



1                    **Assessing the effect of flood restoration on surface-subsurface interactions in**  
2                    **Rohrschollen Island (Upper Rhine River – France) using integrated hydrological**  
3                    **modeling and thermal infrared imaging**

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30 **Abstract**

31 Rohrschollen Island is an artificial island of the large Upper Rhine River whose geometry and  
32 hydrological dynamics are the result of engineering works during the 19<sup>th</sup> and 20<sup>th</sup> centuries.  
33 Before its channelization, the Rhine River was characterized by an intense hydro-  
34 morphological activity which maintained a high level of biodiversity along the fluvial  
35 corridor. This functionality considerably decreased during the two last centuries. Since 2012,  
36 a restoration project was launched to reactivate typical alluvial processes, including bedload  
37 transport, lateral channel dynamics and surface-subsurface water exchanges. An integrated  
38 hydrological model has been applied to the area of Rohrschollen Island to assess the  
39 efficiency of the restoration regarding surface and subsurface flows. This model is calibrated  
40 using measured piezometric heads. Simulated patterns of water exchanges between the  
41 surface and subsurface compartments of the Island are checked against the information  
42 derived from thermal infrared imaging. The simulated results are then used to better  
43 understand the evolutions of the infiltration/exfiltration zones over time and space and to  
44 determine the physical controls of surface-subsurface interactions on the hydrographic  
45 network of Rohrschollen Island. The use of integrated hydrological modeling has proven to be  
46 an efficient approach to assess the efficiency of restoration actions regarding surface and  
47 subsurface flows.

48

49 **Keywords**

50 Surface-subsurface water interactions, Integrated hydrological modeling, flood restoration,  
51 Thermal infrared imagery, Rohrschollen Island, Upper Rhine River.

52

53 **Highlights** (less than 85 characters, including spaces)

54 - Direct hydrological impacts of restoration on a riverine island are modeled.



- 55 - Integrated modeling captures the hydrologic surface-subsurface interactions.
- 56 - Simulated exfiltration areas are also located by thermal infrared imaging.
- 57 - Management practices can be optimized on the basis of simulated system responses.

58

## 59 **1. Introduction**

60 Interactions between surface and subsurface flow processes are key components of the  
61 continental hydrological cycle (Winter, 1995; Sophocleous, 2002), which have received  
62 particular attention in the last decades partly because of their substantial impact on the overall  
63 response of hydrologic systems (Boano et al., 2014; Brunner et al., 2017, and citations  
64 herein). Several studies have recently highlighted the hydrological interactions between  
65 surface and subsurface that have a major impact on the biogeochemical and ecological  
66 responses of hydrosystems (e.g., Stegen et al., 2016; Danczak et al., 2016; Partington et al.,  
67 2017; Stegen et al., 2018). These interactions, which are partly driven by the  
68 geomorphological structure and the channel dynamics (Namour et al., 2015), influence flow  
69 pathways, water mixing, residence time in the hyporheic zone along streambeds, and the  
70 overall ecological functioning (Schmitt et al., 2011). They are complex for several reasons,  
71 including (a) the nonlinearity of the processes involved, (b) the strong heterogeneity of the  
72 hydrological systems, and (c) the incidence of small-scale features on large-scale behavior  
73 (Hester et al., 2017). Although these surface-subsurface interactions have been extensively  
74 investigated in the last decades, several issues relating to them require a deeper understanding  
75 to address contemporary challenges associated with water quality and water resources  
76 management (Brunner et al., 2017). Among these issues, monitoring and modeling the  
77 evolution of these interactions over space and time is fundamental (Krause et al., 2014),  
78 especially in the context of river restoration.



79 River restoration has been applied worldwide to counteract the undesired effects of  
80 anthropogenic actions on river ecosystems and ecosystem services (e.g., Wohl et al., 2015,  
81 and citations herein). From a general perspective, the goal of restoration projects is to enhance  
82 the hydrological, biogeochemical, and ecological functioning of large rivers and stream  
83 hydrosystems through the reactivation of lost geophysical, geochemical, or biological  
84 processes. Due to their firm control on biogeochemical and ecological signatures in the so-  
85 called hyporheic zone (e.g., Peralta-Maraver et al., 2018), the interactions between surface  
86 and subsurface hydrological processes may become a focus of restoration projects (e.g.,  
87 Boulton et al., 2010; Friberg et al., 2017). Many projects try to improve the water quality  
88 and/or ecological processes of the hydrosystem through engineering works that target  
89 hyporheic exchange enhancements. Maintaining or amplifying these interactions could reveal  
90 crucial regarding climate change effects to preserve aquatic species. Nevertheless, it is still  
91 very difficult to assess the efficiency of such restoration projects as this requires a refined  
92 characterization of the location and amplitude of surface-subsurface interactions (e.g.,  
93 Morandi et al., 2014).

94 Several advances in measurement techniques and modeling approaches appear very  
95 promising to improve our current understanding and our forecasting capabilities regarding  
96 surface-subsurface interactions (Krause et al., 2014; Brunner et al., 2017). Many  
97 experimental/field projects are related to the use of temperature as a tracer of hydrological  
98 connectivity and locations where groundwater discharges into surface water bodies (e.g.,  
99 Pfister et al., 2010; Daniluk et al., 2013). Two different thermal techniques—Fiber Optic-  
100 Distributed Temperature Sensing (FO-DTS) and Thermal InfraRed (TIR) survey—have been  
101 used for their potential to inform on spatial and temporal patterns of water fluxes in large  
102 areas of the hyporheic zone through the determination of thermal anomalies. FO-TDS  
103 provides one-dimensional profiles of these anomalies with a fine spatial resolution by



104 submerging fiber optic cables along a streambed. TIR survey can be performed from air and  
105 satellite, and informs on surface temperature with two-dimensional images of various  
106 resolutions (e.g., Hare et al., 2015).

107 For their part, integrated hydrologic models emerged in the late 1990s, and they are  
108 now recognized as suitable tools to investigate streamflow generation processes at the  
109 catchment scale (e.g., Paniconi and Putti, 2015; Fattichi et al., 2016). Although most  
110 integrated models rely on the solution to the 3-D Richards equation to describe subsurface  
111 flow (e.g., Maxwell et al., 2014), alternative low-dimensional approaches that simplify the  
112 description of the subsurface compartment (still with some physical meaning) have recently  
113 appeared (e.g., Hazenberg et al., 2015, 2016; Jeannot et al., 2018). Solving the 3-D Richards  
114 equation with a proper discretization to capture the complex and small-scale physics of flow  
115 in the vadose zone over large areas may require substantial computer resources. Low-  
116 dimensional integrated approaches that are efficient regarding computation time could also  
117 reveal beneficial to tackle practical water management issues. Integrated models, irrespective  
118 of their level of complexity, explicitly account for the interaction between surface and  
119 subsurface hydrological processes. Thus, their application to hydrosystems renders insights on  
120 the evolution over time and space of surface-subsurface interactions (e.g., Partington et al.,  
121 2013; Camporese et al., 2014).

122 Hydrologic modeling has already been used to assess the potential effects of  
123 restoration works on the hydrologic response of a given system (e.g., Martinez et al., 2014;  
124 Ohara et al., 2014; Clilverd et al., 2016). The studies reported in the ongoing literature mostly  
125 deal with the effect of restoration on water table dynamics, flood frequency, ecosystem  
126 services (e.g., thermal refugees for specific species), and vegetation dynamics. To our  
127 knowledge, the prediction with models of hyporheic exchanges has not yet been considered.  
128 No integrated hydrologic model has been applied to a restored fluvial hydrosystem even



129 though the application could reveal noteworthy data in rendering quantitative indicators of  
130 restoration efficiency. In addition, the combined use of thermal information with integrated  
131 hydrological models is not yet common even though comparing and discussing both seems  
132 fruitful. Ala-aho et al. (2015) used thermal imaging and integrated modeling to study the  
133 exchanges between groundwater and lakes in Finland. Glaser et al. (2016) used integrated  
134 modeling and TIR survey to improve the calibration procedure and investigate the dynamics  
135 of the saturated area in a small catchment in Luxembourg. Munz et al. (2017) combined  
136 thermal measurement along the banks of a stream and integrated modeling at the reach scale  
137 to improve the determination of residence times in the hyporheic zone.

138 This paper aims to present how an integrated hydrologic model was used in  
139 combination with data of TIR imaging to specifically investigate the effect of a restoration  
140 project on surface-subsurface water interactions. A main goal, which is also an innovation, is  
141 to propose a method that quantitatively evaluates the efficiency of restoration actions  
142 regarding the enhancement of hyporheic exchanges and their dynamics over time and space.

143

## 144 **2. Data and hydrological modeling**

### 145 *2.1. Study Area – Rohrschollen Island*

#### 146 *2.1.1 General description*

147 Rohrschollen Island is an artificial island located 8 km south of Strasbourg (Upper  
148 Rhine, France, see Fig. 1-a), as the result of historical engineering works carried out along the  
149 Rhine River mainly to prevent flooding and to develop navigation and agriculture. The  
150 hydrological and geomorphological dynamics of the area were massively impacted (Eschbach  
151 et al., 2017; Eschbach et al., 2018). Three structures completely control the current geometry  
152 and hydraulic behavior of Rohrschollen Island (Fig. 1): (a) the diversion dam (built in 1970)  
153 at the southern end of the island that diverts most of the river flow into the Rhine Canal at the



154 western bank of the island, (b) the hydropower plant (built in 1970) located on the Rhine  
155 Canal downstream to Rohrschollen Island, and (3) an agricultural dam (built in 1984) at the  
156 northern part of the Island to keep a constant water level in the by-passed Old Rhine at the  
157 eastern bank of Rohrschollen Island.

158 Rohrschollen Island was regularly flooded in the past (Eschbach et al., 2018). The  
159 main anastomosed channel inside the Island, the Bauerngrundwasser (BGW; Fig. 1), was  
160 disconnected on its upstream mouth from the Rhine River by the excavation of the Rhine  
161 canal. This disconnection, combined with dampened groundwater dynamics along the Island,  
162 degraded the hydrological, geomorphological, and ecological functioning of the hydrosystem.  
163 The former flood dynamics induced large water table fluctuations, lively interactions between  
164 the surface and subsurface domains, intense rejuvenation of habitat mosaic driven by  
165 geomorphological processes, and a high level of biodiversity for species of aquatic and  
166 riverine habitats. As a result of engineering works performed to control the Rhine River, the  
167 ecological services associated with the flood dynamics and the hydrologic connection  
168 between the floodplain of the Island and the river were lost.

169 In 2012, the European Union funded a restoration project (LIFE + program) in order to  
170 counteract the loss of various natural processes and thus re-establish part of the former  
171 dynamics of the system. The Rhine River water is now injected through a floodgate into a 900  
172 m long new artificial channel (south of the Island; Fig. 1-b) when the upstream discharge in  
173 the Rhine River exceeds  $1550 \text{ m}^3\text{s}^{-1}$ . These injections should contribute to (a) enhancing  
174 discharge into the surface water bodies of the Island (especially in the BGW) and partly  
175 recovering floods on the Island (floods occur when the injected rate exceeds the top-edge  
176 discharge of the new channel at  $20 \text{ m}^3\text{s}^{-1}$ ), (b) recovering bedload transport and lateral channel  
177 dynamics (especially along the new channel), (c) activating surface-subsurface interactions,



178 and (d) stimulating the renewal of aquatic and riverine ecosystems. The injected discharges  
179 range between 2 and 80 m<sup>3</sup> s<sup>-1</sup>, according to the total discharge in the Rhine River.

### 180 *2.1.2 Hydrologic monitoring*

181 A large interdisciplinary environmental monitoring was conducted to investigate the  
182 effects and the efficiency of the restoration, but also to check on some risks such as the  
183 eventual collapsing of the new channel banks under strong water injections. As an example, a  
184 dense network of piezometers (yellow squares in Fig. 1-c) was installed along both the  
185 artificial new channel and the BGW. More precisely, ten transects along these channels were  
186 instrumented with a piezometer on each channel bank. The time resolution of measurements  
187 in the 20 piezometers ranges from 5 min along the new channel to 10 min along the BGW.  
188 This network is particularly crucial for hydrological model calibration and to understand the  
189 interactions between groundwater and surface water bodies. Other subsurface head  
190 measurements are also available on the eastern and western sides of the island. The French  
191 National Electricity Company (EDF) is operating devices at the western side of the Island  
192 (along the Rhine Canal) to monitor the state of the dike road (blue squares in Fig. 1-c) and, as  
193 the owner and manager of the Rohrschollen Island Nature Reserve, the city of Strasbourg is  
194 following subsurface water table dynamics at the eastern side (orange squares in Fig. 1-c).

195

### 196 *2.1.3 Historical and sedimentological surveys*

197 Geo-historical and sedimentological surveys were used to reconstruct the morpho-  
198 sedimentary temporal trajectory of the Island since the middle of the 18<sup>th</sup> century. The geo-  
199 historical survey is partly based on six old maps, two sets of aerial photographs, and the actual  
200 digital elevation model of the Island (see Fig. 2, left part). Planimetric data were  
201 georeferenced in a GIS (geographic information system) and processed to highlight the  
202 temporal dynamics of the main morpho-ecological units. The sedimentological study was





203 based on seven coring transects distributed along the BGW. Grain size analysis was also  
204 performed on sediment samples from three transects and two pits in the floodplain to  
205 determine the transport and deposition processes of fine sediments. The combination of the  
206 geo-historical and sedimentological analysis helped to reconstruct the sedimentary deposition  
207 trajectory and to locate precisely historical gravel bars (see Fig. 2, right side). This  
208 information was used to spatialize the parameters of the hydrological model and to preset the  
209 initial values of key parameters related to the composition of the sediment units. More details  
210 on this part of the study can be found in Eschbach et al. (2018).

211

#### 212 *2.1.4. Thermal infrared imaging*

213 Thermal infrared imaging (TIR) was carried out at Rohrschollen Island to investigate  
214 the relationship between the evolution of some geomorphological features (e.g., riffles and  
215 pools) and the interactions between surface and subsurface waters. A FLIR b425 infrared  
216 camera was fixed under a paraglider to take pictures covering the whole island. The camera  
217 was calibrated using several key parameters such as water emissivity and the height above the  
218 topography. The flight took place on January 22, 2015, a date chosen to have minimal canopy  
219 extension and maximal temperature contrast between surface and subsurface waters (with  
220 approximately 4°C surface temperature and 10°C groundwater temperature). The thermal  
221 images were processed to locate thermal anomalies along the new artificial channel and the  
222 BGW. The radiance was first converted into temperature using Planck's law and in-situ  
223 measurements as references. The temperature maps were then georeferenced, and pixels  
224 associated with high uncertainty on temperatures were also discarded. Further treatments  
225 based on optic images (in the visible wavelengths) delineated and located surface objects such  
226 as banks, vegetation, logjams, and gravel bars. Further details about thermal image processing  
227 can be found in Eschbach et al. (2017).



228 2.2. Hydrological modeling strategy

229 2.2.1. The Normally Integrated Model (NIM)

230 The integrated hydrological model used to model Rohrschollen Island is the Normally  
231 Integrated Model (NIM) (Pan et al., 2015; Weill et al., 2017; Jeannot et al., 2018). This tool is  
232 a physically based and spatially fully-distributed model that describes flow processes in the  
233 surface and subsurface domains of a catchment and their couplings. For the sake of simplicity,  
234 only the model parts used for this study are presented here. A detailed presentation of the  
235 model (primarily concerning treatment of the flow equations) is available, for example, in  
236 Jeannot et al. (2018).

237 The subsurface flow processes are described using a low-dimensional equation that  
238 results from the integration of the 3-D Richards equation along a direction normal to the  
239 bedrock (i.e., the impervious bottom of the aquifer). The final equation for subsurface flow  
240 can be written as:

241 
$$\frac{\partial \bar{\theta}}{\partial t} + \bar{S}(h) \frac{\partial h}{\partial t} + \nabla_{x,y} \cdot (-\bar{\mathbf{T}}(\theta) \nabla_{x,y} h) = Q_w \quad [1]$$

242 where  $\bar{\theta}(h) = \int_{z_w}^{z_s} \theta(z) dz$ ,  $\bar{S}(h) = S_{sat} h$ ,  $\bar{\mathbf{T}}(h, \theta) = \mathbf{K}_{sat} h + \int_{z_w}^{z_s} \mathbf{K}(\theta(z)) dz$ .  $\mathbf{K}_{sat}$ , and  $S_{sat}$  are  
243 averages along the integration direction  $z$  of the saturated hydraulic conductivity tensor and  
244 the specific storage capacity in the saturated zone, respectively.  $\theta$  [-] is the water content;  $\mathbf{K}$   
245 [ $\text{LT}^{-1}$ ] is the tensor of hydraulic conductivity;  $h$  [L] is the hydraulic head (or the capillary  
246 head); and  $Q_w$  [ $\text{LT}^{-1}$ ] is a source term that accounts for the subsurface interactions with both  
247 the 1-D river network and the 2-D overland flow. It is worth noting that the 1-D river network  
248 compartment was not used in this study because the precision of the digital elevation model  
249 (Fig. 2, left) was enough to delineate and model streams, channels, and other small water  
250 routing in slight topographic depressions of the 2-D overland flow layer.



251 The 2-D overland flow layer is described using the so-called diffusive wave equation,  
 252 which is written as:

$$253 \quad \frac{\partial(h_s + z_s)}{\partial t} - \nabla_x \cdot (T_{s,x} \nabla_x (h_s + z_s)) - \nabla_y \cdot (T_{s,y} \nabla_y (h_s + z_s)) = q \quad [2]$$

254 with

$$T_{s,x} = \frac{h_s^{5/3}}{N_{man,x}^2 \beta \nabla (h_s + z_s)} \quad ; \quad T_{s,y} = \frac{h_s^{5/3}}{N_{man,y}^2 \beta \nabla (h_s + z_s)}$$

255

$$\beta \nabla (h_s + z_s) = \left[ \left( \frac{\partial (h_s + z_s)}{\partial x} \right)^2 \frac{1}{N_{man,x}^4} + \left( \frac{\partial (h_s + z_s)}{\partial y} \right)^2 \frac{1}{N_{man,y}^4} \right]^{1/4}$$

256  $h_s$  [L] is the water depth at the surface;  $z_s$  [L] is the soil surface elevation;  $u_x$  and  $u_y$  [ $\text{LT}^{-1}$ ]  
 257 are the water velocity components along the  $x$  and  $y$  directions (that are locally defined in the  
 258 plane normal to the direction of integration  $z$  of Eq. (1));  $q$  [ $\text{LT}^{-1}$ ] is a source term including  
 259 the exchanges with the 1-D river flow compartment and with the subsurface; and  $N_{man,x}$  and  
 260  $N_{man,y}$  [ $\text{L}^{-1/3}\text{T}$ ] are the Manning coefficients in the  $x$  and  $y$  directions, respectively.

261 The coupling between Eq. (1) and Eq. (2) relies upon a first order law stating that the  
 262 flux exchanged between surface and subsurface flows is proportional to the head gradient  
 263 between the two compartments. The exchanged flux  $Q_{Ex,2D \leftrightarrow SS}$  [ $\text{LT}^{-1}$ ] can be formalized as:

$$264 \quad Q_{Ex,2D \leftrightarrow SS} = K_{Int} \frac{(z_s + h_s) - h}{l_e} F_s \quad [3]$$

$$265 \quad F_s = \min \left[ \left( \frac{h_s}{h_{ob}} \right)^{2(1-h_s/h_{ob})} ; 1 \right] \quad [4]$$

266 where  $K_{Int}$  [ $\text{LT}^{-1}$ ] is the vertical hydraulic conductivity at the interface between the surface  
 267 and subsurface compartments;  $l_e$  is a user-defined coupling length (i.e., an empirical  
 268 thickness of the interface between surface and subsurface compartments);  $F_s$  [-] is a scaling



269 function accounting for the saturated-unsaturated character of the interface between the  
270 surface and subsurface; and  $h_{ob}$  is the total obstruction height accounting for small  
271 irregularities of the topography.

272         Regarding the numerical solution, both equations are solved together in a fully implicit  
273 manner using advanced numerical schemes. Note that both equations are two-dimensional and  
274 that only one computation mesh mimicking the topographic surface of the system is required  
275 for simulating both surface and subsurface processes, including their interactions.

276

#### 277 *2.2.2 Model setup and parametrization*

278         The computation mesh for all the simulations of the study was built from data from an  
279 airborne LIDAR survey performed in 2015 that produced high-resolution images of the  
280 topography (50 cm in the horizontal plane and 1-2 cm in elevation). The whole Rohrschollen  
281 Island is meshed using triangular elements of 20 m on a side. The exception is a 120 m wide  
282 corridor surrounding the new channel and the BGW where a refined spatial resolution of 10 m  
283 is used. The higher resolution is assumed to better capture the hydrological dynamics and the  
284 surface-subsurface interactions along the surface water bodies of the Island. Prescribed-head  
285 (Dirichlet) boundary conditions are imposed at the western and eastern banks of Rohrschollen  
286 Island for the subsurface model, and they have been documented by measurements collected  
287 by the EDF and the city of Strasbourg. These boundary conditions may vary over time,  
288 depending on the modeled period and availability of data. The northern and southern parts of  
289 the Island were considered as no-flow boundaries. The initial conditions were set up by  
290 running the model with consistent boundary conditions for the subsurface and an injection  
291 rate of  $2 \text{ m}^3 \text{ s}^{-1}$  (which is the routine injection rate) at the new channel inlet until stable  
292 hydrological conditions were reached.



293           The initial parametrization of the model, especially the spatial distribution of  
294 hydrodynamic parameter values, mainly relies upon patterns drawn from the geo-historical  
295 and sedimentological surveys of the island (Eschbach et al., 2018). As an example, Fig. 2  
296 maps three historical snapshots of the main geomorphological units (gravel bars). Results  
297 from particle size analysis also helped to predefine variation ranges of crucial parameters,  
298 such as the hydraulic conductivity and retention curve parameters of the sediments and the  
299 exchange coefficient between surface and subsurface. The spatial distribution of parameters  
300 as various zones (of uniform values within a zone) was directly delineated by relying upon  
301 maps and local information gathered, rendered compatible, and processed via a GIS. Note that  
302 corridors around the new channel, the BGW, and the network of paleo-channels visible in the  
303 floodplain, which the digital elevation model in Fig. 2 identifies, were defined and  
304 parametrized separately to account for specific deposition histories resulting in specific  
305 sediment grain size.

306

### 307 *2.2.3. Model calibration and validation*

308           The integrated model was calibrated and validated using two periods of time for which  
309 high-rate injections in the new artificial channel were carried out. The first period (December  
310 9, 2014–December 15, 2014) was used as a model calibration exercise which encompassed  
311 two peaks of injection with one reaching  $80 \text{ m}^3 \text{ s}^{-1}$ . The second selected period (May 15,  
312 2015–May 21, 2015) was employed as a validation exercise with three injection peaks, two of  
313 them exceeding  $70 \text{ m}^3 \text{ s}^{-1}$ . Fig. 3 reports the evolution of the injected flow rates over time at  
314 the system inlet for both the calibration and validation periods.

315           After a first simulation employing the initial parametrization (defined in Section 2.2.2),  
316 manual calibration was carried out for the first period to improve the fitting between  
317 measured and simulated head levels in the subsurface. Both the Root Mean Square Error



318 (RMSE) and the Kling-Gupta Efficiency (KGE) associated with observed heads at the 10  
319 transects cross cutting the new channel and the BGW were used as indicators to evaluate the  
320 quality of the simulations. Only the hydraulic conductivity and the exchange coefficient  
321 between surface and subsurface were slightly adjusted while trying to preserve the initial  
322 spatial zonation. Fig. 4 maps the final set of parameters for the saturated hydraulic  
323 conductivity and the exchange coefficient, which are the most sensitive parameters of the  
324 model in the present case. The sets of calibrated parameters were then used for simulating the  
325 validation period to check whether the calculated subsurface head levels match up to the  
326 measured values.

327 It is worth noting here that the calibration exercise was performed over a period where  
328 the TIR images were not available, which means, in turn, that the calibration only relied upon  
329 measured groundwater head levels as a reference. The goal of the calibration was not to match  
330 the exfiltration patterns identified through the TIR imaging. When this information became  
331 available, the simulation period used for the calibration was extended to reach the date of the  
332 airborne flight (January 22, 2015), and the boundary conditions were updated. The exfiltration  
333 patterns were then used as verification information to confirm that the model could properly  
334 describe the interactions between surface and subsurface and thus be used as a forecasting  
335 tool. Forecasts discussed hereinafter cover optimizations of injections in the artificial channel  
336 upstream to the Island, which are mainly supposed to maintain active ponding and wetlands  
337 (mainly from groundwater outcrops) over long periods.

338

### 339 **3. Results and discussion**

#### 340 *3.1. Model outputs*

341 Fig. 5 displays the evolution over time of simulated and observed piezometric heads at  
342 two locations (transects) in the island. It also plots simulated versus observed heads for all



343 locations and sampling times used during the calibration period. Heads at transects in Fig. 5  
344 were selected to show the best and worst match concerning RMSE between simulation and  
345 observation. In general, the model adequately reproduces the system dynamics, capturing the  
346 two peaks of head response associated with the injection patterns at the new channel inlet.  
347 The recession part of the response is also captured well with a slight overestimation of the  
348 final head value for transect T8 (Fig. 5, upper left panel). The plot of simulated versus  
349 observed heads (Fig. 5, right) confirms that the model tends to overestimate the piezometric  
350 heads as more points are located above the 1:1 straight line. This feature is associated with  
351 one of the founding assumptions of the model regarding the vadose zone, which is integrated  
352 with the saturated zone and can be excessively or not sufficiently capacitive, depending on the  
353 mean soil moisture (see Weill et al., 2017). The values of the two performance indicators that  
354 are the RMSE and the KGE are satisfying, at 17 cm and 0.93, respectively.

355 Fig. 6 depicts the same information as Fig. 5 but for the validation period. The  
356 agreement between simulated and measured heads remains good with an RMSE of 24 cm and  
357 a KGE of 0.75. As is often the case, the results degrade when passing from calibration to  
358 validation exercises. That being said, both exercises show that the NIM and its calibrated set  
359 of parameters render convincing simulations of the highly transient hydrologic behavior of the  
360 system.

361

### 362 *3.2. Interactions between surface and subsurface in Rohrschollen Island*

363 Once calibration and validation were completed, the ability to capture the interactions  
364 between surface and subsurface was checked by comparing the modeled exfiltration patterns  
365 simulated on January 22, 2015, with the thermal anomalies identified via airborne TIR  
366 imaging performed the same day (see Section 2). In Fig. 7, the thermal anomalies are  
367 represented as pink spots, and the simulated exfiltration patterns are represented as colored



368 patches ranging from blue to red as a function of the exfiltration rate. Fig. 7 focuses on the  
369 area of the Island where a vast majority of the thermal anomalies were identified. The  
370 simulated exfiltration patterns usually coincide with the thermal anomalies from the TIR,  
371 even though their spatial extension may be wider than thermal anomalies. This feature can be  
372 the consequence of multiple factors, such as (a) the substantial sedimentary heterogeneity of  
373 the streambed not sufficiently represented in the model, (b) a spatial resolution of the  
374 computation mesh not fine enough to capture the very small-scale surface-subsurface  
375 interactions, and (c) the measurement uncertainty plaguing the TIR analysis. Keeping these  
376 approximations in mind, the hydrologic model correctly locates the surface-subsurface  
377 interactions in the Island and provides flux values that are not accessible via TIR survey.

378 Fig. 8 and Fig. 9 picture the transient interactions between surface and subsurface and  
379 tell us why the banana-shaped exfiltration zone reported in Fig. 7 is close to the junction of  
380 the new artificial channel and the BGW. Fig. 8 displays maps of the groundwater head, the  
381 surface water thickness, and the exfiltration rates over the whole Island at three different times  
382 of the calibration period that are  $t = 50$  h (i.e., after the first injection peak);  $t = 59$  h (i.e., at  
383 the second injection peak); and  $t = 1072$  h (i.e., the date of the airborne TIR flight). As  
384 evidenced by the snapshots of groundwater head and surface water thickness, the water  
385 injected upstream to the island, flowing into the BGW, its dead-ends, and the associated  
386 floodplain, rapidly infiltrates, producing an important increase in groundwater levels  
387 alongside the new artificial channel (and also the BGW), which had been excavated but was  
388 still not clogged with fine sediments. When the maximum injection rate is reached ( $t = 59$  h),  
389 surface ponding occurs on a significant portion of the Island and the groundwater mounding  
390 invades all the upstream part of the BGW. Note that the exfiltration rates (Fig. 8, right) are  
391 localized in small topographic depressions during the injection period, and the banana-shaped  
392 exfiltration pattern (Fig. 7) is still inactive. The latter pattern only appears during the





393 recession period ( $t = 1072$  h) when the strong injection rates have stopped. It appears  
394 alongside the BGW in the vicinity of the area where the groundwater level previously  
395 increased the most. Fig. 9 represents cross-sections along locations *a* and *b* in Fig. 7 for  $t = 59$   
396 h and  $t = 1072$  h, and reports on the subsurface water head, the surface water elevation (set to  
397 the topography elevation when surface water thickness is zero), and infiltration-exfiltration  
398 rates. It shows that (a) the topography mainly controls the banana-shaped infiltration-  
399 exfiltration zone (depressions in Fig. 9), and (b) the temporal dynamics and amplitude of  
400 exfiltration are the combined effect of surface water rapidly flowing toward the system outlet  
401 (i.e., surface water thickness diminishes), and a slow recession of the groundwater heads after  
402 the main peaks of injected flow rates have vanished.

403 Fig. 10 reports on the evolution over time of the total infiltration and exfiltration  
404 fluxes calculated over the whole surface area of the Island during the two peaks calibration  
405 period. While the injection rate is kept at  $2 \text{ m}^3 \text{ s}^{-1}$ , both infiltration and exfiltration fluxes are  
406 stable with much more infiltration than exfiltration. When the injected flow rate increases, the  
407 infiltrated flux follows a slightly delayed evolution over time, which is very similar to the  
408 injection hydrograph (with a two peaks shape, see Fig. 3). Meanwhile, as the hydraulic  
409 gradient between surface and subsurface changes at some locations, the exfiltration decreases  
410 in areas that turn from an exfiltration to an infiltration regime due to excess of surface water  
411 associated with injection peaks. Once the injection of water into the new artificial channel  
412 stops, the infiltration flux sharply decreases while the exfiltration flux increases. An  
413 exfiltration peak can be observed just at the end of the recession period. It is noteworthy that  
414 during the recession period, the exfiltration flux is almost constant over time and kept at a  
415 value twice that observed before injection (Fig. 10). In the end, forced water injections at the  
416 new channel inlet foster water exfiltration from the subsurface that maintains ponds and



417 wetlands on the surface over long periods (say, approximately 15 days for each injection, as  
418 simulated by the model but not reported in Fig. 10).

419

### 420 *3.3. Efficiency of the restoration actions*

421 One of the issues targeted in this study is to assess the efficiency of hydrological  
422 restoration projects. The previous results indicate that water injections in the new channel  
423 enhance the interactions between surface and subsurface compartments of the Island, noting  
424 that the new channel was excavated in highly conductive sedimentary formations. It may be  
425 interesting to check via a modeling approach what causes differences between the current  
426 restored circumstances and a pre-restoration situation. As the pre-restored island is not well  
427 documented in terms of hydraulic data, we considered a scenario where the pre-restored  
428 island is similar to the current situation (including, e.g., geometry and boundary conditions)  
429 with the exception that the newly excavated channel connecting Rohrschollen Island's BGW  
430 and the Rhine River is absent. Therefore, no forced injection may occur at the southern  
431 boundary of the pre-restored island. The hydrological behavior of the pre-restored situation  
432 has been simulated and compared with an actual case where the injection rate in the new  
433 channel is at the usual year-round configuration of  $2 \text{ m}^3 \text{ s}^{-1}$ .

434 Fig. 11 displays snapshots of exfiltration rates in a subarea of the Island for the pre-  
435 restored and the restored scenarios. Even with an injected flow rate of  $2 \text{ m}^3 \text{ s}^{-1}$ , both the  
436 exfiltration surfaces and exfiltration rates are much higher in the restored situation. In other  
437 words, the base flow regime of the restored situation is sufficient to positively impact the  
438 interactions between surface and subsurface compartments of the Island. When forced  
439 injections enhance the development of wetlands and maintain high rates of exfiltration over  
440 long periods, from the mere hydrological standpoint, restoration works are successful.

441

442 *3.4. Suggestions for management practices*

443 The injection scenarios tested in the hydrological model with maximum peaks  
444 reaching  $80 \text{ m}^3\text{s}^{-1}$  are designed as a routine inlet for feeding Rohrschollen Island with water,  
445 but some other inlet procedures can also be considered to improve the functioning of the  
446 Island. We analyzed with the hydrological model how these routine injections could be  
447 designed to maximize either the spatial extension of exfiltration areas maintaining wetlands in  
448 surface or the time over which exfiltration occurs. Two hypothetical injections superimposed  
449 to a base flow of  $2 \text{ m}^3\text{s}^{-1}$  in the new channel were proposed, the first one being of short  
450 duration (24 h) with an injection rate of  $15 \text{ m}^3\text{s}^{-1}$ , the second one being of longer duration  
451 (120 h) but with a weaker injection rate of  $5 \text{ m}^3\text{s}^{-1}$  (see Fig.12, up). As the total injected water  
452 volume differs between both scenarios (the weaker injection flushes almost twice the volume  
453 of the stronger injection), it can also be determined which of the two configurations—high  
454 rate/small volume or small rate/high volume—maximizes extension and/or duration of  
455 exfiltration.

456 Fig. 12 (down) plots the excess or lack of exfiltration surface areas during injections  
457 compared with surface areas sustained by base flow ( $2\text{m}^3\text{s}^{-1}$ ) in the new channel. The  
458 evolution over time of these excess exfiltration areas (or lack thereof) occurs for both  
459 injection scenarios with a lack of exfiltration areas occurring during the injection periods  
460 when infiltration from the surface dominates. After the injection peak is completed, the  
461 recession period—starting at  $t = 52 \text{ h}$  for the high injection rate and  $t = 162 \text{ h}$  for the small  
462 injection rate (Fig. 12)—always shows an excess of exfiltration areas. The interesting point is  
463 that the high injection rate delivers a smaller volume of water in the system but maintains  
464 increased areas of exfiltration over extensive periods. For its part, the small injection rate has  
465 no effect beyond  $t = 250 \text{ h}$  with a system coming back to its initial state with  $2\text{m}^3\text{s}^{-1}$  of routine  
466 injection at the inlet. Finally, injecting less volume but with high injection rates over short



467 periods is better suited to maintaining exfiltration over long periods as the process feeding  
468 wetlands on the Island (Fig. 12). It is also likely (though not studied in this work) that intense  
469 injections favor the unclogging of the BGW, which are the primary surface water routes  
470 contributing to water renewal on the Island.

471

#### 472 **4. Conclusions**

473 Restoration projects to counterbalance the undesired effects of anthropogenic actions  
474 on the hydrological, geomorphological, and ecological status of riverine ecosystems have  
475 recently spread worldwide. As the interactions between surface and subsurface compartments  
476 of the hydrosystem have a strong impact on hydrological, biogeochemical, and ecological  
477 processes, it makes sense to rely upon integrated hydrological modeling when addressing the  
478 question of restoration efficiency. When feasible (i.e., with tractable problems and models),  
479 hydrological modeling with high resolution in time and space can accurately delineate  
480 infiltration-exfiltration areas and their evolution over time as key factors for maintaining  
481 active surface river networks

482 Relying upon simplified models, not in their physics but rather on their dimensionality  
483 (as done in the present study), renders many problems tractable and calculable. This is the  
484 case with Rohrschollen Island, which shows smooth variations of topography that do not help  
485 to locate ground water outcrops. This comment also extends to the very transient hydraulic  
486 behaviors requiring refined time steps to accurately capture temporal evolutions of the  
487 system.

488 If the focus is placed on infiltration-exfiltration patterns as a reliable indicator of the  
489 effects of restoration in riverine systems, any spatially distributed modeling exercise needs  
490 conditioning regarding both model inputs and outputs. Concerning the conditioning (or  
491 control) of model outputs associated with the delineation of exfiltration areas, the recent



492 technique of airborne, low altitude, and high-resolution thermal infrared imaging is very  
493 promising. The technique is not free of measurement errors and artifacts, but it has been  
494 shown reliable enough to highlight interactions between surface and subsurface compartments  
495 of the hydrosystem that coincide with simulations. Further investigations should duplicate  
496 thermal imaging over time with the aim of grasping the transient behavior of surface-  
497 subsurface interactions and discussing the best versus the worst environmental conditions  
498 where imaging is applicable.

499         Rohrschollen Island (and many other fluvial hydrosystems) is very specific regarding  
500 surface-subsurface interactions, meaning that water heads in the aquifer are often close to  
501 surface water levels. This means that slight variations in both compartments may invert the  
502 direction of exchanged fluxes between compartments. In that case, injecting significant  
503 volumes of water in a system to store them over large periods may be counterproductive, even  
504 though these volumes may contribute to flooding over large areas. Large volumes are diverted  
505 into the rapidly flowing surface water and exit the system. Intense injections of smaller  
506 volumes over short periods foster intense local infiltration into the subsurface. The subsequent  
507 water mounding in the aquifer then results in long-term storage and smooth release of water  
508 via exfiltration. This behavior, hardly foreseeable, was that simulated for Rohrschollen Island  
509 and could also apply to many other configurations of fluvial corridors. These results show that  
510 management rules for a restored system may be developed from modeling exercises handling  
511 various forcing scenarios applied to the system. If it is accepted that exfiltration (sustaining  
512 ponding and wetlands) is a valuable indicator of riverine restoration, additional works should  
513 envision various settings to improve this process. For example, it is not clear if several  
514 smaller inlets could replace a single inlet in the system for higher efficiency. Is water  
515 extraction from the surface and reinjection in the subsurface a valuable process that can



516 generate slow exfiltration over broad areas? Physically-based integrated modeling of

517 hydrosystems might propose some answers.

518

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527



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678



679 **Figure captions**

680

681 Fig. 1. (a) location of the studied area (France), (b) aerial view of Rohrschollen Island, and (c)  
682 network of hydrologic response measurements (mainly hydraulic heads and water fluxes).

683

684 Fig. 2. Digital elevation model of Rohrschollen Island (left) and location of the main gravel  
685 bars reconstructed from the geo-historical and sedimentological studies (right). The black and  
686 white lines correspond to transects of hydrologic measurements (see Figure 1).

687

688 Fig. 3. Evolution over time of flow rates injected in the new artificial channel feeding  
689 Rohrschollen Island during the period selected for calibrating the integrated hydrological  
690 model (up), and the period chosen as a validation (forecasting) exercise (down).

691

692 Fig.4. Calibrated fields of saturated hydraulic conductivity in the subsurface compartment  
693 (left) and exchange coefficient between surface and subsurface compartments (right).

694

695 Fig. 5. Comparison between simulated and measured hydraulic heads in the subsurface during  
696 the calibration period. Left: evolution over time at the two transects, that is, the worst (up) and  
697 best (down) transects regarding RMSE. Right: Local in space and time values of simulated  
698 hydraulic heads as a function of observed ones. RMSE = root of mean square error, and KGE  
699 = Kling-Gupta efficiency.

700

701 Fig. 6. Comparison between simulated and measured hydraulic heads in the subsurface during  
702 the validation period. Left: evolution over time at the two transects, that is, the worst (up) and  
703 best (down) transects regarding RMSE. Right: local in space and time values of simulated  
704 hydraulic heads as a function of observed ones. RMSE = root of mean square error, and KGE  
705 = Kling-Gupta efficiency.

706

707 Fig 7. Comparison between simulated exfiltration patterns and thermal anomalies identified  
708 via thermal infrared imaging close to the junction between the new channel (southeast corner)  
709 and the BGW (Bauerngrundwasser; center of Fig.). Red transects a and b are locations where  
710 surface water and groundwater head are followed to exemplify surface-subsurface interactions  
711 in Fig 9.

712

713 Fig. 8. Groundwater head, surface water thickness, and exfiltration rate over the whole of  
714 Rohrschollen Island for three different periods (in hours after the beginning of injection) of  
715 the calibration period. Notably, the last period is also the date of the airborne thermal infrared  
716 imaging.

717

718 Fig. 9. Evolution of surface water elevation (blue), groundwater head (red), and exchange  
719 fluxes (arrows) along transects a and b (located in Fig. 7) at two periods (hours after the  
720 beginning of injection) of the calibration period. A thick grey line represents the topographic  
721 profile. The grey scale indicates values of the saturated hydraulic conductivity at the interface  
722 between surface and subsurface.

723

724 Fig. 10. Evolution of the infiltration and exfiltration volumetric fluxes during the first steps of  
725 the calibration period (where evolutions are essential).

726

727 Fig. 11. Patterns of exfiltration for the pre-restored and the restored situations. The focus is on  
728 the most active zone of Rohrschollen Island regarding surface-subsurface interactions.



729

730

Fig. 12. Up: injection rates of two scenarios seeking optimal exfiltration surface areas and durations at Rohrschollen Island. Down: Evolution over time of excess or lack of exfiltration surface area compared with exfiltration surface produced by a routine injection rate of  $2 \text{ m}^3 \text{ s}^{-1}$  at the inlet of the system.

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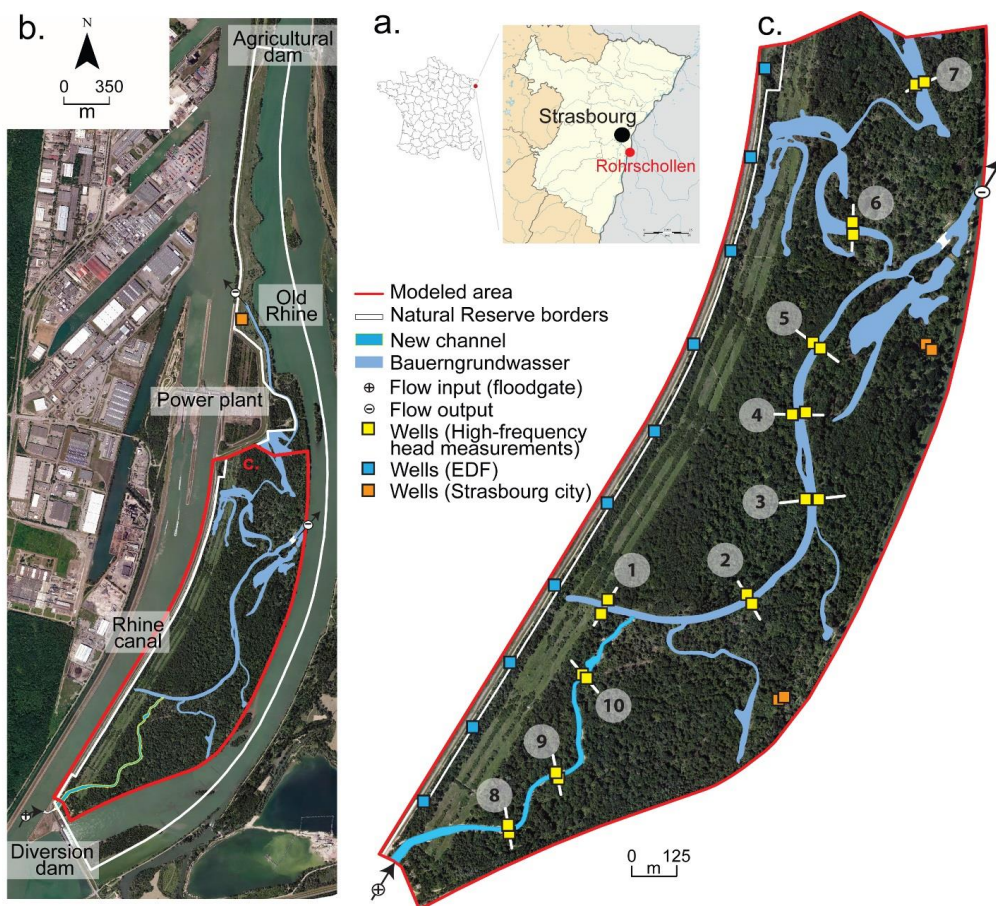
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781 **Fig 1.** (a) location of the studied area (France), (b) aerial view of Rohrschollen Island, and (c)  
782 network of hydrologic response measurements (mainly hydraulic heads and water fluxes).

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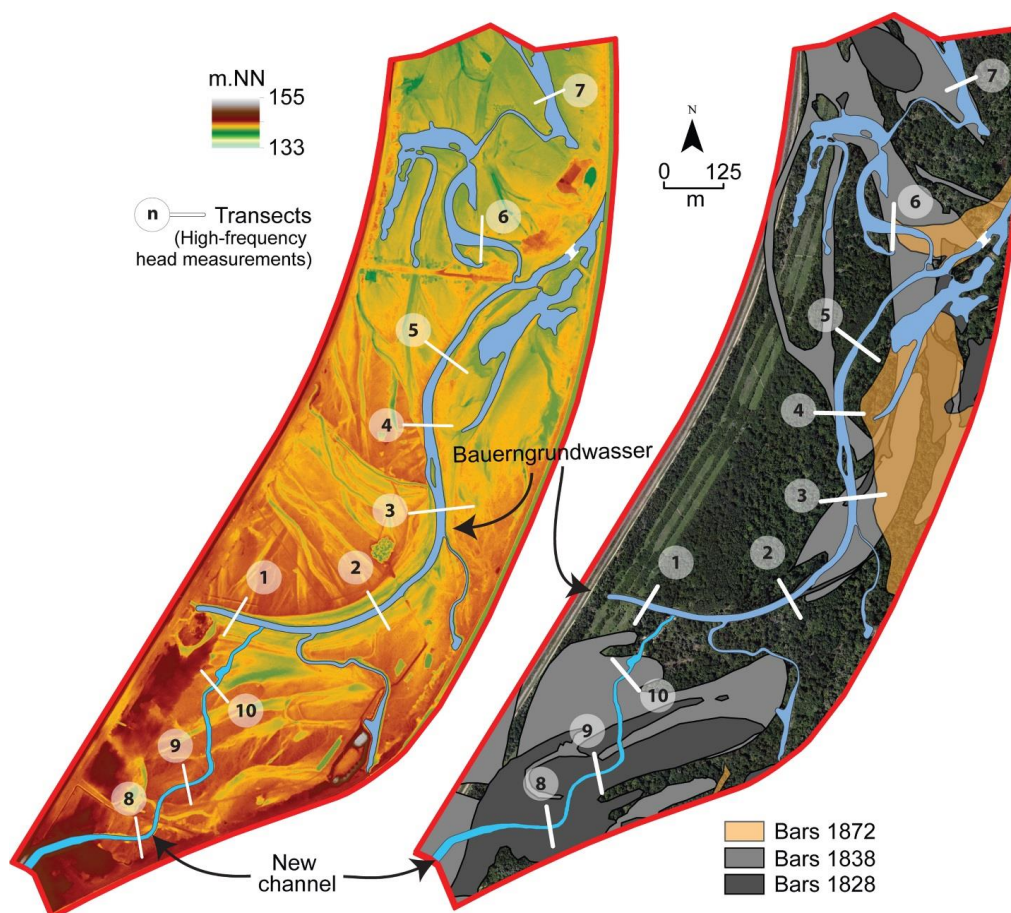
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791 **Fig 2.** Digital elevation model of Rohrschollen Island (left) and location of the main gravel  
792 bars reconstructed from the geo-historical and sedimentological studies (right). The black and  
793 white lines correspond to transects of hydrologic measurements (see Figure 1).

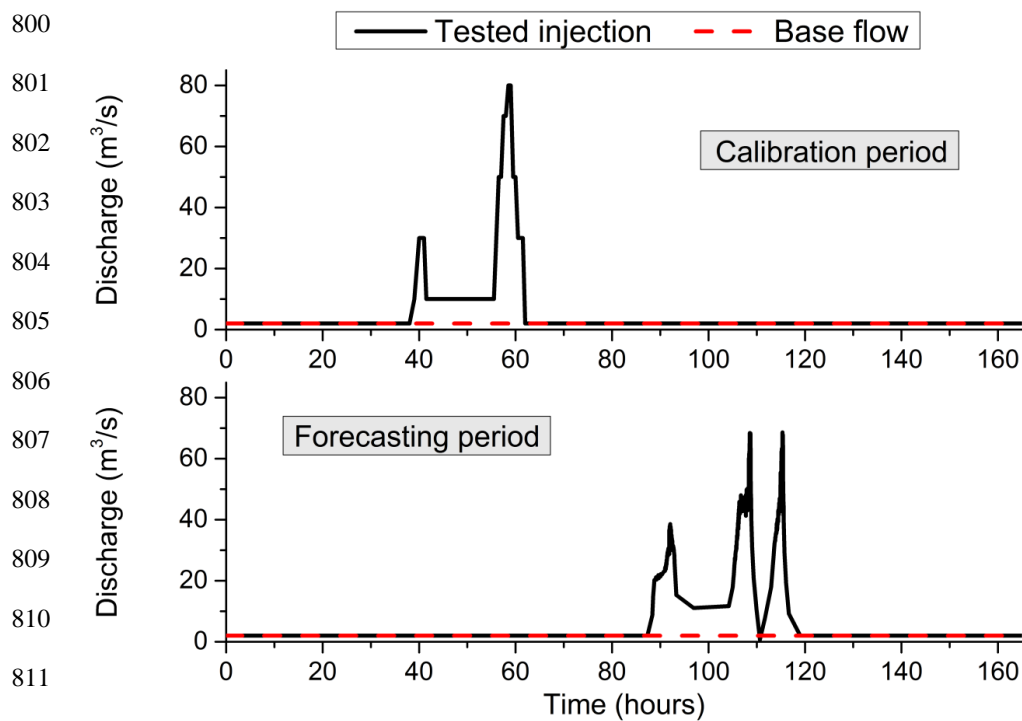
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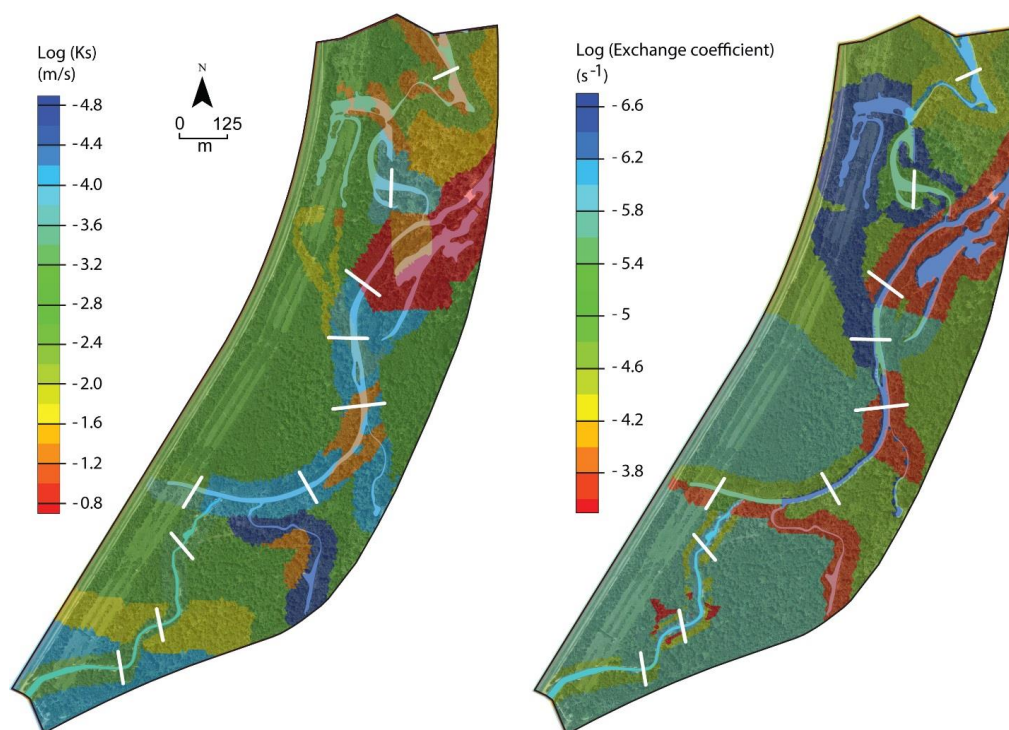
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813 **Fig. 3.** Evolution over time of flow rates injected in the new artificial channel feeding  
814 Rohrschollen Island during the period selected for calibrating the integrated hydrological  
815 model (up), and the period chosen as a validation (forecasting) exercise (down).  
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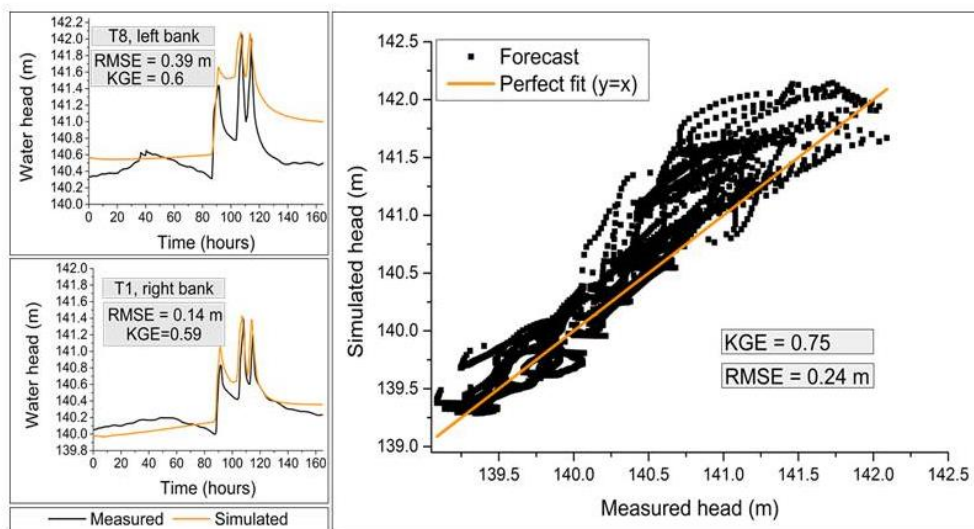
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819 **Fig 4.** Calibrated fields of saturated hydraulic conductivity in the subsurface compartment  
820 (left) and exchange coefficient between surface and subsurface compartments (right).

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824 **Fig. 5.** Comparison between simulated and measured hydraulic heads in the subsurface during  
825 the calibration period. Left: evolution over time at the two transects, that is, the worst (up) and  
826 best (down) transects regarding RMSE. Right: Local in space and time values of simulated  
827 hydraulic heads as a function of observed ones. RMSE = root of mean square error, and KGE  
828 = Kling-Gupta efficiency.

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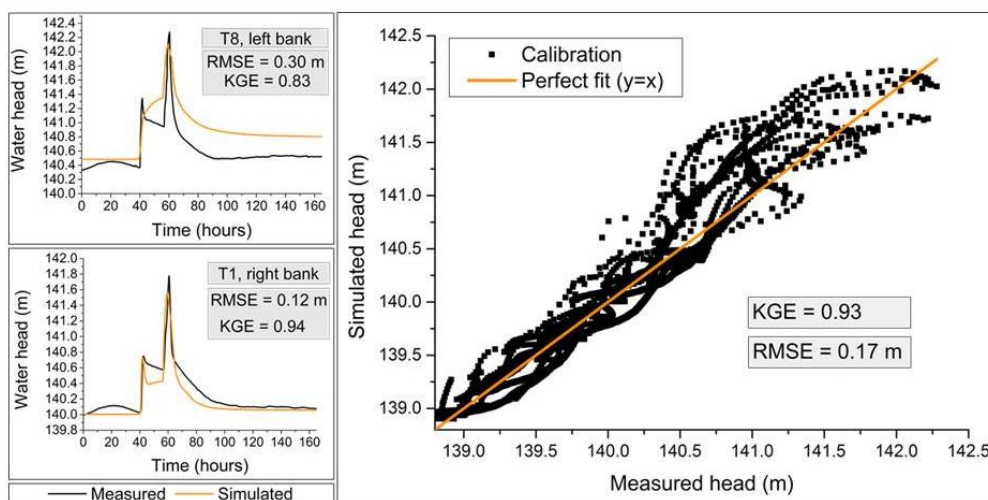
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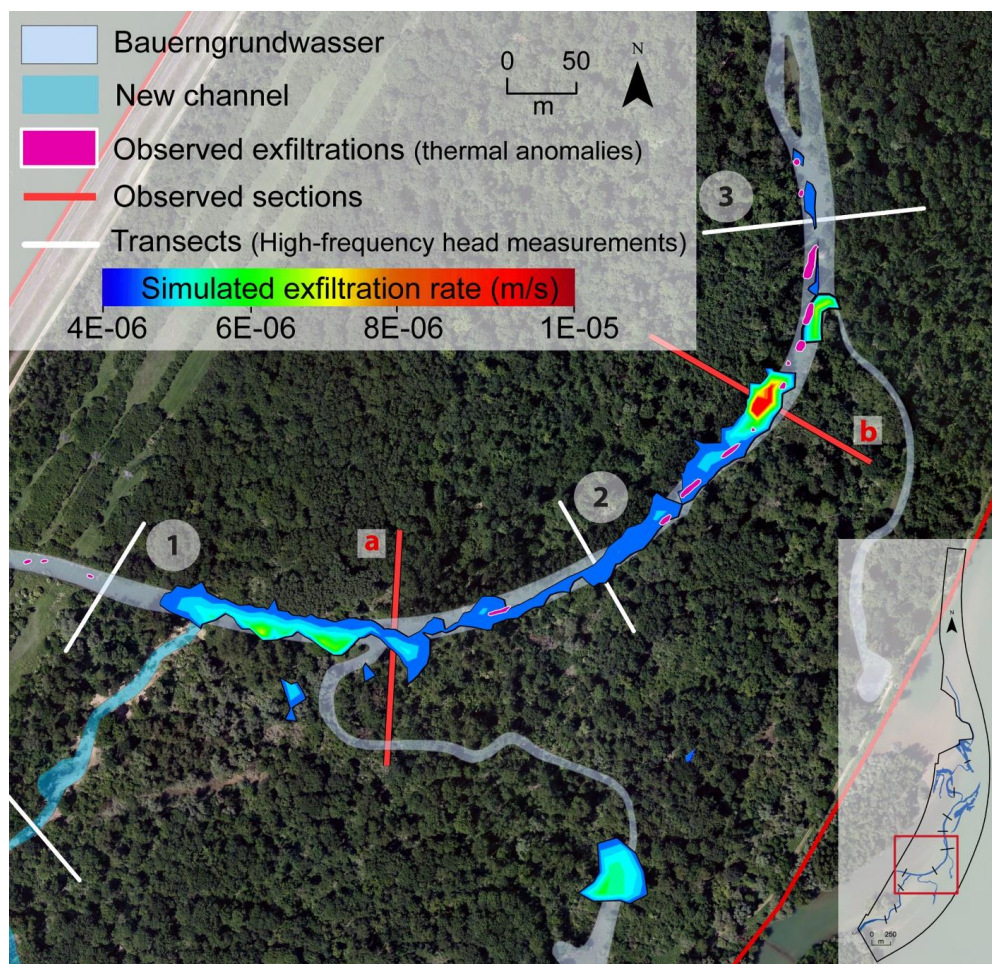
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839 **Fig. 6.** Comparison between simulated and measured hydraulic heads in the  
840 subsurface during the validation period. Left: evolution over time at the two transects, that is,  
841 the worst (up) and best (down) transects regarding RMSE. Right: local in space and time  
842 values of simulated hydraulic heads as a function of observed ones. RMSE = root of mean  
843 square error, and KGE = Kling-Gupta efficiency.

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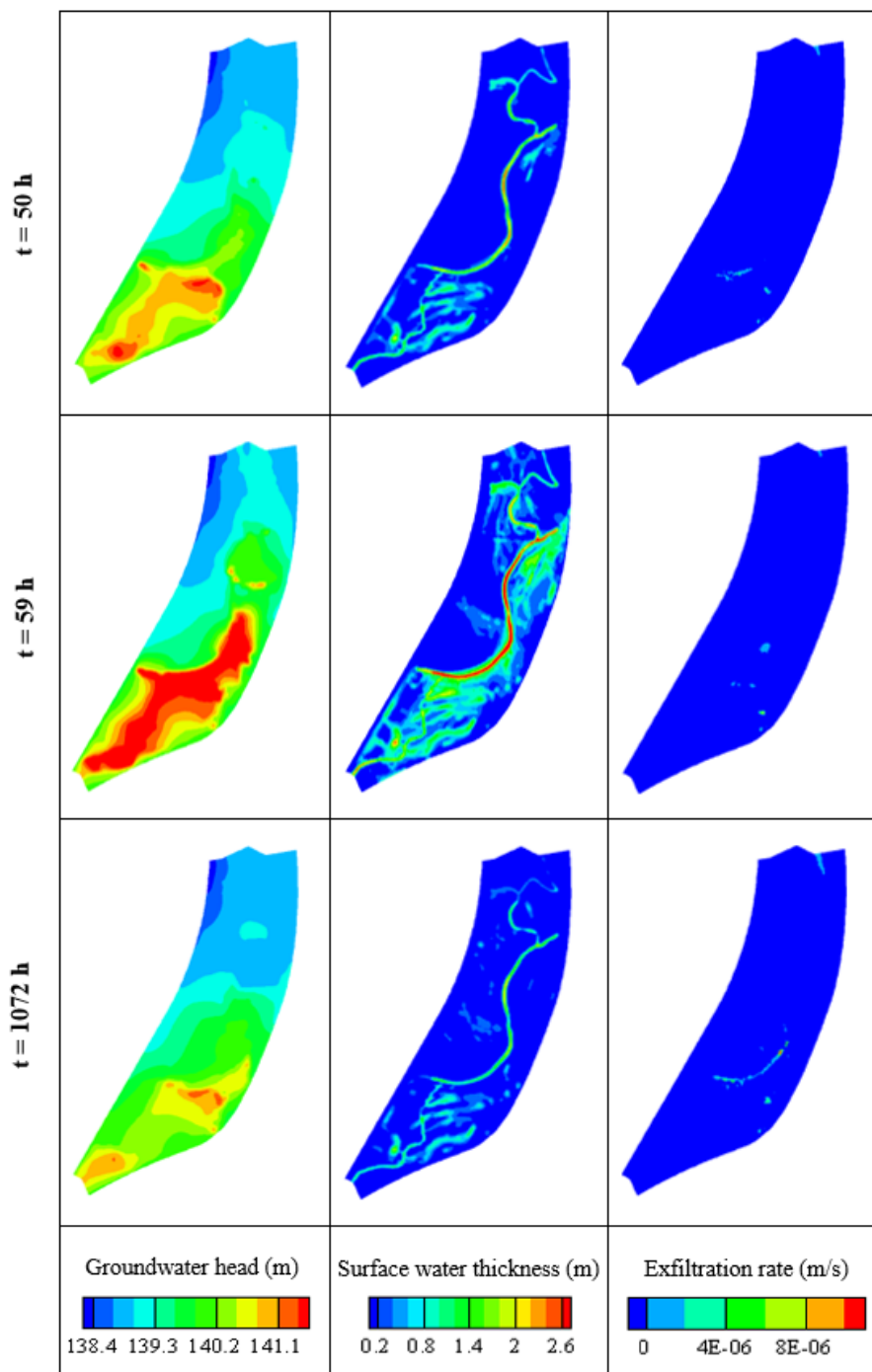
848 **Fig 7.** Comparison between simulated exfiltration patterns and thermal anomalies identified  
849 via thermal infrared imaging close to the junction between the new channel (southeast corner)  
850 and the BGW (Bauerngrundwasser; center of Fig.). Red transects a and b are locations where  
851 surface water and groundwater head are followed to exemplify surface-subsurface interactions  
852 in Fig 9.

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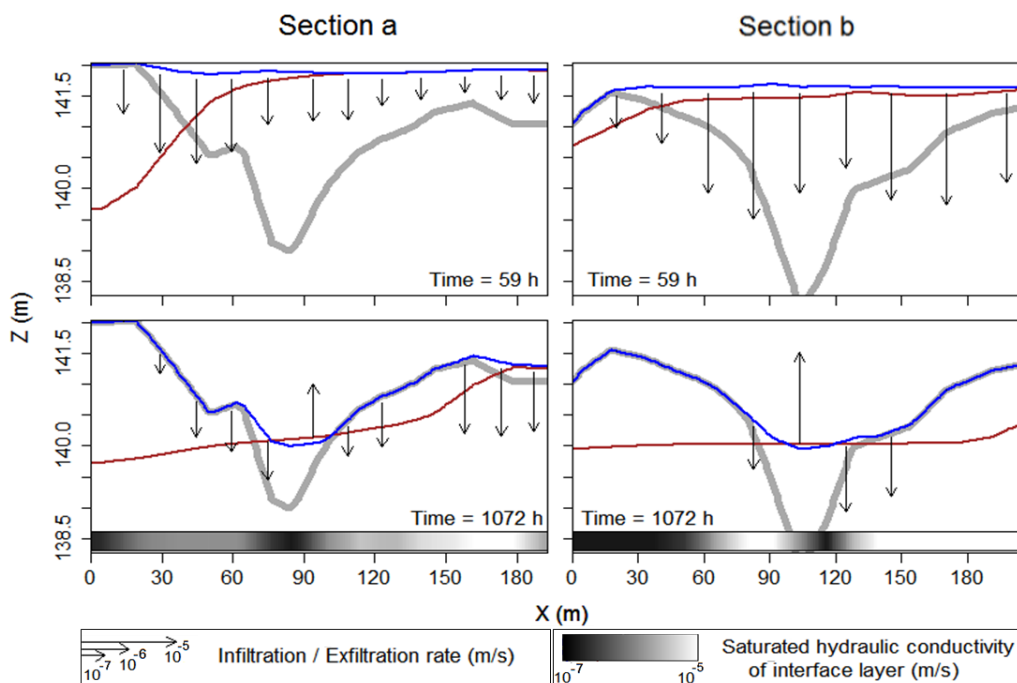
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857 **Fig 8.** Groundwater head, surface water thickness, and exfiltration rate over the whole of  
 858 Rohrschollen Island for three different periods (in hours after the beginning of injection) of  
 859 the calibration period. Notably, the last period is also the date of the airborne thermal infrared  
 860 imaging.



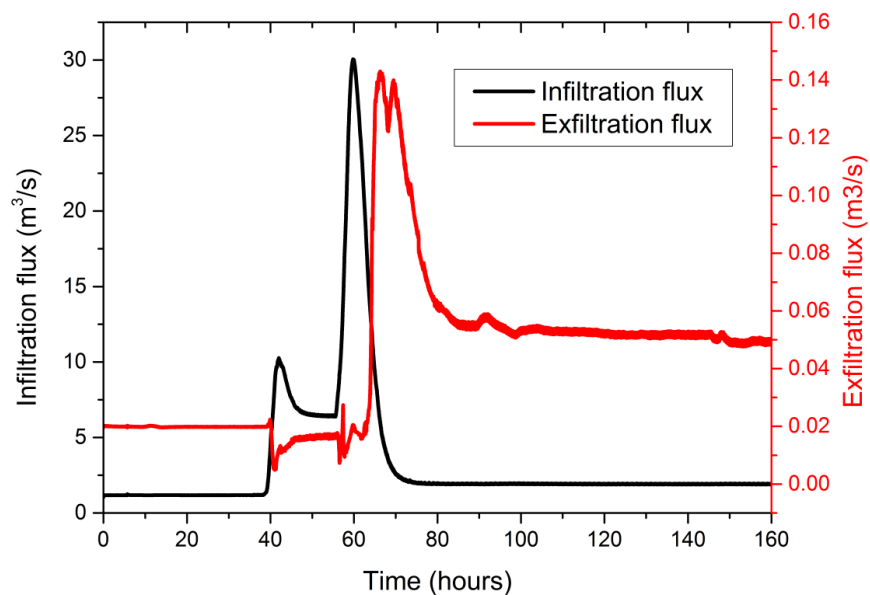
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863 **Fig. 9.** Evolution of surface water elevation (blue), groundwater head (red), and exchange  
 864 fluxes (arrows) along transects a and b (located in Fig. 7) at two periods (hours after the  
 865 beginning of injection) of the calibration period. A thick grey line represents the topographic  
 866 profile. The grey scale indicates values of the saturated hydraulic conductivity at the interface  
 867 between surface and subsurface.

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871 **Fig 10.** Evolution of the infiltration and exfiltration volumetric fluxes during the first steps of  
872 the calibration period (where evolutions are essential).

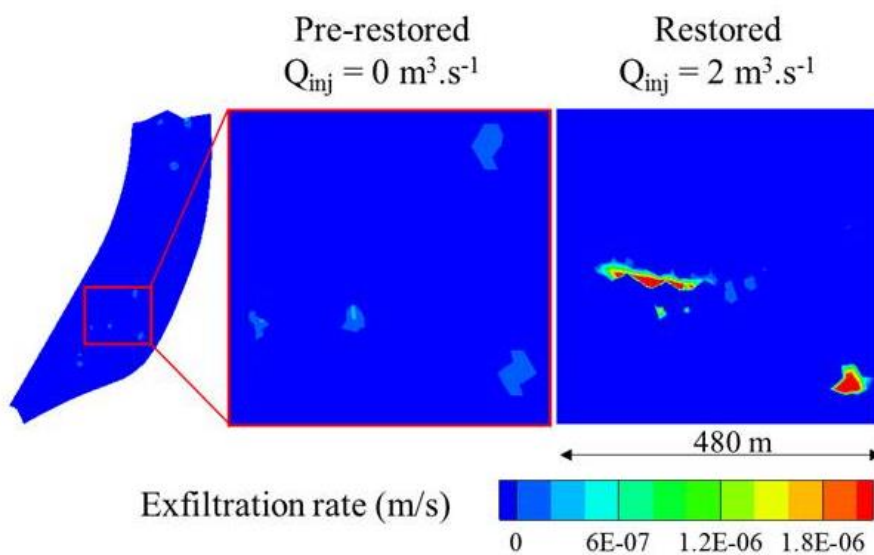
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878 **Fig. 11.** Patterns of exfiltration for the pre-restored and the restored situations. The focus is on  
879 the most active zone of Rohrschollen Island regarding surface-subsurface interactions.

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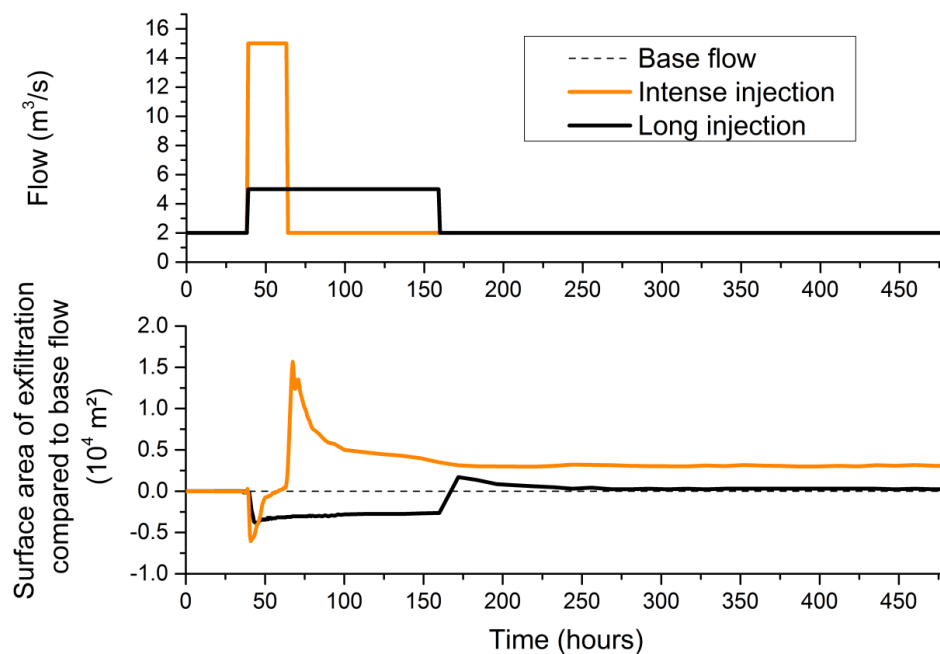
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885 **Fig 12.** Up: injection rates of two scenarios seeking optimal exfiltration surface areas and  
886 durations at Rohrschollen Island. Down: Evolution over time of excess or lack of exfiltration  
887 surface area compared with exfiltration surface produced by a routine injection rate of  $2 \text{ m}^3 \text{ s}^{-1}$   
888 at the inlet of the system.  
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