Dear Dr. Riva,

Thank you very much for the opportunity to integrate the revisions proposed by the two reviewers. Furthermore, we like to thank Dr. Pianosi for her thoughtful and important comments.

Our responses below are written in italics.

Response to Dr. Pianosi

This said, I think the manuscript could really do a better job at valuing the underpinning work if it was written in a more concise and clear way. Many sentences are rather long-winded and there are several language mistakes, including some potentially very misleading confusion in technical terms (e.g. "sensitivities" for "uncertainties" or "ranges" for "values"; some specific examples are given below). Overall this makes the text quite hard to follow. I think that the entire manuscript should be reread and revised before publication.

Thank you very much for your input that helped to clarify our work. Additionally, to your suggestions below we improved the text in multiple small changes shown in the markup document.

1) P. 2 L. 39-75: I think this addition is a bit odd. The content is useful but the way it is placed here really breaks the flow of the Introduction. First, given that it is a comment on the limitations of Morris, I would place it after the use of Morris is presented in the context of this work (i.e. after lines 80-83: "...we present an application of the Morris method (...) to the Global Gradient-based Groundwater model ...") not before. Second, I would shorten it, and possibly move some of the more technical details to the methodology section (2.2.2). It is odd that 35 lines in the Introduction are dedicated to a detailed discussion of pros and contras of Morris method, while the general introduction to global groundwater models took less than 25 and the review of SA applications less than 30!

We agree that the placement of that paragraph was not optimal and moved it as you suggested.

It now can be found on P. 5 at the beginning of section 2.2.2.

2) P. 6 L. 11-16. I would at least mention here that the robustness of parameter ranking will also be assessed, and that details of how this is done are in Appendix 1. This is an important detail of the methodology, and should at least be mentioned here. Also, either here or in the Appendix, it should be clarified where the distribution of mu* values, and hence their Cls, stem from - i.e. how bootstrapping works. I find Figure A1 somehow misleading. It seems to suggest that the Cls are relative to the distribution of the Elementary Effects (EEs) for a given sample, i.e. as if each white point referred to the individual EE calculated for a certain trajectory. However, I guess the distribution should stem from the re-sampling of the 1848 available simulations, i.e. each white point in Figure A1 is a different mu* (mean EEs) calculated from a different bootstrap resamples. This is crucial but is never really clearly stated, either in the main text or in the Appendix!

We agree that the manuscript was imprecise.

The robustness is now mentioned on P. 5 L. 94 and reads:

"The robustness of the parameter ranking is assessed by calculating confidence intervals as described in detail in Appendix 1."

The bootstrapping is now explained in the Appendix and the description in Fig. A1 has been changed to further clarify.

Now reads (P. 16 L. 1): "Confidence intervals are determined based on 1000 bootstrap resamples following Archer et al. (1997) for all simulation outputs. Bootstrapping is an established statistical method that relies on random sampling with replacement using the original data. This sampling from a set of independent, identically distributed data is equivalent to sampling from the empirical distribution function of the data allowing to determine confidence intervals (Archer et al., 1997)."

Figure A1 reads: "[..] $\mu *$ is calculated based on the EEs (circles), however the CI is calculated

based on bootstrap resamples of the simulation outputs."

LANGUAGE AND TYPOS

P. 1 L. 20: remove "for a computationally expensive model"

The application of a global sensitivity study to a computationally expensive and complex model is a key contribution of the paper that we believe should be mentioned in the abstract.

P. 1 L. 40: add (I suppose): "... and CHANGES are projected to continue due to climate change"

Global groundwater dynamics have been significantly altered by human withdrawals, and are projected to be further modified under climate change (Taylor et al., 2013)

P. 2 L. 20-22: "...have led to more widespread application e.g. (...) For this reason, existing studies of global models...". Something convoluted and unclear in this sequence. Maybe better: "... have facilitated their application e.g. (...) Still, existing studies of global models..."

Revised and now reads (P. 2 L. 14): "The large number of model evaluations required can render global methods unfeasible for computationally demanding models, though increased computational resources have facilitated their application e.g. [..]"

P. 2 L. 105: "a Monte Carlo experiment to investigate sensitivities of simulated hydraulic head ..." This sentence is very confusing. It is unclear what it refers to and how this analysis is different from the subsequent Morris analysis. I think the confusion arises from the incorrect use of the term "sensitivities". If this sentence refers to Figure 4 and 5, then what is investigated here are the output "uncertainties", not "sensitivities", and the sentence should be rephrased as: "a Monte Carlo experiment to quantify uncertainty in simulated hydraulic head"

Now reads (P. 2 L. 72): "[..] eight parameters are selected for a Monte Carlo experiment to quantify uncertainty in simulated hydraulic head and groundwater-surface water interactions."

P. 3 L. 47: "calculated river discharge calculated by WaterGAP". Remove the first "calculated" *Removed.*

P. 3 L. 36: missing ")" after R

Added.

P. 3 L. 47: "h_swb" is undefined

It is defined in the previous equation, but was inconsistent with Fig. 1 which contains E_swb instead of h_swb. This was corrected. All equations and figures now read E_swb.

P. 4 L. 4: "a flow from the cell to a surface water body is negative and positive if the opposite is true." why making things so complicated!? Replace by "a flow from the cell to a surface water body is negative and viceversa."

Now reads (P. 3 L. 67): "The in- and outflows Q are described similar to MODFLOW as flows from the cell: a flow from the cell to a surface water body is negative, and the reverse flow is positive."

Figure 1: I would add "h_swb" in the Figure, given it is the most mentioned variable in the text, it would be good to have it clearly displayed in the schematic.

See previous comment. Now consistent mentioning of E_swb.

P. 5 L. 13: "the river conductance Criv in a steady-state groundwater model needs to be set in a way that the river is the sink for all the inflow to the grid cell (R and inflow from neighbouring cells) that is not transported laterally to neighbouring cells." Too long and hard to follow, please consider breaking into two sentences.

Now reads (P. 3 L. 93): "According to \citet{miguez2007incorporating}, the river conductance $C_{riv}\$ in a steady-state groundwater model needs to be set in a way that the river is the sink for all the inflow to the grid cell that is not transported laterally to neighbouring cells. This inflow consists of \$R\$ and inflow from neighbouring cells."

P. 5, titles of Sec. 2.2.1 and 2.2.2: "choice in " should be "choice of"

Changed.

P. 5 L. 66: "we apply a basic sensitivity method" Given what follows, maybe better "we calculate a basic sensitivity index"

Changed (P. 5 L. 29).

P. 6 L. 11: "To achieve that, mu* and sigma are presented in this study in ranks". Very unclear. If I was not familiar with Morris method and the parameter ranking, I would have a hard time understand what this means.

Now reads (P. 5 L. 88): "To achieve that, $\mu *$ and σ i are used to rank the most sensitive parameters. Values for all parameters are sorted from highest to lowest, and the parameter with the highest value is selected as the most influential parameter with the highest rank (hereafter called rank 1). The parameter with the second highest value (rank 2) is the second most influential parameter and so on. The robustness of the parameter ranking is assessed by calculating confidence intervals as described in detail in Appendix 1."

P. 6 L. 24: "my" should be "by"

Changed.

P. 6 L. 33: "equally" should be "equal"

Changed.

P. 6 L. 62: "we introduce the use of a Global Hydrological Response Unit (GHRU)." should be "we introduce the use of Global Hydrological Response Units (GHRU)."

Changed.

P. 6 L. 68-71: "All multipliers for a given parameter for all regions are based on the same random distribution inside a given range of uncertainty for that parameter." Again very unclear. Looking at Table 1 I would say that the same random distributions (i.e. uniform with ranges given in Table 1) are used for the parameter multipliers in all GHRUs. Is this the point? Or something else?

Now reads (P. 6 L. 51): "A uniform random distribution within the ranges given in Table 1 is used to sample the parameter multipliers for all GHRUs."

P. 6 L. 78: "to the mean in a cluster" maybe "to the mean in that cluster"?

Changed.

P. 7 L. 2-15. This paragraph is still very unclear. First, I would swap the order of presentation. In its present form, it is unclear where the number 1848 on L. 5 comes from. I would first introduce how

you determine the maximum number of model evaluations ("For 7 parameters (without ocean boundary), n GHRUs... the total number of simulation (1848)." and then explain how you select the 42 optimised trajectories ("10,000 initial trajectories were sampled in total are selected (Ruano et al., 2012)". Also, in the sentence "We assume 42 for the number of optimised trajectories ...", I would clarify that this is the number of elementary effects and is the variable "r" in the formula that gives N (it may not be obvious to the reader not familiar with Morris).

This paragraph was rewritten and now reads (P. 6 L 75 ff.):

"The total number of necessary simulations N is determined with N = r(k+1)citep{campolongo2007effective}, where r is the number of elementary effects and k is the number of parameters.

For 7 parameters (without ocean boundary) and 6 GHRUs we get a total number of parameters k=42+1 where +1 stands for the ocean boundary, which is not varied by GHRU resulting in 1848 simulations.

Elementary effects are based on an initial random sampling of 10 000 trajectories using \citet{campolongo2007effective} and then reduced by assuming 42 (number of parameters times *GHRUs without ocean boundary*) so called optimized trajectories following \citet{RUANO2012103}.

Only random sampling might result in non-optimal coverage of the input space; thus the initial random trajectories are used to select only those that maximise the dispersion in the input space.

This optimal set of trajectories is approximated with a reasonable computational demand using the methodology developed by \citet{RUANO2012103}."

P. 7 L. 21-24: "Each simulation was an OAT experiment (an extended explanation of OAT and other sensitivity experiment setups and methods can be found in Pianosi et al. (2016))." Why this comment here? It is very generic and does not seem appropriate for an "experimental configuration" section. Either make it more specific or move to the methodology section?

Removed. And citation added to methodology at place where OAT is introduced (P. 6 L. 31).

P. 7 L. 47: "(see Sect. 4)" I would remove the reference.

Removed.

P. 8 L. 1-3. Confidence intervals and bootstrapping were never mentioned before! So this sentence can only be understood if in the point was anticipated in the methodology section (see also point 2 above).

Now explained in appendix and appendix referenced in methodology (see above).

P. 8 L. 65: "to analyse the outcomes of 1848 model realisations" Vague. I'd be more specific: "to quantify the output uncertainty as given in the 1848 available model realisations"

Changed accordingly.

P. 8 L. 79: "in regions of the model where..." I suppose should be "in regions of the domain where..." (unless the sentence actually refers to regions of the model input-output response surface?)

Now reads (P. 8 L. 61): "can be observed in the model where a strong nonlinear relation may produce solutions that fit the convergence"

P. 9 L. 34: "independently of the applied parameter ...". This wording suggests we are only looking at regions where 100% of MC realisations behave the same. Otherwise, it should be rephrased as "for most applied parameter ...". Also, I suppose "parameter ranges" should be replaced by "parameter values" (the ranges of variability stay the same, it's the sampled values that are changing, I guess?).

Now reads (P. 9 L. 12): "Regions with a higher percentage are in losing conditions for most of the applied parameter values."

Caption of Table 3: "Percentage fractions of simulated cells with parameter sensitivity mu^{*} and parameter interaction sigma per model output h and Qswb, where the respective output is most sensitive to the listed parameter." Very convoluted, please rephrase.

Now reads: "Percentage of cells for which parameters are ranked 1 to 3 based on $\mu *$ and σ . Percentages are shown for each model output, h and Q swb. For example, h is the most sensitive to parameter E swb (Rank 1) in 57.2% of all grid cells, while R is the most important parameter for Q swb in 59.8% of those cells."

P. 11 L. 41-44: "The values shown in Fig. 10 (a) should be judged with caution as they also include the regions Fig. A2 shown to be unreliable. Reliability means that due to overlapping CIs (any overlapping) the ranking of the parameters can't be clearly determined". Unclear. Maybe "Fig. A2" should be in parenthesis? What does the side note "(any overlapping)" is expected to point at?

The note refers to that we are not considering a certain percentage of overlapping CIs, as one might assume, but rather any overlapping of Cis.

Now reads (P. 11 L. 18): "The values shown in Fig. 10 (a) should be judged with caution as they also include regions with possibly unreliable results, i.e., those where any overlap in CIs indicates that the ranking of the parameters cannot be clearly determined (see additional explanation Fig. A1)."

Caption of Figure 9: "ranked by Sigma value" - maybe the capital sigma should be a small sigma? *Yes! Changed.*

P. 13 L. 24-25: "statistically zero sensitivity values (overlapping CI with zero)". Unclear what the problem is. If the sensitivity index has small CI centred around zero, I would conclude that that input factor is probably uninfluential. Why this result should be regarded as problematic? If instead the CI is very large, then the estimated sensitivity index could be statistically not very reliable, and that would be problematic - regardless of the fact that the CI is centred around zero or above. Pls clarify.

Now reads (P. 13 L. 55): "However, the large number of grid cells with either statistically zero sensitivity values (overlapping CI with zero) or unreliable results limit the relevance and applicability of the study results. For most of the statistically zero sensitivity values the CI is very large, and it is therefore very unlikely that the parameter is not influential."

P. 15: L. 76: "a feasible the number". Remove "the"

Removed.

P. 16 L. 20-22: "Results of the method of Morris need to be contemplated in a ranking based scheme that relies on metrics that summarize the calculated EEs." Vague and unclear, please clarify what a "ranking based scheme" is and which "metrics" are used, or rephrase the entire sentence.

Now reads (P. 16 L. 14): "The derived metrics \$\mu *\$ and \$\sigma_i\$ both are measures of intensity (higher values are more sensitive/interactive) and do not represent absolute values of sensitivity.

Both can only be interpreted meaningfully in comparison with values derived for other parameters.

To achieve that, \$\mu *\$ and \$\sigma_i\$ should be presented in so called \emph{ranks}.

Values for all parameters are sorted from highest to lowest, and the parameter with the highest value is selected as the most influential parameter with the highest rank.

The parameter with the second highest value is the second most influential parameter and so on."

Response to Referee #2

Page 4 Line 2 "exp(-50mf-1)-1": What is m?

The SI unit meter. Now reads (P. 3 L. 38): $exp(af^{-1})^{-1}$ where a = -50 (m)

Spatially distributed sensitivity of simulated global groundwater heads and flows to hydraulic conductivity, groundwater recharge and surface water body parameterization

Robert Reinecke¹, Laura Foglia³, Steffen Mehl⁵, Jonathan D. Herman⁴, Alexander Wachholz¹, Tim Trautmann¹, and Petra Döll^{1,2}

¹Institute of Physical Geography, Goethe University Frankfurt, Frankfurt am Main, Germany

²Senckenberg Leibniz Biodiversity and Climate Research Centre Frankfurt (SBiK-F), Frankfurt am Main, Germany

³Department of Land, Air and Water Resources, University of California, Davis, USA

⁴Department of Civil & Environmental Engineering, University of California, Davis, USA

⁵Department of Civil Engineering, California State University, Chico, USA

Correspondence: Robert Reinecke (reinecke@em.uni-frankfurt.de)

Abstract. In global hydrological models, groundwater storages and flows are generally simulated by linear reservoir models. Recently, the first global gradient-based groundwater models were developed in order to improve the repre-5 sentation of groundwater-surface water interactions, capil-

- lary rise, lateral flows and human water use impacts. However, the reliability of model outputs is limited by a lack of data and by uncertain model assumptions that are necessary due to the coarse spatial resolution. The impact of data qual-
- ¹⁰ ity is presented in this study by showing the sensitivity of a groundwater model to changes in the only available global hydraulic conductivity data-set. To better understand the sensitivity of model output to uncertain spatially distributed parameters, we present the first application of a global sen-
- ¹⁵ sitivity method for a global-scale groundwater model using nearly 2000 steady-state model runs of the global gradientbased groundwater model G³M. By applying the Morris method in a novel domain decomposition approach that identifies global hydrological response units, spatially distributed
- ²⁰ parameter sensitivities are determined for a computationally expensive model. Results indicate that globally simulated hydraulic heads are equally sensitive to hydraulic conductivity, groundwater recharge and surface water body elevation, though parameter sensitivities vary regionally. For large ar-
- ²⁵ eas of the globe, rivers are simulated to be either losing or gaining, depending on the parameter combination, indicating a high uncertainty of simulating the direction of flow between the two compartments. Mountainous and dry regions show a high variance in simulated head due to numerical instabilities

of the model, limiting the reliability of computed sensitivities ³⁰ in these regions. This is likely caused by the uncertainty in surface water body elevation. We conclude that maps of spatially distributed sensitivities can help to understand complex behaviour of models that incorporate data with varying spatial uncertainties. The findings support the selection of possible calibration parameters and help to anticipate challenges for a transient coupling of the model.

1 Introduction

Global groundwater dynamics have significantly changed due to been significantly altered by human withdrawals, and are 40 projected to continue due to be further modified under climate change (Taylor et al., 2013). Groundwater withdrawals have led to lowered water tables, decreased base flows, and groundwater depletion around the globe (Konikow, 2011; Scanlon et al., 2012; Wada et al., 2012; Döll et al., 2014; 45 Wada, 2016). To represent groundwater-surface water body interactions, lateral and vertical flows, and human water use impacts on head dynamics, it is necessary to simulate the depth and temporal variation of the groundwater table. Global-scale hydrological models have recently moved to 50 include these processes by implementing a gradient-based groundwater model approach (de Graaf et al., 2015; Reinecke et al., 2019). This study is based on G³M (Reinecke et al., 2019) one of the two global groundwater models ca-

Robert Reinecke: Sensitivity of simulated global groundwater

pable of calculating hydraulic head and surface water body interaction on a global scale. However, the lack of available input data and the necessary conceptual assumptions due to the coarse spatial resolution limit the reliability of model out-

5 put. These substantial uncertainties suggest an opportunity for diagnostic methods to prioritize efforts in data collection and parameter estimation.

Sensitivity analysis is a powerful tool to assess how uncertainty in model parameters affects model outcome, and can 10 provide insights about how the interactions between parameters influence the model results (Saltelli et al., 2008). Sensitivity methods can be separated into two classes: local and global methods. Local methods compute partial derivatives of the output with respect to an input factor at a fixed point

- 15 in the input space. By contrast, global methods explore the full input space, though at higher computational costs (Pianosi et al., 2016). The large number of model evaluations required can render global methods unfeasible for computationally demanding models, though increased computational
- 20 resources have led to more widespread facilitated their application e.g. (Herman et al., 2013a, b; Ghasemizade et al., 2017). For this reasonStill, existing studies of global models either focus on exploring uncertainties by running their model with a limited set of different inputs for a quasi local sensitivity
- 25 analysis (Wada et al., 2014; Müller Schmied et al., 2014, 2016; Koirala et al., 2018) or applying computationally inexpensive methods based on a limited set of model evaluations (Schumacher et al., 2015). For example, de Graaf et al. (2015, 2017) determined the coefficient of variation for head
- 30 results in a global groundwater model with 1000 model runs evaluating the impact of varying aquifer thickness, saturated conductivity and groundwater recharge. To the knowledge of the authors, the only other study that applied a global sensitivity analysis to a comparably complex global model is
- 35 Chaney et al. (2015). An overview of the application of different sensitivity analysis methods for hydrological models can be found in Song et al. (2015); Pianosi et al. (2016).

This study relies on the G³M uses input from, and it is intended to be coupled and integrated into, the global hydrologi-

- 40 cal model WaterGAP Global Hydrology Model (WGHM) (Döll et al., 2014). This study investigates the sensitivity of steady-state hydraulic heads and exchange flows between groundwater and surface water to variations in main model parameters (e.g. groundwater recharge, hydraulic conduc-
- ⁴⁵ tivity, and riverbed conductance). To this end the method of Morris (Morris, 1991) in the context of global sensitivity methods. Morris (Morris, 1991) is applied.

Morris is a global sensitivity method as it provides an aggregated measure of local sensitivity coefficients for each pa-

⁵⁰ rameter at multiple points across the input space and analyses the distribution properties (Razavi and Gupta, 2015). Compared to other global methods, like the more robust variance based methods e.g. Sobol (1993), Morris has drawbacks as it may provide false conclusions (Razavi and Gupta, 2015). The attribution of what is a direct effect (model response only due to one parameter

55 change) and what an effect of interaction (response to non-linear interaction of pa-

rameters on model output) is not trivial. Morris is prone to scale issues, that is that the step size of the analysis can have significant impact on the conclusions drawn especially for significantly nonlinear responses (Razavi and Gupta, 2015). In this study we address this by limiting the parameter ranges of the multipliers where we suspect non-linearity in the model response. In general the choice of the chosen global sensi- 60 tivity method may yield different results (Dell'Oca et al., 2017). On the other hand, Janetti et al. (2019) showed for a regional scale groundwater study that different global methods showed similar results for hydraulic conductivity parameterization. Nevertheless, Morris is a well established and recognized method (Razavi and Gupta, 2015) that has the advantage of computational efficiency compared to variance-based methods to 65 screen the most sensitive parameters (Herman et al., 2013a). It requires significantly fewer model runs, compared to other global methods, to provide a meaningful ranking of sensitive parameters enabling the exploration of computationally demanding models (Herman et al., 2013a). The application of a global sensitiv- 70 ity method for a complex world-wide model of groundwater flows is unique, and Morris is currently the best available method to handle the computational constraints.

To reduce the number of necessary model runs when conducting global sensitivity analysis for computationally de-75 manding models we introduce the concept of Global Hydrological Response Units (GHRUs) (Sect. 2.2.3) (similar to e.g. Hartmann et al. (2015)). Using the GHRUs we present an application of the Morris method (Morris, 1991) to the Global Gradient-based Groundwater Model G³M (Reinecke et al., 80 2019).

G³M uses input from, and it is intended to be coupled and integrated into, the global hydrological model WaterGAP Global Hydrology Model (WGHM) (Döll et al., 2014). This study investigates the sensitivity of steady-state hydraulic heads and exchange flows between groundwater and surface water to variations in main model parameters 85 (e.g. groundwater recharge and other model parameters like the riverbed conductance).

Sensitivities of the model are explored in three steps: (1) To understand the impact of improved input data, in particular hydraulic conductivity, we investigate the changes in 90 simulated hydraulic head that result from changing the hydraulic conductivity data from the GLHYMPS 1.0 dataset (Gleeson et al., 2014) to 2.0 (Huscroft et al., 2018). (2) Based on prior experiments (de Graaf et al., 2015; Reinecke et al., 2019) eight parameters are selected for a Monte Carlo exper- 95 iment to investigate sensitivities of quantify uncertainty in simulated hydraulic head and groundwater-surface water interactions. The parameters are sampled with a newly developed global region-based sampling strategy and build the framework for the (3) Morris analysis. Elementary Effects (EE), a metric 100 of sensitivity, are calculated and their means and variances ranked to determine global spatial distributions of parameter sensitivities and interactions. The derived global maps show, for the first time, the sensitivity and parameter interactions of simulated hydraulic head and groundwater-surface 105 water flows in the simulated steady-state global groundwater system to variations in uncertain parameters. Foremost, these maps help future calibration efforts by identifying the most influential parameters and answer the question if the calibration should focus on different parameters for differ- 110

ent regions helping to understand regional deviations from observations. Additionally, they guide the further development of the model especially in respect to the coupling efforts highlighting which parameters will influence the cou-

⁵ pled processes the most. Lastly, they show in which regions global groundwater models might benefit the most from efforts in improving global datasets like global hydraulic conductivity maps.

2 Methodology and Data

10 2.1 The model G³M

 $G^{3}M$ (Reinecke et al., 2019) is a global groundwater model intended to be coupled with WaterGAP (Döll et al., 2003, 2012, 2014; Müller Schmied et al., 2014) and is based on the Open Source groundwater modelling framework $G^{3}M$ -

¹⁵ f¹(Reinecke, 2018). It computes lateral and vertical ground-water flows as well as surface water exchanges for all land areas of the globe except Antarctica and Greenland on a resolution of 5' with two vertical layers with a thickness of each 100 m representing the aquifer. The groundwater flow be-²⁰ tween cells is computed as

$$\frac{\partial}{\partial x} \left(K_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left(K_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left(K_z \frac{\partial h}{\partial z} \right) \tag{1}$$

$$+\frac{Q}{\Delta x \Delta y \Delta z} = S_s \frac{\partial h}{\partial t} \tag{2}$$

where $K_{x,y,z}$ [LT⁻¹] is the hydraulic conductivity along the x,y, and z axis between the cells with size $\Delta x \Delta y \Delta z$, $25 S_s$ [L⁻¹] the specific storage, h the hydraulic head [L] the hydraulic head, and Q [L³T⁻¹] the in- and outflows of the cells to or from external sources e.g. groundwater recharge groundwater recharge from soil (R) and surface water body flows (Q_{swb}) (see also Reinecke et al. (2019)[Eq.(1,2)]). The evaluation

- ³⁰ presented in this study is based on a steady-state variant of the model representing a quasi-natural equilibrium state, not taking into account human interference (a full description of the steady-state model and indented coupling can be found in Reinecke et al. (2019)). The stand-alone steady-state sim-
- ³⁵ ulations were performed as initial step to identify the dominant parameters that are also likely important for controlling transient groundwater flow. In the fully coupled transient model h_{swb} will be changed according to calculated river discharge calculated by WaterGAP (Fig. 1). Q_{swb} will be used to replace the current calculated flows in WaterGAP between
 ⁴⁰ groundwater and surface water bodies.

2.1.1 Groundwater recharge

Groundwater recharge (R) is based on mean annual R computed by WaterGAP 2.2c for the period 1901-2013. Human groundwater abstraction was not taken into account; not be-⁴⁵ cause it is not computed by WaterGAP but rather because there is no meaningful way to include it into a steady-state model which represents an equilibrium (abstractions do not equilibrize).

2.1.2 Hydraulic conductivity

Hydraulic conductivity (*K*) is derived from GLHYMPS 2.0 ⁵⁰ (Huscroft et al., 2018) (shown in Fig. 2 (a)). The original data was gridded to 5' by using an area-weighted average and used as *K* of the upper model layer. For the second layer, *K* of the first layer is reduced by an e-folding factor *f* used by Fan et al. (2013) (a calibrated parameter based on terrain slope) assuming that hydraulic conductivity decreases exponentially with depth. Conductivity Hydraulic conductivity of the lower layer is calculated by multiplying the upper layer value by $exp(-50mf^{-1})^{-1} exp(af^{-1})^{-1}$ where a = -50 (m) (Fan et al., 2013, Eq. 7).

Currently only two datasets, GLHMYPS 1.0 and 2.0 (Gleeson et al., 2014; Huscroft et al., 2018), are available and are used by a number of continental and global models (de Graaf et al., 2015; Maxwell et al., 2015; Keune et al., 2016; Reinecke et al., 2019). GLHMYPS 1.0 (Gleeson et al., 65 2014) is compiled based on the global lithology map GLiM (Hartmann and Moosdorf, 2012) and data from 92 regional groundwater models and derives permeabilities (for the first 100 m vertically) based on Gleeson et al. (2011), differentiating the sediments into the categories fine-, coarse-grained, 70 mixed, consolidated, and unconsolidated. Permafrost regions are assigned a K value of 10^{-13} ms⁻¹ based on Gruber (2012). Areas of deeply weathered laterite soil (mainly in tropical regions) are mapped as unconsolidated sediments as they dominate K (Gleeson et al., 2014). 75

The global permeability map was further improved with the development of GLHYMPS 2.0 by Huscroft et al. (2018). A two-layer set up was established in GLHYMPS 2.0 with the lower layer matching the original GLHYMPS 1.0. For the upper layer in GLHYMPS 2.0, a global database of unconsolidated sediments (Börker et al., 2018) was integrated into GLHYMPS 2.0 resulting in overall slightly increased *K* (Fig. 2 (a)). The thickness of the upper layer was deduced from the *depth-to-bedrock* information available from Soil-Grid (Hengl et al., 2017). No thickness was assigned to the blower layer.

2.1.3 Surface water body conductance

The in- and outflows Q are described similar to MODFLOW as flows from the cell: a flow from the cell to a surface water body is negative and positive if the opposite is true, and the reverse flow is positive. Thus gains and losses from surface water bodies (lakes, wetlands and rivers) are described as

$$Q_{swb} = \begin{cases} C_{swb}(E_{swb} - h) & h > B_{swb} \\ C_{swb}(E_{swb} - B_{swb}) & h \le B_{swb} \end{cases}$$
(3)

¹Available on globalgroundwatermodel.org



Figure 1. Parameterization and outputs of the G^3M model. Where Q_{swb} is the flow between the aquifer and surface water bodies, h is the simulated hydraulic head, K the hydraulic conductivity, K_{e-fold} is K scaled by an e-folding factor (see Sect. 2.1.2), E_{swb} the surface water body elevation head, B_{swb} the bottom elevation of the surface water body, C_{swb} the conductance of the surface water bodies, and R the groundwater recharge. In red the outputs and parameters that are foremost important for coupling.



Figure 2. Impact of hydraulic conductivity datasets GLHYMPS 1.0 and GLHYMPS 2.0. (a) GLHYMPS 2.0 $[ms^{-1}]$, (b) *K* differences, expressed as *K*(GLHYMPS 2.0)/*K*(GLHYMPS 1.0). Blue indicates higher values in GLHYMPS 2.0. (c) *h*(GLHYMPS 2.0) minus *h*(GLHYMPS 1.0) [m], (d) the sensitivity of *h* to change in the GLHYMPS dataset based on Eq. (7) (white indicates that no index could be calculated).

where h is the simulated hydraulic head, $h_{swb} E_{swb}$ is the head of the surface water body, and B_{swb} the bottom elevation. The conductance C_{swb} of the surface water body bed is calculated as

$$SC_{swb} = \frac{KLW}{h_{swb} - B_{swb}} \frac{KLW}{\mathsf{E}_{swb} - \mathsf{B}_{swb}}$$
(4)

where K is the hydraulic conductivity, L the length and W the width of the surface water body. For lakes (including reservoirs) and wetlands, the conductances C_{lak} and C_{wet} are estimated based on K of the aquifer and surface water

body area divided by a static thickness of 5 m ($h_{swb} - B_{swb} = 10$ $5mE_{swb} - B_{swb} = 5m$). For a steady-state simulation the surface water body data shows the maximum spatial extent of wetlands, an extent that is seldom reached in particular in case of wetlands in dry areas. To account for that we assume for global wetlands ($C_{gl.wet}$) that only eighty percent 80% of their maximum extent is reached in the steady-state. Global wetlands are defined as wetlands that are recharged by streamflow coming from an upstream 5' grid cell in WaterGAP (Reinecke et al., 2019). For gaining rivers, the conductance is quantified individually for each grid cell follow-20

Robert Reinecke: Sensitivity of simulated global groundwater

ing an approach proposed by Miguez-Macho et al. (2007). According to Miguez-Macho et al. (2007), the river conductance C_{riv} in a steady-state groundwater model needs to be set in a way that the river is the sink for all the inflow to the

 $_5$ grid cell (*R* and inflow from neighbouring cells) that is not transported laterally to neighbouring cells. This inflow consists of *R* and inflow from neighbouring cells.

$$C_{riv} = \frac{R + Q_{eq_{lateral}}}{h_{eq} - h_{riv}} \frac{R + Q_{eq_{lateral}}}{h_{eq} - \mathsf{E}_{riv}} \quad h > h\mathsf{E}_{riv} \tag{5}$$

- where $Q_{eq_{lateral}}$ is the lateral flow based on the equilibrium ¹⁰ head h_{eq} of Fan et al. (2013) and $h_{riv} E_{riv}$ the head of the river ($E_{swb} = h_{swb,riv} E_{swb,riv}$ in Table 1). These conductance equations are inherently empirical as they use a onedimensional flow equation to represent the three-dimensional flow process that occurs between groundwater and surface ¹⁵ water. Future efforts will investigate using approaches ap-
- propriate for large scale models, such as described by Morel-Seytoux et al. (2017). An extensive description on the chosen equations and implications can be found in Reinecke et al. (2019).

20 2.1.4 Surface water body elevation

The vertical location of surface water bodies has a great impact on model outcome (Reinecke et al., 2019). Their vertical location $h_{swb} E_{swb}$ is set to the 30th percentile of the 30" land surface elevation values of Fan et al. (2013) per 5' cell, e.g.

²⁵ the elevation that is exceeded by 70 % of the hundred 30" elevation values within one 5' cell. B_{swb} is calculated based on that head elevation with different values for wetlands and lakes (Reinecke et al., 2019, Table 1). For rivers, B_{swb} is equal to h_{riv} - 0.349 × Q_{bankfull}^{0.341} (Allen et al., 1994),
³⁰ where Q_{bankfull} is the bankfull river discharge in the 5' grid cell (Verzano et al., 2012).

2.1.5 Ocean boundary

The outer boundary condition in the model is described by the ocean and uses an equation similar to MODFLOW's gen-³⁵ eral head boundary condition as flow

$$Q_{ocean} = C_{oc}(h_{ocean} - h) \tag{6}$$

where h_{ocean} is the elevation of the ocean water table set 0 m worldwide and C_{oc} the conductance of the boundary condition set to $10^{-6}m^2s^{-1}$ 10 m^2d^{-1} based on average K and 40 aquifer thickness.

2.2 Sensitivity Analysis

2.2.1 Sensitivity of simulated head to choice in of hydraulic conductivity dataset

Parameterization of aquifer properties based on hydrogeo-45 logical data is an important decision in groundwater modeling. We first investigate the effect of switching to a newly available global permeability dataset to explore the sensitivity of h to the variability in geologic data. The results are then compared to the effects of parameter variability, as quantified by the Monte Carlo experiments.

GLHYMPS 2.0 (Huscroft et al., 2018) provides an update of the only available global permeability map (Gleeson et al., 2014). To quantify how the new hydraulic conductivity estimates change the simulation outcome of the groundwater model we apply Calculate a basic sensitivity method. index

$$S = \frac{\frac{h_2 - h_1}{h_1}}{\frac{K_2 - K_1}{K_1}} \tag{7}$$

where the sensitivity S of h to a change in K is calculated based on the change in h (h_1 is the hydraulic head calculated with GLHYMPS 1.0 and h_2 with GLHYMPS 2.0) and change in K_1 and K_2 the hydraulic conductivity based on ⁶⁰ GLHYMPS 1.0 and 2.0, respectively.

2.2.2 Sensitivity of head and surface water body flow to choice in parameters

Along with K, additional parameters influence the model outcome. In this study we apply the method of Morris (Mor-65 ris, 1991) as a screening method to identify which parameters are most important for the two main model outcomes, namely h and groundwater-surface water interactions (Q_{swb}) . The Morris method provides a compromise between accuracy and computational cost in comparison to other Monte Carlo 70 like methods (Campolongo et al., 2007). Compared to other global methods, like the more robust variance based methods e.g. Sobol (1993), Morris has drawbacks as it may provide false conclusions (Razavi and Gupta, 2015). The attribution of what is a direct effect (model response only due 75 to one parameter change) and what an effect of interaction (response to non-linear interaction of parameters on model output) is not trivial. Morris is prone to scale issues, that is that the step size of the analysis can have significant impact on the conclusions especially for significantly non-80 linear responses (Razavi and Gupta, 2015). In this study we address this by limiting the parameter ranges of the multipliers where we suspect non-linearity in the model response. In general the choice of the chosen global sensitivity method may yield different results (Dell'Oca et al., 15 2017). On the other hand, Janetti et al. (2019) showed for a regional scale groundwater study that different global methods showed similar results for hydraulic conductivity parameterization. Nevertheless, Morris is a well established and recognized method (Razavi and Gupta, 2015) 30 that has the advantage of computational efficiency compared to variance-based methods to screen the most sensitive parameters (Herman et al., 2013a).

Each model execution represents an individually randomized One Factor At a Time (OAT) experiment (Pianosi 95 et al., 2016), where one parameter is changed per simulation. Based on these model executions, the Morris method

50

55

calculates an Elementary Effect (EE) d for every trajectory of a *i*-th parameter (in this study parameter multipliers).

$$d_i(\mathbf{X}) = \left(\frac{y(X_1, \dots, X_{i-1}, X_i + \Delta, X_{i+1}, \dots, X_k) - y(\mathbf{X})}{\Delta}\right)$$
(8)

where Δ is the trajectory step size for the parameter multi-⁵ plier X_i , **X** is the vector of model parameters multipliers of size k and $y(\mathbf{X})$ the model output e.g. in the presented model h or Q_{swb} . The total effect of the *i*th parameter is computed as the absolute mean of the EEs for all trajectories and is denoted as μ * (Campolongo et al., 2007). The standard de-

- ¹⁰ viation of EEs (σ_i) is an aggregated measure of the intensity of the interactions of the *i*th parameter with the other parameters, representing the degree of non-linearity in model response to changes in the *i*th parameter (Morris, 1991). The derived metrics μ * and σ_i both are measures of intensity
- ¹⁵ (higher values are more sensitive/interactive) and do not represent absolute values of sensitivity. Both can only be interpreted meaningfully in comparison with values derived for other parameters.

To achieve that, μ * and σ_i are presented in this study in *ranks*. Thus, ²⁰ values used to rank the most sensitive parameters. Values for all parameters are ranked sorted from highest to lowest, and the parameter with the highest value is selected as the most influential parameter with the highest rank (hereafter

called rank 1). The parameter with the second highest value ²⁵ (*rank* 2) is the second most influential parameter and so on. The robustness of the parameter ranking is assessed by calculating confidence intervals as described in detail in Appendix 1.

Previous experiments (de Graaf et al., 2015; Reinecke ³⁰⁰ et al., 2019) showed the importance of hydraulic conductivity, groundwater recharge, and surface water body elevation to the simulated hydraulic head. Together with the highly uncertain surface water body and ocean conductance we thus selected eight model parameters for the sensitivity analysis.

³⁵ The analysis was conducted my by using randomly sampled multipliers in the ranges presented in Table 1.

Throughout the analysis the following parameters including the convergence criterion and spatial resolution stay fixed: global mean sea-level, bottom elevation of surface 40 water bodies and their width, length. The baseline parameters are assumed equally equal to Reinecke et al. (2019). Hydraulic conductivity is based on a global data set (2.1.2), the conductance is calculated as previously shown (2.1.3), and the groundwater recharge baseline is equally equal to the

- ⁴⁵ mean annual values calculated by WaterGAP (2.1.1). Parameter ranges were chosen to ensure that a high percentage of model realizations converge numerically. For example, the uncertainty of E_{swb} in the model is higher than the ranged ranges used in this study, but the sampling range was re-
- ⁵⁰ stricted because the parameter is especially important for model convergenceal larger range led to non-convergence. Furthermore, the cho-

sen river conductance approach uses R as parameter and includes a nonlinear threshold between losing and gaining surface water bodies, which strongly affects numeric stability. As in any sensitivity analysis, the choice of parameter ranges involves some subjectivity that may influence the ranking of sensitive parameters in the results.

2.2.3 Global hydrological response units

Even though the number of model evaluations are comparably less for OAT-based less for OAT experiments than for All-At-a-Time experiments (Pianosi et al., 2016), varying every parameter independently in every spatial grid cell leads to an unfeasible amount of model runs. On the other hand, the use of global multipliers that vary a parameter uniformly for all computational cells may lead to inconclusive results, as the sensitivity for every cell to this change is spread to the whole computational domain. A possible solution would be to separate the globe into zones with similar geological characteristics based on the GLHYMPS dataset, but this may still result in an infeasible number of required simulations. Each simulation takes about 30 min to 1 h on a commodity computer (more if the parameters hinder a fast convergence).

To overcome these limitations, we introduce the use of a Global Hydrological Response Unit Units (GHRU). Every GHRU represents a region of similar characteristics regard-75 ing three characteristics: E_{swb} (Sect. 2.1.3,2.1.4), K (Sect. 2.1.2), and R (Sect. 2.1.1). This does not constitute a zoning approach often used for calibration in traditional regional groundwater modelling, only a separation into parameter multipliers. All multipliers for a given parameter for all regions are based 80 on the same random distribution inside a given range of uncertainty for that parameter A uniform random distribution within the ranges given in Table 1 is used to sample the parameter multipliers for all GHRUs. Characteristics for each model cell are normalized to [0,1] and used to create a 3d point space (based on 85the three characteristics for each model cell). We apply a kmeans (Lloyd, 1982) clustering algorithm to identify these regions.

K-means clustering partitions n points into k clusters where each point belongs to the cluster with a minimized ⁹⁰ pairwise squared distance to the mean in a that cluster. Figure 3 (a) shows a map of k-means clustering (6 clusters) categories based on normalized three-dimensional space of E_{swb} , K, and R per grid cell.

The number of clusters was determined based on the feasible number of model evaluations. *k-means* constitutes an unsupervised machine learning approach that builds the required number of clusters automatically, thus it is necessary afterwards to examine what main characteristics these clusters represent (shown in Table 2). Characteristics are encoded as relative values (high (\uparrow), medium (\sim), low (\downarrow)) of the three parameter values based on their mean value per cluster. These characteristics are used to connect calculated parameter sen-

Robert Reinecke: Sensitivity of simulated global groundwater

Parameter	P. Unit	Multiplier Range	Description
K	LT^{-1}	0.1 - 100	Saturated hydraulic conductivity
E_{swb}	\mathbf{L}	$10^{-0.001}$ 0.9977 - $10^{0.001}$ 1.0023	SWB elevation
C_{lak}	$L^2 T^{-1}$	0.5 - 2	Conductance of lakebed
C_{wet}	$L^2 T^{-1}$	0.5 - 2	Conductance of wetland bed
$C_{gl.wet}$	$L^2 T^{-1}$	0.5 - 2	Conductance of global wetland bed
C_{riv}	$L^2 T^{-1}$	0.5 - 2	Conductance of riverbed
R	LT^{-1}	0.5 - 2	Groundwater recharge
C_{oc}	$L^2 T^{-1}$	0.1 - 10	Conductance of the ocean boundary

Table 1. Range of parameter multipliers used in the Morris experiments. Each parameter multiplier is sampled in log space $(\log_{10}(Multiplier))$ with sampling based on Campolongo et al. (2007) and optimized with Ruano et al. (2012).

 C_{oc} is equal for all ocean cells



Figure 3. Map of k-means clustering categories each representing a GHRU (a). Each color identifies a region where the combination of all three parameters is similar.

sitivities to GHRUs when analyzing the results of the experiment.

2.2.4 Experiment Configuration

- With seven parameters per GHRU plus the ocean boundary, 10 000 initial trajectories 5 were sampled in total (Campolongo et al., 2007) and optimized using Ruano et al. (2012) resulting in 1848 optimized trajectories for each parameter. Random sampling might result in non-optimal coverage of the input space; thus a high number of trajectories is sampled first and only trajectories with a maximized spread are selected (Ruano et al., 2012)The total number of necessary simulations
- ¹⁰ N is determined with N = r(k+1) (Campolongo et al., 2007), where r is the number of elementary effects and k is the number of parameters. For 7 parameters (without the ocean boundary), n GHRUs (and 6 in this paper) GHRUs we get a total number of parameters k = 42+1 where +1 stands
- ¹⁵ for the ocean boundary, which is not varied by GHRU . We assume 42 for the number of optimized trajectories (Ruano et al., 2012) resulting in N = r(k+1) (Campolongo et al., 2007), where N is the total number of simulation (resulting in 1848) simulations. Elementary effects are based on an initial random sampling of 10 000 trajectories ²⁰ using Campolongo et al. (2007) and then reduced by assuming 42 (number of parameters times GHRUs without ocean boundary) so called optimized trajectories following

Ruano et al. (2012). Only random sampling might result in non-optimal coverage of the input space; thus the initial random trajectories are used to select only those that ²⁵ maximise the dispersion in the input space. This optimal set of trajectories is approximated with a reasonable computational demand using the methodology developed by Ruano et al. (2012).

The experiment resulted in 1848 simulations with an over- 30 all runtime of two months on a machine with 20 computational cores (enabled hyper-threading) and 188 GB RAM. Each simulation required about 8 GB of RAM and was assigned four computational threads while running the simulations in cohorts of 10 simulations at once. Each simulation was 35 an OAT experiment (an extended explanation of OAT and other sensitivity experiment setups and methods can be found in Pianosi et al. (2016)). Changes in parameters were stacked over all experiments. Thus, an experiment may have changed R (also affecting C_{riv} for gaining conditions) while containing a C_{riv} multiplier from a previous ex- 40 periment. Sampling and analysis was implemented with the Python library SALib (Herman and Usher, 2017). For each experiment, the model was run until it reached an equilibrium state (steady-state model). All other parameters and convergence criteria can be found in Reinecke et al. (2019). If a 45 simulation failed (6 of 1848 did not converge) the missing results were substituted randomly from another simulation within the cohort to preserve the required ordering of parameter samples for the used Python implementation of Morris. This number is low enough that it does not bias the results in 50 any significant way (Branger et al., 2015).

A converged simulation does not necessarily constitute a valid result for all computed cells. Numeric difficulties based on the model configuration (due to the selected parameter multipliers) may lead to cells with calculated h that are unreasonable. More specifically, a hydraulic head that is far above or below the land surface and/or leads to a large mass budget error. In the presented study these simulations are retained as a removal would require to either rerun simulations with a different convergence criterion (see Sect. 4) and include 60

Table 2. Mean values of GHRU characteristics and their summarized description, where \uparrow is read as a relatively high value, \sim as medium, and \downarrow as low; e.g. $\uparrow\uparrow$ E indicates a cluster with very high and relatively high (\uparrow) average E_{swb} . Additionally, the last two columns show the percentage of cells per GHRU where μ * of h and Q_{swb} could be reliably determined (described in Sect. 3.2.6).

					% of reliable $\mu *$	
GHRU	$\mu(E_{swb})$ [m]	$\mu(K) [{\rm m~s^{-1}}]$	$\mu(R)$ [mm day ⁻¹]	GHRU description	h	Q_{swb}
1	454	10^{-4}	0.15	\sim E, \uparrow K, \sim R	9.54 %	6.58 %
2	286	10^{-6}	0.15	\downarrow E, ~ K, ~ R	12.07 %	14.41 %
3	4107	10^{-6}	0.13	$\uparrow\uparrow \mathrm{E},\sim\mathrm{K},\downarrow\mathrm{R}$	0.08~%	4.09 %
4	1355	10^{-6}	0.11	\uparrow E, \sim K, \downarrow R	3.17 %	17.19 %
5	303	10^{-6}	1.24	\downarrow E, ~ K, \uparrow R	31.62 %	26.37 %
6	194	10^{-4}	1.25	\downarrow E, \uparrow K, \uparrow R	29.00 %	14.36 %

this in the analysis or modify the Morris method to allow removal of simulations.

Confidence intervals (95 %) are derived via bootstrapping using 1000 bootstrap resamples , following Archer et al. (1997)(See 5 Appendix 1).

3 Results

3.1 Sensitivity to updated GLHMYPS dataset

Global-scale hydrogeological data is limited. Figure 2 (b) shows the change in K between GLHYMPS 1.0 (Gleeson to et al., 2014) and the upper layer of GLHYMPS 2.0 (Huscroft et al., 2018) where an overall increase can be observed due to the change in unconsolidated sediments. Although uncon-

- solidated sediments cover roughly 50 % of the world's terrestrial surface, their extent was underestimated in previous ¹⁵ lithologic maps by half (Börker et al., 2018). The largest increase of K can be found between 50 and 70 °N because of glacial sediments that were assigned high K values. Different lithologies, e.g. alluvial terrace sediments and glacial
- tills, have all been grouped into the hydrolithological cate-²⁰ gory of sand. Areas of decreased hydraulic conductivity are e.g. the Great Lakes, south of Hudson Bay, and parts of Somalia. The area around Hudson Bay was assumed to consist of unconsolidated sediments in GLHYMPS 1.0 (Gleeson et al., 2014) and was changed to consolidated. In Somalia,
- evaporites, which are known for low K, were incorporated from the Global Unconsolidated Sediments Map Database (GUM) (Börker et al., 2018). Furthermore, GUM provides a detailed mapping of loess and loess-like depositions, which were assigned lower K values. These regions can be ob-
- $_{30}$ served to be the only regions with reduced K (Fig. 2 (b)). Overall, the increase in unconsolidated sediments is probably the main cause for the increased K.

Due to the change in K, the simulated h changes accordingly (Fig. 2(c)). In areas where the K decreased h increased ³⁵ e.g. eastern North America. Overall heads decreased, especially in central Russia by up to 10 to 100 m. A slight increase in head can be observed in areas with no change in K. This can be either due to changes in groundwater flow patterns due to the overall increase in K or due to numerical noise.

40

Based on these results, a local sensitivity index was calculated using Eq. (7), shown in Fig. 2 (d). White constitutes areas where either the relative change of K was zero or the head of the GLHYMPS 1.0 simulation was zero. Areas with a sensitivity index below (-)0.1 probably constitute variations that can be accounted to nu-45 merical differences in simulation outcome. Overall, h and K change in the opposite directions (positive values indicate a change into the same direction). An overall increase in K has led to a overall decrease in h as the higher K values are able to transport more water for a given hydraulic gradient, especially along 50 coastlines and mountainous areas. Increased sensitivity indexes can be observed at boundaries of areas of large spatial extent where the initial K was equal, whereas the h changes inside that area are relatively small (e.g. Arabian Peninsula). In regions where an increase in K leads to a decrease in 55 head, an increase of h at the boundary to other hydrolithological structures can be observed. Areas with changing indexes next to each other, e.g. in the Sahara, possibly point to a numerically unstable model region with a general sensitivity to parameter changes. GLHYMPS 2.0 represents the best available global data for hydraulic conductivity, and the results of this initial experiment indicate a significant sensitivity to updating the model with this new dataset.

3.2 Monte Carlo experiments

To assess the variability of model outputs we used the Monte ⁶⁵ Carlo-like OAT experiments to analyze the outcomes of quantify the output uncertainty as given in the 1848 model realizations.

3.2.1 Variability of hydraulic head

The spatial distribution of variability in the main model output *h* provides insights into model stability and highlights regions which are most sensitive to parameter changes. Observable differences between simulations can be caused by: (1) the parameter change of the OAT experiment, (2) the interactive effects due to combinations of parameter changes,

(3) numerical noise (slight variations in outcome due to the nature of the numerical algorithm or floating point errors that cannot be attributed to a specific parameter change), and (4) a non-optimal solution of the groundwater equation (Eq. (1))

- ⁵ even if the convergence criterion is met. The latter error (4) can be observed in regions of the model where a strong nonlinear relation may produce solutions that fit the convergence criterion but should be considered non-valid, e.g., because of a mass-balance mass balance that is unacceptably inprecise.
- Figure 4 shows the absolute coefficient of variation (ACV) of h per cell over all Monte Carlo experiments. The ACV is used to make a sound comparison of variance taking into account the mean of the h value per cell (because the mean might be negative the absolute value is used). Yellow indi-
- ¹⁵ cates that h changed little (mostly for regions with shallow groundwater), white to gray values indicate a growing difference in model results, and red values indicate a high variation of h over all model realizations. The latter areas represent either very low R (Sahara, Australia, South Africa) or
- ²⁰ a high variance in elevations, e.g., Himalaya, Andes and the Rocky Mountains. These are expected to have a high sensitivity to parameter changes as the multiplier of E_{swb} produces the highest shifts in regions with high elevation. Large Any changes in E_{swb} might cause a switch from gaining to
- ²⁵ losing conditions and vice versa (discussed in Sect. 3.2.2). Additionally, a change in R directly influences the conductance term C_{riv} that might also be changed by a multiplier. These combinations may yield conditions that are exceptionally challenging for the numerical solver. Switches between
- ³⁰ the two conditions constitute a non-linearity in the equation which might require a smaller temporal step-size to be solved. In a nutshell, if an iteration leads to a gaining condition and the next to a losing condition, the switch renders the approximated heads of the preceding iterations invalid as the
- ³⁵ equation changed. In the worst case this can lead to an infinite switch between the two conditions without finding the correct solution.

Areas with a high variance in results hydraulic heads will also produce wide confidence intervals and for parameters which are highlighted in Fig. A2.

Figure 5 relates the uncertainty in h, due to a change from GLHYMPS 1.0 to 2.0 to the interquartile range of h of all Monte Carlo realizations, thus uncertainty in h due to parameter variation. Parameter variation is the dominant cause for

- ⁴⁵ h variability in mountainous regions, whereas the change in geologic data has a dominant impact in northern latitudes and the upper Amazon. In Australia, central Africa, and northern India the impact of increasing K is almost as high as the variability caused by the variation of parameters in the Monte ⁵⁰ Carlo experiments. This suggests that a reduced uncertainty
- in K in these regions will improve the model results.



Figure 4. Absolute coefficient of variation $(\sigma(h)\mu(|h|)^{-1})$ [%] of simulated *h* per cell over all Monte Carlo realizations. Yellow indicates that *h* results changed very little, white to gray values indicate a growing difference in model results, and red values indicate a very high variation of *h* over all model realizations.



Figure 5. Uncertainty in h caused by variability in geologic structure hydraulic conductivity data between GLHYMPS 1.0 and 2.0 (dominant in blue brown to light bluegreen) in relation to uncertainty in h caused by variability in parameters based on Monte Carlo

in *h* caused by variability in parameters based on Monte Carlo simulations (dominant in brown blue to greenlight blue) calculated as $\frac{|h1-h2|}{|QR(h_{mc})|}$ where h1/2 is the simulated head based on GLH-MYPS 1.0 and 2.0 and h_{mc} the simulated head of all Monte Carlo experiments.

3.2.2 Variability of losing/gaining surface water bodies

Surface water bodies that provide focused, indirect groundwater recharge to the aquifer system are an important recharge mechanism to support ecosystems alongside ⁵⁵ streams (Stonestrom, 2007). Especially in arid regions, they are important for agriculture and industrial development.

Losing or gaining surface water bodies are determined by h in relation to E_{swb} . When h drops below E_{swb} water is lost to the aquifer (Eq. (5)) Figure 6 shows for each grid cell the percentage of the model runs in which the surface water bodies in the cell lose water to the groundwater. Regions with a higher percentage are regions that are in losing conditions independently for most of the applied parameter changes Values. Areas with the highest deviation in h (Fig. 4), thus the lowest agreement over all model realizations, are similar to the regions where some parameter combinations lead to losing



Figure 6. Percentage of all Monte Carlo realizations that resulted in a losing surface water body in a specific cell.

surface water bodies, while others lead to gaining surface water bodies (Fig. 6). Overall arid and mountainous regions show high percentages of Monte Carlo realizations with losing conditions, with dominantly 20-50 % of the realizations

 $_5$ resulting in losing surface water bodies. h in these regions falls below E_{swb} either due to low recharge or high gradients. Surface water-groundwater interaction in these regions should be more closely investigated to improve model performance. The Sahara region stands out with large areas that

¹⁰ contain losing surface water bodies in almost all model realizations. Values close to 100 % are furthermore reached in the Great-Lakes, the Colorado Delta, the Andes, the Namib Desert, along the coast of Somalia, the Aral lake, lakes and wetlands in northern Siberia, and partially in Australian wet-15 lands. Wetlands in Australia and the Sahara are likely to be

overestimated in size in the context of a steady-state model.

3.2.3 Parameter sensitivities as determined by the method of Morris

The global-scale sensitivity of h and Q_{swb} is summarized ²⁰ in Table 3 that lists the percentage fractions of all cells for which a certain parameter has a certain rank regarding sensitivity and parameter interaction.

Overall, E_{swb} and R are the most important parameters for both model outputs over all ranks, followed by K. Q_{swb} ²⁵ is more sensitive to R than h, whereas h is more sensitive to E_{swb} . C_{riv} appears only dominant in the second and third rank for both model outputs. This means that for the majority of cells a change in E_{swb} and R, rather than C_{riv} dominates changes in Q_{swb} and h. K and R directly influence the cal-³⁰ culation of C_{riv} and thus show a higher sensitivity.

The standard deviation of EEs (σ_i) is an aggregated measure of the intensity of the interactions of the *i*th parameter with the other parameters, representing the degree of non-linearity in the model response to changes in the *i*th param-

³⁵ eter Morris (1991). A high parameter interaction indicates that the total output variance rises due to the interaction of the parameter with other parameters.

Robert Reinecke: Sensitivity of simulated global groundwater

Table 3. Percentage fractions of simulated cells with parameter sensitivity for which parameters are ranked 1 to 3 based on μ * and parameter interaction σ_{per} . Percentages are shown for each model output, h and Q_{swb} , where the respective output is most sensitive to the listed parameter. For example, h is the most sensitive to parameter E_{swb} (Rank 1) in 57.2% of all grid cells, while K R is the second most important parameter for $h Q_{swb}$ in 24.259.8% of those cells.Fractions are shown for the first three ranks.

		% of cells						
		Rank 1		Rank 2		Rank 3		
Para.	Output	$\mu *$	σ	$\mu *$	σ	$\mu *$	σ	
K	h	24.2	18.8	21.7	12.9	7.1	4.3	
	Q_{swb}	18.4	15.4	21.1	7.3	8.8	4.7	
E_{swb}	h	57.2 57.2	46.3	14.8	19.9	13.4	18.	
	Q_{swb}	18.5	14.3	11.2	27.7	36.0 36.0	34.	
C_{lak}	h	1.0	0.5	3.9	2.4	4.3	2.5	
	Q_{swb}	0.5	0.6	2.2	0.9	2	0.9	
C_{wet}	h	1.4	0.5	3.4	1.4	5.3	4.5	
	Q_{swb}	0.5	0.8	3.6	2.1	4.2	2.8	
a	h	0.9	0.9	1.8	10.2	8.4	8.1	
$C_{gl.wet}$	Q_{swb}	0.4	0.8	2.3	15.2	9.4	7.8	
C_{riv}	h	2.0	28.0	32.8 32.8	29.3	28.7	18.	
	Q_{swb}	1.4	62.6	47.8 47.8	16.2	28.8	10.	
R	h	13.4	4.1	22.7	23.6	33.8 33.8	43.	
	Q_{swb}	59.8 59.8	5.1	11.3	30.5	10.7	39.	
C_{oc}	h	1.3	1.0	0.3	0.2	0.5	0.4	
	Q_{swb}	0.5	0.4	0.5	0.2	0.2	0.2	

Percentage of cells with non-overlapping CIs (see App. 1 and Sect. 3.2.6) μ *: 11.8 % (*h*) and 13.3 % (Q_{swb}). C_{oc} is rank 1 for *h* in 23% of all ocean cells and in 11% for Q_{swb} .

 E_{swb} shows higher interactions for h than for Q_{swb} . C_{riv} shows a high interaction on the first rank even if it is not the dominant effect. This interaction is likely due to changes and K and R that directly influence the computation of C_{riv} . Both model outputs are sensitive to changes in R but show a relatively low degree of interaction for the first rank. A higher percentage of cells with an increased interaction of R is only visible in the second and third rank.

Lakes and wetlands show low sensitivity and interaction in relation to total number of cells in Table 3 because they only exist in a certain percentage of cells. Table 4 shows the percentage fractions relative for cells with more than 25 % coverage of a lakes, global wetlands, and/or wetlands. The dominant parameter (by percentage) for all cells with respective surface water body is always E_{swb} for h (in 79.2 % of the lakes and in (79.9 %) 66.3 % of the (global)wetlands) and R (~54-77 % of all cells) for Q_{swb} . For the second rank the conductance of the surface water body $C_{lak,wet,gl.wet}$ dominated h, C_{riv} for Q_{swb} . Thus for lakes and wetlands E_{swb} and R are more relevant to h and Q_{swb} than the conductance of these surface water bodies.

 $\mu * (h)$ $\mu * (Q_{swb})$ % R. 2= $C_{lak,wet,gl.wet}$ % R. 1= E_{swb} % R. 1=R % R. 2= C_{riv} 79.2 Lakes 64.6 54.2 38.8 Wetlands 46.9 66.3 47.3 77.2 ¹31.7 Gl. Wetlands 79.9 56.4 66.3

Table 4. Percentage fractions of the most frequent parameter for rank 1 and 2 of all cells with with more than 25 % coverage of a lakes, global wetland, or wetland.

 $^{1}C_{riv}$ =31.7 %, $C_{gl.wet}$ =40.6 %.

Percentage of second most frequent parameter not shown. Percentage in relation to cells with lakes, global wetland, or wetland > 25 %. Percentage-wise R. $1(\mu * (h))$ was always followed by R except for global wetlands were the second most frequent R. 1 was $C_{gl.wet}$. R. $1(\mu * (Q_{swb}))$ was followed percentage-wise by E_{swb} except for local wetlands with K, R. $2(\mu * (Q_{swb}))$ by $C_{lak,wet,gl.wet}$ except for global wetlands with C_{riv} .

3.2.4 Maps of global sensitivity

To show the spatial distribution of the parameters that affect h and Q_{swb} the most, ranked parameters were plotted for every cell in Fig. 7. The top of Fig. 7 represents the most 5 sensitive parameters in terms of h (left) and Q_{swb} (right). Areas that should be judged with caution due to overlapping CIs that are shown in Fig. A2.

For $h E_{swb}$ stands out for mountainous regions and in mountainous regions with spots of C_{riv} and in regions with low

- ¹⁰ rechargealigned with regions. These regions align with highly variable outputs shown in Fig. 4and Fig. A4 with spots of C_{riv} . K is most important for h in Australia, the northern Sahara, the Emirates, and across Europe. The second rank (second row in Fig. 7) shows values that are not as important as
- ¹⁵ the top row but dominant over all other parameters. In the regions with large output variations (compare 4) K and for parts of the Himalaya R are dominant in the second rank (for h). C_{lak} is clearly visible in parts of Nepal and along the Brahmaputra.
- For $Q_{swb} E_{swb}$ is dominant for Q_{swb} in the first rank in e.g. Rocky Mountains, Andes, Hijaz Mountains in Saudi Arabia and the Himalaya. R stands out in regions in the Tropical Convergence Zone with large R and as well as in northern latitudesfor. C_{wet} appears as dominant parameter in areas
- ²⁵ with large wetlands with a bigger impact on Q_{swb} results than on h. K seems to be equally spatially distributed for h as well as for Q_{swb} . It is most important for h in Australia, the northerm Sahara, the Emirates, and across Europe. There seems to be no correlation between the initial K spatial distribution and a highly
- ³⁰ ranked K sensitivity for both model outputs. Areas with a dominant K are possibly influenced by a high interaction with other model components (K shows a high interaction Table 3 that is also reflected spatially in Sect. 3.2.5). E_{swb} stands out in the Sahara where likely overestimated wetland extents (Reinecke et al.,
- ³⁵ 2019) have a high impact on *h*. For the second rank in the Tropical Convergence Zone C_{riv} and *K* dominate for Q_{swb} . In general Q_{swb} seems to be more robust to show the effects in the highly variable regionsand. That is Q_{swb} is not responding as extreme as *h* to parameter changes. This further indi-

cates the assumption that E_{swb} is also mainly responsible for ⁴⁰ the *h* variations observed in Sect. 3.2.1.

The second rank (second row in Fig. 7) shows values that are not as important as the top row but dominant over all other parameters. In the highly variable regions Kand for parts of the Himalaya R are dominant in the second rank. The C_{wet} appears as dominant parameter in areas with large wetlands with a bigger impact on Q_{swb} results 45 than on h. C_{lak} is clearly visible in parts of Nepal and along the Brahmaputra. In the Tropical Convergence Zone C_{riv} and K dominate for Q_{swb} , whereas results for hshow a mix of $C_{gl.wet}$ C_{wet} and C_{riv} .

Zooming in on Europe (Fig. 8) for h, as an example, shows a similar trend Similar to the global picture that R and K have the highest impact on h along with E_{swb} . E_{swb} is dominant in mountainous regions like the Alps and the Apennines as well in regions with lots of surface water bodies e.g. southern part of Sweden in the area of lake Vättern and Vänern and in the Finnish Lakeland. R appears dominant in east Italy in the lagoon of Venice and MaranoPo Valley, the Netherlands, and the wetlands in southwestern France. Almost invisible in the global picture is C_{oc} , a dominant parameter for most cells that have the ocean as boundary condition (only observable for h). Predominantly C_{riv} follows E_{swb} as second most important parameter. Only visible in the second rank are the wetlands e.g. in west Scotland.

3.2.5 Maps of global parameter interaction

Similar to the spatial parameter sensitivities Fig. 9 shows the parameter interactions for h and Q_{swb} . Parallel to Fig. 7, the first row of Fig. 9 represents the most interactive parameters in terms of h change (left) and Q_{swb} (right). The highest interaction with other parameters can be observed for E_{swb} for regions with high h variability similar to Fig. 7. C_{riv} shows a high interaction in regions sensitive to R (compare Fig. 7) ⁷⁰ and is more visible for Q_{swb} .

K regions in the second rank are similar to where K already showed a high sensitivity for h (compare Fig. 7). In the Himalaya R and C_{riv} show a large spatial pattern. For Q_{swb} , $C_{gl.wet}$ is clearly visible where C_{riv} was most interactive before.



Figure 7. Ranking of parameter sensitivity μ^* of h (left) and Q_{swb} (right). The upper maps show the first rank, the middle the second, and the bottom the last third rankby μ^* values.



Figure 8. Zoom in of Europe of Fig. 7. Ranking of parameter sensitivity $\mu *$ of h (left: rank 1, right: rank 2).

3.2.6 Sensitivity per GHRU

Average sensitivities and parameter interactions for each of the six GHRUs are shown in Fig. 10 (a). A dominant average per GHRU does not imply a rank 1 in each cell but rather 5 provides an indication of its average importance per GHRU. Each GHRU is described by the notation in Table 2. The shown average sensitivities and interactions are normalized to [0,1] because the calculated μ * and σ present no absolute measure of sensitivity. Mean values of μ * and σ that are very 10 close to zero are not shown in Fig. 10. The values shown in Fig. 10 (a) should be judged with caution as they also include the regions Fig. A2 shown to be unreliable. Reliability means that due to overlapping CIs (any overlapping) that show possibly unreliable results, i.e., those where any overlap in CIs indicates that the ranking of the parameters can't cannot 15 be clearly determined (compare Fig. A2 and See additional explanation Fig. A1).

To judge the reliability of the outcomes per GHRU Table 2 shows the percentage of reliable results for h and Q_{swb} for each GHRU, where reliable results exclude over 80% of all 20 sensitivity values.



Figure 9. Ranking of parameters interaction ($\sigma \sigma *$ of EE is an indicator for parameter interaction) based on *h* (left) and Q_{swb} (right). Parameters are ranked from top to The upper maps show the first rank, the middle the second, and the bottom by Σ values the third rank.

Figure 10 (b) shows only cells with reliable results, based on their confidence intervals, resulting in 11.8 % of all grid cells for h and 13.3 % for Q_{swb} . GHRUs in high and very high elevations show low reliability concerning h results as 5 expected (compare Fig. 4). Q_{swb} appears as more robust in these regions.

Figure 10 (a) shows a similar picture to the two global maps (Fig. 7, 9). All GHRUs show a linear correlation of sensitivity and degree of interaction. The GHRU with average 10 elevation, average recharge, and high K (GHRU 1) shows higher average response in Q_{swb} than h. h is most sensitive to C_{riv} , and less sensitive to the other parameters. Q_{swb} is clearly most sensitive to K and $C_{gl.wet}$ and shows a high interaction in this GHRU. Lower-lying regions with average K

- ¹⁵ and R (GHRU 2) show high sensitivity of h only to E_{swb} with a high interaction while Q_{swb} is affected in decreasing order by $C_{gl.wet}$ and K. Results for h sensitivity in GHRU 3, with very high elevations, average K and low R, should be judged with caution because only a very low fraction is based
- ²⁰ on results with non-overlapping CIs (Table 2). Compared to other GHRUs, 3 shows rather clustered sensitivities and parameter interactions. h is most sensitive to E_{swb} and R and Q_{swb} to C_{lak} , K, and C_{wet} . GHRU 4, which differs from GHRU 3 by its high but not very high land surface elevation,
- ²⁵ shows E_{swb} , K, and R as clearly most dominant and interactive parameter for Q_{swb} , followed by C_{wet} . Similar Q_{swb} is most sensitive to E_{swb} and K. In low-lying and rather flat

regions with high groundwater recharge (GHRU 5), sensitivities of h are close to zero except for K possibly because changes in h are to small in flat regions (compare Fig. 4) ³⁰ due to small h gradients. Q_{swb} is most sensitive to E_{swb} and $C_{gl.wet}$. GHRU 6 is relatively small and like GHRU 5 only occurs in the tropical zone (Fig. 3 (a)). In this GHRU, which differs from GHRU 5 only by K being high instead of average, the dominant parameters of Q_{swb} are similar to other GHRUs where E_{swb} is clearly the most dominant followed by R and K. h shows a response to wetlands but again like in 5 a very low response to E_{swb} .

Taking into account only the reliable regions changes the perception in Fig. 10 (b). GHRU 1 shows rather similar sen-40 sitivities and parameter interactions as compared to other GHRUs. h is most sensitive to E_{swb} , and only somewhat less sensitive to C_{riv} and C_{wet} . Q_{swb} is clearly most sensitive to C_{riv} and shows a high interaction in this GHRU. GHRU 2 shows high sensitivity of h only to E_{swb} with a high in- 45 teraction while Q_{swb} is equally affected by K, E_{swb} and R. Results for h sensitivity in GHRU 3 are not very representative for the whole GHRU as only a very small fraction of cells shows reliable results (Table 2). Like in GHRU 2, Q_{swb} is equally affected by by K, E_{swb} and R. GHRU 4 shows 50 E_{swb} as clearly most dominant and interactive parameter for h, followed by K and C_{wet} . For GHRU 5, sensitivities of hcould not be determined reliably possibly because changes in h are to small in flat regions (compare Fig. 4) due to small

h gradients. Q_{swb} is most sensitive to *R* (as rivers are gaining rivers that need to drain groundwater recharge) followed by *K*. In GHRU 6 the dominant parameters of Q_{swb} are the same as for GHRU 5 (except for E_{swb}) while *h* is most sensitive to C_{lak} .

4 Discussion

This study presents a novel spatially distributed sensitivity analysis for a high-resolution global gradient-based groundwater model encompassing 4.3 million grid cells. While these maps are challenging to interpret, they yield new ways of understanding model behaviour based on spatial differences and help to prepare calibration efforts by identifying parameters that are most influential in specific regions. Furthermore, they guide the future development of the model to the hydrological model. Especially, the sensitivity of Q_{swb} and the interded coupling efforts of the groundwater model to the hydrological model. Especially, the sensitivity of Q_{swb}

and the importance of E_{swb} , which are the two major coupling components, are of interest.

- However, the large number of grid cells with either statis-²⁰ tically zero sensitivity values (overlapping CI with zero) or unreliable results limit the relevance and applicability of the study results. For most of the statistically zero sensitivity values the Cl is very large, and it is therefore very unlikely that the parameter is not influential. The study suggests that
- ²⁵ the highly non-linear and conceptual approach to the surface water body conductance (in particular the sudden change of conductance between gaining and losing rivers) needs to be revised as it may affect the stability of transient model results. Additionally the results suggest that elevation of the
 ³⁰ water table of surface water bodies is a promising calibration

parameter alongside with hydraulic conductivity.

The presented results need to be considered against the backdrop of the high h variability of the Monte Carlo experiments (Sect. 3.2.1). Some of these simulations cannot be ³⁵ considered as a valid result for a h distribution, an issue

- not faced with other simpler traditional bucket-like hydrological models. This is due to multiple model challenges: (1) the evaluated model approximates a differential equation and can show non-linear behaviour for different parameteri-
- ⁴⁰ zations, (2) the equations used for rivers present a non-linear model component (switch between equations for gaining and losing conditions as well as relation to K and R), (3) the convergence criterion for the steady-state solution is solely based on a vector norm of residuals (metric of changes of the solu-
- ⁴⁵ tion inside the conjugate gradient approach) and maximum h change between iterations and do not contain an automated check for a reasonable mass balance. On the other hand, it is challenging to include a validation mechanism in the presented analysis to alleviate these problems while maintaining
- ⁵⁰ a reasonable model runtime (as a stricter convergence criterion will most likely increase the number of necessary iterations) and/or number of necessary model runs. It is question-

able whether results based on different convergence criteria can be compared. This would necessitate including the numeric stability in the sensitivity analysis as well.

However, the results help to answer the research questions at hand. While overlapping CIs blur the ranking of the parameters in some regions, they still provide evidence on what parameters the calibration should focus and how the importance of parameters varies per region. The sensitivity of Q_{swb} to parameters, especially E_{swb} , will help to guide the future model development and coupling to the hydrological model. In general, the analysis helped to identify the elevation of surface water bodies as a focus for future research.

Around 30 % of all μ * values had a confidence interval ⁶⁵ that was larger than 10 % of the μ * value. This suggests that even more model runs are required and that large extents of the model experienced numerically unstable results as the spatial distribution of head variance and large confidence intervals overlap. ⁷⁰

The selection of parameter ranges can influence the results of a sensitivity analysis significantly (Pianosi et al., 2016). Even parameters that are suspected of not being sensitive can show highly nonlinear behavior in certain parts of the parameter space that are only activated when one expands the 75 ranges of the parameters. The presented ranges in this study do not explore the full assumed uncertainty range. Specifically, the small range of E_{swb} is likely influencing the outcome of the parameter rankings. The range was chosen to allow a reasonable number of simulations to converge as the 80 range of E_{swb} directly influences the numerical stability CONVergence of the model. The presented results, however, do show that the model output is highly sensitive to changes in E_{swb} in most areas of the globe. The response in mountainous regions can be attributed to applying E_{swb} as a multiplier, ⁸⁵ which has a higher impact in regions where the initial water body elevation is high. On the other hand, this is accounting for the fact that the uncertainty of E_{swb} is largest in regions with highly variable topography per 5' grid cell.

The only previous sensitivity analysis of a global gradient-90 based groundwater model to out knowledge was done by de Graaf et al. (2015). Based on varying K, aquifer thickness, and R, the coefficient of variation of the steady-state hydraulic head was computed (de Graaf et al., 2015, Fig. 5). From that analysis it was determined that K has the highest $_{95}$ impact and aquifer thickness the lowest. It is not clear how the coefficient of variation determined these outcomes. The relatively low impact of aquifer thickness was observed also by Reinecke et al. (2019). Therefore, this parameter was not included in this study. Both de Graaf et al. (2015) and this 100 study show a high h variance in parts of Australia and the Sahara (de Graaf et al., 2015, Fig. 5) possibly due to the low initial R. Variations in the mountainous regions, on the other hand, are not reflected in de Graaf et al. (2015) as their analysis did not vary E_{swb} . 105

Besides the large h variance, which is likely the main cause for the low percentage of reliable cells, the confidence

55



Figure 10. Normalized average sensitivity and parameter interaction per GHRU for *h* and Q_{swb} (a). If a parameter is not present the mean sensitivity for that GHRU was close to zero (overlapping CI with zero). Does not include ocean parameter sensitivity. Mean characteristics, their symbols for each GHRU, and the reliability of the sensitivity measure (only μ * not σ) are shown in Table 2. (b) Only reliable results (after removing overlapping CI).

intervals of the sensitivity indices in this experiment suggest that additional simulations are necessary to determine more reliable results. Additionally, the small parameter ranges, required for stable model runs, influenced the overall outcome 5 and might be a reason for cells with inconclusive results.

For cells with lakes and wetlands, E_{swb} dominates over the variations in conductance for h (Table 4), confirming the importance in determining the surface water body elevation. For Q_{swb} , on the other hand, R is most influential in these to cells even though it does not affect the conductance equation for these surface water bodies. Apparently, available recharge is driving the interaction more than it influences changes in head. In regions with high recharge (GHRU 5) Q_{swb} was more robust to parameter changes than h. This is possibly due to the generally lower response in Q_{swb} to changes in ¹⁵ E_{swb} , which can be explained by the constant flow for losing surface water bodies (incl. rivers) as soon as h drops below E_{swb} . Thus changes is E_{swb} do not affect Q_{swb} afterwards (as long as the surface water body remains in losing conditions). Both model outcomes show a high sensitivity to R ²⁰ while the interaction of R is only visible at the 3rd rank suggesting that if R changes other parameter changes do not influence the model response further.

Separating the complex global domain into a selected number of GHRUs enables a sensitivity analysis in accordance with computational constraints (e.g. maximum number of core hours). It alleviates the drawbacks of global-scale multipliers while keeping a reasonable number of total simuand surface water body characteristics should be investigated ⁵ as additional characteristics for GHRUs.

5 Conclusions

For the first time, spatially distributed sensitivities of the global steady-state distribution of hydraulic head and flows between the groundwater and the surface water bodies were ¹⁰ calculated and presented. We found the Morris sensitivity analysis method can yield insights for computationally challenging (concerning computation time and numerical difficulties) models with reasonable computational demand. This study applied a novel approach for domain decomposition

¹⁵ into GHRUs. Applying parameter multipliers simultaneously to all grid cells within each of the six GHRUs allowed a more meaningful sensitivity calculation, than it would be possible if the parameters would have varied simultaneously in all grid cells, while maintaining a feasible the number of simu-²⁰ lations.

Based on only a small fraction of grid cells for which parameters could be ranked reliably according to their importance for simulated model output, steady-state hydraulic heads (h) were found to be comparably affected by hydraulic

- ²⁵ conductivity (K), groundwater recharge (R) and the elevation of the water table of surface water bodies (E_{swb}). Rankings for individual grid cells varies, but globally none of the three dominates with respect to h. The simulated flows between groundwater and surface water bodies (Q_{swb}) are
- ³⁰ clearly most sensitive to R. This is due to the model parameterization of river conductance that is computed as a function of R, assuming under steady-state conditions, groundwater discharge to rivers should tend to increase with increasing R (Eq. (5)). The results indicate that changes in
- $_{35}$ R between timesteps for a fully coupled transient model could pose a challenge to the model convergence and that the equations might need to be reconsidered for a fully coupled model. In general the uncertainty due to the parameterization of groundwater-surface water exchange flows (E_{swb} and
- ⁴⁰ $C_{riv,gl.wet,wet,lak}$) needs to be further investigated as they have a high impact on h distribution and Q_{swb} .

In high mountainous regions (Rocky Mountains, Andes, Ethiopian Highlands, Arabian Peninsula, Himalaya) and regions with low recharge (Sahara, southern Africa) the com-

- ⁴⁵ puted *h* showed an unreasonably high variance due to the numeric numerical instability of the simulations in these areas. In case of high elevations and thus large variations in E_{swb} or in case of low groundwater recharge, it is not possible to solve steady-state groundwater flow equations with arbitrary
- ⁵⁰ parameter combinations and a constant convergence parameter. Q_{swb} was found to somewhat be more robust than h in these regions. These results suggest that the parameterization

of E_{swb} needs to be reconsidered and is a likely parameter for future calibration. In general more robust global sensitivity methods are required that allow exclusion of certain 55 simulations from the analysis.

The lack of reliable data at the global scale, in particular hydraulic conductivity data with high horizontal and vertical resolution, hinders the development of global groundwater models. A simple sensitivity analysis on the impact of small changes to an existing global hydraulic conductivity dataset (GLHYMPS 1.0 (Gleeson et al., 2014) to 2.0 (Huscroft et al., 2018)) showed that knowledge about the distribution of *K* is pivotal for the simulation of *h* as even slight changes in *K* may change model results by up to 100 m.

The presented study results refer to the uncoupled steadystate groundwater model G^3M . As G^3M is currently being integrated into the global hydrological model WaterGAP, future work will extend this sensitivity analysis to fully coupled transient simulations.

1 Appendix

Confidence intervals are determined based on 1000 bootstrap resamples following Archer et al. (1997) for all simulation outputs. Bootstrapping is an established statistical method that relies on random sampling with replacement 75 using the original data. This sampling from a set of independent, identically distributed data is equivalent to sampling from the empirical distribution function of the data allowing to determine confidence intervals (Archer et al., **1997**). Results of the method of Morris need to be contemplated in a ranking based 80 scheme that relies on metrics thatsummarize the calculated EEs. The derived metrics $\mu *$ and σ_i both are measures of intensity (higher values are more sensitive/interactive) and do not represent absolute values of sensitivity. Both can only be interpreted meaningfully in comparison with values derived for 85 other parameters. To achieve that, $\mu *$ and σ_i should be presented in so called ranks. Values for all parameters are sorted from highest to lowest, and the parameter with the highest value is selected as the most influential parameter with the highest rank. The parameter with the second 90 highest value is the second most influential parameter and so on.

Figure A1 shows the conceptual issues that are entailed with this ranking approach. The absolute mean (μ *) of all EEs of parameter 1 (P1) might be bigger than μ * of P2 but as their CIs are overlapping a clear ranking is not possible. On the other hand it is evident that P1 and P2 are clearly more sensitive than P3. An overlapping suggests that even if the $mu* \mu$ * values are different a ranking should be considered with care as the two parameters could be equally important or in some regions inside one GRHU their importance could be the other way around. But even if they overlap, the mu* μ * provides a valuable measure of the overall importance of the parameters also in comparison with much less important parameters.

70



Figure A1. Illustration of derivation of presented metrics. Blue circles show the two criteria used to judge the quality of the results. $\mu *$ is calculated based on the EEs (circles), however the CI is calculated based on bootstrap resamples of the simulation outputs.

Additionally, not only the overlapping should be considered but also the size of the CI in comparison to the $mu*\mu*$. It is a useful indicator on whether the sampling of the parameter space was to small and more simulations are required 5 to gain a clearer picture. 15% is an arbitrary value that we considered an appropriate boundary. Other studies used 10%

(Herman et al., 2013a) or 3.5% (Vanrolleghem et al., 2015).

Figure A2 shows regions where the applied sampling was sufficient (CIs where smaller than 15% of the calculated μ * of the first ¹⁰ rank) and regions where likely more simulations, or a more

sophisticated approach to ensure numerical stability, is required.



Figure A2. Confidence interval (95) in relation to the μ * for rank 1 of *h* and Q_{swb} . Yellow regions indicate a sufficient sampling size.

Author contributions. RR led conceptualization, formal analysis, methodology, software, visualization, and writing of the original draft. JH, LF, SM, TT supported review and editing as well as the ¹⁵ development of the methodology. AW supported visualization and writing of original draft of section 3.1. PD supervised the work of RR and made suggestions regarding analysis, structure, and wording of the text and design of tables and figures.

Acknowledgements. Funding: Friedrich-Ebert Foundation PhD fel- 20 lowship

References

- Allen, P. M., Arnold, J. C., and Byars, B. W.: Downstream channel geometry for use in planning-level models, JAWRA Journal of the American Water Resources Association, 30, 663–671, 2 https://doi.org/10.1111/j.1752-1688.1994.tb03321.x, 1994.
- Archer, G., Saltelli, A., and Sobol, I.: Sensitivity measures, ANOVA-like techniques and the use of bootstrap, Journal of Statistical Computation and Simulation, 58, 99–120, 1997.
- Börker, J., Hartmann, J., Amann, T., and Romero-Mujalli, ³⁰
 G.: Global Unconsolidated Sediments Map Database v1.0 (shapefile and gridded to 0.5° spatial resolution), https://doi.org/10.1594/PANGAEA.884822, supplement to: Börker, J et al. (accepted): Terrestrial Sediments of the Earth: Development of a Global Unconsolidated Sediments Map ³⁵ Database (GUM). Geochemistry, Geophysics, Geosystems, https://doi.org/10.1002/2017GC007273, 2018.

Robert Reinecke: Sensitivity of simulated global groundwater

- Branger, F., Giraudet, L.-G., Guivarch, C., and Quirion, P.: Global sensitivity analysis of an energy–economy model of the residential building sector, Environmental Modelling & Software, 70, 45 – 54, https://doi.org/https://doi.org/10.1016/j.envsoft.2015.03.021,
- Campolongo, F., Cariboni, J., and Saltelli, A.: An effective screening design for sensitivity analysis of large models, Environmental modelling & software, 22, 1509–1518, https://doi.org/10.1016/j.envsoft.2006.10.004, 2007.
- Chaney, N., Herman, J., Reed, P., and Wood, E.: Flood and drought hydrologic monitoring: the role of model parameter uncertainty, Hydrology and Earth System Sciences, 19, 3239–3251, https://doi.org/10.5194/hess-19-3239-2015, 2015.
- ¹⁵ de Graaf, I. E., Sutanudjaja, E., Van Beek, L., and Bierkens, M.: A high-resolution global-scale groundwater model, Hydrology and Earth System Sciences, 19, 823–837, https://doi.org/10.5194/hess-19-823-2015, 2015.

de Graaf, I. E., van Beek, R. L., Gleeson, T., Moosdorf, N., Schmitz,

20 O., Sutanudjaja, E. H., and Bierkens, M. F.: A global-scale twolayer transient groundwater model: Development and application to groundwater depletion, Advances in Water Resources, 102, 53–67, https://doi.org/10.1016/j.advwatres.2017.01.011, 2017.

Dell'Oca, A., Riva, M., and Guadagnini, A.: Moment-based

- metrics for global sensitivity analysis of hydrological systems, Hydrology and Earth System Sciences, 21, 6219–6234, https://doi.org/10.5194/hess-21-6219-2017, 2017.
- Döll, P., Kaspar, F., and Lehner, B.: A global hydrological model for deriving water availability indicators: model tun-
- ³⁰ ing and validation, Journal of Hydrology, 270, 105–134, https://doi.org/10.1016/S0022-1694(02)00283-4, 2003.
- Döll, P., Hoffmann-Dobrev, H., Portmann, F. T., Siebert, S., Eicker, A., Rodell, M., Strassberg, G., and Scanlon, B.: Impact of water withdrawals from groundwater and surface water on continental
 ³⁵ water storage variations, Journal of Geodynamics, 59, 143–156,
- https://doi.org/10.1016/j.jog.2011.05.001, 2012.
- Döll, P., Müller Schmied, H., Schuh, C., Portmann, F. T., and Eicker, A.: Global-scale assessment of groundwater depletion and related groundwater abstractions: Combining hydrologi-
- 40 cal modeling with information from well observations and GRACE satellites, Water Resources Research, 50, 5698–5720, https://doi.org/10.1002/2014WR015595, 2014.
- Fan, Y., Li, H., and Miguez-Macho, G.: Global patterns of groundwater table depth, Science, 339, 940–943, 45 https://doi.org/10.1126/science.1229881, 2013.
- Ghasemizade, M., Baroni, G., Abbaspour, K., and Schirmer, M.: Combined analysis of time-varying sensitivity and identifiability indices to diagnose the response of a complex environmental model, Environmental Modelling & Software, 88, 22 – 34, https://doi.org/10.1016/j.envsoft.2016.10.011, 2017.
- Gleeson, T., Smith, L., Moosdorf, N., Hartmann, J., Dürr, H. H., Manning, A. H., van Beek, L. P. H., and Jellinek, A. M.: Mapping permeability over the surface of the Earth, Geophysical Research Letters, 38, https://doi.org/10.1029/2010GL045565, 2011.
- ⁵⁵ Gleeson, T., Moosdorf, N., Hartmann, J., and Van Beek, L.: A glimpse beneath earth's surface: GLobal HYdrogeology MaPS (GLHYMPS) of permeability and porosity, Geophysical Research Letters, 41, 3891–3898, https://doi.org/10.1002/2014GL059856, 2014.

- Gruber, S.: Derivation and analysis of a high-resolution estimate ⁶⁰ of global permafrost zonation, The Cryosphere, 6, 221–233, https://doi.org/10.5194/tc-6-221-2012, 2012.
- Hartmann, A., Gleeson, T., Rosolem, R., Pianosi, F., Wada, Y., and Wagener, T.: A large-scale simulation model to assess karstic groundwater recharge over Europe and the Mediterranean, Geoscientific Model Development, 8, 1729–1746, https://doi.org/10.5194/gmd-8-1729-2015, 2015.
- Hartmann, J. and Moosdorf, N.: Global Lithological Map Database v1.0 (gridded to 0.5° spatial resolution), https://doi.org/10.1594/PANGAEA.788537, 2012.

70

90

100

- Hengl, T., Mendes de Jesus, J., Heuvelink, G. B. M., Ruiperez Gonzalez, M., Kilibarda, M., Blagotić, A., Shangguan, W., Wright, M. N., Geng, X., Bauer-Marschallinger, B., Guevara, M. A., Vargas, R., MacMillan, R. A., Batjes, N. H., Leenaars, J. G. B., Ribeiro, E., Wheeler, I., Mantel, S., 75 and Kempen, B.: SoilGrids250m: Global gridded soil information based on machine learning, PLOS ONE, 12, 1–40, https://doi.org/10.1371/journal.pone.0169748, 2017.
- Herman, J. and Usher, W.: SALib: an open-source Python library for sensitivity analysis, The Journal of Open Source Software, 2, 80 https://doi.org/10.21105/joss.00097, 2017.
- Herman, J., Kollat, J., Reed, P., and Wagener, T.: Method of Morris effectively reduces the computational demands of global sensitivity analysis for distributed watershed models, Hydrology and Earth System Sciences, 17, 2893–2903, ⁸⁵ https://doi.org/10.5194/hess-17-2893-2013, 2013a.
- Herman, J. D., Reed, P. M., and Wagener, T.: Time-varying sensitivity analysis clarifies the effects of watershed model formulation on model behavior, Water Resources Research, 49, 1400–1414, https://doi.org/10.1002/wrcr.20124, 2013b.
- Huscroft, J., Gleeson, T., Hartmann, J., and Börker, J.: Compiling and mapping global permeability of the unconsolidated and consolidated Earth: GLobal HYdrogeology MaPS 2.0 (GL-HYMPS 2.0), Geophysical Research Letters, 45, 1897–1904, https://doi.org/10.1002/2017GL075860, 2018.
- Janetti, E. B., Guadagnini, L., Riva, M., and Guadagnini, A.: Global sensitivity analyses of multiple conceptual models with uncertain parameters driving groundwater flow in a regional-scale sedimentary aquifer, Journal of Hydrology, 574, 544 – 556, https://doi.org/10.1016/j.jhydrol.2019.04.035, 2019.
- Keune, J., Gasper, F., Goergen, K., Hense, A., Shrestha, P., Sulis, M., and Kollet, S.: Studying the influence of groundwater representations on land surface-atmosphere feedbacks during the European heat wave in 2003, Journal of Geophysical Research: Atmospheres, 121, 13,301–13,325, 105 https://doi.org/10.1002/2016JD025426, 2016.
- Koirala, S., Kim, H., Hirabayashi, Y., Kanae, S., and Oki, T.: Sensitivity of global hydrological simulations to groundwater capillary flux parameterizations, Water Resources Research, 54, https://doi.org/10.1029/2018WR023434, 2018.
- Konikow, L. F.: Contribution of global groundwater depletion since 1900 to sea-level rise, Geophysical Research Letters, 38, https://doi.org/10.1029/2011GL048604, 2011.
- Lloyd, S.: Least squares quantization in PCM, IEEE Transactions on Information Theory, 28, 129–137, 115 https://doi.org/10.1109/TIT.1982.1056489, 1982.
- Maxwell, R. M., Condon, L. E., and Kollet, S. J.: A highresolution simulation of groundwater and surface water over

2015.

Robert Reinecke: Sensitivity of simulated global groundwater

most of the continental US with the integrated hydrologic model ParFlow v3, Geoscientific Model Development, 8, 923–937, https://doi.org/10.5194/gmd-8-923-2015, 2015.

- Miguez-Macho, G., Fan, Y., Weaver, C. P., Walko, R., and
 Robock, A.: Incorporating water table dynamics in climate modeling: 2. Formulation, validation, and soil moisture simulation, Journal of Geophysical Research: Atmospheres, 112,
- https://doi.org/10.1029/2006JD008112, 2007. Morel-Seytoux, H. J., Miller, C. D., Miracapillo, C., and Mehl,
- S.: River seepage conductance in large-scale regional studies, Groundwater, 55, 399–407, https://doi.org/10.1111/gwat.12491, 2017.
- Morris, M. D.: Factorial sampling plans for preliminary computational experiments, Technometrics, 33, 161–174, https://doi.org/10.1080/00401706.1991.10484804, 1991.
- Müller Schmied, H., Eisner, S., Franz, D., Wattenbach, M., Portmann, F. T., Flörke, M., and Döll, P.: Sensitivity of simulated global-scale freshwater fluxes and storages to input data, hydrological model structure, human water use and calibration, Hydrology and Earth System Sciences, 18, 3511–3538,
- https://doi.org/10.5194/hess-18-3511-2014, 2014.
- Müller Schmied, H., Adam, L., Eisner, S., Fink, G., Flörke, M., Kim, H., Oki, T., Portmann, F. T., Reinecke, R., Riedel, C., et al.: Variations of global and continental water balance compo-
- nents as impacted by climate forcing uncertainty and human water use, Hydrology and Earth System Sciences, 20, 2877–2898, https://doi.org/10.5194/hess-20-2877-2016, 2016.
- Pianosi, F., Beven, K., Freer, J., Hall, J. W., Rougier, J., Stephenson, D. B., and Wagener, T.: Sensitivity analysis of envi-
- 30 ronmental models: A systematic review with practical workflow, Environmental Modelling & Software, 79, 214–232, https://doi.org/10.1016/j.envsoft.2016.02.008, 2016.
- Razavi, S. and Gupta, H. V.: What do we mean by sensitivity analysis? The need for comprehensive characteriza-
- tion of "global" sensitivity in Earth and Environmental systems models, Water Resources Research, 51, 3070–3092, https://doi.org/10.1002/2014WR016527, 2015.
- Reinecke, R.: G³M-f a global gradient-based ground-water modelling framework, JOSS, 3, 548,
 https://doi.org/10.21105/joss.00548, 2018.
- Reinecke, R., Foglia, L., Mehl, S., Trautmann, T., Cáceres, D., and Döll, P.: Challenges in developing a global gradient-based groundwater model (G³M v1.0) for the integration into a global hydrological model, Geoscientific Model Development, 12, 2401–2418, https://doi.org/10.5194/gmd-12-2401-2019, 2019.
- Ruano, M., Ribes, J., Seco, A., and Ferrer, J.: An improved sampling strategy based on trajectory design for application of the Morris method to systems with many input factors, Environmental Modelling & Software, 37, 103 109, https://doi.org/10.1016/j.envsoft.2012.03.008, 2012.
- Saltelli, A., Ratto, M., Andres, T., Campolongo, F., Cariboni, J., Gatelli, D., Saisana, M., and Tarantola, S.: Global sensitivity analysis: the primer, John Wiley & Sons, 2008.
- Scanlon, B. R., Faunt, C. C., Longuevergne, L., Reedy,
- R. C., Alley, W. M., McGuire, V. L., and McMahon, P. B.: Groundwater depletion and sustainability of irrigation in the US High Plains and Central Valley, Proceedings of the National Academy of Sciences, 109, 9320–9325, https://doi.org/10.1073/pnas.1200311109, 2012.

- Schumacher, M., Eicker, A., Kusche, J., Schmied, H. M., and Döll, 60
 P.: Covariance analysis and sensitivity studies for GRACE assimilation into WGHM, in: IAG 150 Years, pp. 241–247, Springer, https://doi.org/10.1007/1345_2015_119, 2015.
- Sobol, I. M.: Sensitivity estimates for nonlinear mathematical models, Mathematical Modelling and Computational Experiments, 1, 65 407–414, 1993.
- Song, X., Zhang, J., Zhan, C., Xuan, Y., Ye, M., and Xu, C.: Global sensitivity analysis in hydrological modeling: Review of concepts, methods, theoretical framework, and applications, Journal of Hydrology, 523, 739 – 757, 70 https://doi.org/10.1016/j.jhydrol.2015.02.013, 2015.
- Stonestrom, D. A.: Ground-water recharge in the arid and semiarid southwestern United States, 1703, USGS, http://pubs.usgs.gov/ pp/pp1703, 2007.
- Taylor, R. G., Scanlon, B., Döll, P., Rodell, M., Van Beek, R., Wada, 75
 Y., Longuevergne, L., Leblanc, M., Famiglietti, J. S., Edmunds, M., et al.: Ground water and climate change, Nature Climate Change, 3, 322, https://doi.org/10.1038/nclimate1744, 2013.
- Vanrolleghem, P. A., Mannina, G., Cosenza, A., and Neumann, M. B.: Global sensitivity analysis for urban water quality ⁸⁰ modelling: Terminology, convergence and comparison of different methods, Journal of Hydrology, 522, 339 – 352, https://doi.org/https://doi.org/10.1016/j.jhydrol.2014.12.056, 2015.
- Verzano, K., Bärlund, I., Flörke, M., Lehner, B., Kynast, E., 85 Voß, F., and Alcamo, J.: Modeling variable river flow velocity on continental scale: Current situation and climate change impacts in Europe, Journal of hydrology, 424, 238–251, https://doi.org/10.1016/j.jhydrol.2012.01.005, 2012.
- Wada, Y.: Modeling Groundwater Depletion at Regional and Global scales: Present State and Future Prospects, Surveys in Geophysics, 37, 419–451, https://doi.org/10.1007/s10712-015-9347-x, 2016.
- Wada, Y., Beek, L. P. H., and Bierkens, M. F. P.: Nonsustainable groundwater sustaining irrigation: A 95 global assessment, Water Resources Research, 48, https://doi.org/10.1029/2011WR010562, 2012.
- Wada, Y., Wisser, D., and Bierkens, M. F. P.: Global modeling of withdrawal, allocation and consumptive use of surface water and groundwater resources, Earth System Dynamics, 5, 15–40, 100 https://doi.org/10.5194/esd-5-15-2014, 2014.