions can lead to much higher subsurface runoff (1~2 orders of magnitude
329 higher than that of RCM-HRR), which contributes to the lower performance in reproducing the
330 total volume of discharge. This also explains that VIC-HRR generates the highest subsurface
331 runoff during the wet season (Figure 4). In addition, VIC-HRR also generates the most surface
332 runoff during wet season (Figure 4). This is because when soil is almost saturated, surface runoff
333 in VIC-HRR is almost a linear function of precipitation with a coefficient of 1 (much larger than
334 RCM-HRR which is 0.2 (C_2) and STP-HRR which is around 0.5 depending on the watershed
335 topography). The higher surface and subsurface runoff generated by VIC-HRR leads to the
336 overestimation of mean annual flow (Figure 3d). However, there are no in-situ measurement of
337 surface and subsurface runoff fluxes, and it is difficult to evaluate model performance for these
338 quantities. **In Figure 4, the simulated surface and subsurface runoff from National Land Data
339 Assimilation Systems VIC model (NLDAS-VIC) (Xia et al., 2012) outputs are shown for the
340 purpose of comparison. The NLDAS-VIC runoff simulations are from the same runoff
341 generation model (i.e., VIC) as used in this work, and have similar spatial/temporal resolutions to
342 those in this study, which makes it a suitable reference for comparison.** A similar pattern, i.e., a
343 very high subsurface runoff, even higher than surface runoff, during wet season, can be found
344 from NLDAS-VIC simulations. The surface runoff of NLDAS-VIC is lower than those
345 generated by the models in this study, which is probably because of the difference in

346 precipitation inputs. The NLDAS precipitation input is lower during wet season than that used in
347 this study for the study region. In addition, the difference in spatial resolutions of precipitation
348 (0.125° for NLDAS vs. 0.0625° for this study) can also contribute to the difference in simulated
349 runoff.

350 These results may suggest that STP-HRR is more suitable than VIC-HRR in representing
351 hydrologic processes in Mediterranean regions where 80% annual precipitation is concentrated
352 in a short period (roughly 3 months). As the wet season proceeds, the soil is close to saturation
353 conditions, under which the saturation excess overland flow is dominant. That explains why
354 STP-HRR performs best in this study region. VIC-HRR is probably more suitable to the regions
355 where precipitation events are sparsely distributed where soil is not easy to get saturated.
356 Although RCM is an empirical method, it performs fairly well in this study, mainly because it
357 captures the nonlinearity of hydrologic processes through a switch between dry and wet surface
358 runoff coefficients (C_1 and C_2) based on the soil moisture conditions.

359 Ten sets of parameters were selected for each model (Figure 5). Most optimal parameter
360 sets (red circles in Figure 5) are very close, except for C_1 , K_{s_all} in RCM-HRR and K_{s_all} , D_s in
361 VIC-HRR, suggesting that most parameters are important factors controlling model performance.
362 For the randomly selected parameters (green circles in Figure 5), most of them spread over the
363 whole range, suggesting sufficient space for uncertainty analysis.

364 3.2 Impacts and Uncertainty analysis

365 The projected changes in monthly runoff (surface, subsurface and total) during 2081-
366 2100 compared to 1986-2005 range between -100% and 300% (Figure 6a). The median changes
367 indicate that surface runoff will probably increase in February and March, and decrease in other
368 months (Figure 6a). This is because in the future, the onset of wet season will be delayed and
369 more severe storm events will occur during the shorter wet season (mainly during February and
370 March) (Feng et al., 2019). The decrease in subsurface runoff in all months is probably because
371 the decrease in the frequency (or total number) of storm events (Feng et al., 2019). The changes
372 of monthly total runoff show similar pattern with the surface runoff, suggesting the more
373 pronounced changes in surface runoff as compared to subsurface runoff. The major uncertainty
374 sources are GCM and RCP, which account for $\sim 45\%$ of total uncertainty (Figure 6b). Hydrologic

375 models contribute to ~10% of total uncertainty (Figure 6b). This suggests that the climate
376 patterns (e.g., storm event frequency and intensity) are more important factors controlling the
377 runoff generation than the hydrologic model algorithms.

378 For the 28 major watersheds in SBC, the projected changes in Q_m during 2081-2100 as
379 compared to historical period 1986-2005, range from -100% to 220% (Figure S4). The median
380 changes for each of these major watersheds are slightly above 0%, varying between 1% and 8%.
381 The major uncertainty sources are GCM and RCP, which account for ~54% of the total
382 uncertainty. Among the first order factors (i.e., GCM, RCP, hydrologic model and
383 parameterization), hydrologic model ranks third after GCM and RCP, accounting for 10-15% of
384 total uncertainty. In contrast, parameterization only induces less than 2% of the total uncertainty.
385 The remaining 25-35% uncertainty is from the second, third and fourth order interactions
386 between the four major sources. The projected relative changes in Q_p and Q_{100} are similar in
387 magnitudes, both varying from -90% to 250% (Figure S5 and Figure 7). The median changes in
388 Q_p and Q_{100} for each watershed are higher than those of Q_m , ranging between 10-40%. For most
389 of watersheds, GCM and RCP are the two major uncertainty contributors for Q_p and Q_{100} ,
390 accounting for ~45% of total uncertainties. Hydrologic model contributes ~14% of total
391 uncertainties in Q_p and Q_{100} . Compared to Q_m , Q_p and Q_{100} get more uncertainty from the
392 hydrologic models, which is likely due to highly nonlinear rainfall-runoff behavior and larger
393 differences between runoff generation methods in generating peak flows as compared to average
394 flow conditions.

395 Changes in Q_m , Q_p and Q_{100} are higher under RCP 8.5, but the uncertainties are also
396 higher (Figure 8), which suggests the higher contribution of RCP 8.5 in the uncertainties of
397 higher-order interactions between RCP and other factors (i.e., GCM, hydrologic model and
398 parameters). In Mission Creek watershed (USGS gauge No. 11119750), the probability of
399 increase in Q_m under RCP 4.5 is only 51%. However, this probability increases to 64% under
400 RCP 8.5. For the less frequent events (Q_p and Q_{100}), the probabilities of positive changes are
401 higher: 78% and 85% for Q_p and Q_{100} , respectively, under RCP 8.5. This implies that if RCP 8.5
402 happens in the future, the extreme events will probably get intensified.

403 Consistent with the work of Feng et al. (2019), this study suggests a delayed onset and
404 shorter duration of wet season (Figure 9a). The median changes show that the wet season will
405 start later by 3 days, and become shorter by ~6 days. The major uncertainty sources for both
406 onset and duration of wet season are GCM (~20%) and hydrologic models (~15%). Different
407 from discharge and runoff, the seasonality shows more uncertainty from hydrological models
408 (15% vs 12%) and model parameters (~6% vs 2%) (Figure 9b). This is because the seasonality
409 integrates the runoff generation, paths and transport processes for both surface and subsurface
410 runoff, which are important for the timing and quantity of simulated discharge.

411 As the major carrier of nutrients/sediment, surface runoff and discharge are crucial for
412 beach ecosystems in the study region (Myers et al., 2019;Aguilera and Melack, 2018). Nutrients
413 and sediment build up over land surface and in channels during dry season, and get flushed with
414 the initiation of wet season (Scott and Williams, 1978;Keller and Capelli, 1992;Bende-Michl et
415 al., 2013;Aguilera and Melack, 2018). The nutrients/sediment fluxes are positively correlated
416 with hydrologic variability, and the majority of them occurs at the beginning of the wet season
417 (Aguilera and Melack, 2018;Homyak et al., 2014). Therefore, both timing and magnitude of
418 runoff and discharge will impact the nutrients/sediment export to the coastal ecosystems. The
419 findings in this study reveal that the surface runoff and river discharge (especially the extremes)
420 will increase but get delayed during wet season (Figures 6 and 9), implying that the
421 nutrients/sediment fluxes will likely increase and occur in a shorter and delayed period. The
422 decrease in runoff (both surface and subsurface) during the dry season suggests that the soil
423 moisture will be lower under future climate conditions in the study region. The longer and drier
424 dry season will probably increase the occurrence of severe droughts and wildfires.

425 Compared to previous studies (e.g., Vetter et al. (2015), Schewe et al. (2014), Hagemann
426 et al. (2013);Troin et al. (2018), and Asadieh and Krakauer (2017)), this work identifies
427 relatively low uncertainty contributions from hydrologic models. The main reason for this is
428 probably that the hydrologic model uncertainty in this study was only from runoff generation
429 algorithms and associated parameters. As is, the three hydrologic models share common
430 algorithms for ET and plane/channel routing, and the same model configuration (e.g., soil matrix
431 and model unit definition). These similarities among models likely reduced the differences in
432 simulated runoff and discharge. In addition, the uniform calibration approach and parameter
433 selection criteria were also likely to eliminate user/method bias which is common in studies that

434 consider more than one hydrologic model. In contrast, the hydrologic models used in previous
435 studies have their own model component algorithms (e.g., ET and routing algorithms), and
436 model configurations. For example, the VIC model (here VIC refers to the original VIC model,
437 and is different from the model used in this study; to clarify, in following text, VIC refers to the
438 original VIC model while VIC-HRR refers to the model used in this study) applies an ET
439 algorithm different from the one used in this study (Raoufi and Beighley, 2017), uses the grid-
440 based model units ignoring the spatial arrangement, and has its own routing scheme which
441 adopts the synthetic unit hydrograph concept. When comparing models owning their own
442 component algorithms, the differences between models likely resulted in larger uncertainties in
443 the simulation from hydrologic models in previous studies.

444 This study can also provide useful information for hydrologic model evaluation and
445 selection. As discussed in section 3.1, the STP-HRR model is more suitable than the other two
446 models for the study region, mainly due to its ability to represent the highly non-linear
447 hydrological response to precipitation forcings. This implies hydrologic models adopting the
448 saturation excess runoff generation algorithms may be more suitable for areas with a
449 Mediterranean climate. The uncertainties from hydrologic models are larger than those from the
450 hydrologic model parameters for all variables (i.e., discharge, runoff and seasonality), suggesting
451 the inter-model variability is larger than the intra-model variability (from model parameters).
452 This implies that model selection is more important than the parameter selection, and that the
453 parameter equifinality (or non-uniqueness) is less of a concern when quantifying climate change
454 impacts on hydrologic fluxes using an ensemble of GCM forcings. In this study, only the runoff
455 generation algorithm was investigated. Other hydrologic model components, such as ET
456 algorithms and routing methods, also have variants. The choice of these components may also
457 make a difference in the total uncertainties in simulated runoff and streamflow. In addition, the
458 methods for GCM downscaling can also contribute to the uncertainty in predicted changes in
459 hydrology. Further study integrating different algorithms for hydrologic model components as
460 well as GCM downscaling methods can be conducted in the future. Such analysis can be useful
461 to guide stakeholders to select appropriate hydrologic algorithms and to develop actionable
462 adaptation and mitigation strategies to accommodate climate change.

463 This is the first study investigating hydrologic model uncertainty solely from runoff
464 generation algorithms for a region with the Mediterranean climate. The framework developed in

465 this study can be potentially used to identify the internal uncertainties of hydrologic models, i.e.,
466 uncertainties from hydrologic model components (e.g., runoff generation algorithms, ET
467 algorithms and routing models), which is particularly important for assessing model performance
468 and quantifying the relative roles of different components in the uncertainty of simulations. This
469 study region is a representative Mediterranean area characterized by dry summers and wet
470 winters. This climate pattern and the highly non-linear relationship between climate and
471 hydrology significantly impact local society, agriculture and ecosystems as discussed before. The
472 findings in this study including the favorability of STP algorithm, the important role of GCM
473 selection and the negligible role of hydrologic model parameters in the uncertainty, can be useful
474 for studies associated with hydrologic model evaluation and climate change impact analysis for
475 other Mediterranean regions.

476 **4. Conclusions**

477 A modeling framework which integrates multiple runoff generation algorithms (VIC,
478 STP and RCM) with the HRR routing model was developed. Forced with an ensemble of GCM
479 outputs under different emission scenarios, this framework is able to quantify the climate change
480 impacts on surface and subsurface runoff, streamflow and hydrologic seasonality, and evaluate
481 the associated uncertainties from different sources (i.e., RCPs, GCMs, hydrologic process
482 models and parameterization). The results show that the surface runoff will likely increase in
483 February and March, while decrease in other months, and the subsurface runoff will likely
484 decrease due to changes in the patterns of storm events. The median changes in mean annual
485 discharge for the major watersheds in SBC are 1-8%, with an uncertainty of 320% (here,
486 uncertainty refers to the range of predicted relative changes among models, that is, from -100%
487 to +220%); the median changes in annual peak discharge and 100-yr flood discharge are higher
488 than those of mean annual discharge, varying between 10% and 40%, but with a higher
489 uncertainty of 340% (-90% to +250%). The results based on the BMA analysis indicate that there
490 is a high probability (up to 85%) that streamflow, especially the extreme quantities (e.g., Q_{100})
491 under RCP 8.5, will increase. The seasonality analysis shows that the wet season will be delayed
492 (by 3 days, median) and shortened (by 6 days, median). For the uncertainties in the projected
493 changes in runoff and discharge, GCM and RCP are the top two contributors, accounting for

494 roughly 50% of total uncertainties at most major watersheds in SBC, while hydrologic process
495 models (i.e., runoff generation modules) contribute ~12% on average with the remaining 30-40%
496 of the uncertainty coming from the interactions between these individual sources. Hydrologic
497 model parameters alone contribute less than 2% of the uncertainty. In contrast, for the changes in
498 seasonality, the uncertainty contributions from hydrologic models (~15%) and hydrologic model
499 parameters (~6%) are higher as compared to those for runoff and discharge, making GCMs and
500 hydrologic models the two major uncertainty sources.

501 Unique to the framework in this study, the uncertainties from different hydrologic model
502 components (e.g., runoff generation process) and associated model parameterizations can be
503 identified and quantified. The results can be useful for practices and studies in many fields, e.g.,
504 water resources, risk controls and ecosystem conservation, for the study region as well as other
505 Mediterranean regions.

506 **Code availability**

507 The source code supporting this work is available on Github:
508 <https://github.com/dongmeifeng-2019/HydroUncertainty>

509 **Author contribution**

510 D. Feng designed the experiments, developed the models, performed the simulations, and prepared
511 the manuscript. E. Beighley conceptualized the project, and reviewed and edited the manuscript.

512 **Competing interests**

513 The authors declare that they have no conflict of interest.

514 **Acknowledgments**

515 This research was supported by the Santa Barbara Area Coastal Ecosystem Vulnerability
516 Assessment (SBA CEVA) with funding from the NOAA Climate Program Office Coastal and
517 Ocean Climate Applications (COCA) and Sea Grant Community Climate Adaptation Initiative
518 (CCAI), and the National Science Foundation's Long-Term Ecological Research (LTER) program
519 (Santa Barbara Coastal LTER - OCE9982105, OCE-0620276 and OCE-123277). The authors
520 thank Dr. David Hadka at Pennsylvania State University and Chinedum Eluwa at University of

521 Massachusetts, Amherst, for their help with setting up the Borg MOEA. The authors acknowledge
522 Dr. Konstantinos Andreadis and two anonymous reviewers for their valuable comments that
523 significantly improved the manuscript.

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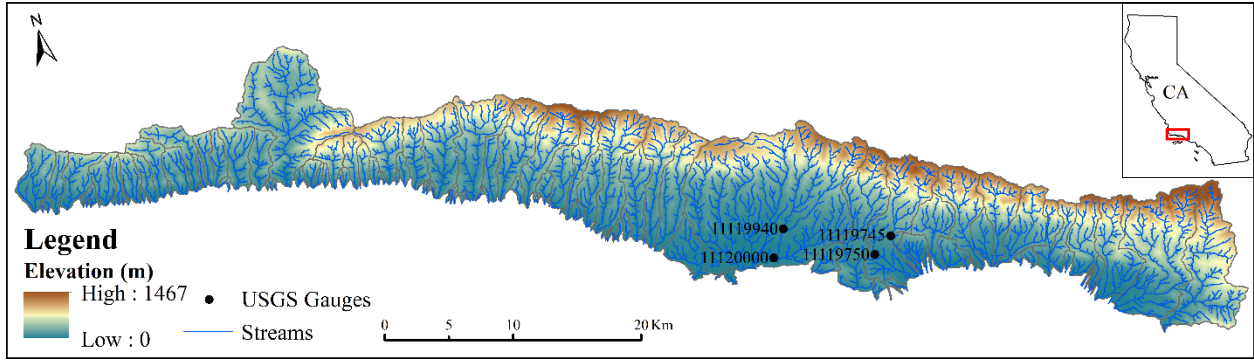
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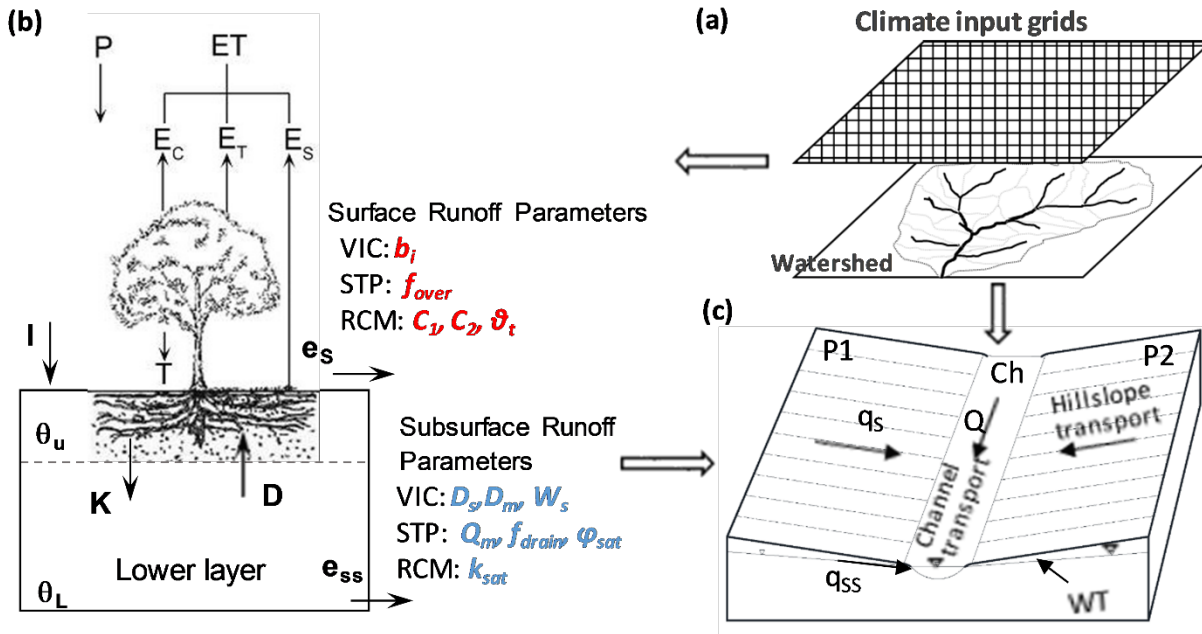
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660 **Table 1:** Calibrated parameters for hydrologic models

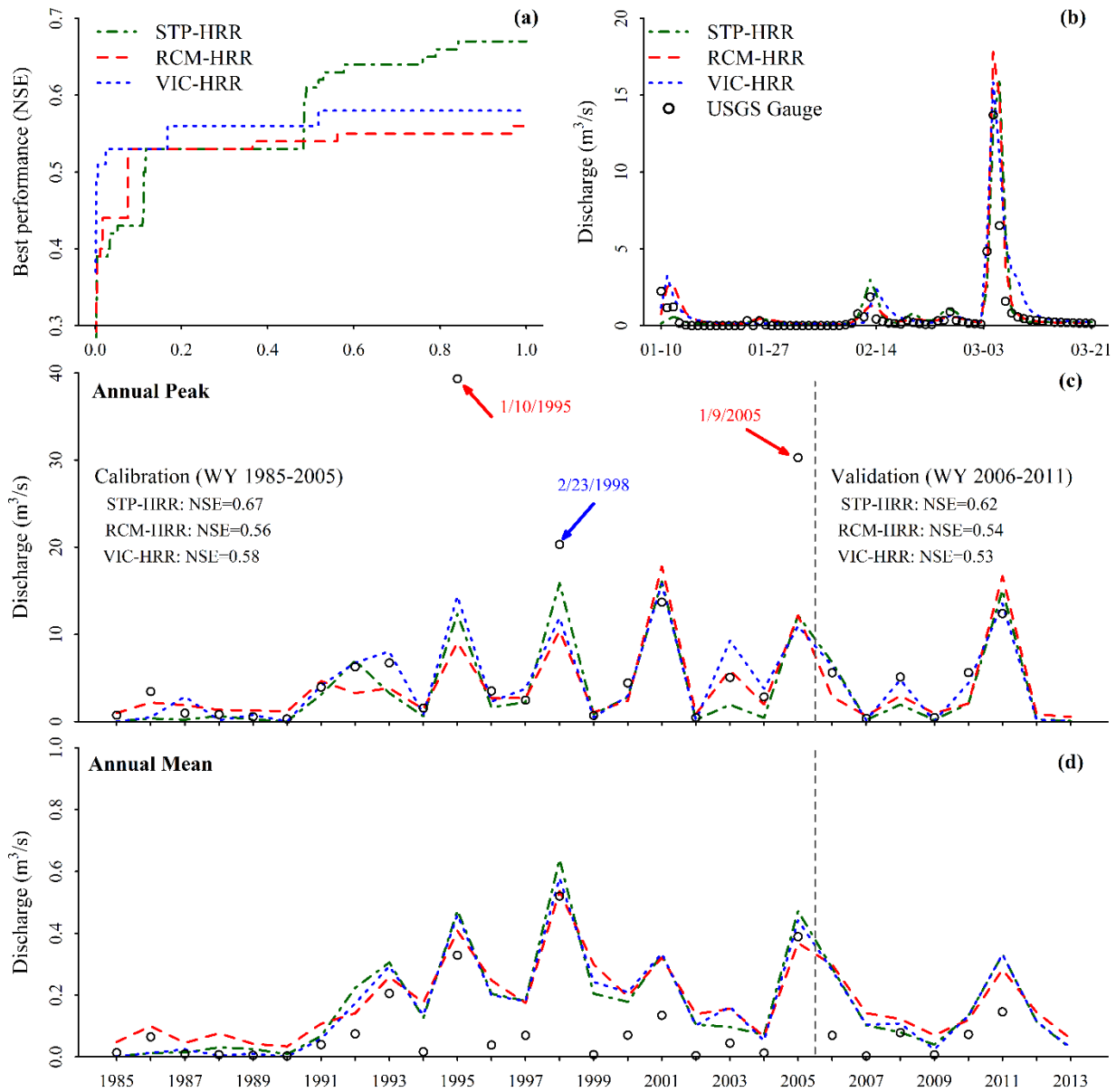
Parameters	Description	Unit	Range	RCM-HRR	VIC-HRR	STP-HRR
K_{s_all}	coefficient to adjust surface roughness	-	1-20	✓	✓	✓
K_{ss_all}	coefficient to adjust horizontal hydraulic conductivity	-	10-200	✓	✓	✓
K_{sat_all}	coefficient to adjust vertical hydraulic conductivity	-	0.01-5.0	✓		
C_1	dry runoff coefficient	-	0-0.3	✓		
C_2	wet runoff coefficient	-	0.2-0.8	✓		
θ_t	soil moisture threshold separating dry and wet conditions	-	0.2-0.8	✓		
b_{in}	Infiltration curve shape parameter	-	0.005-0.5		✓	
D_m	maximum baseflow	$m \cdot d^{-1}$	0 -0.037		✓	
D_s	fraction of D_M where non-linear baseflow begins	-	0 -0.005		✓	
W_s	fraction of the maximum soil moisture where non-linear baseflow occurs	-	0.92-1.0		✓	
f_{over}	Surface runoff coefficient	m^{-1}	0.1-5			✓
f_{drain}	Subsurface runoff coefficient	m^{-1}	0.1-5			✓
Q_m	maximum baseflow	$m \cdot d^{-1}$	0.864-1728			✓
φ_{sat}	Saturated suction head in the soil	m	-3.05-0			✓



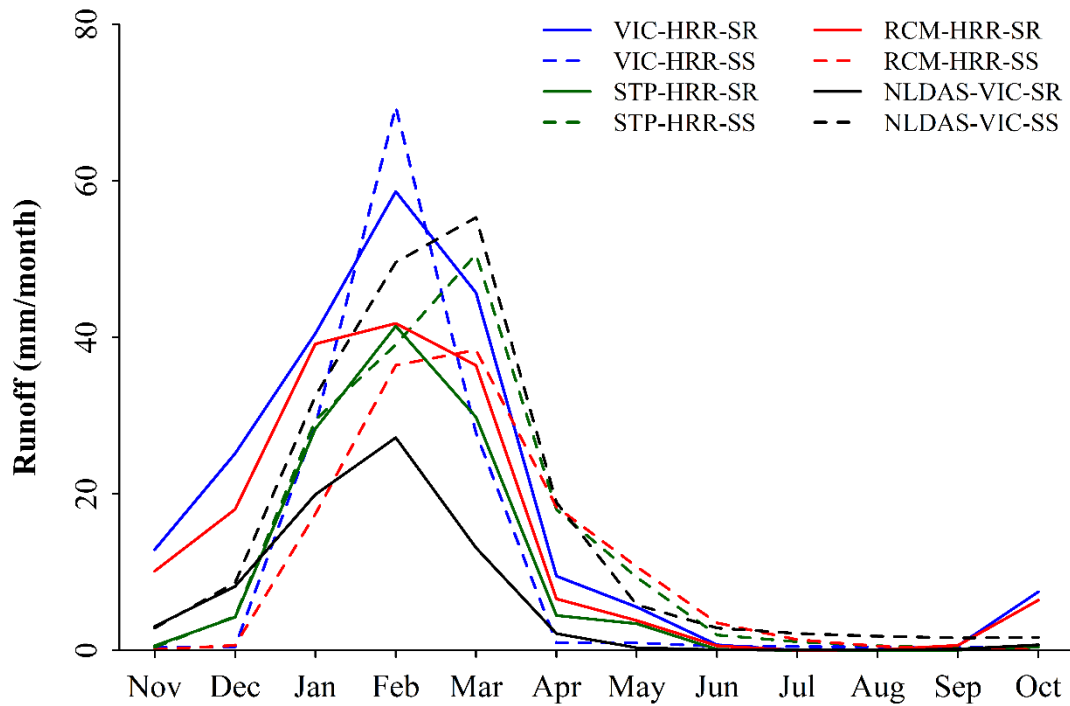
661 **Figure 1:** Study region with USGS streamflow gauges. The inset figure indicates the location of
 662 SBC in the state of California (CA).



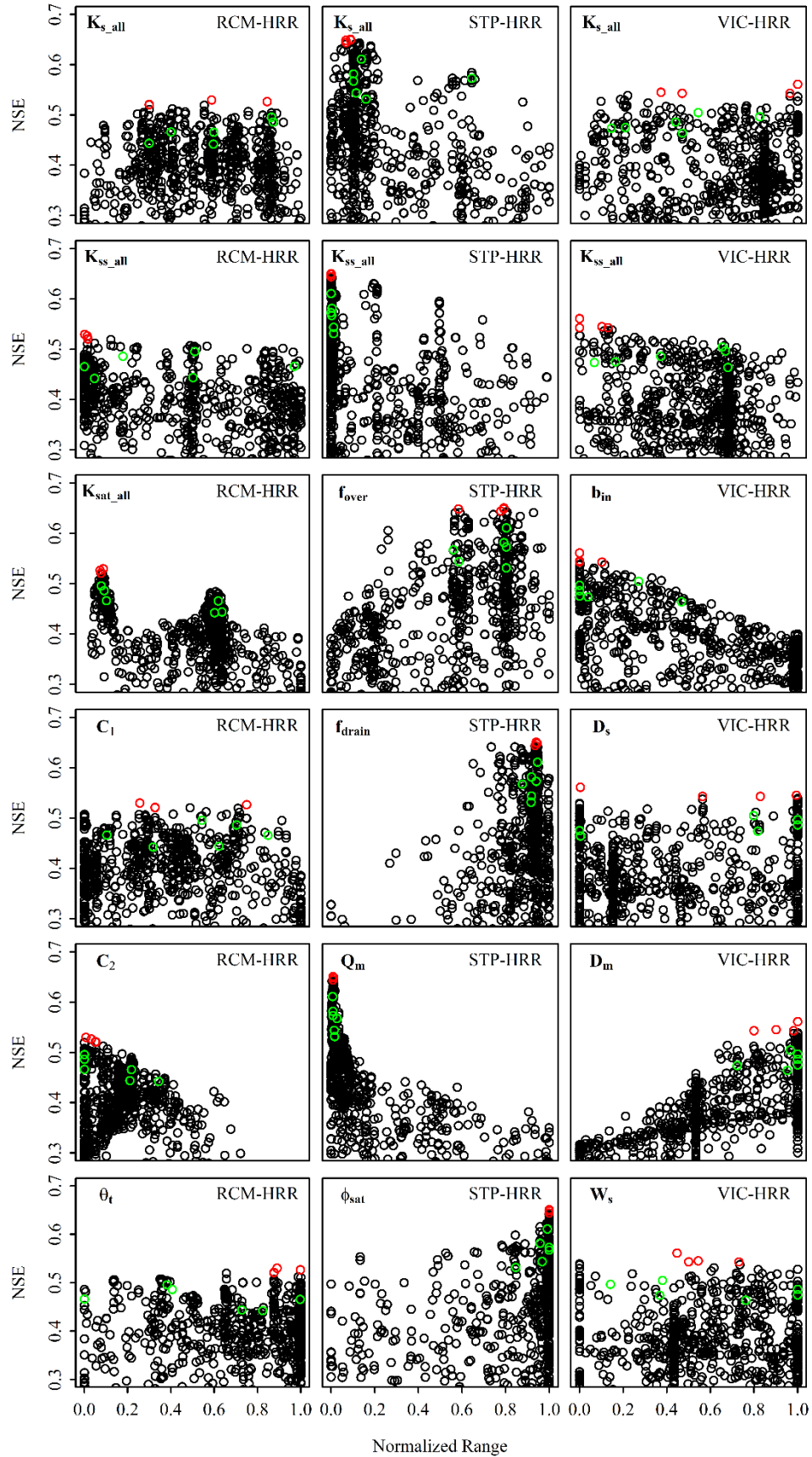
663 **Figure 2:** The conceptual framework about the hydrologic models used in this study. Portions of
 664 this figure were adapted from the work of Beighley et al. (2009). (a) shows the grid-based climate
 665 inputs for hydrologic models; (b) shows water balance models; P is precipitation; ET is
 666 evapotranspiration; E_s is soil evaporation; E_c is canopy evaporation; E_T is transpiration; e_s is water
 667 available for surface runoff; e_{ss} is water available for subsurface runoff; θ_u is relative soil moisture
 668 in upper soil layer; θ_L is relative soil moisture in lower soil layer; I is infiltration; K is water flux
 669 from the upper layer to the lower layer; and D is diffusive water flux from the lower layer to the
 670 upper layer; and (c) shows HRR routing model; the “open-book” assumption: two identical planes
 671 (P1 and P2) with the channel (Ch) in the center of each sub-basin; q_s is the surface runoff; q_{ss} is
 672 subsurface runoff; Q is discharge in the river channel, and WT is groundwater table. The
 673 parameters in red italic are for surface runoff generation, the parameters in blue italic are for
 674 subsurface runoff generation. The first columns in the tables indicate the models that the
 675 parameters are used for. The definition of these parameters can be found in the supporting
 676 information.



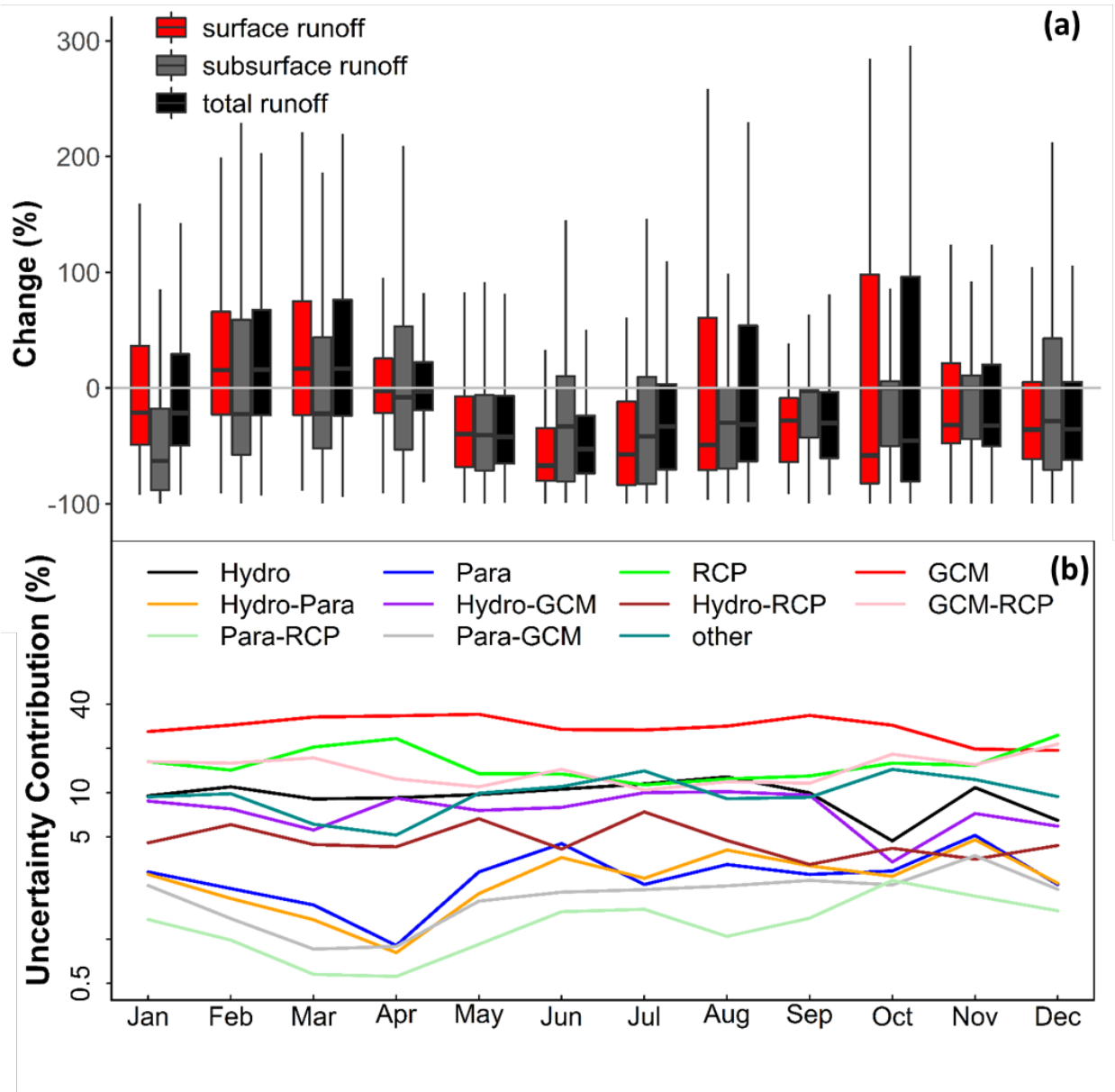
677 **Figure 3:** Model performance for calibration and validation periods: (a) model performance (assessed by
678 NSE) during calibration process, the x axis is the normalized calibration process; the “normalized
679 calibration process” means the x axis range is normalized by the number of iterations during calibration;
680 (b) hydrographs simulated by three calibrated models and measured by the USGS gauge; in order to show
681 the details of the hydrographs, they are zoomed in to the wet season in 2001; the model performance is
682 similar in other years; (c) simulated annual peak flow during calibration (water year 1985-2005) and
683 validation (water year 2006-2011) periods as compared with in situ observations; black texts indicate model
684 performance (i.e., NSE); the points highlighted in red arrows indicate the events were not reproduced by
685 models due to the input (e.g., precipitation or discharge observation) bias; the point highlighted in blue
686 arrow is similar to those in red but at a lower probability; and (d) simulated and observed annual mean flow
687 during calibration and validation periods. For clarity, only results for the Mission Creek watershed (USGS
688 gauge NO. 11119750) are shown here; results for other gauged watersheds are similar and can be found in
689 the Supporting Information (Figure S1-S3).



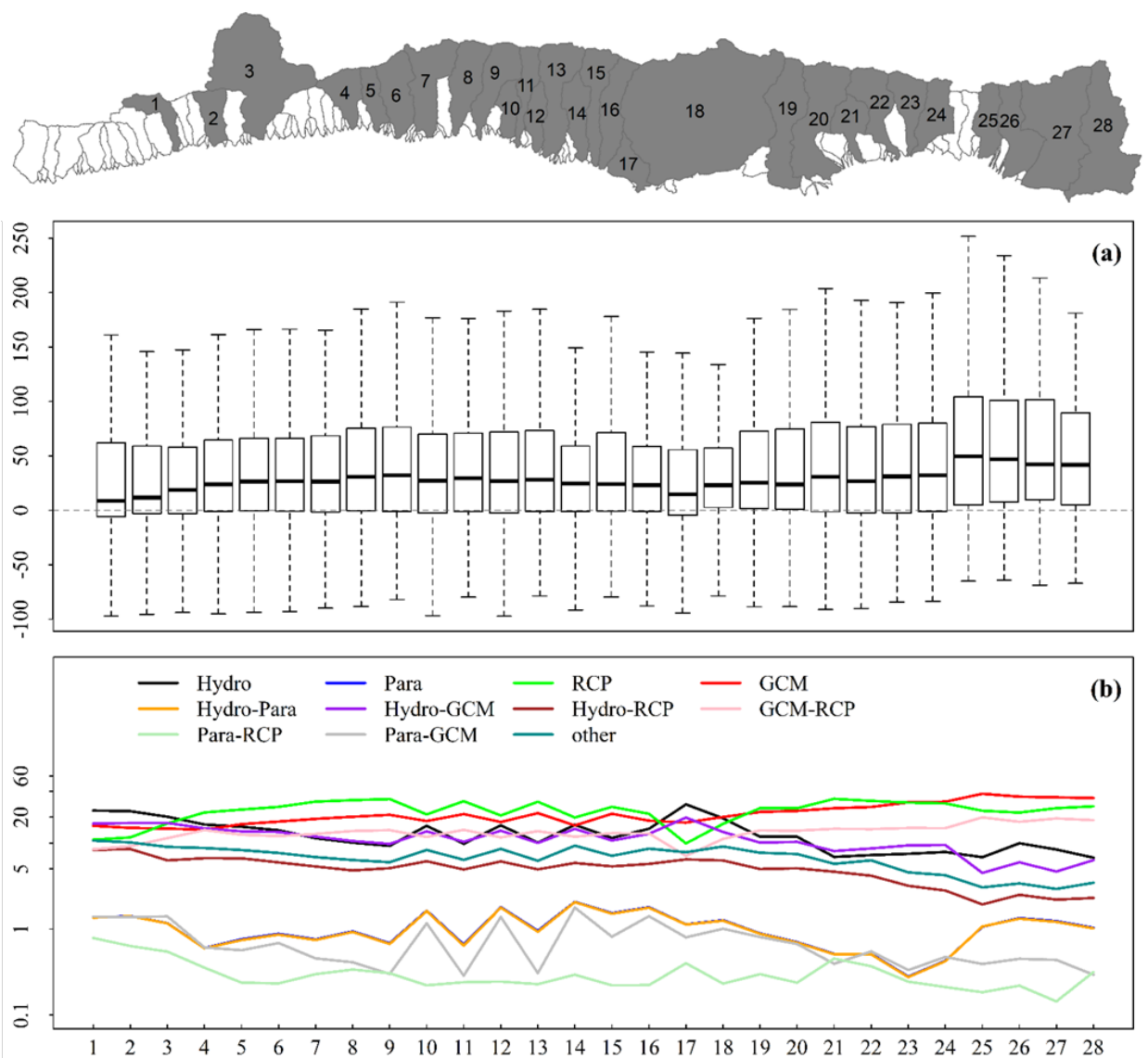
690 **Figure 4:** Simulated monthly surface and subsurface runoff for the Mission Creek watershed (USGS
 691 gauge NO. 11119750) by three models for the calibration period (water year 1985-2005). Surface runoff
 692 is denoted by 'SR' and subsurface runoff is denoted by 'SS' in this figure. Monthly surface and
 693 subsurface runoff from National Land Data Assimilation Systems (NLDAS) VIC model simulation for
 694 the same period are shown here for comparison purpose.



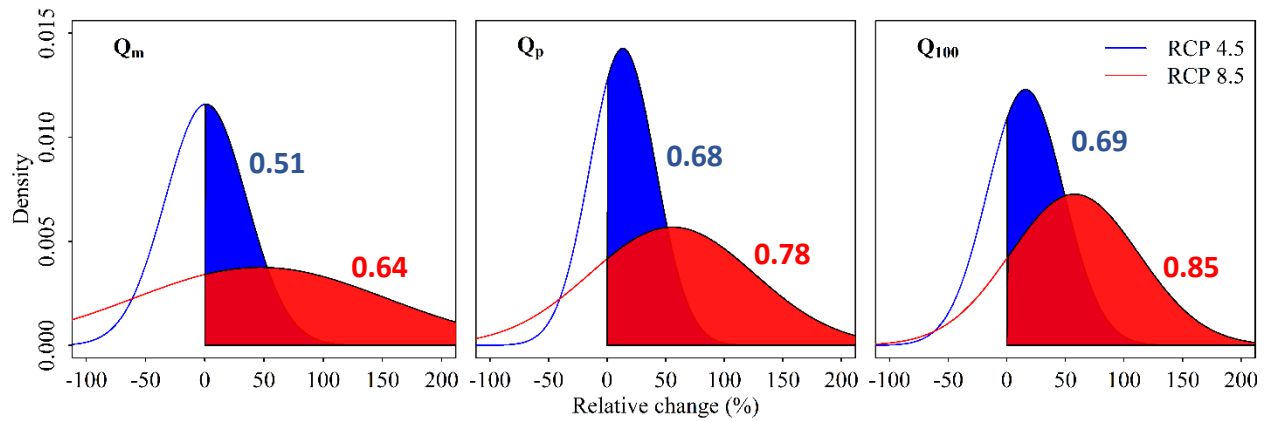
696 **Figure 5:** Parameters (black circles) sampled during calibration process and their corresponding
697 performance (assessed by NSE). The red circles indicate the 4 parameter sets with highest NSE
698 values, and the green circles indicate 6 randomly selected parameter sets from the top 20%
699 samples (ranked by NSE). These ten parameter sets were used for uncertainty analysis. In this
700 figure, the parameter values are normalized by their ranges (shown in Table 1), so the range of
701 the x axis is 0-1. The parameters were sampled throughout their whole ranges, however, for
702 clarity, samples with NSE lower than 0.3 are not shown in this figure.



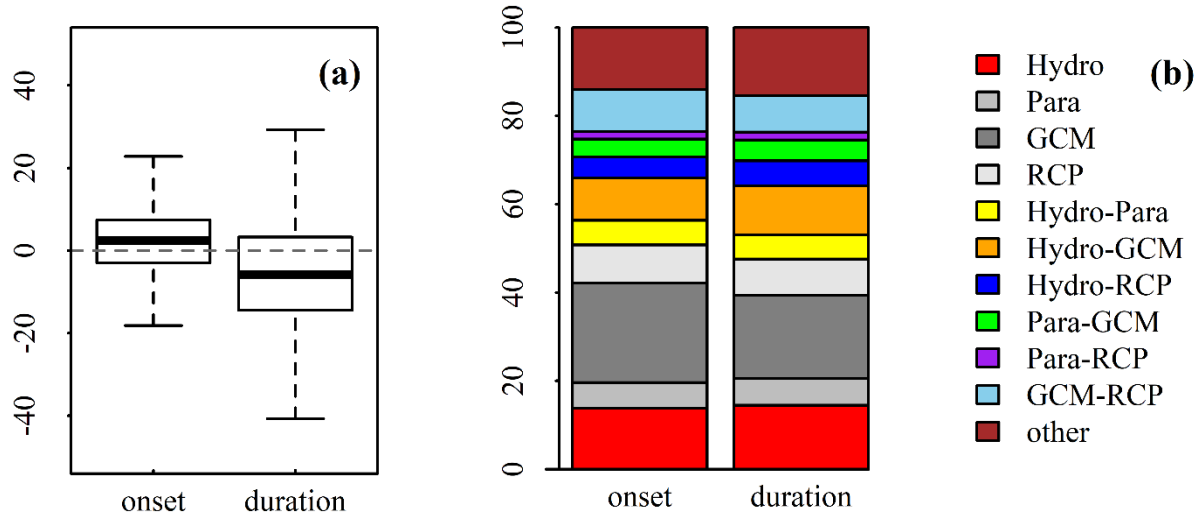
703 **Figure 6: (a)** Projected relative changes (%) in monthly surface runoff, subsurface runoff and total
704 runoff in the whole study region during 2081-2100 as compared to historical period (1986-2005);
705 **(b)** Relative contributions (%) of the uncertainties for the projected changes in the monthly total
706 runoff; Hydro = Hydrologic models; Para = hydrologic model parameters; GCM = General
707 Circulation Models; RCP = Representative concentration pathways (emission scenarios); “other”
708 is the uncertainty from the 3rd and 4th orders of interactions between the 4 major sources (i.e.,
709 GCMs, RCPs, Hydrologic models and parameters).



710 **Figure 7: (a)** Projected relative changes (%) in 100-yr flood discharge (Q_{100}) in the major SBC
 711 watersheds (indicated by the grey watersheds in the map) during 2081-2100 as compared to
 712 historical period (1986-2005); each bar depicts relative changes in minimum, maximum, median,
 713 1st and 3rd quartiles for the ensemble outputs; bars from left to right spatially corresponding to
 714 watersheds from west to east. For clarity, only watersheds with drainage areas larger than 7 km²,
 715 which account for roughly 83% of the study area, are shown. **(b)** Relative contributions (%) of the
 716 uncertainties in the projected changes at each of these watersheds; Hydro = Hydrologic models;
 717 Para = hydrologic model parameters; GCM = General Circulation Models; RCP = Representative
 718 concentration pathways (emission scenarios); “other” is the uncertainty from the 3rd and 4th orders
 719 of interactions between the 4 major sources (i.e., GCMs, RCPs, Hydrologic models and
 720 parameters).
 721



722 **Figure 8:** Probability of changes in Q_m , Q_p and Q_{100} at the Mission Creek watershed (No. 20 in
 723 Figure 7 map). The numbers in the plot are the probabilities of positive changes in Q_m , Q_p and Q_{100}
 724 (areas of shaded regions) under each emission scenario (blue numbers are for RCP 4.5 and red
 725 numbers are for RCP 8.5).



726 **Figure 9: (a)** Projected change (days) in the onset and duration of wet season in SBC; positive
 727 (negative) values indicate later (earlier) onset or longer (shorter) duration of the wet season; **(b)**
 728 relative contributions (%) of the uncertainties of the projected changes in seasonality. Hydro =
 729 Hydrologic models; Para = hydrologic model parameters; GCM = General Circulation Models;
 730 RCP = Representative concentration pathways (emission scenarios); “other” is the uncertainty
 731 from the 3rd and 4th orders of interactions between the 4 major sources (i.e., GCMs, RCPs,
 732 Hydrologic models and parameters).