1	Crossing hydrological and geochemical modeling to understand the spatiotemporal variability
2	of water chemistry in an elementary watershed (Strengbach, France)
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#### Abstract

Understanding the spatiotemporal variability of the chemical composition of surface waters is a major issue for the scientific community, especially given the prospect of significant environmental changes over the next decades. To date, the study of concentration-discharge relationships has been widely used to assess the spatiotemporal variability of the water chemistry over watersheds. However, the lack of independent estimations of water transit times within catchments limits our ability to model and predict the water chemistry by relying upon geochemical approaches only. This study shows the potential of coupling hydrological and hydrogeochemical modeling to better understand the spatiotemporal variability of the composition of surface waters. In a first step, a dimensionally reduced hydrological model coupling surface flow with subsurface flow (i.e., the Normally Integrated Hydrological Model, NIHM) has been used to constrain the distribution of the flow lines that are feeding the springs. In a second step, hydrogeochemical simulations with the code KIRMAT (KInectic Reaction and MAss Transport) have been performed to calculate the evolution of the water chemistry along the flow lines. The results indicate that the concentrations of dissolved silica (H<sub>4</sub>SiO<sub>4</sub>) and basic cations (Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup>, and Ca<sup>2+</sup>) in the spring waters are correctly reproduced with a simple integration along the flow lines. The water chemistry and clay mass fractions are also correctly captured when clays are handled as solid solutions. The weak variabilities over time in the spatial flow distribution and water velocities render mean transit time of waters that span the narrow range of 1.5 to 3 months in the watershed. These findings indicate that the chemostatic behavior of the spring chemistry is a direct consequence of the strong hydrological control exerted on water transit times within the catchment. The good matching between the measured and modeled concentrations while respecting durations of water-rock interactions provided by hydrological simulations also shows that the chemical composition of waters can be captured by relying upon simply determined reactive surfaces and experimental kinetic constants. These results reinforce the idea that the low surfaces (< 1 m²/g) calculated from the geometrical shapes of primary minerals are valuable estimates of the reactive surfaces within natural environments. The originality of this study is to cross hydrological and geochemical modeling to understand the spatiotemporal variability of hydrogeochemical processes in a mountainous catchment with highly transient hydrological behavior and short water transit times in the subsurface.

#### 1- Introduction

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Understanding the effects of the ongoing climatic changes on the environment is a major issue for the coming years. The global increase of temperature is expected to affect the hydrological cycle at a large scale, and providing a precise estimation of its repercussion on the evolution of soils and on the chemistry of waters remains challenging. This challenge is associated with the diversity of hydrological, geochemical, biological processes, and their coupling, that operate over continental land surfaces (e.g., Gislason et al., 2009; Goddéris et al., 2013; Beaulieu et al., 2012; 2016). Up to now, the study of concentration-discharge relationships has been widely used to assess the coupling between hydrological and geochemical processes at the watershed scale (Kim et al., 2017; Ameli et al., 2017). However, these concentration-discharge relationships are mainly qualitative, and the lack of independent estimates of water transit times limits the ability to model and predict solute mass transfers within catchments. A precise knowledge of the water flow paths and their variability from wet to dry seasons is an important new step to constrain the water transit times within catchments, and then decipher the seasonal fluctuations of the composition of waters. Understanding the variability of water geochemical compositions will require further development of modeling approaches able to combine hydrological and geochemical processes (Kirchner, 2006). Recent efforts in hydrological modeling were conducted to develop spatially distributed approaches that better consider the interplay between surface and subsurface processes (e.g., Gunduz and Aral, 2005; Kampf and Burges, 2007; Camporese et al., 2010). Due to the complexity of flows in the hydrological processes, several modeling approaches are based on the full resolution of the Richards and Saint-Venant equations to correctly describe the interactions between stream, overland and subsurface waters (Kampf and Burges, 2007). These approaches have shown their ability to capture the hydrological functioning of various watersheds, knowing that the full resolution of the Richards and Saint-Venant equations is computationally demanding and faces calibration and parameterization difficulties (Ebel and Loague, 2006; Mirus et al., 2011). Questions have been raised regarding the optimal complexity of the equations that are needed to correctly treat the hydrology of catchments in their surface and subsurface compartments with reasonable computation times (Gunduz and Aral, 2005). Low-dimensional and depth-integrated models have attracted growing interest because they represent an interesting compromise between the system complexity, the calculation efforts, and the quality of results (Pan et al., 2015; Hazenberg et al., 2016; Weill et al., 2013; 2017; Jeannot et al., 2018). These depth-integrated models recently demonstrated their ability to reproduce the results from fully dimensioned approaches in small catchments while reducing computational costs (Pan et al., 2015; Jeannot et al., 2018). Nonetheless, the water transit times calculated from these depth-integrated models are rarely confronted with the water-rock interaction times inferred from hydrogeochemical modeling of water chemistry in watersheds. For its part, the understanding of the hydrogeochemical functioning of the critical zone has been significantly improved by the implementation of reactive-transport processes in geochemical modeling tools (Steefel et al., 2005; Lucas et al., 2010; 2017; Goddéris et al., 2013; Li et al., 2017). These developments allow for considering a variety of processes, such as flow and transport, ion exchanges, biogeochemical reactions, and the interplay between primary mineral dissolution and secondary mineral precipitation (Moore et al., 2012; Lebedeva and Brantley, 2013; Ackerer et al., 2018). Reactive transport models have been used to explore a

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wide variety of scientific issues, including the study of global atmospheric CO<sub>2</sub> consumption by weathering reactions (Goddéris et al., 2013; Li et al., 2014), the formation and evolution of soil and regolith profiles (Maher et al., 2009; Navarre-Sitchler et al., 2009; Lebedeva and Brantley, 2013), and the variability of water quality and chemistry in the environment (Lucas et al., 2010; 2017; Ackerer et al., 2018). However, these approaches usually refer to a simple one-dimensional flow path through a regolith column or along a hill slope to model flow in the system (e.g., Maher et al., 2011; Moore et al., 2012; Lucas et al., 2017; Ackerer et al., 2018). If these approaches are useful to discuss the key processes involved in the regolith formation and the acquisition of the water chemical composition, such one-dimensional transport reactive modeling cannot take into account the diversity or the complexity of the flow trajectories in watersheds; hence, its effects on the water chemistry at the watershed scale.

A new step is therefore necessary for the development of hydrogeochemical modeling approaches that are applicable at the watershed scale and are able to integrate the complexity of the water flows and the diversity of the water-rock interaction processes. Recent efforts have been undertaken in this direction by merging hydrological and geochemical codes, as for example the reactive transport code ParCrunchFlow (Beisman et al., 2015), or the coupled hydrogeochemical code RT-Flux-PIHM (Li et al., 2017). An alternative to solving fully dimensioned problems is given in the present study by considering an original dimensionally-reduced approach, with modest computation times even when applied at the scale of a whole watershed. The approach combines for the first time in this manner the results from a hydrological depth-integrated and spatially distributed model (NIHM) with a reactive transport model (KIRMAT). Such coupling allows for modeling the spatial and temporal distribution of the

flow trajectories and associated flow rates, the weathering reactions, and the evolution of the water chemistry within an elementary watershed. The Strengbach catchment targeted by this study is one of the reference observatories of the French critical zone network (OZCAR, http://www.ozcar-ri.org ), where multidisciplinary studies, including hydrological, geochemical have been performed and geological investigations, since 1986 ("Observatoire Hydrogéochimique de l'Environnement", OHGE; http://ohge.unistra.fr ; El Gh'Mari, 1995; Fichter et al., 1998; Viville et al., 2012; Gangloff et al., 2014; 2016; Pierret et al., 2014; Prunier et al., 2015; Pan et al., 2015; Ackerer et al., 2016; 2018; Beaulieu et al., 2016; Chabaux et al., 2017; Schmitt et al., 2017; 2018; Daval et al., 2018). The method proposed in this work will yield precise knowledge of the water flow paths and their variability from wet to dry seasons, which is an important new step to better constrain the water transit times within catchments and to correctly understand the seasonal fluctuations in water chemistry.

### 2- Site presentation and data acquisition

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The Strengbach catchment is a small watershed (0.8 km²) located in the Vosges Mountains of northeastern France at altitudes between 883 and 1147 masl. Its hydroclimatic characteristics can be found in Viville et al. (2012) or in Pierret et al. (2014). It is marked by a mountainous oceanic climate, with an annual mean temperature of 6 °C and an annual mean rainfall of approximately 1400 mm, with 15 to 20% falling as snow during two to four months per year. The snow cover period is quite variable from year to year, and may not be continuous over the entire winter. The annual mean evapotranspiration is of approximately 600 mm, and the annual mean runoff of approximately 800 mm (in Viville et al., 2012). The watershed is currently covered by a beech and spruce forest. The bedrock is a base-poor Hercynian granite covered by

a 50 to 100 cm-thick acidic and coarse-in-texture soil. The granitic bedrock was fractured and hydrothermally altered, with a stronger degree of hydrothermal overprinting in the northern than the southern part of the catchment (Fichter et al., 1998). The granite was also affected by surface weathering processes during the Quaternary (Ackerer et al., 2016). The porous and uppermost part of the granitic basement constitutes an aquifer from 2 to approximately 10 meters thickness. In the Strengbach watershed, the major floods and high-flow events usually occur during snowmelt periods at the end of the winter season or in the early spring. In contrast, the low-flow periods commonly happen at the end of the summer or during the autumn. Several springs naturally emerge along the slopes (figure 1). The watershed has been equipped with several piezometers and boreholes since 2012, those being located along the slopes on both sides of the watershed (figure 1; Chabaux et al., 2017). Spring waters are regularly collected and analyzed since 2005, with monthly sampling campaigns completed by occasional specific samplings to cover the entire range of water discharges in the system. Piezometer waters have only been collected during specific sampling campaigns over the period 2012-2015, and as for the spring waters, these samplings cover different hydrological conditions from wet to dry periods. The soil solutions are collected with a monthly frequency on the southern slope at a beech plot (named HP) and to the north at a spruce plot (named VP; figure 1; more details are provided in Prunier et al., 2015). For all the collected waters, the concentrations of the major dissolved species and the pH were determined by following the analytical techniques used at LHyGeS (Strasbourg, France) and detailed in Gangloff et al. (2014) and Prunier et al. (2015). Discharges of water from the springs were measured during the sampling campaigns, as were the water levels within the piezometers. The mineralogy and the

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porosity of the bedrock have been studied in detail in previous studies (El Gh'Mari, 1995; Fichter et al., 1998). On the southern part of the catchment, the weakly hydrothermally altered granite (named HPT, figure 1) is mainly composed of quartz (35%), albite (31%), K-feldspar (22%) and biotite (6%). It also contains small amounts of muscovite (3%), anorthite (2%), apatite (0.5%) and clay minerals (0.5%). On the northern part of the catchment, the lithology is more variable, with the presence of gneiss close to the crest lines and the occurrence of hydrothermally altered granite on the rest of the slopes (El Gh'Mari, 1995, figure 1). The hydrological, geochemical and petrological data obtained from these field investigations are the basis of the modeling work presented in this study. More precisely, this study is based on hydrogeochemical data from 2005 to 2015 for waters from four springs of the southern part (CS1, CS2, CS3 and CS4) and one spring of the northern part (RH3) of the watershed. Hydrogeochemical data obtained over the period 2012-2015 for two piezometers (PZ3, PZ5) of the southern part of the watershed are also studied. The complete hydrogeochemical database is available as supplementary material appended to this work (tables EA1 to EA9). The specific chemical data from spring and piezometer waters modeled in this study are reported in table 1.

### 3- Modeling methods

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The modeling developments presented herein are a new step in the efforts undertaken at LHyGeS to constrain the mechanisms controlling the geochemical composition of surface waters and to understand their spatial and temporal variability at the scale of elementary mountainous watersheds (Schaffhauser et al., 2014; Lucas et al., 2017; Ackerer et al., 2018). The main innovation of this work is to couple a spatially distributed hydrological model with a reactive transport model to constrain the spatiotemporal variability of chemical composition of spring

and piezometer waters from the Strengbach watershed. To the best of our knowledge, this is the first time that such a coupling between hydrological and hydrogeochemical modeling approaches has been attempted at the watershed scale. The hydrological model determines the distribution of the water flow lines within the watershed and thus constrains the water transit times for any period (summer or fall droughts, winter or spring floods). Then, the hydrogeochemical model is used to simulate the acquisition and the evolution of the water chemistry along the determined flow lines within the catchment.

## 3-1 Hydrological modeling

To assess the water flows in the watershed, several simulations were performed with the hydrological code NIHM (Normally Integrated Hydrological Model; Pan et al., 2015; Weill et al., 2017; Jeannot et al., 2018). This code is a coupled stream, overland, and depth-integrated subsurface flow model developed at LHyGeS and already tested in the Strengbach watershed (Pan et al., 2015). The stream and overland flows are described by a diffusive-wave equation, and the subsurface flow is handled through an integration (in a direction normal to bedrock) of the unsaturated-saturated flow equation from the bedrock to the soil surface (Weill et al., 2017). Water exchange between the surface and the subsurface compartments are addressed via the hydraulic head differences between the compartments (Jeannot et al., 2018).

Regarding the hydrological simulations, the parameters of the aquifer were adjusted in NIHM through a calibration-validation procedure. Several zones of heterogeneity were defined based on field observations (Ackerer et al., 2016; Chabaux et al., 2017). In each zone, the saturated hydraulic conductivity, the depth of the substratum, and the porosity, were set to uniform

values, but varying from one zone to the other. Other parameters were set to uniform values over the whole catchment (see table 2). The aquifer thickness that was used for the simulations varied from 2 m near the main crests to up to 8 m in the middle of the watershed (figure 2), in agreement with data collected during the recent geological investigations and drilling campaigns undertaken at the catchment (Ackerer et al., 2016; Chabaux et al., 2017). The uniform precipitations over space applied at the surface of the catchment are drawn from data of the rain gauge station located at the highest elevation of the watershed (site PA, figure 1). The hydrological model NIHM was then run on a first time period (year 1996-1997). The model parameters (table 2) were gradually modified within a simple trial and error process to improve the fit between observed and simulated flow rates of the stream at the outlet of the catchment (these flow rates are the only reliable hydrological data informing on surface and subsurface flow at the catchment scale). The quality of fitting was evaluated via the root mean squared error (RMSE) between observations and simulations, and the Kling-Gupta efficiency coefficient (KGE; Gupta et al., 2009). Once the best fit was obtained, the model was then run over another time period (2010-2015) without changing the parameters anymore, and the quality of the fit was re-assessed on this new time period via the RMSE and KGE indicators. Figure 2 shows the result for the 2010-2015 time period. Once the water discharges were correctly reproduced at the outlet, a backtracking approach was used to constrain the origin of subsurface water exiting the system at prescribed locations, and the spatiotemporal variability of the flow lines within the watershed. To back track the water particles, the velocity fields calculated by the NIHM model were inverted in their direction, and the locations of the backtracked particles were saved at each time-step. A daily time-step was used for the backtracking, as a compromise

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between computational efforts and a refined description of the transient velocity fields. A schematic representation of the backtracking approach is given in figure 3. This methodology allows for delineating the flow paths that bring water at a given time and a given location within the catchment. This information is of major interest to determine the origin of the spring and piezometer waters. It is shown at the catchment scale, that flow is mainly driven by gravity in association with the steep slopes of the watershed, the latter being almost evenly drained over its whole surface area (figure 4). For each water sampling area, ten flow lines that bring water to the location of interest were determined (figure 4), together with a few features of the flow lines, including: local velocities, mean velocities, and length of the flow paths. It is worth noting that times calculated along the streamlines correspond to a date, x days before arrival, at which a water particle entered the subsurface or passed at a given location along the streamline. Streamlines calculated via backtracking and reaching sampling sites only consider flow in the subsurface compartment (but there is no diffuse surface flow at the Strengbach catchment except routing via the stream network) and are conditional to an arrival date at a prescribed location. As streamlines are not associated with calculations of water flux values, the time distributions drawn from streamline calculations are only an approximation of the actual transit time distributions. An even weight is given to each calculated time, when an exact distribution should weight each time by the mass of water conveyed.

# 3-2 Hydrogeochemical modeling

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The simulations of the water chemical composition along the flow lines were performed with the hydrogeochemical KIRMAT code (KInectic of Reaction and MAss Transport; Gérard et al., 1998; Lucas et al., 2010; Ngo et al., 2014). KIRMAT is a thermo-kinetic model based on the

Transition State Theory (TST, Eyring, 1935; Murphy and Helgeson, 1987) that simultaneously solves equations describing geochemical reactions and transport mass balance in a 1D-porous medium. The mass transport includes the effects of one-dimensional convection, diffusion and kinematic dispersion. Chemical reactions account for the dissolution of primary minerals and oxido-reduction reactions, in addition to the formation of secondary minerals and clay minerals. The clay fraction is defined as a solid solution made up of a combination of pure clay endmembers. The clay end-members are defined on the basis of X-ray diffraction analyses of clay minerals present in bedrock samples collected in the field (Fichter et al., 1998; Ackerer et al., 2016; 2018). During the hydrogeochemical simulations, the clay solid solution is precipitated at thermodynamic equilibrium and its composition varies over time, depending on the evolution of the water chemistry and the bedrock mineralogy (Ackerer et al., 2018). This multicomponent solid solution reproduces the non-pure composition of clay phases resulting from lowtemperature water-rock interactions (Tardy and Fritz, 1981). The KIRMAT code also accounts for the feedback effects between mineral mass budgets, reactive surfaces, and porosity evolution (Ngo et al., 2014). The reactive surfaces of the primary minerals were calculated by assuming a simple spherical geometry for all the minerals, and the mean size of the minerals was estimated from thin section observations of the bedrock samples. During the simulations, the clay mineral precipitation and the evolution of reactive surfaces of primary minerals are tracked together with chemical processes and water chemical composition. However, in view of the short time scales of transport renderer by the hydrological simulations (weekly to monthly timescale), the change in reactive surfaces of primary minerals became negligible. Precipitation of other secondary minerals such as carbonates, hematite or amorphous silica was tested, but these

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minerals were not formed given the hydroclimatic context of the Strengbach catchment. The secondary mineral precipitation is therefore controlled by the formation of clay minerals. The KIRMAT code has already been applied in geochemical modeling of alluvial groundwaters (Lucas et al., 2010) and surface waters (Lucas et al., 2017; Ackerer et al., 2018).

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For this study, the modeling strategy is adapted from Ackerer et al. (2018) to consider the new transit time and water mixing constrains provided by the hydrological code NIHM. To capture the chemical composition of the spring and the piezometer waters, numerical simulations were performed along the flow lines that were determined through the backtracking approach. A sketch of the hydrogeochemical modeling strategy is provided in figure 5. For each flow line, several KIRMAT simulations were performed with different starting positions along the active part of the line. The starting positions represent the locations at which the soil solutions percolate through the subsurface shallow aquifer. These variable starting positions are spaced with a constant distance along the flow line. The deepest soil solutions collected to the south of the catchment at the beech plot (HP) and to the north at the spruce plot (VP) were assumed representative of the soil solutions for the whole southern and northern slopes of the catchment, respectively. The data of the soil solution chemistry used in this study are available in Prunier et al. (2015) and in supplementary tables (tables EA6 and EA7). These soil solutions aggregate the effects of the various surface processes occurring before percolation into the bedrock. As the soil solution evolutions over time are monitored and injected as such into the modeled aquifer, the temporal variability of the soil solution chemistry and its repercussion on the water-rock interactions along the flow paths are taken into account by the modeling approach. Data related to the bedrock properties, such as the mineralogical compositions, the

mineral reactive surfaces, and the kinetic constants of dissolution reactions, are given in Ackerer et al. (2018) and in supplementary tables (tables EA10 to EA13). By following this strategy, the simulations that consider soil solutions percolating at the upper part of the catchment reflect the chemical evolution of waters with long path lengths and long transit times within the aquifer. By contrast, shorter path lengths and shorter transit times are associated with the percolation of soil solutions that occurs in the vicinity of the sampling locations (figure 5). Because the springs or the piezometers collect waters from different origins and with contrasted transit times, integration along each water flow line was performed. The aim of the integration is to determine the mean chemical composition resulting from the mixing of the waters characterized by variable transit times (figure 5). The integrated chemical composition of the waters provided by a given flow line is calculated by taking the arithmetic mean of the solute concentrations calculated by the succession of the KIRMAT simulations along the flow line (figure 5). This arithmetic mean reflects a simple full mixing of uniform water fluxes irrespective of their short or long transit times. In other words, the geochemical simulations are based on the hypothesis of spatially homogenous water-rock interactions within the watershed. The soil solutions are assumed to percolate uniformly within the aquifer and are then conveyed along the slopes by uniformly distributed mass of water until reaching the sampling locations.

### 4- Hydrological modeling results

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## 4-1 Spatial variability of the flow lines

The results provided by the hydrological code NIHM show that to first order, the Strengbach catchment is well drained and that the topography exerts an important control on the flow line

distribution (figure 4). Along the hillsides with uniform or slightly convex slopes, the water flow lines show simple characteristics. The flow paths are nearly parallel, and the water velocities are similar along the different flow lines on this type of hillside. The water velocities tend to increase when moving downstream (longer traveled distances for a given transit duration, figure 4), with slower velocities near the main crests and higher velocities on the steepest parts of the hillsides. The waters collected along this type of hillside are therefore characterized by small variability of transit times. This is the case for the CS1, CS3 and RH3 spring waters located on the southern and northern parts of the catchment (figure 4). This is also the case for the piezometers PZ3 and PZ5 in the southern part of the watershed (figure 4). For the samplings located on uniform or slightly convex slopes (CS1, CS3, RH3, PZ3 and PZ5), the characteristics of the different flow lines that feed each site are therefore comparable for a given site and for a given date. By contrast, in the vicinity of the valley and in the topographic depressions, the hydrological modeling indicates that the flow line characteristics are more variable. Because flow lines coming from different hillsides can feed a topographic depression, the mixing of different flow lines with variable flow paths and contrasting water velocities can occur at these locations. The waters collected in valleys or in topographic depressions are therefore characterized by a higher variability of transit times. This is the case for the CS2 and CS4 springs, which are located in a depression in the axe of the small valley and surrounded by slopes with various orientations and a complex flow line distribution (figure 4). For these two springs, the characteristics of the different flow lines can be different for a given date.

## 4-2 Temporal variability of the flow lines

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Hydrological modeling under general transient conditions can render the evolution over time of water flows in the Strengbach watershed but also of other hydraulic variables or parameters. As an example, after an important rainfall event (30/03/2010, in figure 6), snapshots of the average hydraulic conductivity in the subsurface show increasing values with decreasing elevation in the watershed. The same observation holds for hydraulic conductivity during drought periods (see 29/11/2011, in figure 6). Provided that the hydraulic head gradient is largely dominated by the topography and therefore almost constant over time (figure 6), the water velocities are increasing along the flow lines from crests to valleys, irrespective of the wet versus dry hydrological periods. For the CS1 spring, the mean flow velocities along the flow lines vary from approximately 1 m/day to 7 m/day between the severe drought of 29/11/2011 and the strong flood of 30/03/2010 (figures 7A and 7B). These events correspond to the annual maximum and minimum observed flow rates of the stream at the outlet of the Strengbach watershed. For the same dates, the mean velocities vary from 2 - 12 m/day, 1 - 4 m/day and 1 - 9 m/day for the springs CS2, CS3 and CS4, respectively. The variations from drought to flood are very similar for the piezometer waters, with velocities in the ranges 2 - 10 m/day and 2 - 12 m/day for the PZ3 and PZ5 piezometers, respectively. The RH3 spring located on a steeper part of the northern slopes exhibits flow velocity variations from 5 to 20 m/day from dry to flood conditions. In addition to the flow velocity variations, the hydrological simulations also reveal variability in the lengths of the active parts of the flow lines. Such variability is triggered by the particular seasonal variations of the hydraulic conductivities within the catchment. During periods of drought, the simulations indicate a strong decrease of hydraulic conductivities close to the main crests and much smaller variations at mid-slopes (figure 6). The crests rapidly dry out, whereas

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the areas at mid-slopes still supply some water to the stream network. These contrasting hydrological behaviors result from the differences in aquifer thickness and water storage between the crests and the other parts of the catchment (figure 2). A thin aquifer, flow divergence and the absence of feeding areas prevent large water storage on the crests, in opposition to mid-slope parts with much thicker aquifers and the presence of feeding areas upstream. This particular pattern simulated for the hydraulic conductivities implies that the active parts of the flow lines extend up the main crests during important floods, whereas they are limited to mid-slopes after a long dry period. The consequence of this hydrological functioning is to moderate the seasonal variations of the transit times of waters, as the active lengths of flow lines vary simultaneously with water flow rates. Calculations indicate that for the spring and piezometer waters collected in this study, the mean transit times of waters only vary from approximately 1.75 to 4 months between the strongest flood and the driest conditions. These short subsurface water transit times are explained by the small size of the catchment and gravity driven flow along steep slopes.

### 5- Hydrogeochemical modeling results

Modeling the geochemical composition of waters from the different springs and piezometers selected for this study was performed following the procedure described in paragraph 3-2. The results are presented below by grouping sources and piezometers according to their hydrogeological characteristics.

### 5-1 CS1 and CS3 springs (southern slope)

The CS1 and CS3 springs emerge on the same slope and drain the same rocks. Their hydrological behavior is also very similar in terms of flow lines and water transit times. The interesting consequence of the simple flow line distribution for these springs is that a single flow line can be considered as representative of all the flow lines that are feeding the spring, irrespective of the hydrological conditions. Hydrogeochemical simulations were performed along a single flow line for different hydrological periods using the methodology illustrated in figure 5. The case of CS1 spring is used below to highlight the main results obtained from this approach. For the strong flood of 30/03/2010, the KIRMAT simulations modeling the waters coming from the proximity of the spring and characterized by short transit times produced too much diluted solutions, whereas the waters coming from the main crests are too much concentrated to reproduce the spring water chemical composition. However, after an integration of all the waters arriving at CS1 with the different transit times employed for the simulation, the resulting geochemical composition correctly reproduces the chemical composition of CS1 spring water at this date (H<sub>4</sub>SiO<sub>4</sub>, Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup>, and Ca<sup>2+</sup> concentrations, figure 7D). A similar conclusion is obtained for the important drought of 29/11/2011. Again, geochemical integration of all the waters arriving at CS1 along a water line but with different transit times correctly reproduces the chemical composition of the CS1 spring waters collected on this date (figure 7C). This is actually the case regardless of the time period considered. The coupled hydrological and hydrogeochemical approach has been applied for the CS1 spring for 6 dates covering the whole range of the water discharges of the spring (table 1). The modeling results reveal the seasonal variations of the water chemical composition of the CS1 spring over the whole range of observed flow rates at CS1 (figure 8). Simulations especially account for the 20-30% variation in H<sub>4</sub>SiO<sub>4</sub> concentrations,

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the 10-20% variation in Na<sup>+</sup> concentrations, and the relatively stability of the pH of the CS1 waters (figures 8A, 8C, 8D). The response in concentration of each chemical element to a change in water discharge is associated with the initial soil solution concentrations, the nature of primary minerals leached by water, and the degree of its incorporation into the clay solid solutions. For example, Na is only provided by a single primary mineral (albite) and is weakly incorporated into clays. Si is provided by several primary minerals (albite, biotite, K-feldspar, ...) and strongly incorporated in clays that are characterized by varying precipitation rates with hydrological conditions. These points explain why the response of solute concentrations to hydrological changes is variable for each element. Similar results are obtained for the CS3 spring (figure EA1), showing, as for the CS1 spring, that the proposed modeling approach is able to correctly capture the water chemical composition of the CS3 spring.

### 5-2 PZ3 and PZ5 piezometers (southern slope)

The two piezometers PZ3 and PZ5 are located on the southern part of the catchment, and their waters drain granitic bedrock similar to that drained by the CS sources. As for the CS1 and CS3 springs, the NIHM modeling results show that the flow lines arriving at the PZ3 piezometer are characterized by a relatively simple distribution. The flow lines are close to each other, and they render similar water velocities on the slopes (figure 4). For the PZ5 piezometer located downstream, the flow lines cover a larger area on the slope, especially during droughts (figure 4). However, for a given date, all the flow lines show similar velocities, with particularly fast flows on a lower portion of the hillslope. These results imply that, as for the CS1 and CS3 springs, the hydrogeochemical simulations of PZ3 and PZ5 piezometer waters can be performed by relying upon a single flow line representative of all the waters collected by the piezometers

on a given date. The geochemical integration along the flow line has been performed in the same manner as detailed above, and this approach is able to reproduce the chemical composition of the waters of the two piezometers, as illustrated in figure 9 for the flood of the 05/05/2015 and in figure EA2 for the dry conditions of 10/11/2015. Together, these modeling results show that the linear or slightly convex slopes on the southern part of the catchment allow to correctly capture the water chemistry of each sampling site with a straightforward integration along a single and representative flow line.

## 5-3 The CS2 and CS4 springs (in the valley axe)

CS2 and CS4 spring waters drain the same granitic bedrock as the CS1 and CS3 waters, but are located in the axe of the small valley of the Strengbach stream and surrounded by slopes of various orientations and inclinations (figure 4). Consequently, the distribution of the flow lines is much more scattered than for the CS1 and CS3 springs. The modeling strategy applied for these two springs and the results are detailed below for the CS2 spring. For this spring, and for all the hydrological conditions, two different groups of flow lines have been determined by the backtracking approach: a northern group characterized by relatively slow velocities and a southern group with higher velocities (figure 4). When the hydrological conditions vary from a strong flood (30/03/2010) to an important drought (29/11/2011), the flow rates tend to decrease along all the flow lines (figures 10A and 10B). For example, the mean flow velocities along the flow lines vary from approximately 12 m/day to 2 m/day between these two dates. However, for a given date, the northern group systematically renders slower velocities than the southern group. This scattered distribution of the flow lines implies that a single specific flow line cannot be representative of all the waters collected by the spring. The flow lines calculated

using the NIHM model allow for constraining the trajectories of the waters within the watershed; however, the simulations performed in this study cannot provide the mass fluxes of water carried by each flow line. Consequently, a straightforward calculation of the chemistry of the CS2 spring, such as detailed above for CS1, is not applicable because the mixing proportions between the different flow lines are unknown. Alternatively, it is possible to determine the concentrations in the waters carried by the slowest and the fastest flow lines that are feeding the spring and to compare the results with the observed chemistry of the spring water. The results indicate that for all the hydrological conditions, the concentrations calculated from the geochemical integration along the slowest and the fastest flow lines are able to correctly frame the chemical composition in terms of H<sub>4</sub>SiO<sub>4</sub>, Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup>, and Ca<sup>2+</sup> of the CS2 spring waters (results are presented for H<sub>4</sub>SiO<sub>4</sub> and Na<sup>+</sup> in figures 10C and 10D). The observed chemistry of the CS2 spring is bounded by the chemical compositions of the waters carried by the slowest and fastest flow lines. The modeling results also suggest that the contributions of the slow and fast flow lines are comparable over most of the hydrological conditions, as the observed concentrations are in general at the midpoint between the min (i.e., fast) and max (i.e., slow) boundaries (see figures 10C and 10D). It is only for the important droughts that the spring chemistry seems to be mainly controlled by the southern and faster group of flow lines. Further works to precisely estimate the mass fluxes of water carried by each flow line are necessary to calculate the chemistry of the CS2 spring water with a weighted mixing calculation. The same conclusions apply to the CS4 spring located in the proximity of CS2 spring.

# 5-4 The RH3 spring (northern slope)

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The RH3 spring is located on the northern part of the catchment (figure 4), where steep slopes imply fast water velocities and subparallel flow lines. However, if the distribution of the flow lines on the RH3 hillside is simple (as for the CS1 and CS3 springs) the precise lithological nature of the bedrock drained by the RH3 waters is more difficult to constrain (see also Ackerer et al., 2018). Unlike the southern slope, the bedrock of the northern part of the catchment exhibits a complex lithology, with gneiss outcropping in the upper part of the slope and granite of variable degree of hydrothermal overprinting in the intermediate and lower parts. These lithological variations can explain the differences in chemical composition between the RH3 spring waters and the waters of the southern part of the catchment: the RH3 spring waters are characterized by systematically higher concentrations of K<sup>+</sup> and Mg<sup>2+</sup> cations but show similar concentrations for the other major elements (Ackerer et al., 2018; Pierret et al., 2014). The vertical extension of the gneiss formation and the spatial variability of the hydrothermal overprinting along the northern slopes of the catchment are not very well known, which renders impossible the straightforward modeling of the RH3 spring water composition, as it was done for the CS1 and CS3 sources. Alternatively, simulations of two extreme cases can be performed by assuming that the flow lines only run, either on gneiss or on hydrothermally altered granite. When only considering the hydrothermally altered granite (VS facies), the simulated concentrations of  $H_4SiO_4$  and  $Na^+$  are close to the measured ones. However, the concentrations of  $K^+$  and especially Mg<sup>2+</sup> are clearly underestimated (figure 11B). In the case of the flow lines only running on gneiss (GN facies), the simulated concentrations of H<sub>4</sub>SiO<sub>4</sub> and Na<sup>+</sup> also match the data. However, due to the higher abundance of biotite in the gneiss, the simulated concentrations of K<sup>+</sup> and Mg<sup>2+</sup> are higher than the measured ones (figure 11A). At this stage, it is

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therefore reasonable to propose that the chemical composition of the RH3 spring waters reflects mixing of the two lithological influences. By assuming a geochemical conservative mixing, which is likely a too simplistic scenario, the results would indicate that the flow lines portions running on gneiss and on hydrothermally altered granite count for approximately 40-50% and 50-60% of the total water path length, respectively. Further works to estimate the location of the contact between gneiss and granite are required for more realistic modeling and hence a deeper interpretation of the chemical composition of RH3 spring waters. In any case, the important point to stress here based on the above simulations is that the complex lithology and bedrock heterogeneity mainly impact the K<sup>+</sup> and the Mg<sup>2+</sup> budget of the RH3 waters, but not or only slightly the H<sub>4</sub>SiO<sub>4</sub> and Na<sup>+</sup> concentrations, which control the main part of global weathering fluxes carried by the Strengbach spring waters. These results readily explain why although the RH3 spring waters exhibits higher Mg<sup>2+</sup> and K<sup>+</sup> concentrations than the other CS springs, they carry relatively similar global weathering fluxes (Viville et al., 2012; Ackerer et al., 2018).

### 6- Discussion

The modeling approach proposed in this study and based on the coupling of the NIHM and KIRMAT codes, allows for building a better modeling scheme than those commonly used in previous studies regarding the hydrogeochemical modeling of surface waters at the watershed scale. In such previous works, the geochemical simulations were performed mainly along a single 1D flow line, only characterized by homogeneous mean hydrological properties (Goddéris et al., 2006; Maher et al., 2011; Moore et al., 2012; Lucas et al., 2017; Ackerer et al., 2018). In the previous study on the Strengbach watershed (Ackerer et al., 2018), the soil solutions were

also assumed to percolate in the bedrock only at a single starting point of the flow lines. Although these previous approaches were useful for determining the long-term evolution of regolith profiles and/or the mean chemistry of waters at the multiyear scale, they cannot be used to discuss the seasonal variations of the water chemical composition. The NIHM-KIRMAT coupling approach makes this possible, as it provides the spatial distribution of the flow lines at the watershed scale and their variations over time. Furthermore, the proposed modeling approach also integrates a soil solution percolation scheme with inlets uniformly distributed along the slope, which is more realistic than a scheme assuming that each sampled site is fed by a single flow line carrying waters with a unique transit time. The consistency of the modeling results with the measured concentrations over the whole range of the hydrological conditions certainly gives weight to the application of the proposed modeling approach to the Strengbach catchment. Such consistency also gives weight to the assumptions made regarding the modeling parameters used in this work, i.e., reactive surfaces and kinetic constants. It also gives weight to the conclusions and implications that can be deduced regarding the hydrogeochemical functioning of the watershed, and the origin of the chemostatic character of these waters. These different points are detailed below.

## 6-1 Choices of the reactive surfaces and the kinetic constants

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For the geochemical simulations performed in this study, the kinetic constants that were used to describe the dissolution reactions of the primary minerals are standard constants determined through laboratory experiments (supplementary table EA12). The reactive surfaces of the primary minerals were calculated by assuming a simple spherical geometry for all the minerals (supplementary table EA10). Such choices might appear surprising as over the last years, several

studies have suggested that the kinetic constants determined through laboratory experiments overestimate the rates of the dissolution reactions in natural environments (White and Brantley, 2003; Zhu, 2005; Moore et al., 2012; Fischer et al., 2014). The origin of this laboratoryfield discrepancy is still a matter of debate (Fischer et al., 2014). Different processes have been proposed to explain the gap between laboratory and field estimates, such as the crystallographic anisotropy (Pollet-Villard et al., 2016), progressive occlusion of the primary minerals by clays (White and Brantley, 2003), or the formation of passivation layers at the surfaces of the minerals (Wild et al., 2016; Daval et al., 2018). The difficulty to reconcile field and laboratory estimates can also be related to the challenge of defining relevant reactive surfaces at different space scales (Li et al., 2006; Navarre-Sitchler and Brantley, 2007). The present modeling work regarding the Strengbach catchment shows that the chemical composition variability of the spring and piezometer waters is fully captured via geometric reactive surfaces and standard kinetic constants, while respecting the water-rock interaction times within the catchment. This result suggests that the mean rates of the weathering reactions employed in this modeling work are realistic, which in turn implies that the modeling approach developed in this study does not underline significant mismatches between field and laboratory reaction rates. More details are given in the following to investigate why geometric reactive surfaces and standard kinetic constants are able to correctly capture the water chemistry. The calculated rates of the dissolution reactions depend on the product between the kinetic constants of the reactions and the mineral reactive surfaces. In the experimental studies performed for determining the kinetic constants of dissolution reactions, the constants are usually determined by normalizing the experimental weathering rates with the Brunauer-

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Emmett-Teller surfaces determined from experiments of gas absorption (BET surfaces; Chou and Wollast, 1986; Lundstrom and Ohman, 1990; Acker and Bricker, 1992; Amrhein and Suarez, 1992; Berger et al., 1994; Guidry and Mackenzie, 2003). In table 3, the BET surfaces are compared with the geometric surfaces of the minerals involved in the dissolution experiments, recalculated from the size ranges of the minerals. For most of the minerals (apatite, quartz, albite, K-feldspar, and anorthite), the geometric surfaces are within the same order of magnitude as the BET surfaces, even if often slightly lower (table 3). However, as the BET surfaces are determined with fairly large uncertainties, especially for low BET surfaces (up to ± 70%), and as they can be very different depending on the gas used (up to 50% of difference between N2 or Kr absorption; Brantley and Mellott, 2000), the above differences between the geometrical and the BET surfaces cannot be considered significant for the majority of minerals used in the Strengbach simulations. A significant difference only appears for biotite, with the geometric surfaces one order of magnitude less than the BET surfaces (table 3). However, for biotite, due to its layered structure, it has been shown that approximately 80 - 90% of the surface area accessible by the gases used to estimate BET surfaces is not accessible for weathering reactions (Nagy, 1995). In the case of biotite, the effective surface area for the water-rock interactions would thus be, in a rather fortuitous manner, a surface area close to the geometric one. The above considerations and observations thus explain why for a granitic bedrock as found in the Strengbach catchment, the geometric surfaces are relevant to describe the surfaces of water-rock interactions at the space and time scales of this study. An immediate corollary is that the values of the standard kinetic constants (table EA12) are also appropriate to calculate reaction rates with mineral geometric surfaces in our modeling approach. This ability

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may be related to the fact that all the minerals that have been used in the dissolution experiments and in the kinetic studies were collected in the field (e.g., Acker and Bricker, 1992; Amrhein and Suarez, 1992). These minerals were likely affected by anisotropy, passivation layers, and any types of aging effects related to long-term water-rock interactions. Our results might therefore mean that the standard kinetic constants obtained in such experiments integrate the aging effects that have affected the reactivity of the primary minerals in natural environments. This would explain why it is possible to capture the full variability of the water chemistry in an elemental catchment with simple geometric reactive surfaces and standard kinetic constants. It is important to emphasize at this stage that the results of our simulation strengthen the idea that the low surfaces calculated from the geometrical shapes of minerals provide good estimates of the reactive surfaces within the natural environment (Brantley and Mellott, 2000; Gautier et al., 2001; White and Brantley, 2003; Zhu, 2005; Li et al., 2017). They are certainly the values to be used for hydrogeochemical modeling such as that performed in this work, in addition to the use of the experimental kinetic constants for mineral dissolution. These conclusions are certainly not specific to the Strengbach catchment and could be applicable to many other granitic catchments.

## 6-2 Implications for the acquisition of the water chemistry

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The results of the NIHM-KIRMAT hydrogeochemical modeling have strong implications regarding the hydrogeochemical functioning of the Strengbach watershed. The NIHM modeling shows that the hydrological functioning of the watershed is correctly simulated by water circulations in the shallow subsurface, i.e., in a saprolitic aquifer. No contribution of waters circulating in the deep fracture network of the granitic bedrock and observed during the drilling

campaigns is necessary. The deep-water circulation pathways are probably disconnected from the shallow subsurface, or with mean hydraulic heads less than those of the subsurface, at least at the Strengbach catchment scale, and does not significantly impact the water budget of the Strengbach catchment. As detailed in section 4-1, the modeling results show that water in the shallow aquifer flows along streamlines with fairly simple geometries. At the scale of the watershed (figure 4), the geometry of the flow lines validates the hypothesis built on the basis of the geochemical and Sr-U isotopic data that the spring waters of these mid-mountain basins (i.e., the Ringelbach and Strengbach watersheds; Schaffhauser et al., 2014; Pierret et al., 2014) are supplied by waters from distinct flow paths without real interconnections. More importantly, the modeling results emphasize the importance of water transit times within the watershed as a main feature controlling the chemical composition of subsurface waters at the Strengbach catchment. Along all the slopes, the waters coming from the proximity of the crests and characterized by a long transit time systematically render higher concentrations than the waters with shorter pathways and transit times. When the hydrological conditions change from wet to dry periods, the solute concentrations also tend to increase with the increase in the mean transit time of waters. Our results demonstrate in particular that for the CS1 source and for the PZ3 and PZ5 piezometers, all located on the southern slope of the watershed, over a homogeneous granitic bedrock, and all characterized by flow lines of fairly simple geometries (section 4), the spatial and temporal variations of their geochemical composition are fully explained by differences in water residence times (figure 12). Residence time variations between high and low discharge periods explain the temporal variations of geochemical signatures within each site, and the differences in mean residence times of waters supplying the

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different sources and piezometers explain the various chemical compositions between the different sites (figure 12). Only the CS2 and CS4 springs, located in a depression, are supplied by two different types of water flow lines, the contribution of which could change over time. However, the mixing of different flow lines has probably a relatively modest impact, and at the scale of the watershed, the results show that the duration of water-rock interaction exerts a first-order control on the chemical composition of waters, in addition to the lithological parameter. This study brings also strong constrains on the spatial repartition of the weathering processes. For the modeling strategy developed in this study, the chemical composition of the spring and piezometer waters are calculated by integrating the chemical composition of waters introduced at different starting positions along the active part of the flow lines (figure 5). In each of the simulations, a fixed distance between the initial positions of the KIRMAT simulations along the flow lines was used. The modeling results show that through the geochemical integration, the concentrated waters coming from the main crests are naturally counterbalanced by the diluted waters infiltrating close to the sampling sites. From flood to drought events, the mean transit times are obviously impacted by the variable velocities along the flow lines, but regardless of the hydrological conditions, it is always possible to explain the water chemistry of the sampling sites with the above integration scheme. Such repeatable consistency between data and simulations indicates that this circulation scheme is certainly quite realistic for the Strengbach catchment. This scheme supports the idea suggested in Ackerer et al. (2016) that at the scale of the watershed, the solute chemistry is acquired through reactions and weathering processes that are spatially relatively homogenous within the watershed.

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### 6-3- Origin of the chemostatic behavior in the Strengbach catchment

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The hydrogeochemical monitoring of the spring, piezometer, and stream waters performed in the Strengbach catchment clearly shows that this catchment has a chemostatic behavior (e.g., Viville et al., 2012; Ackerer et al., 2018; this study). All the spring and the piezometer waters have chemical concentrations impacted by changes in the hydrological conditions, but the concentration variation ranges are by far narrower than variation ranges of water discharges, which define the chemostatic behavior of a hydrological system. For the waters exhibiting the largest concentration variations (spring CS1), a moderate increase of approximately 10-30% in the concentrations of H4SiO4 and Na+ is observed from floods to severe drought events, while the water discharges may vary by a factor of 15 (figures 8A and 8C). This weak variability of the solute concentrations over a wide range of water discharges is not specific to the Strengbach catchment; it has rather been observed in several watersheds spanning different climates and hydrological contexts (Godsey et al., 2009; Clow and Mast, 2010; Kim et al., 2017). Different origins for the chemostatic behavior have been proposed, such as a modification of the mineral reactive surfaces during changing hydrological conditions (Clow and Mast, 2010), a small concentration difference between slow and fast moving waters (Kim et al., 2017), or the fact of reaching an equilibrium concentration along the water pathway (Maher, 2010). To date, the study of concentration-discharge relationships has been intensively used to assess the chemostatic behavior of waters (Godsey et al., 2009; Kim et al., 2017; Ameli et al., 2017). However, the lack of precise estimates of water transit times limits the ability to clearly discuss the origin of the chemostatic behavior on the single basis of the concentration-discharge relationships. The coupled approach presented in this study offers a renewed opportunity to discuss the origin of the chemostatic behavior in catchments because the acquisition and the evolution of the water chemistry can be simulated along flow lines determined via timely and spatially distributed hydrological modeling. The strength of this approach is to constrain water transit times independently and before any geochemical simulation.

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The results from the hydrological model show that the characteristics of the flow lines are affected by the changes in the hydrological conditions. After important precipitations, high water contents and large hydraulic conductivities (as the local mean value integrated over the aquifer thickness including the vadose and saturated zones) are simulated in the vicinity of the crests and all along the small valley of the catchment (figure 6). During drought periods, the crest lines have progressively dried out, and the hydraulic conductivities strongly decrease on the upper parts of the watershed. Only some locations at mid-slopes and along the direction of the principal valley exhibit modest hydraulic conductivities (figure 6). This response of the hydraulic conductivities implies that during floods, the water velocity significantly increases along the flow lines, but the length of the active parts of the flow lines also increase as waters collected downstream may also come from the neighborhood of the main crests. During drought periods, the water velocity is slower, but the length of the active parts of the flow lines also tends to decrease, as the waters are principally supplied by mid-slope areas characterized by a thicker aguifer. For illustration, and for the CS1 spring, the water velocities varied along the flow lines between 7 and 0.5 m/day during the flood of 30/03/2010 and were approximately 0.5-1 m/day during the important drought of the 29/11/2011 (figure 6). At the same time, the active parts of the flow lines were reduced from 160 m to 110 m from the flood to the drought events (figures 7A and 7B). This hydrological functioning implies that the water velocities along the flow lines and the active lengths of the flow lines vary in opposite manners from drought to flood events. This hydrological behavior buffers the variations of the water transit times over changing hydrological conditions and explains why the mean transit times span much narrower variation ranges than the discharges of water at the collected springs. For example, the calculated mean transit times of waters for the CS1 spring vary from 1.75 to 3.13 months between the strongest flood and the driest period that have been studied, whereas the water discharges vary from 1.523 L/s to 0.098 L/s (figure 8B). Because the time of the water-rock interactions exerts a first-order control on the chemical composition of waters, the modest variability of the mean transit times is directly responsible for the relative stability of the chemical composition of waters within the catchment.

It is worth noting that the hydrological modeling with the NIHM code is performed independently and before any geochemical simulation with the KIRMAT code. The fact that the flow rates are well reproduced for all the hydrological contexts between 2010 and 2015 supports the idea that water transit times inferred with NIHM are realistic. With chemical composition of waters well captured by simulations, the combination of the geochemical parameters used in KIRMAT renders realistic reaction rates, as chemistry is well reproduced while respecting water transit times. No modifications of the reactive surfaces and of the dissolution kinetic constants were necessary to reproduce the seasonal variability of the water chemistry. It is also important to emphasize that the simulated chemical compositions of waters remain far from a state of chemical equilibrium with respect to primary minerals. The calculated Gibbs free energy for the primary minerals ranges from -120 to -100 kJ/mol for apatite, -90 to -80 kJ/mol for biotite and anorthite and -30 to -20 kJ/mol for albite and K-feldspar. These far-

from-equilibrium values for the Gibbs free energy imply that the reaction rates calculated using hydrogeochemical codes such as KIRMAT, which are based on the transient state theory (TST, Eyring, 1935; Murphy and Helgeson, 1987), are realistic for most of the primary minerals in this type of hydrological context. Regarding the simulations performed in this study, the relatively short residence times of waters and the precipitation of clay minerals prevent reaching a state of chemical equilibrium between waters and primary minerals. The results also indicate that introducing a clay solid solution in the geochemical system is a good way to capture the clay mineral dynamics, with a solid solution precipitated at thermodynamic equilibrium able to generate reliable water chemistry (this study) and realistic clay precipitation rates (more detail in Ackerer et al., 2018). Further development could consider a more precise approach to the formation of the clay phases but would imply to simulate a kinetically-controlled nucleation and growth of clay particles (Fritz et al., 2009, Noguera et al., 2011). Further comparisons facing the results from the hydrological modeling with water isotope variability could also be interesting to discuss the accuracy of the water transit times inferred by simulations. Taken together, the results of this study show that the solute concentrations are not limited by a chemical equilibrium; they simply are weakly variable over time because of the short and moderately variable water residence times in the watershed. The chemostatic behavior of the surface and the shallow subsurface waters is therefore only due to a strong hydrological control of the water transit times within the watershed. This conclusion could probably extend to other mountainous and relatively steep watersheds, in which water pathways and short transit times are mainly controlled by gravity driven flow along slopes.

#### 7- Conclusion

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This study emphasizes the potential of coupling low-dimensional and depth-integrated hydrological modeling with hydrogeochemical modeling as a way to better understand variability over time and space of the composition of surface and subsurface waters. The independent estimation of the water transit times provided by hydrological simulations is a clear added value to constrain the geochemical modeling approaches. This study shows that the durations of water-rock interactions exert a first-order control on the chemical composition of waters and that the acquisition of the water chemistry can be explained by weathering processes that are spatially fairly homogeneous over the catchment. The hydrological functioning of the watershed also indicates that the chemostatic behavior of the water chemistry is a direct consequence of the strong control exerted by hydrological processes on water transit times. The variations in flow lines distributions from drought to flood events result in a moderate seasonal variability of mean water transit times, which in turn explains the relative stability of the solute concentrations in waters. The consistency between measured and modeled concentrations while respecting the water-rock interaction times provided by the hydrological simulations shows that it is possible to capture the chemical composition of waters with simply determined reactive surfaces and standard kinetic constants. The results of our simulations strengthen the idea that the low surfaces calculated from the geometrical shapes of minerals are a good estimate of the reactive surfaces within the natural environment and certainly the values to be used for hydrogeochemical modeling such as that performed in this work, in addition to the use of the experimental kinetic constants for mineral dissolution.

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## Figure captions

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Figure 1: sampling locations within the Strengbach catchment. Blue stars represent springs, blue diamonds represent piezometers, and the blue circle represents the stream at the outlet of the watershed. Green circles represent soil solution locations, and black diamonds represent bedrock facies locations. Figure 2: on the left: field of thicknesses of the weathered material constituting the shallow unconfined aguifer at the Strengbach catchment used for the simulations of NIHM. The 1D surface draining network used in NIHM is represented by the black lines. On the right: fitting observed flow rates from the Strengbach stream at the outlet of the catchment with simulations of flow within the watershed (illustrated from 2010 to 2015). The subsurface compartment inherits from the aquifer thicknesses reported in the left panel, and the topography makes the natural outlet of the subsurface compartment the surface draining network. Figure 3: principle of the method of backtracking used to determine flow lines that generate flow at the outlet of the Strengbach catchment. Particles are dispatched along the dry fraction of the 1D river network (only one is represented here at a position  $\alpha$  on 01/01/2010 at 23:59). NIHM generates an output heterogeneous velocity field at that date for the whole watershed, denoted  $V_{01/01/2010}$ . By applying a velocity field of the same magnitude but opposite direction to the particle, the position of the particle can be backtracked until 31/12/2009 23:59. Then, to further backtrack the trajectory of the particle, the velocity field is updated accordingly. The frequency of updating of the velocity field was set to 1 day, as a compromise between the

accuracy of results and computational time considerations.

Figure 4: at the top, flow lines of the subsurface that feed with water the surface draining network on March 1<sup>st</sup>, 2010 (on the left, high-flow period) and July 1<sup>st</sup>, 2010 (on the right, low-flow period). The color scale indicates that a water particle reaching the river at a given date started its travel along the streamline or passed at a given location on the streamline x days before. The density of streamlines is associated with the flowing versus dry fraction of the river network at a prescribed date. Below, flow lines of the subsurface that feed with water the geochemical sampling sites on March 30<sup>th</sup>, 2010 (on the left, flood event) and November 29<sup>th</sup>, 2011 (right, drought event) according to NIHM simulations. For each sampling site, 10 particles were dispatched in the direct neighborhood of the site and then backtracked. The color scale indicates that a water particle reaching the sampling site at a given date started its travel along the streamline or passed at a given location on the streamline x days before.

Figure 5: conceptual scheme used in the modeling of the water chemistry. The soil solutions are used as input solution. The bedrock is discretized into a 1D succession of cells along the active parts of the flow lines previously determined by the hydrological NIHM model. Within each cell, the geochemical and transport equations are numerically solved using the KIRMAT hydrogeochemical code. To calculate the integrated chemical composition of the spring water, several simulations with different entering points of soil solutions along the flow path were performed, and the integrated chemistry was calculated by taking the arithmetic mean of all the simulated solute concentrations.

Figure 6: maps of piezometric gradient and mean hydraulic conductivity for the Strengbach catchment, as simulated by NIHM, on 29/11/2011 (dry period) and 30/03/2010 (high flows

period). The mean hydraulic conductivity is the mean of all hydraulic conductivities integrated over the depth of the aquifer and thus depends on the water saturation.

Figure 7: simulation results for the CS1 spring for an important drought (29/11/2011) and a strong flood event (30/03/2010). At the top, active parts of the flow lines that bring the waters to the CS1 spring for the two sampling dates (7A and 7B). Below, simulated chemical compositions of the CS1 spring waters after integration along the flow lines and comparison with the initial soil solution and the spring chemistry data (7C and 7D). Error bars show analytical uncertainties on measured concentrations and subsequent uncertainties in model results.

Figure 8: simulation results for the CS1 spring over the whole range of the water discharges from the spring. Results are presented for H<sub>4</sub>SiO<sub>4</sub> and Na<sup>+</sup> concentrations (8A and 8C), pH (8D) and mean water transit time (8B). Red lines indicate simulated parameters after integration along the flow lines, and blue points show measured values from the field campaigns realized between 2005 and 2015 (data in table 1 and in supplementary table EA1). Error bars show analytical uncertainties on measured concentrations and subsequent uncertainties in model results.

Figure 9: simulation results for the PZ3 and PZ5 piezometers for a strong flood event (05/05/2015). At the top, active parts of the flow lines that bring the waters to the two sampling sites are shown (9A and 9B). Below, simulated chemical compositions of the piezometer waters after integration along the flow lines and comparison with the initial soil solution and the water

chemistry data (9C and 9D). Error bars show analytical uncertainties on measured concentrations and subsequent uncertainties in model results.

Figure 10: simulation results for the CS2 spring. At the top, active parts of the flow lines that bring the waters to the CS2 spring for an important drought (29/11/2011) and a strong flood event (30/03/2010) are shown (10A and 10B). The location of the CS2 spring implies a more scatted distribution of the flow lines than for the CS1 spring. Below, simulation results for the CS2 spring over the whole range of the water discharges from the spring are presented (10C and 10D). Blue lines indicate simulated parameters after integration along the slowest flow line, yellow lines indicate simulated parameters after integration along the fastest flow line, and blue points show measured values from the field campaigns realized between 2005 and 2015 (data in table 1 and in supplementary table EA2). Error bars show analytical uncertainties on measured concentrations and subsequent uncertainties in model results.

Figure 11: simulation results for the RH3 spring chemistry and for a flood event (30/03/2010). On the left, simulated concentrations for the case assuming that the flow lines only run on gneiss (GN) are shown (11A). On the right, simulated concentrations for the case assuming that the flow lines only run on hydrothermally altered granite (VS) are presented (11B). Error bars show analytical uncertainties on measured concentrations and subsequent uncertainties in model results.

Figure 12: overview of the flow lines of the subsurface that feed with water the geochemical sampling sites CS1, PZ3 and PZ5 on May 5<sup>th</sup>, 2015 according to the NIHM simulations. The

simulated chemical compositions after geochemical integration along the flow lines are also presented for this transect on the southern part of the watershed (CS1, PZ3 and PZ5) and compared with the initial soil solution and the spring chemistry data. Table 1: measured pH, water discharges and chemical concentrations of H<sub>4</sub>SiO<sub>4</sub>, Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup>, and Ca<sup>2+</sup> in the waters collected from the sampling sites in the Strengbach catchment. The sampling sites include springs (CS1, CS2, RH3) and piezometers (PZ3, PZ5). Table 2: Initial and calibrated values of the hydrodynamic parameters of the aguifer in the simulation of the Strengbach catchment by NIHM. 

Table 3: Comparison between BET surfaces and geometric surfaces for the major primary minerals present in a granitic context. BET surfaces were measured via gas absorption experiments by <sup>1</sup> Berger et al., 1994; <sup>2</sup> Chou and Wollast, 1985; <sup>3</sup> Lundstrom and Ohman, 1990; <sup>4</sup> Amrhein and Suarez, 1992; <sup>5</sup> Acker and Bricker, 1992; and <sup>6</sup> Guidry and Mackenzie, 2003. Geometric surfaces were recalculated from the granulometric ranges of the minerals and by assuming a spherical geometry.

	Na⁺	K⁺	Mg <sup>2+</sup>	Ca <sup>2+</sup>	H <sub>4</sub> SiO <sub>4</sub>	рН	Water Discharge
	(mmol/L)	(mmol/L)	(mmol/L)	(mmol/L)	(mmol/L)		(L/s)
Spring CS1							
16/09/2008	0.071	0.013	0.017	0.044	0.129	6.28	0.954
30/03/2010	0.074	0.014	0.015	0.043	0.120	5.61	1.523
29/03/2011	0.074	0.013	0.015	0.038	0.145	6.23	0.345
04/10/2011	0.080	0.012	0.016	0.042	0.176	6.57	0.122
29/11/2011	0.088	0.015	0.019	0.034	0.177	6.30	0.098
05/05/2015	0.065	0.012	0.012	0.054	0.121	5.33	1.410
Spring CS2							
30/03/2010	0.090	0.020	0.020	0.080	0.122	6.15	6.274
29/03/2011	0.090	0.020	0.020	0.070	0.144	6.18	0.956
02/08/2011	0.090	0.020	0.020	0.060	0.170	6.50	2.171
04/10/2011	0.100	0.020	0.020	0.070	0.177	6.76	0.413
29/11/2011	0.100	0.020	0.020	0.060	0.180	6.22	0.285
05/05/2015	0.077	0.016	0.018	0.074	0.123	6.14	7.500
Spring RH3							
30/03/2010	0.083	0.028	0.032	0.081	0.127	6.28	-
Piezometer PZ3							
05/05/2015	0.074	0.013	0.011	0.053	0.153	6.29	-
Piezometer PZ5							
05/05/2015	0.072	0.013	0.017	0.058	0.132	6.16	-

Table 1

Parameter	Unit	Initial Value	Calibrated value
Depth of substratum	m	4	See figure 2
Saturated hydraulic conductivity (all zones except the low depth zone at the catchment peak (see figure 2))	m.s- <sup>1</sup>	1.10 <sup>-4</sup>	8.10 <sup>-5</sup>
Saturated hydraulic conductivity (catchment peak)	m.s <sup>-1</sup>	1.10-4	1.10-4
porosity (all zones except the low depth zone at the			
catchment peak)	-	0.1	0.08
Porosity (catchment peak)	-	0.1	0.2
Residual water content (all zones)	-	0.01	0.01
Specific storage (all zones)	m <sup>-1</sup>	1.10-8	1.10-8
n (Van genuchten coefficient, all zones)	-	2	2
A (Van genuchten coefficient, all zones)		1	1.5

Table 2

Mineral	Mineral	Granulometric	Particle	Spherical	BET
	density	range	radius	geometric surface	surface
	(g/cm³)	(µm)	(µm)	(m²/g)	(m²/g)
Quartz <sup>1</sup>	2.62	< 50	1 - 25	1.150 - 0.046	0.310
Albite <sup>2</sup>	2.60	50 - 100	25 - 50	0.046 - 0.023	0.075
K-feldspar <sup>3</sup>	2.56	< 50	1 - 25	1.170 - 0.047	1.420
Anorthite <sup>4</sup>	2.73	20 - 50	10 - 25	0.044 - 0.111	0.500
Biotite <sup>5</sup>	3.09	150 - 400	75 - 200	0.013 - 0.005	0.240
Apatite <sup>6</sup>	3.19	100 - 200	50 - 100	0.018 - 0.009	0.026

Table 3

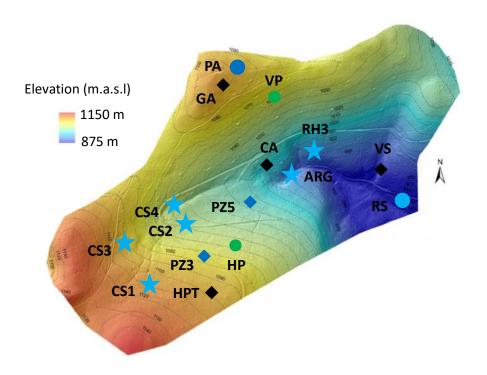


Figure 1

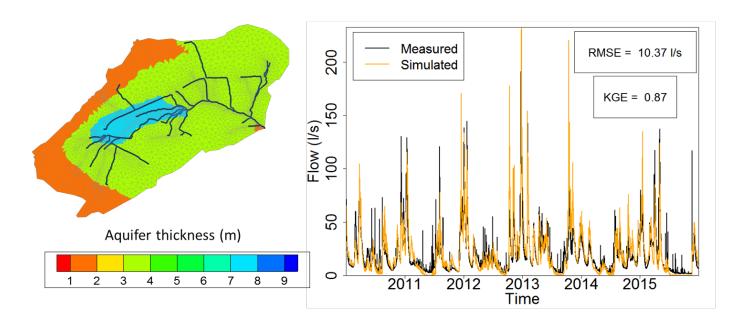


Figure 2

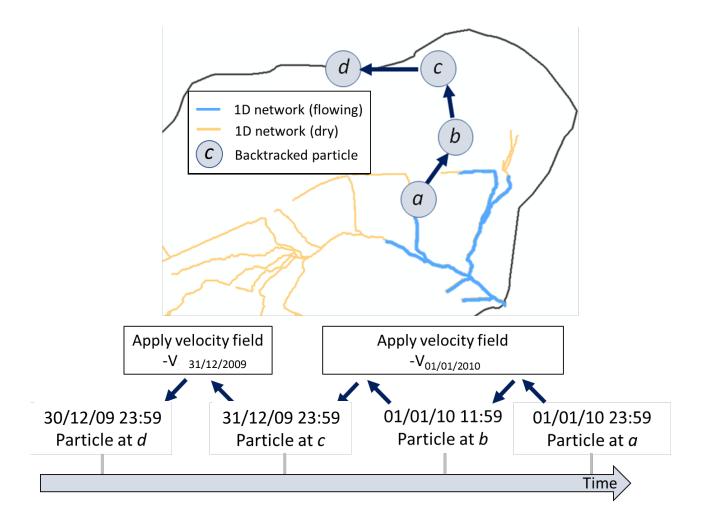


Figure 3

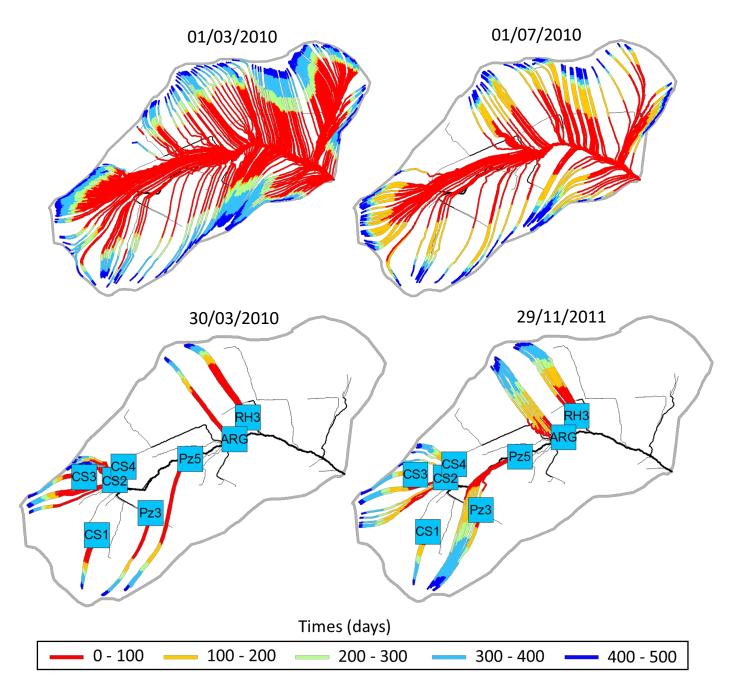


Figure 4

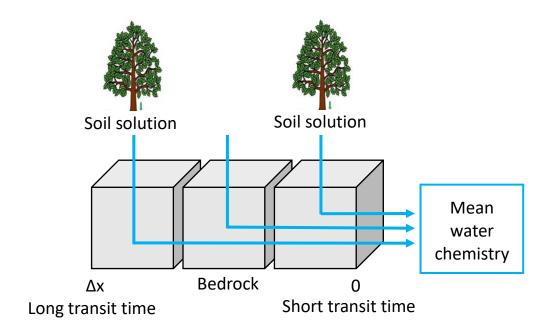


Figure 5

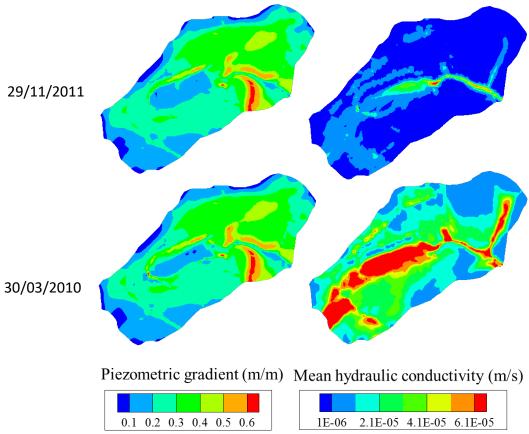


Figure 6

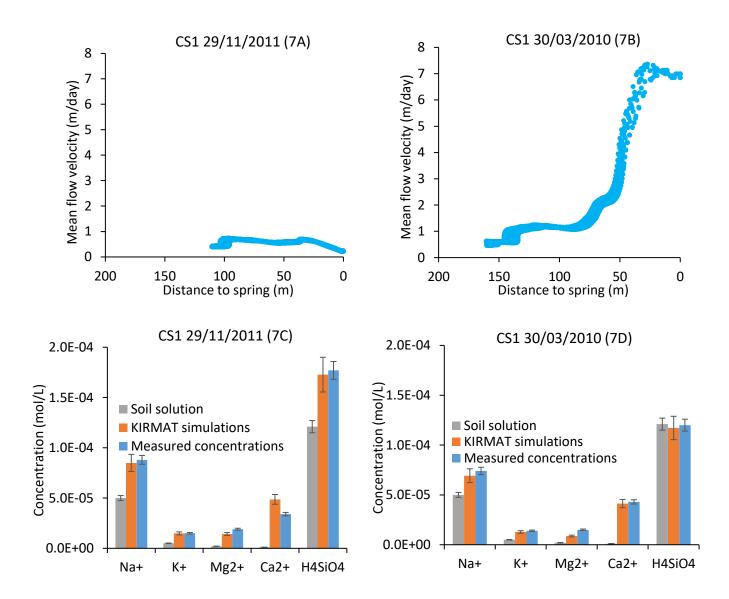


Figure 7

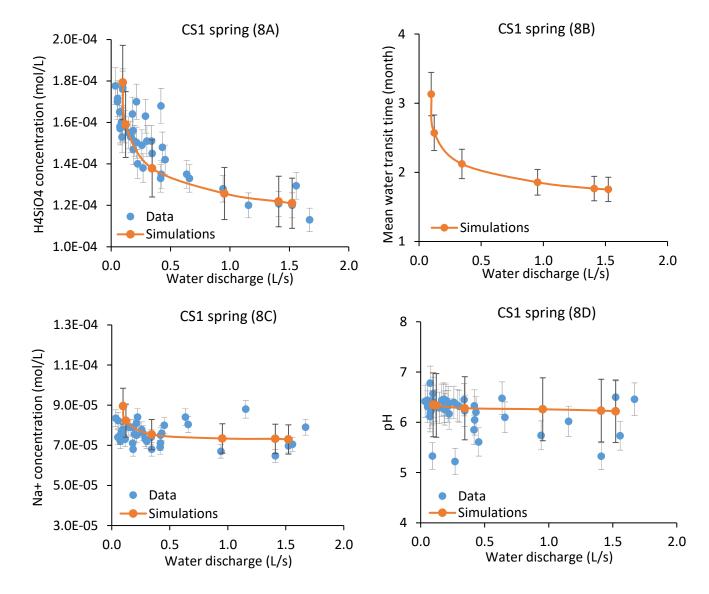


Figure 8

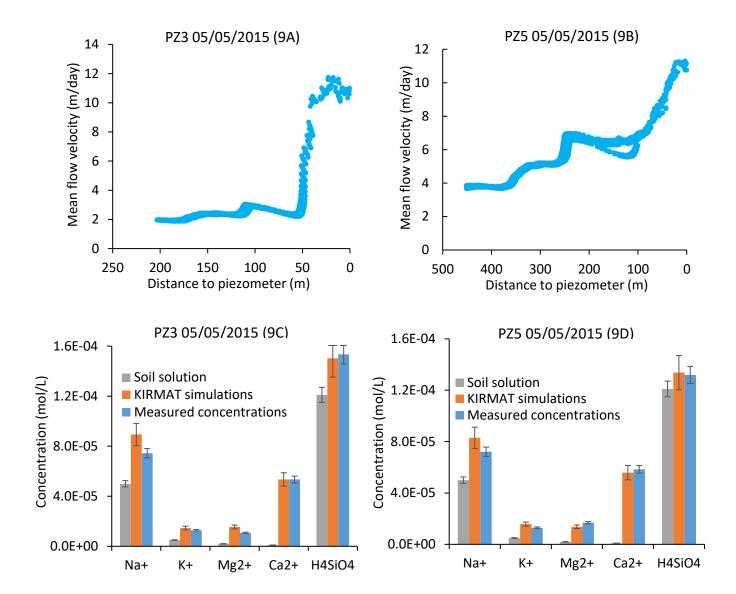


Figure 9

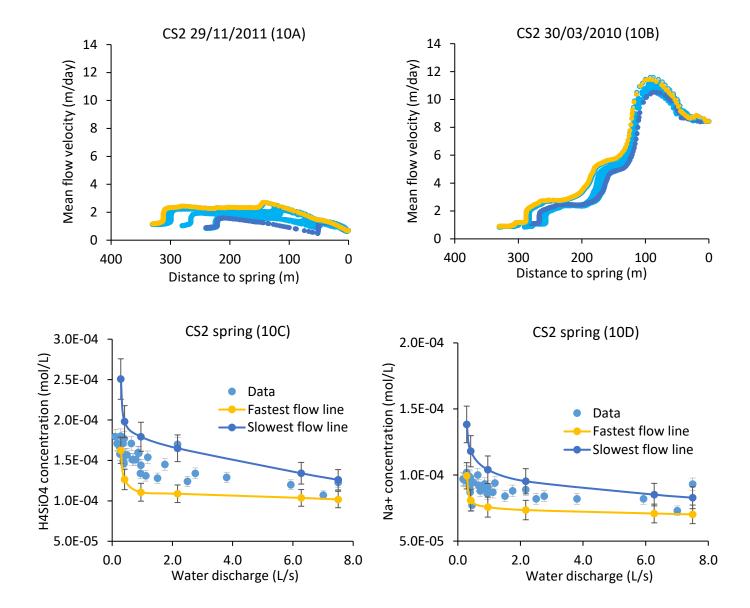


Figure 10

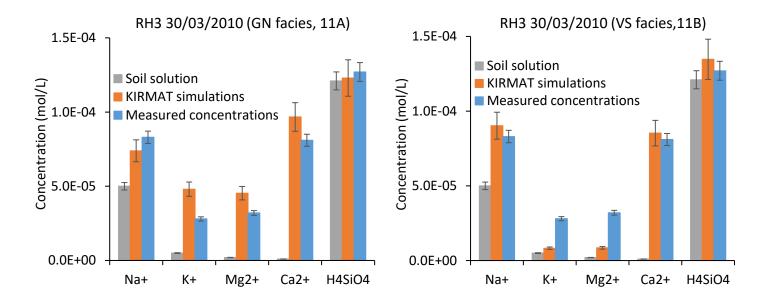


Figure 11

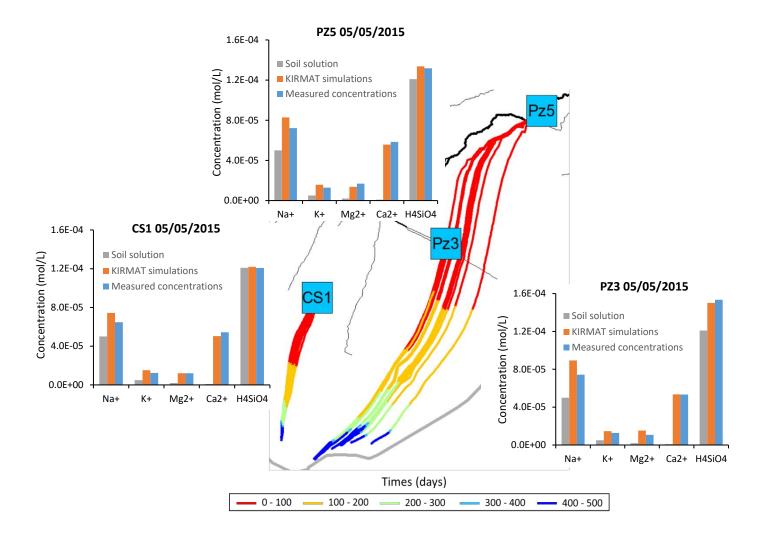


Figure 12