



- 1 Technical note: Comparison between two generalized Nash models
- 2 with a non-zero initial condition
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6 Abstract Initial condition can impact the forecast precision especially in a real-time 7 forecasting stage. The discrete linear cascade model (DLCM) and the generalized Nash model (GNM), expressed in different ways, are both the generalization of the Nash 8 9 cascade model considering the initial condition. This paper investigates the relationship and difference between DLCM and GNM both mathematically and experimentally. 10 11 Mathematically, the main difference lies in the way to estimate the initial storage state. 12 In the case of n=1, it was shown theoretically that the difference between the two models is whether the current outflow is estimated (DLCM) or observed (GNM). The 13 GNM is the unique solution of the Nash cascade model with a non-zero initial condition, 14 while the DLCM is an approximate solution and it can be transformed to the GNM 15 16 when the initial storage state is calculated by the approach suggested in the GNM. At 17 last, a test example obtained by the solution of the Saint-Venant equations is used to illustrate this difference. The results show that the GNM provides a unique solution 18 while the DLCM has multiple solutions depending on the estimate accuracy of the 19 20 current state.

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- 21 **Keywords** generalized Nash model; discrete linear cascade model; initial storage state;
- 22 unique solution
- 23 1. Introduction

24 In hydrology, the concept of linear reservoir cascade suggested by Nash (1957) is 25 widely used in connection with the mathematical modeling of surface runoff. Several Nash cascade based models have been developed to model the rainfall runoff process 26 27 and river flow routing (Yan et al., 2015). In the original linear reservoir cascade model, 28 the initial storage of each reservoir is assumed to be zero, or equivalently the reservoirs 29 are empty. The initial state is usually thought to be insignificant in the forecasting as its effect will vanish after a sufficiently long simulation time. But for some short time 30 prediction situations, just like the identification of the impulse-response function and 31 32 the real-time forecasting, the initial state will produce relatively great impact. Szollosi-33 Nagy (1982) formulated a state-space description of the Nash cascade model i.e. the discrete linear cascade model (DLCM) in a matrix form whereby the initial state was 34 included that can be thought of a generalization of the Nash cascade model. The 35 36 determination of the initial state of the DLCM was then proposed by Szollosi-Nagy 37 (1987) via observability analysis. The DLCM was discretized originally in a pulse-data system framework which seems more suitable for the irregularly changing precipitation 38 but not necessarily for the gradually changing streamflow. Under a linear change 39 40 assumption of the input, the DLCM was extended by Szilagyi (2003) to a sample-data system framework. Since then, Szilagyi and his team have made great effort to develop 41 this model (Szilagyi, 2006; Szilagyi and Laurinyecz, 2014). With so many advantages 42





that have been summarized by Szilagyi (2006), the DLCM has been in operational use
for over 30 years in Hungary. However, it has not yet been applied more broadly except
in Hungary, or furthermore by Szilagyi and his team. One possible reason may be due
to the complicated mathematical expression and calculation. The development of a
simpler expression of the DLCM is necessary to make it more popular and applicable
in practice.

49 Recently, Yan et al. (2015) published a paper "The generalized Nash model for river 50 flow routing" in Journal of Hydrology. In that paper, the Laplace transform and the 51 principle of mathematical induction were used to solve the *n*th order nonhomogeneous linear ordinary differential equation (NLODE) of the Nash cascade model with a non-52 zero initial condition. The generalized Nash model (GNM), i.e. the analytical solution, 53 54 with a simpler expression of the Nash cascade model was obtained. What's more, the 55 GNM has been physically interpreted, which makes it to be a conceptual model and not only a mathematical formulation. The DLCM was also obtained from the Nash cascade 56 model with the same initial condition. But whether the expressions or the simulation 57 58 results of these two models are differently exhibited. There may be some confusions to the model users. It is necessary to distinguish these two models for the users. Hence, 59 this paper try to investigate the relationship and difference between DLCM and GNM 60 both mathematically and experimentally. 61

62 2. Relationship between the DLCM and the GNM

In the derivation of the DLCM, a state-space matrix approach was used. The stateand output equations of the Nash cascade model are formulated as follows (Szollosi-





65 Nagy, 1982; Szilagyi, 2003)

66
$$\mathbf{S}(t) = \mathbf{\Phi}(t, t_0) \mathbf{S}(t_0) + \int_{t_0}^t \mathbf{\Phi}(t, \tau) \mathbf{G} I(\tau) d\tau$$
(1)

$$O(t) = \mathbf{HS}(t) \tag{2}$$

68 where S(t) is the storage state vector and denotes the stored water volumes of the *n*

69 linear cascade reservoirs,

67

70
$$\mathbf{\Phi}(t,t_0) = \begin{bmatrix} e^{\frac{t-t_0}{K}} & 0 & \cdots & 0\\ \frac{t-t_0}{K} e^{\frac{-t-t_0}{K}} & e^{\frac{-t-t_0}{K}} & \cdots & \vdots\\ \vdots & \ddots & \ddots & 0\\ \frac{(t-t_0)^{n-1}}{K^{n-1}(n-1)!} e^{\frac{t-t_0}{K}} & \cdots & \frac{t-t_0}{K} e^{\frac{-t-t_0}{K}} \end{bmatrix}.$$
(3)

is the state transition matrix, t_0 is the initial time, K is the storage coefficient, $G=[1,0,\ldots,0]^{T}$, I(.) is the instantaneous inflow of the first reservoir, O(t) is the

73 outflow, and **H**=[0,0,....,1/*K*].

Combining Eqs. (1) and (2) and assuming $t_0=0$, one obtains (Szilagyi, 2006)

75
$$O(t) = \mathbf{H}\boldsymbol{\Phi}(t,0)\mathbf{S}(0) + \int_0^t u(t-\tau)I(\tau)d\tau$$
(4)

76 where u(.) is the instantaneous unit hydrograph.

Eq. (4) is the basic formula for DLCM. For the discrete streamflow data system, assuming that both input and output are sampled at equidistant sampling intervals Δt ,

79 the recursive form of the DLCM can be written as follows (Szilagyi, 2006)

80
$$O(t + \Delta t) = \mathbf{H} \mathbf{\Phi}(\Delta t, 0) \mathbf{S}(t) + \int_{t}^{t + \Delta t} u(t + \Delta t - \tau) I(\tau) d\tau$$
(5)

Once the initial storage state vector S(0) is obtained, the outflow can be estimated recursively by using Eqs. (1) and (5). The identification of S(0) is an inverse problem, which can be computed by inverting Eq. (4) and from the first n input-output pairs, as





84 originally proposed by Szollosi-Nagy (1987) and Szilagyi (2003), i.e.
85
$$S(0) = \Omega_n^{-1} (c_1, c_2, \dots, c_n)^T$$
 (6)
86 where
87 $\Omega_n = \left[\mathbf{H} \Phi(\Delta t, 0), \mathbf{H} \Phi^2(\Delta t, 0), \dots, \mathbf{H} \Phi^n(\Delta t, 0) \right]^T$ (7)
88 and
89 $c_i = O(i\Delta t) - \int_0^{i\Delta t} u(t-\tau) I(\tau) d\tau, \ i = 1, \dots, n.$ (8)
90 That's the complete procedure of the DLCM. It is a discrete solution of the Nash
91 cascade model. Actually, the initial storage state vector $\mathbf{S}(0)$ can be calculated by
92 another simpler approach that has been proposed by Yan et al. (2015). From the linear
93 storage-outflow relationship suggested in the Nash cascade model, we have
94 $\mathbf{S}(0) = [KO_i(0), KO_2(0), \dots, KO_n(0)]^T$ (9)
95 where $O_j(0)$ ($j = 1, \dots, n$) is the initial outflow of the *j*th reservoir and can be
96 computed by (Yan et al., 2015)
97 $O_j(0) = \sum_{i=0}^{n-1} C_{n-i}^i K^i O^{(i)}(0)$ (10)
98 where $O^{(i)}(0)$ is the *i*th derivative of $O(0)$, and
99 $C_n^r = \frac{n!}{r!(n-r)!}$ (11)
100 is the combination formula. Note that $O_n(0)$ is equal to the initial downstream outflow
101 $O(0)$. Then
102 $\mathbf{H} \Phi(t, 0) \mathbf{S}(0) = \sum_{j=1}^{n} \frac{e^{-\frac{K}{L}}}{(n-j)!} (\frac{1}{L})^{n-j} \sum_{i=0}^{n-j} C_{n-j}^i K^i O^{(i)}(0)$

103
$$= \sum_{j=0}^{n-1} \frac{e^{\frac{-t}{K}}}{j!} (\frac{t}{K})^j \sum_{i=0}^j C_j^i K^i O^{(i)}(0)$$
(12)





104 Note that $\mathbf{H}\Phi(t,0)\mathbf{S}(0)$ is just equal to $R_0(t)$ that has been defined in the GNM (Yan

105 et al., 2015). Substituting Eqs. (3) and (9) into Eq. (4) gives

106
$$O(t) = e^{-\frac{t}{K}} \sum_{j=0}^{n-1} \sum_{i=0}^{j} O^{(i)}(0) \frac{t^{j}}{i!(j-i)!K^{j-i}} + \int_{0}^{t} u(t-\tau)I(\tau)d\tau$$
(13)

107 That's just the GNM that has been proposed by Yan et al. (2015). Hence, the DLCM

108 can be transformed to the GNM when the initial storage state is calculated by the linear

109 storage-outflow relationship.

110 3. Difference between the DLCM and the GNM

111 The main difference between the two models lies in the estimation of the initial 112 storage state. In the DLCM, the initial storage state S(0) is expressed as a function of 113 the first n input-output pairs, while in the GNM, it is expressed as a function of the *i*th 114 derivative of the initial outflow.

115 To further illustrate this difference, take the special case of n=1 as an example. In

116 the DLCM, the initial storage *S*(0) can be estimated by (Szollosi-Nagy, 1987)

117
$$S(0) = Ke^{\frac{\Delta t}{K}} \left[O(\Delta t) - (1 - e^{-\frac{\Delta t}{K}})I(0) \right]$$
(14)

118 It is suggested that the initial storage is estimated by the input/output pair [I(0), 119 $O(\Delta t)$]. In fact, when n=1, the river flow routing system can be described by the 120 following NLODE (Szollosi-Nagy, 1982; Yan et al., 2015)

121
$$KO'(t) = I(t) - O(t)$$
 (15)

122 It is easy to get the solution of this NLODE with a result of

123
$$O(t) = O(0)e^{-\frac{t}{K}} + \int_0^t u(t-\tau)I(\tau)d\tau.$$
 (16)

124 Provided that I(t) is taken to be constant at the value it obtains at time t, in the [t, t+





125 Δt] interval (Szilagyi, 2003), for one step ahead, we obtain

126
$$O(\Delta t) = O(0)e^{-\frac{\Delta t}{K}} + (1 - e^{-\frac{\Delta t}{K}})I(0)$$
(17)

127 Then the initial outflow can be estimated by

128
$$O_{est}(0) = e^{\frac{\Delta t}{K}} \left[O(\Delta t) - (1 - e^{-\frac{\Delta t}{K}}) I(0) \right]$$
(18)

129 where $O_{est}(0)$ is the estimated initial outflow.

130 Combing equations (14) and (18), yields

131
$$S(0) = KO_{est}(0)$$
 (19)

132 On contrary, in the GNM, the initial state is directly obtained by equation (9) based

- 133 on the concept of linear reservoir with a result of
- 134 $S(0) = KO_{obs}(0)$ (20)
- 135 where $O_{obs}(0)$ is the observed initial outflow.

Comparison of Eqs. (19) and (20) shows that the difference between the two models 136 137 in the case of n=1 lies in the fact that whether the initial outflow is estimated or observed. 138 In the DLCM, the initial outflow O(0) is estimated by the observed input/output pair $[I(0), O(\Delta t)]$, as shown in Eq. (18). In fact, at initial time, the outflow for the next time 139 step $O(\Delta t)$ is still unknown, while the observed initial outflow O(0) is available at 140 that time and doesn't need to be estimated. Instead, this observed value is directly used 141 142 in the GNM. Theoretically, they are equivalent with the same numerical values if no predict error exists. However, the predict error is virtually inevitable. Though this error 143 may be ignored in some cases, it's at least a truth for a real-time forecasting that the 144 estimation of the current state S(t) depends on the current inflow I(t) and the outflow 145 146 for the next time step $O(t + \Delta t)$ when the recursive DLCM is employed according to





- 147 Eq. (5). It seems paradoxical because the outflow for the next time step $O(t + \Delta t)$ is
- still unknown at the current time and is to be predicted by using the current state S(t).
- 149 The approach used in the DLCM to deal with this paradox is to estimate the current
- state S(t) by applying the transition matrix to the initial state from Eq. (1). In the case
- 151 of n=1, S(t) calculated from Eq. (1) can be simplified as follows

152
$$S(t) = S(0)e^{-\frac{t}{K}} + \int_{0}^{t} e^{-\frac{t-\tau}{K}}I(\tau)d\tau$$
(21)

where S(0) is estimated by Eq. (14). Then the recursive DLCM can be written as

154
$$O(t + \Delta t) = \frac{1}{K}S(t + \Delta t)$$

155
$$= \frac{1}{K} \left[S(t) e^{-\frac{\Delta t}{K}} + \int_{t}^{t+\Delta t} e^{-\frac{t+\Delta t-\tau}{K}} I(\tau) d\tau \right]$$

156
$$= \frac{1}{K} S(t) e^{-\frac{\Delta t}{K}} + (1 - e^{-\frac{\Delta t}{K}}) I(t).$$
(22)

It is suggested from Eq. (21) that the current state S(t) depends to some extent on the initial state S(0), or equivalently, the current state is not unique since any time before current time can be taken as the initial time. As a result, the outflow for the next time step $O(t + \Delta t)$ determined by S(t) and I(t) from Eq. (22) will have multiple solutions. While in the recursive GNM, the current state is uniquely determined by the current outflow O(t) according to Eq. (9) in which the initial time is set to the current time. In this case, the recursive GNM has the following unique expression

164
$$O(t + \Delta t) = O(t)e^{-\frac{\Delta t}{K}} + (1 - e^{-\frac{\Delta t}{K}})I(t)$$
 (23)

165 Comparison of Eqs. (22) and (23) suggests that the only difference between the 166 recursive form of the two models in the case of n=1 lies in whether the current outflow 167 is estimated or observed. Similarly, for n>1, the current outflow of the last reservoir





(i.e. *n*th reservoir) in the Nash model is also estimated rather than observed in the 168 169 DLCM. Hence, the DLCM is an approximate solution but not the exact solution of the Nash cascade model. As an analytical solution, the GNM is applicable to the natural 170 continuous streamflow system. However, in practice, the streamflow data are usually 171 172 discretely measured. The derivative term in the GNM doesn't exist in the discrete streamflow data system. To make the GNM practically applicable, the numerical 173 174 calculation approach such as the finite difference method is often used. While the 175 DLCM, as a discrete solution, can be directly applied to the discrete streamflow data 176 system.

177 4. An illustrative example

A test example was used to further illustrate this difference. This example was obtained by numerically integrating the Saint-Venant equations of open channel flow over a rectangular channel of L=120 km in length, B = 20 m in width and a constant channel slope $S_0 = 0.0002$. The Manning's roughness parameter n_0 was set to 0.004 for the entire length of the channel. The upstream boundary condition was defined by the following inflow hydrograph (Camacho and Lees, 1999)

184
$$I(t) = I_b + (I_p - I_b) \left(\frac{t}{t_p}\right)^{\frac{1}{\gamma - 1}} \exp\left(\frac{1 - t/t_p}{\gamma - 1}\right)$$
(23)

where I_b is the initial steady flow (100 m³/ s) in the reach; I_p is the peak flow (300 m³/ s); t_p is the time to peak (20 h) and γ is the skewness factor (1.2). The downstream boundary condition, fixed at 120 km downstream, was defined by a looped-rating curve based on the Manning equation for normal flow.





189	The hydrograph was routed to distances of 20, 40, 60, 80, 100 and 120 km from the
190	inflow section. To minimize somewhat artificial nature of the upper and lower boundary
191	conditions (Szilagyi, 2006), the middle reach between 40 km and 80 km was selected
192	for flow routing, i.e. the flowrate values given by the Saint-Venant equations at 40 km
193	and 80 km served as the "observed" upstream and downstream flow values, respectively.
194	The SCE-UA global optimization algorithm (Duan et al., 1994) was used to optimize
195	parameters in the two models by directly minimizing the root mean squared error, with
196	same optimized values of $n = 1$ and $K = 4.6$ h. In the real-time forecasting, for example,
197	take $t=16$ h as the current time, then any time before $t=16$ h can be taken as the initial
198	time t_0 in the DLCM. If $t_0 = 1$ h, the current state can be estimated by combing Eq. (14)
199	and (21), and further the current outflow, i.e. $O(t=16 \text{ h})$ can be calculated by linear
200	storage-outflow relationship, with a result of 126.13 m ³ /s. If $t_0 = 15$ h, the current
201	outflow O (<i>t</i> =16 h) was estimated by the same procedure with a result of 118.58 m ³ /s.
202	Then this value was used to estimate the following outflow by using the Eq. (22). While
203	for the GNM, the "observed" value of O (t=16 h) =113.92 m ³ /s was directly used to
204	estimate the outflow recursively by using the Eq. (23). The hydrographs obtained by
205	the DLCM with different initial time as well as the GNM were illustrated in Fig. 1.
206	With different current outflow, the DLCM correspondingly provided different
207	forecasted discharge values, especially the first few ones. The Nash-Sutcliffe efficiency
208	coefficient (E_{NS}) values for $t_0 = 1$ h and $t_0 = 15$ h were 0.9882 and 0.9919, respectively.
209	The GNM provided the unique and also the best forecasted results, with a result of E_{NS}
210	= 0.9928. It is shown from this example that the DLCM has multiple solutions and the







211 forecast precision depends upon the estimate accuracy of the current state.

212



Figure 1. Routing results for the DLCM and the GNM

214 5. Conclusion

The DLCM formulated the continuous Nash cascade model in a matrix form based 215 on the principles of state space analysis. The identification of the initial state is required 216 217 when performing the DLCM. There is a paradox in the identification process that the outflow at the next time step used to estimate the initial storage is still unknown at initial 218 time. To deal with this paradox in the real-time forecasting stage, the current state is 219 220 estimated by applying the transition matrix to the initial state. Due to the nonuniqueness 221 of the initial time, the DLCM will have multiple solutions. So the DLCM is an approximate solution of the Nash cascade model but not the exact solution. The GNM 222 has been derived theoretically by solving the *n*th order NLODE of the Nash routing 223 224 theory. It's the unique analytical solution of the Nash cascade model. With an analytical expression, the initial state is implicitly written in a form of derivative, and it does not 225





- 226 need to be estimated separately. Besides, the DLCM can be transformed to the GNM
- 227 when the initial storage state is calculated by the approach used in the GNM.
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