



Sources and fate of nitrate in groundwater at agricultural operations overlying glacial sediments

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10 **Abstract.** Leaching of nitrate (NO_3^-) from animal waste or fertilizers at agricultural operations can result in NO_3^- contamination of groundwater, lakes, and streams. Understanding the sources and fate of nitrate in groundwater systems in glacial sediments, which underlie many agricultural operations, is critical for managing impacts of human food production on the environment. Elevated NO_3^- concentrations in groundwater can be naturally attenuated through mixing or denitrification. Here we use snapshots of the stable isotope values of NO_3^- to quantify denitrification in groundwater at two confined feeding operations overlying glacial sediments in Alberta, Canada. 15 Uncertainty in $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ values of the NO_3^- source and denitrification enrichment factors are accounted for using a Monte Carlo approach. When denitrification could be quantified, we reconstructed the initial $\text{NO}_3\text{-N}$ concentration and $\text{NO}_3\text{-N/Cl}^-$ ratio at the point of entry to the groundwater system. The addition of NO_3^- to the local groundwater system from temporary manure piles and pens equalled or exceeded NO_3^- additions due to leaching from earthen manure storages at these sites. Nitrate attenuation at both sites is attributed to a spatially variable combination of mixing and denitrification, but is dominated by denitrification. On-site denitrification reduced agriculturally derived NO_3^- concentrations by at least half and, in some wells, completely. These results indicate that infiltration to groundwater systems in glacial sediments where NO_3^- can be naturally attenuated is likely preferable to off-farm export via runoff or drainage networks. The application of isotopes of nitrate to 20 constrain a mixing model based on concentrations of Cl^- and NO_3^- , which can be routinely monitored in groundwater, provides a relatively simple method to assess the sources and fate of agriculturally derived NO_3^- in these settings.

1 Introduction

25 The contamination of soil and groundwater with nitrate from agricultural operations is a global water quality issue that has been extensively documented (Power and Schepers, 1989; Spalding and Exner, 1993; Rodvang and Simpkins, 2001; Galloway et al., 2008; Zirkle et al., 2016; Arauzo, 2017; Ascott et al., 2017). Leaching of nitrate (NO_3^-) from animal waste or fertilizers can result in groundwater NO_3^- concentrations that exceed drinking water guidelines and pose human health risks (Fan and Steinberg, 1996; Gulis et al., 2002; Yang et al., 2007). The discharge of high- NO_3^- groundwater, runoff, or drainage can contaminate streams and lakes, resulting in eutrophication and ecosystem decline (Deutsch et al., 2006; Kaushal et al., 2011). In saturated groundwater systems with low oxygen concentrations, elevated NO_3^- can be naturally attenuated by microbial denitrification



(Wassenaar, 1995; Robertson et al., 1996; Smith et al., 1996; Tesoriero et al., 2000; Singleton et al., 2007). Concentrations of NO_3^- will also decrease along groundwater flow paths due to attenuation via dilution by hydrodynamic dispersion (referred to hereafter as mixing). Because of these natural attenuation mechanisms, infiltration to groundwater may be preferable to off-site drainage and runoff of nitrate-rich waters. Many agricultural operations are undertaken on fertile soils associated with glacial sediments (Spalding and Exner, 1993; Ernstsens et al., 2015; Zirkle et al., 2016). Understanding the sources and fate of agriculturally derived nitrate in groundwater systems in glacial sediments is therefore critical for managing impacts of human food production on the environment.

Identification of the sources and fate of NO_3^- at agricultural operations can be challenging because of spatial and temporal variations in sources (e.g. earthen manure storage, temporary manure piles, or fertilizer) and the complexity of hydrogeologic systems (Spalding and Exner, 1993; Rodvang et al., 2004; Showers et al., 2008; Kohn et al., 2016). These spatial and temporal variations can result in complex subsurface solute distributions that are difficult to interpret using classical transect studies or numerical groundwater models (Green et al., 2010; Baily et al., 2011).

Groundwater containing significant agriculturally derived NO_3^- also typically has elevated chloride (Cl^-) concentrations (Saffigna and Keeney, 1977; Rodvang et al., 2004; Menció et al., 2016). Decreasing $\text{NO}_3\text{-N}/\text{Cl}^-$ (or $\text{NO}_3^-/\text{Cl}^-$) ratios have been used to define denitrification based on the assumption that NO_3^- is reactive while Cl^- is non-reactive (conservative), such that denitrification results in a decrease in the $\text{NO}_3\text{-N}/\text{Cl}^-$ ratio (Kimble et al., 1972; Weil et al., 1990; Liu et al., 2006; McCallum et al., 2008). However, $\text{NO}_3\text{-N}/\text{Cl}^-$ ratios can also change in response to mixing of groundwater with different $\text{NO}_3\text{-N}/\text{Cl}^-$ ratios or when groundwater sampling traverses hydraulically disconnected formations (Bourke et al., 2015b). If $\text{NO}_3\text{-N}/\text{Cl}^-$ ratios vary among potential sources and the $\text{NO}_3\text{-N}/\text{Cl}^-$ ratio at the point of entry to the groundwater system can be reconstructed, this information could be used to show that anthropogenic NO_3^- at different locations within an aquifer is derived from the same or different sources.

The stable isotopes of NO_3^- ($\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$) provide an alternative approach to characterize the source and fate of NO_3^- in groundwater systems. In agricultural areas, multiple sources of NO_3^- are common and could include precipitation, soil NO_3^- , inorganic fertilizer, manure, and septic waste (Komor and Anderson, 1993; Liu et al., 2006; Pastén-Zapata et al., 2014; Clague et al., 2015; Xu et al., 2015). While source identification is theoretically possible using $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ (particularly with a dual-isotope approach), in practice this can be difficult due to geologic heterogeneity, overlapping source values, and the complexity of biologically mediated reactions (Aravena et al., 1993; Wassenaar, 1995; Mengis et al., 2001; Choi et al., 2003; Granger et al., 2008; Vavilin and Rytov, 2015; Xu et al., 2015). NO_3^- attenuation by denitrification in groundwater systems can be identified based on the characteristic enrichment of $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$. Numerous studies have made qualitative assessments of denitrification using the stable isotope approach (Böttcher et al., 1990; Wassenaar, 1995; Singleton et al., 2007; Baily et al., 2011; Clague et al., 2015; Xu et al., 2015). However, very few published field studies report quantitative assessments of denitrification based on isotopic enrichment of $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ and, to our knowledge, none account for uncertainties in source values or enrichment factors (Böttcher et al., 1990; Otero et al., 2009; Xue et al., 2009).

A synthesized analysis of stable isotopes of NO_3^- with additional ionic tracers can improve the assessment of NO_3^- attenuation mechanisms and sources of NO_3^- in agricultural settings (Showers et al., 2008; Vitòria et al., 2008;



Xue et al., 2009; Xu et al., 2015). If the amount of denitrification can be quantified based on $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$, then the ratio of $\text{NO}_3\text{-N}/\text{Cl}^-$ at the point of entry to the groundwater system can be calculated from measured NO_3^- and Cl^- concentrations (see Section 2.3) and this ratio used to assess the source of the NO_3^- . These data can also be used to quantify attenuation by mixing and the initial concentrations of NO_3^- and Cl^- at the point of entry to the groundwater system. Uncertainties in source values and enrichment factors can be constrained using measured data and explicitly accounted for using a Monte Carlo approach (Joerin et al., 2002; Bourke et al., 2015a).

In this study, we present the application of this approach at two confined feeding operations (CFOs) in Alberta, Canada, with differing lithologies and durations of operation (Fig. 1). The first study area (CFO1), located 25 km northeast of Lethbridge, Alberta, was established in 1928 and had approximately 150 head of dairy cattle at the time of the study. An associated earthen manure storage (EMS) facility for storing liquid dairy manure was constructed in the 1960s. A 2000-head beef feedlot, established in the 1960s, was also present at CFO1. The second study area (CFO4), located approximately 30 km north of Red Deer, Alberta and 300 km north of CFO1, was constructed in 1995 (including an EMS) and had 350 head of dairy cattle at the time of the study. To the best of our knowledge, fertilizers have not been applied at either of these sites, and infiltration of manure waste is assumed to be the cause of elevated NO_3^- concentrations in the local groundwater. Concentrations of Cl^- and nitrogen species (N-species) and the stable isotopes of NO_3^- were measured in groundwater samples collected from monitoring wells and continuous soil cores, as well as manure filtrate at both sites. These data were interpreted to (1) assess the extent of agriculturally derived NO_3^- in groundwater, (2) identify sources and initial concentrations of NO_3^- at the point of entry to the groundwater system, and (3) assess the dominant attenuation mechanisms controlling subsurface NO_3^- distributions at these sites.

2 Materials and methods

2.1 Sampling and instrumentation

2.1.1 Groundwater monitoring wells

Groundwater samples were collected from water table wells and piezometers (hereafter both are referred to as wells) installed at both sites (Fig. 1, Table 1) At CFO1, groundwater samples were collected from six individual water table wells (DMW1, DMW2, DMW3, DMW4, DMW5, DMW6) and eight sets of nested wells with one well screened at the water table and one well screened 20 m below ground (BG) (DP10-2 and DP10-1, DMW10 and DP11-10b, DMW11 and DP11-11b, DMW12 and DP11-12b, DMW13 and DP11-13b, DMW14 and DP11-14b, DMW15 and DP11-15b, and DMW16 and DP11-16b). Wells DP10-2 and DP10-1 were located directly adjacent to the EMS on the hydraulically downgradient side. At CFO4, groundwater samples were collected from eight water table wells (BC1, BC2, BC3, BC4, BC5, BMW1, BMW3, BMW7) and four sets of nested wells, with wells screened across the water table and at 15 m BG. Two of these nests were located adjacent to the EMS (BMW2 and BP10-15e, BMW4 and BP10-15w) and two were hydraulically downgradient of the EMS (BMW5 and BP5-15, BMW6 and BP6-15).

Groundwater samples were collected for ion analysis (Cl^- and N species) quarterly between April 2010 and August 2015. All water samples were collected using a bailer after purging (1–3 casing volumes) and stored at $\leq 4^\circ\text{C}$ prior to analysis. Samples for $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ were collected from wells at CFO1 on 1 January 2013 and 1 May 2013. Samples for $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ at CFO4 were collected on 27 October 2014. Wells were purged



prior to sample collection (1–3 casing volumes), and samples filtered into high-density polyethylene (HDPE) bottles in the field and frozen until analysis.

Hydraulic heads in monitoring wells were determined using manual measurements (approximately monthly, 2010–2015). Rising head response tests (slug or bail tests) were conducted to determine hydraulic conductivity (K) of the formation media surrounding the intake zone on the majority of the wells at the sites.

2.1.2 Continuous core

Continuous core was collected at CFO1 immediately adjacent to well DP11-13b on 1 May 2013 (Fig. 1). Additional core samples were collected from 1 to 5 June 2015 along a transect hydraulically downgradient of the southeastern side of the EMS at CFO1 where hydrochemistry data suggested leakage from the EMS (see Section 3). During this 2015 drilling campaign, core samples were collected at four locations (DC15-20, DC15-21, DC15-22, DC15-23) to depths of up to 15 m below surface and distances of up to 100 m from the EMS between wells DMW3 and DP11-14.

Continuous core samples were retrieved using a hollow stem auger (1.5-m core lengths) with 0.3-m sub-samples collected at approximately 1-m intervals ensuring that visually consistent lithology could be sampled. Core samples for Cl⁻ were stored in Ziploc™ bags and kept cool until analysis. Core samples for N-species analysis were stored in Ziploc bags filled with an atmosphere of argon (99.9% Ar) to minimize oxidation and kept cool until analysis. Subsamples of each core (250–300 g) were placed under 50 MPa pressure in a Carver Series NE mechanical press with a 0.5-µm filter placed at the base of the squeezing chamber, which was placed within an Ar atmosphere to minimize oxidation. A syringe was attached to the base of the apparatus and 15 mL of filtered pore water were collected for analyses within 3.5 to 6.0 h (Hendry et al., 2013).

2.1.3 Liquid manure storages

Samples of liquid manure slurry were collected directly from the EMS at both sites and the catch basin (containing local runoff from the feedlot) at CFO1 using a pipe and plunger apparatus to sample from approximately 0.5 m below the surface. The slurry collected was subsequently filtered (0.45 µm) to separate the liquid and solid components. The water filtered from samples collected from the EMS or catch basin is hereafter referred to as manure filtrate.

2.2 Laboratory analysis

For groundwater samples from wells, concentrations of Cl⁻ were determined using potentiometric titration of H₂O, with a detection limit of 5.0 mg L⁻¹ and accuracy of 5% (APHA 4500-Cl⁻ D). Concentrations of NH₃ as N (NH₃-N), NO₃⁻ as N (NO₃-N), and NO₂⁻ as N (NO₂-N) in groundwater samples from wells were measured by air-segmented continuous flow analysis (APHA 4500-NH₃ G, APHA 4500-NO₃- F). Total nitrogen (TN) was determined by high temperature catalytic combustion and chemiluminescence detection using a Shimadzu TOC-V with attached TN unit (ASTM D8083-16). Total Kjeldahl nitrogen (TKN) was then calculated by subtracting the concentrations of NO₃-N and NO₂-N from TN. Bicarbonate (HCO₃⁻) was analyzed by titration (APHA 2320 B). Dissolved organic carbon (DOC) was analyzed by a combustion infrared method (APHA 5310 B) using a Shimadzu TOC-V system.



Pore-water samples squeezed from continuous core were analyzed for Cl⁻, NO₃-N, and NO₂-N using a Dionex IC25 ion chromatograph (IC) coupled to a Dionex As50 autosampler (EPA Method 300.1, accuracy and precision of 5.0%) (Hautman and Munch, 1997). Ammonia as N (NH₃-N) was measured by Exova Laboratories using the automated phenate method (APHA Standard 4500-NH₃ G, detection limit of 0.025 mg L⁻¹, accuracy of 2% of the measured concentration, and a precision of 5% of the measured concentration).

$\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ in groundwater samples (from wells and pore water from continuous core) and manure filtrate were measured at the University of Calgary (Calgary, Alberta) using the denitrifier method (Sigman et al., 2001) with an accuracy and precision of 0.3‰ for $\delta^{15}\text{N}_{\text{NO}_3}$ and 0.3‰ for $\delta^{18}\text{O}_{\text{NO}_3}$. Groundwater samples collected for NO₃⁻ isotope analysis in January 2013 were also analyzed for NO₃-N by the University of Calgary (denitrifier technique, Delta+XL).

2.3 Modelling approach

2.3.1 Quantification of denitrification based on $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$

Groundwater that has undergone denitrification can be identified by enrichment of $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ with a characteristic slope of about 0.5 on a cross-plot (Clark and Fritz, 1997). The relationship between isotopic enrichment of $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ and the fraction of NO₃-N remaining during denitrification can be described by a Rayleigh equation:

$$R = R_0 f_d^{\left(\frac{1}{\beta} - 1\right)}, \quad (1)$$

where R_0 is the initial isotope ratio of the NO₃⁻ ($\delta^{18}\text{O}_{\text{NO}_3}$ or $\delta^{15}\text{N}_{\text{NO}_3}$), R is the isotopic ratio when fraction f_d of NO₃⁻ remains, and β is the kinetic fractionation factor (> 1) (Clark and Fritz, 1997). Kinetic fraction effects are commonly also expressed as the enrichment factor, $\epsilon = 1000(\beta - 1)$. In the case of a constant enrichment factor, f_d can be calculated from:

$$f_d = \exp\left(\frac{R - R_0}{\epsilon}\right). \quad (2)$$

The extent of denitrification, as indicated by the fraction of NO₃-N remaining (f_d), was quantified in a sub-set of 20 samples with isotopic values of NO₃⁻ indicative of denitrification. For each sample, f_d (mean and standard deviation) was calculated from Eq. (2) using a Monte Carlo approach with 500 realizations. The value of R was given by the measured isotopic ratio for each sample ($\delta^{18}\text{O}_{\text{NO}_3}$ or $\delta^{15}\text{N}_{\text{NO}_3}$). R_0 was allowed to vary randomly within a range of values determined from measured data and literature values. If the initial $\delta^{15}\text{N}_{\text{NO}_3}$ is known, ϵ for $\delta^{15}\text{N}_{\text{NO}_3}$ ($\epsilon_{15\text{N}}$) can be determined from the slope of the linear regression line on a plot of $\ln(f_d)$ vs. $\delta^{15}\text{N}_{\text{NO}_3}$ (Böttcher et al., 1990). If the initial $\delta^{15}\text{N}_{\text{NO}_3}$ and f_d are not known, as is the case here, $\epsilon_{15\text{N}}$ can be determined from the slope of the regression line on a plot of $\ln(\text{NO}_3\text{-N})$ vs. $\delta^{15}\text{N}_{\text{NO}_3}$, which will be the same as on a plot of $\ln(f_d)$ vs. $\delta^{15}\text{N}_{\text{NO}_3}$. The enrichment factor for $\delta^{18}\text{O}_{\text{NO}_3}$ ($\epsilon_{18\text{O}}$) was calculated by multiplying the $\delta^{15}\text{N}_{\text{NO}_3}$ by a linear coefficient of proportionality determined for each CFO from the slope of the denitrification trend on an isotope cross-plot (see Section 3.2). This approach neglects the effect of mixing of groundwater with differing isotopic values, and is valid if the concentration of NO₃⁻ in the source is much greater than background concentrations such that the isotopic composition of NO₃⁻ is dominated by the agriculturally derived end-member.



2.3.2 Quantification of mixing and initial concentrations of Cl⁻ and NO₃-N

A binary mixing model that also accounts for decreasing NO₃-N concentrations in response to denitrification was used to quantify NO₃⁻ attenuation by mixing and estimate the initial concentrations of Cl⁻ and NO₃-N. The measured concentration of Cl⁻ was assumed to be a function of two end-member mixing, described by

$$5 \quad Cl = f_m Cl_i + (1 - f_m) Cl_b, \quad (3)$$

where Cl is the measured concentration of Cl⁻ in the groundwater sample, Cl_i is the concentration of Cl⁻ at the initial point of entry of the agriculturally derived NO₃⁻ to the groundwater system, Cl_b is the concentration of Cl⁻ in the background ambient groundwater, and f_m is the fraction of water in the sample from the source of agriculturally derived Cl⁻ (and NO₃⁻) remaining in the mixture.

10 The concentration of NO₃-N was also assumed to be a function of two end-member mixing but with an additional coefficient, f_d (the fraction of NO₃-N remaining after denitrification), applied to account for denitrification. The measured NO₃-N concentration was thus described by

$$NO_3-N = f_d (f_m NO_3-N_i + (1 - f_m) NO_3-N_b), \quad (4)$$

15 where NO_3-N is the concentration of NO₃-N measured in the groundwater sample, NO_3-N_i is the concentration of NO₃-N in the source of agriculturally derived NO₃⁻ at the initial point of entry to the groundwater system, and NO_3-N_b is the concentration of NO₃-N in the background ambient groundwater.

If Cl_i is much greater than Cl_b and NO_3-N_i is much greater than NO_3-N_b , then f_m is insensitive to background concentrations and these terms can be neglected (see Section 4 for further discussion of this assumption). In this case, Eqs. (3) and (4) reduce to

$$20 \quad Cl = f_m Cl_i, \quad (5)$$

$$NO_3-N = f_d (f_m NO_3-N_i). \quad (6)$$

Solving Eq. (6) for f_m and substituting into Eq. (5) yields

$$\frac{NO_3-N_i}{Cl_i} = \frac{1}{f_d} \frac{NO_3-N}{Cl}. \quad (7)$$

Thus, for each groundwater sample, the ratio of NO₃-N/Cl⁻ at the initial point of entry of the agriculturally derived NO₃⁻ to the groundwater system ($\frac{NO_3-N_i}{Cl_i}$) can be simply calculated using measured concentrations, and f_d estimated from NO₃⁻ isotope data. This provides a relatively simple method to identify agriculturally derived NO₃⁻ from different sources (e.g., EMS vs. manure piles) if they have different NO₃-N/Cl⁻ ratios. Estimated Cl_i and NO_3-N_i are reported as the mid-range value with uncertainty described by the minimum and maximum values. These initial concentrations are at the water table for top-down inputs, or at the saturated point of contact between the EMS and the aquifer for leakage from the EMS. This analysis assumes that a sampled water parcel consists of water with agriculturally derived NO₃⁻ that entered the aquifer from one source at one point in time and space and has since mixed with natural ambient groundwater. Any NO₃⁻ produced during nitrification after the anthropogenic source water enters the aquifer is implicitly included in NO_3-N_i . The error in $\frac{NO_3-N_i}{Cl_i}$ was assumed to be dominated by error in the estimated f_d , with the measurement error in NO₃-N and Cl⁻ considered negligible.

35 The amount of mixing is indicated by the fraction of source remaining (f_m) and, therefore, the initial concentrations of the agriculturally derived NO₃⁻ source (NO_3-N_i and Cl_i) were estimated by simultaneously solving Eqs. (5) and (6) using Excel Solver (GRG nonlinear). The absolute minimum values of NO_3-N_i and Cl_i were defined by measured concentrations (e.g., if $Cl_i=Cl$, $f_m=1$). Maximum values of NO_3-N_i and Cl_i were defined based on



measured concentrations of $\text{NO}_3\text{-N}$ and Cl^- in groundwater and manure filtrate ($\text{NO}_3\text{-N} \leq 150 \text{ mg L}^{-1}$ and $\text{Cl}^- \leq 1300 \text{ mg L}^{-1}$; see Section 3.2). These maximum values of $\text{NO}_3\text{-N}_i$ and Cl_i correspond to the minimum f_m . The value of f_d was assumed to be the mean f_d estimated from NO_3^- isotopes using Eq. (2), and $\frac{\text{NO}_3\text{-N}_i}{\text{Cl}_i}$ was required to be within one standard deviation of the estimate from Eq. (7). The resulting estimates of f_m are reported as the mid-range, with uncertainty described by the minimum and maximum values. Larger values of f_m indicate less mixing (a shorter path for advection-dispersion) and suggest a source close to the well. Smaller values of f_m indicate extensive mixing (a longer path for advection-dispersion) and suggest a source further away from the well. The relative contributions of mixing and denitrification to NO_3^- attenuation at each site were evaluated by comparing f_m and f_d for each sample. This analysis was conducted using isotope values from the samples collected on 1 May 2013 at CFO1, which were combined with the Cl^- and $\text{NO}_3\text{-N}$ data from 6 June 2013. At CFO4, results from stable isotopes collected on 27 October 2014 were combined with Cl^- and $\text{NO}_3\text{-N}$ data collected on 7 October 2014.

3. Results

3.1 Site hydrogeology

3.1.1 CFO1

The geology at CFO1 consists of clay and clay-till interspersed with sand layers of varying thickness to the maximum depth of investigation (20 m BG, bedrock not encountered). Hydraulic conductivities (K) calculated from slug tests on wells ranged from 1.2×10^{-7} to $4.2 \times 10^{-5} \text{ m s}^{-1}$ ($n=10$) for sand, 1.1×10^{-8} to $2.8 \times 10^{-8} \text{ m s}^{-1}$ ($n=2$) for clay-till, and 1.6×10^{-9} to $3.0 \times 10^{-7} \text{ m s}^{-1}$ ($n=8$) for clay. Depth to the water table throughout the study site ranged from 0.5 m at DMW14 to 3.8 m at DMW11. Seasonal water table variations were about 0.5 m with no obvious change in the annual average during the 6-year measurement period. Water table elevation was highest at DMW10 and DMW1 on the west side of the site and lowest at DMW11 on the northeast side of the site (see Supplementary Material). Measured heads indicate groundwater flow from the vicinity of the EMS to the northeast and southeast. Mean horizontal hydraulic gradients at the water table ranged from 4.4×10^{-3} to $1.4 \times 10^{-2} \text{ m m}^{-1}$. Vertical gradients were predominantly downward in the upper 20 m of the profile (mean gradients ranging from 1.8×10^{-3} to 0.18 m m^{-1}), with the exception of DMW11 where the vertical gradient was upward (mean gradient $-2.8 \times 10^{-2} \text{ m m}^{-1}$). Using the geometric mean K for the sand ($5.0 \times 10^{-6} \text{ m s}^{-1}$) and a lateral head gradient of $1.4 \times 10^{-2} \text{ m m}^{-1}$ yields a specific discharge (Darcy flux, q) of 2.2 m y^{-1} . Assuming an effective porosity of 0.3 (Rodvang et al., 1998), the average linear velocity (\bar{v}) is 7.4 m y^{-1} . This suggests that, in the absence of attenuation by mixing or denitrification, agriculturally derived NO_3^- could have been transported through the groundwater system by advection about 400 m from the EMS since 1960 and 630 m since 1930.

3.1.2 CFO4

The geology at CFO4 consists of about 5 m of clay (with minor till) underlain by sandstone, to the maximum depth investigated (20 m BG). Hydraulic conductivities measured using slug tests on wells were 1.0×10^{-8} to $1.0 \times 10^{-5} \text{ m s}^{-1}$ ($n=12$) for the clay and sandstone (many shallow wells were screened across the clay-till and into the sandstone) and 1.0×10^{-5} to $2.9 \times 10^{-5} \text{ m s}^{-1}$ ($n=4$) for the sandstone. The depth to water table ranged from 1.0 to 3.4 m, increasing from west to east across the study site. Seasonal water table variations were on the order of 1.5



m with water table declines on the order of 0.3 m y^{-1} . The horizontal hydraulic gradient was consistently from west to east, with a mean gradient at the water table of $3.9 \times 10^{-3} \text{ m m}^{-1}$ between BC2 and BMW2 and $4.3 \times 10^{-3} \text{ m m}^{-1}$ between BMW2 and BMW7. Vertical hydraulic gradients were 4.2×10^{-2} to $4.6 \times 10^{-2} \text{ m m}^{-1}$ downward. Using the geometric mean K for the site ($2.9 \times 10^{-5} \text{ m s}^{-1}$) and a lateral head gradient of $4.3 \times 10^{-3} \text{ m m}^{-1}$ yields a q of 0.4 m y^{-1} . Assuming an effective porosity of 0.3 yields a \bar{v} of 1.3 m y^{-1} . These values suggest that, in the absence of attenuation by mixing or denitrification, anthropogenic NO_3^- could have been transported through the groundwater systems about 10 m by advection between 1995 and the time of sampling.

3.2 Values and evolution of stable isotopes of nitrate

Manure filtrate from the EMS at CFO1 had $\delta^{15}\text{N}_{\text{NO}_3}$ ranging from 0.4 to 5.0‰ and $\delta^{18}\text{O}_{\text{NO}_3}$ ranging from 7.1 to 19.0‰. The evolution of $\delta^{15}\text{N}_{\text{NO}_3}$ during nitrification can be modelled as a Rayleigh distillation process if the fraction factor is constant (Kendall and Aravena, 2000). A curve showing the co-evolution of $\delta^{18}\text{O}_{\text{NO}_3}$ (mixing of atmospheric $\delta^{18}\text{O}$ with groundwater-derived $\delta^{18}\text{O}$) and $\delta^{15}\text{N}_{\text{NO}_3}$ (Rayleigh distillation, $\beta = 1.005$) during nitrification is shown in Fig. 2. Isotopic values in DMW3, where direct leakage from the EMS was evident, are consistent with partial nitrification following this trend of isotopic evolution ($\delta^{18}\text{O}_{\text{NO}_3}$ of -1.2‰ and $\delta^{15}\text{N}_{\text{NO}_3}$ of 7.8‰).

The range of isotopic values of NO_3^- in groundwater is similar at both sites (Fig. 2). At CFO1, $\delta^{18}\text{O}_{\text{NO}_3}$ ranged from -5.9 to 20.1‰ and $\delta^{15}\text{N}_{\text{NO}_3}$ from -5.2 to 61.0‰. At CFO4, $\delta^{18}\text{O}_{\text{NO}_3}$ ranged from -1.9 to 31.6‰ and $\delta^{15}\text{N}_{\text{NO}_3}$ from -1.3 to 70.5‰. The isotopic values of $\delta^{18}\text{O}_{\text{NO}_3}$ in groundwater are commonly assumed to be derived from a mix of a 1/3 atmospheric-derived oxygen (+23.5‰) and 2/3 water-derived oxygen (Xue et al., 2009). Given the average $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ for both sites (-16‰, see Supplementary Material), a 1/3 atmospheric 2/3 groundwater mix would result in a $\delta^{18}\text{O}_{\text{NO}_3}$ of -3.7‰.

At both sites, co-enrichment of $\delta^{18}\text{O}_{\text{NO}_3}$ and $\delta^{15}\text{N}_{\text{NO}_3}$ characteristic of denitrification was evident in some samples (slopes of 0.42 and 0.72 in Fig. 2a). At CFO1, this includes samples from DP10-2, DMW5, DMW11, DMW12, DP11-12b, and DMW13 (and associated core) and some pore water from cores DC15-22 and DC15-23. These samples had $\text{NO}_3\text{-N}$ concentrations of 0.6 to 23.7 mg L^{-1} , $\delta^{18}\text{O}_{\text{NO}_3}$ ranging from 4.8 to 20.6‰, and $\delta^{15}\text{N}_{\text{NO}_3}$ ranging from 22.9 to 61.3‰. At CFO4, samples exhibiting evidence of denitrification were from BMW2, BMW5, BMW6, BMW7, and BC4. These samples had $\text{NO}_3\text{-N}$ concentrations ranging from 0.4 to 35.1 mg L^{-1} , $\delta^{18}\text{O}_{\text{NO}_3}$ ranging from 1.6 to 22.1‰, and $\delta^{15}\text{N}_{\text{NO}_3}$ ranging from 20.9 to 70.1‰. Although the isotopic values of DMW5 suggest enrichment by denitrification, the data plot away from the rest of the CFO1 data and close to the denitrification trend at CFO4 (Fig. 2), suggesting these samples were affected by some other process (possibly mixing or nitrification); therefore, the fraction of $\text{NO}_3\text{-N}$ remaining in this well was not calculated. Also, well DMW3, which clearly receives leakage from the EMS, did not contain substantial $\text{NO}_3\text{-N}$ and so f_d was not calculated.

The potential range of original isotopic values of the NO_3^- source prior to denitrification (R_0) varied from 5 to 27‰ for $\delta^{15}\text{N}_{\text{NO}_3}$ and from -2 to 7‰ for $\delta^{18}\text{O}_{\text{NO}_3}$ based on isotopic values measured during this study (Fig. 2a). These values are consistent with literature values for manure-sourced NO_3^- , which report $\delta^{15}\text{N}_{\text{NO}_3}$ ranging from 5 to 25‰ and $\delta^{18}\text{O}_{\text{NO}_3}$ ranging from -5 to 5‰ (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008; Baily et al., 2011). The enrichment factor of $\delta^{15}\text{N}_{\text{NO}_3}$ was defined by a normal distribution with a mean of -10‰ and standard deviation of 2.5‰. At CFO1, the coefficient of proportionality between the enrichment factor of $\delta^{15}\text{N}_{\text{NO}_3}$ and $\delta^{18}\text{O}_{\text{NO}_3}$ was described by a normal distribution with mean of 0.72 and standard



deviation of 0.05. At CFO4, the coefficient of proportionality was also described by a normal distribution with a mean of 0.42 and standard deviation of 0.035 (see Fig. 2a). These enrichment factors are consistent with values from denitrification studies that report ϵ_{15N} ranging from -4.0 to -30.0‰ and ϵ_{18O} ranging from -1.9 to -8.9‰ (Vogel et al., 1981; Mariotti et al., 1988; Böttcher et al., 1990; Spalding and Parrott, 1994; Mengis et al., 1999; Pauwels et al., 2000; Otero et al., 2009).

3.3 Distribution and sources of agricultural nitrate in groundwater

3.3.1 CFO1

Agriculturally derived NO_3^- was predominantly restricted to the upper 20 m (or less) at CFO1 ($\text{NO}_3\text{-N} \leq 0.2 \text{ mg L}^{-1}$ and $\text{Cl}^- \leq 57 \text{ mg L}^{-1}$ in seven wells screened at 20 m). The one exception was DP11-12b, which had up to 4.1 mg L^{-1} of $\text{NO}_3\text{-N}$. The southeast portion of the site also does not appear to have been significantly contaminated by agriculturally derived NO_3^- , with $\text{NO}_3\text{-N}$ concentrations $< 1 \text{ mg L}^{-1}$ in five water table wells (DMW4, DMW6, DMW14, DMW15, DMW16). In DMW6, Cl^- and TKN concentrations were elevated (see Supplementary Material) but $\text{NO}_3\text{-N}$ concentrations were $< 2 \text{ mg L}^{-1}$. Collectively, these data suggest the catch basin is not a significant source of NO_3^- to the groundwater at this site.

Leakage of manure slurry from the EMS at CFO1 is clearly indicated by the data from DMW3, which feature the highest concentrations of TN in groundwater (up to 548 mg L^{-1}) and elevated Cl^- , HCO_3^- , and DOC in concentrations similar to EMS manure filtrate (see Supplementary Material). Nevertheless, $\text{NO}_3\text{-N}$ concentrations in this well were consistently low ($1.1 \pm 2.7 \text{ mg L}^{-1}$, $n=22$). The potential for nitrification in the vicinity of this well is indicated by $\text{NO}_2\text{-N}$ production ($2.7 \pm 8.3 \text{ mg L}^{-1}$, $n=22$). However, the data demonstrate that only a small proportion of the $\text{NH}_3\text{-N}$ in DMW3 ($373.4 \pm 79.4 \text{ mg L}^{-1}$, $n=22$) could have been converted to NO_3^- within the subsurface ($\text{NO}_3\text{-N}$ in groundwater $\leq 66 \text{ mg L}^{-1}$) ($\text{NO}_3\text{-N}/\text{Cl}^-$ ratio of 0.95).

The maximum $\text{NO}_3\text{-N}$ concentration in groundwater was measured in core sample DC15-23 (clay at 2 m bgl, 7 m hydraulically downgradient of DMW3). The $\text{NO}_3\text{-N}$ in this core sample was most likely introduced into the groundwater system by vertical infiltration or diffusion from above. Pore water extracted from the unsaturated zone (sand) at the top of this core profile contained 865 mg L^{-1} of $\text{NO}_3\text{-N}$ and had a $\text{NO}_3\text{-N}/\text{Cl}^-$ ratio of 1.04, consistent with the ratio of 0.95 in the core sample.

Contamination by agricultural NO_3^- that exceeds the drinking water guidelines ($\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$) was observed in wells up to 40 m hydraulically downgradient of the EMS (DMW13, DP10-2) and in well DMW11 situated 470 m from the EMS (Fig. 3). DMW1, located upgradient of the EMS, also had concentrations of $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$ with an increasing trend, but the source of this NO_3^- is not clear. DMW2 and DMW12 also had $\text{NO}_3\text{-N}$ concentrations that were elevated but did not exceed the drinking water guideline ($\leq 3.7 \text{ mg L}^{-1}$).

Given the evidence of incomplete partial nitrification in DMW3, the $\text{NO}_3\text{-N}/\text{Cl}^-$ ratio of contamination from the EMS was assumed to be best represented by DP10-2, which is located directly downgradient of the EMS. Data for this well indicate values of $\text{NO}_3\text{-N}/\text{Cl}^-$ predominantly ranging from 0.1 to 0.3 with $\text{NO}_3\text{-N}/\text{Cl}^-$ estimated at 0.3 ± 0.13 (Fig. 4). Advective transport from DMW3 is also the likely source of $\text{NO}_3\text{-N}$ (up to 21.1 mg L^{-1}) within the sand between 6 and 12 m depth in DC15-23. $\text{NO}_3\text{-N}/\text{Cl}^-$ ratios in these samples ranged from 0.07 to 0.31, consistent with DP10-2. Stable isotope values in pore water from this sand layer do not indicate substantial denitrification ($\delta^{18}\text{O} \leq 5.9\text{‰}$, $\delta^{15}\text{N} \leq 16.7\text{‰}$), suggesting these ratios will be similar to the initial ratios at the point of entry to the groundwater system.



In contrast, the ratio of NO_3-N_i/Cl_i in DMW13 (33 m downgradient from DP10-2) was 0.75 ± 0.29 , which is more similar to the NO_3-N/Cl^- ratio in DC15-23 at 2 m (0.95), which is interpreted as reflecting a top-down source. The NO_3^- in DMW13 is therefore unlikely to be sourced solely from leakage from the EMS, and could be sourced from the adjacent dairy pens or a temporary manure pile that was observed adjacent to this well during core collection in 2015 (or a combination of EMS and top-down sources).

The NO_3-N_i/Cl_i ratio in DMW12 is not inconsistent with an EMS source, but the hydraulic gradient between DMW2 and DMW12 is negligible, indicating a lack of driving force for advective transport from the EMS towards DMW12. This is also the case for well DMW1, which is upgradient of the EMS but had elevated NO_3-N concentrations (6.5 ± 3.6 , $n=18$). The source of nitrate in these wells is therefore unlikely to be related to leakage from the EMS, but alternative sources (i.e., nearby temporary manure piles) are not known.

Well DMW11 had consistently low NO_3-N/Cl^- ratios (< 0.05). The NO_3-N_i/Cl_i ratio indicated by DMW11 was similar to DP10-2, but estimates of Cl_i indicate Cl^- sourced from inputs with three-fold higher Cl^- concentrations than the source to DP10-2 (Fig. 4b). Well DMW11 is located hydraulically downgradient of feedlot pens and adjacent to a solid manure storage area. Well DMW11 is also in a local topographic low and is likely receiving NO_3-N and Cl^- from surface runoff and infiltration in addition to subsurface groundwater flow. Well DMW11 had high NO_3-N_i and Cl_i consistent with measured values in that well, indicating a local top-down source that is likely the nearby solid manure pile.

3.3.2 CFO4

At CFO4, measured data indicate that effects from agricultural operations on NO_3^- concentrations in groundwater are restricted to the upper 15 m of the subsurface. NO_3-N concentrations in wells screened at 15 m depth were $< 0.5 \text{ mg L}^{-1}$, with the exception of one sample from BP10-15w (May 2012) with 4.3 mg L^{-1} of NO_3-N . Water table wells in the west and north of the study site (BC1, BC2, and BC3) also indicate negligible impacts of agricultural operations, with $Cl^- < 10 \text{ mg L}^{-1}$ and $NO_3-N < 0.1 \text{ mg L}^{-1}$.

Concentrations of $NO_3-N > 10 \text{ mg L}^{-1}$ were measured in three water table wells (BMW2, BMW3, BMW4) installed adjacent to the EMS (Fig. 5). Of these, BMW2 had much higher Cl^- concentrations ($502 \pm 97 \text{ mg L}^{-1}$, $n=22$), and therefore lower NO_3-N/Cl^- ratios (< 0.05). Given the elevated Cl^- concentrations in this well were consistent with concentrations in the EMS, direct leakage from the EMS was assumed to be the source. Stable isotopes of NO_3^- indicate substantial denitrification in BMW2, with estimated $NO_3-N_i \geq 127 \text{ mg L}^{-1}$ and an NO_3-N_i/Cl_i ratio of 0.1 to 0.3 (Fig. 6). This ratio is consistent with data from well BMW4, which is immediately adjacent to the EMS (on the upgradient side) and likely reflects leakage from the EMS without denitrification (based on stable isotopes of NO_3^-). NO_3-N/Cl^- ratios measured in BMW4 were predominantly 0.1 to 0.3, consistent with the reconstructed NO_3-N_i/Cl_i ratio in BMW2.

Agriculturally derived NO_3^- in other wells not immediately adjacent to the EMS is unlikely to be related to leakage from the EMS. Wells BMW5 and BMW7 are 60 and 140 m hydraulically downgradient from the EMS, respectively. NO_3-N_i/Cl_i ratios in these wells were not inconsistent with BMW2 (i.e., the range of values overlap), but advective transport is only likely to have transported solutes around 10 m since the EMS was installed (see Section 3.1.2). As such, the source of NO_3-N in these wells is likely the dairy pens rather than the EMS. Concentrations of $NO_3-N > 10 \text{ mg L}^{-1}$ were also measured in BC4, which is located 95 m hydraulically upgradient of the EMS. The ratio of NO_3-N_i/Cl_i at BC4 was the highest at CFO4 (0.6) and did not overlap with BMW2. This



indicates that the NO_3^- in this well was sourced from an adjacent manure pile, which was observed during the study.

3.4 Mechanisms of attenuation of agriculturally derived NO_3^-

5 Attenuation of agriculturally derived NO_3^- in groundwater is dominated by denitrification at CFO1 and CFO4, with estimates of f_m consistently higher than estimates of f_d (Table 2, Fig. 7). Calculated f_d values suggest that at least half of the $\text{NO}_3\text{-N}$ present at the initial point of entry to the groundwater system has been removed by denitrification. The substantial uncertainty in f_m is related to the range of $\text{NO}_3\text{-N}_i$ and Cl_i , with the largest uncertainty corresponding to the lowest measured concentrations (i.e., furthest from the upper limit).

At both sites, the stable isotope values of NO_3^- indicate that denitrification proceeds within metres of the source. At CFO1, calculated f_d in well DP10-2 (2 m from the EMS) is 0.52 ± 0.22 ; at CFO4, f_d in well BMW2 (3 m from the EMS) is 0.13 ± 0.06 . Denitrification also substantially attenuated $\text{NO}_3\text{-N}$ concentrations in wells where the source is not the EMS but instead is adjacent solid manure piles (e.g., DMW11 at CFO1, BC4 at CFO4). In BMW6 at CFO4, denitrification completely attenuated the agriculturally derived NO_3^- . This well had negligible $\text{NO}_3\text{-N}$ ($0.4 \pm 0.2 \text{ mg L}^{-1}$, $n=8$) and the lowest f_d of 0.01. Measured DOC in this well was consistent with other wells at both sites ($6.9 \pm 1.7 \text{ mg L}^{-1}$, $n=3$), suggesting DOC depletion does not limit denitrification at these CFO operations. Calculated f_d and f_m should decrease with increasing subsurface residence time and distance from source. Data from wells support the source identification based on concentrations of $\text{NO}_3\text{-N}$ and Cl^- and $\text{NO}_3\text{-N}/\text{Cl}^-$ ratios (see Section 3.3). Well DMW11 (470 m from the EMS) had the highest f_m at CFO1 (0.83), indicating less mixing and suggesting the anthropogenic source of NO_3^- in this well is relatively close, which is consistent with the adjacent the solid manure pile being the source of NO_3^- to this well. At CFO4, well BMW2, which is adjacent to the EMS, had the highest f_m (0.92), indicating the least attenuation of NO_3^- by mixing and consistent with the EMS being the source of NO_3^- to this well.

4. Discussion

Agriculturally derived NO_3^- at these two sites with varying lithology is generally restricted to depths < 20 m, consistent with previous studies at CFOs (Robertson et al., 1996; Rodvang and Simpkins, 2001; Rodvang et al., 2004; Kohn et al., 2016). Attenuation of agriculturally derived NO_3^- in groundwater is a spatially varying combination of mixing and denitrification, with denitrification playing a greater role than mixing at both sites. In the samples for which f_d could be determined, denitrification reduced NO_3^- concentrations by at least half and, in some cases, back to background concentrations. Given that the range of source isotopic composition was allowed to vary to its maximum justifiable extent, these quantitative estimates of denitrification based on stable isotopes of NO_3^- are likely to be conservative. Denitrification appears to proceed within metres of the NO_3^- source, suggesting relatively short residence times and redox conditions at the water table may be conducive to denitrification reactions (Critchley et al., 2014; Clague et al., 2015). The combination of the approach outlined here with measurement of groundwater age indicators would allow for better constraints on groundwater flow velocities and determination of denitrification rates (Böhlke and Denver, 1995; Katz et al., 2004; McMahon et al., 2004; Clague et al., 2015).



The substantial role of denitrification within the saturated glacial sediments at these study sites indicates the potential for significant attenuation of agriculturally derived NO_3^- by denitrification in similar groundwater systems across the North American interior and Europe (Ernstsen et al., 2015; Zirkle et al., 2016). Denitrification in the unsaturated zone is limited by low water contents and oxic conditions, resulting in substantial stores of NO_3^- in vadose zones (Turkeltaub et al., 2016; Ascott et al., 2017). NO_3^- in water that is removed rapidly from site is also unlikely to be substantially attenuated by denitrification due to oxic conditions and rapid transit times (Ernstsen et al., 2015). Therefore, water management focussed on reducing the effects of NO_3^- contamination in similar hydrogeological settings to this study should aim to maximize infiltration into the saturated zone where NO_3^- concentrations can be naturally attenuated.

Infiltration of NO_3^- rich water that has passed through temporary solid manure piles and dairy pens has resulted in groundwater $\text{NO}_3\text{-N}$ concentrations as high as those associated with leakage from the EMS (e.g., DMW11, DMW13, BC4). At CFO4, this is in spite of the presence of clay at surface, which is attributable to secondary porosity in the upper part of the profile that has led to hydraulic conductivities comparable to sand. This result is consistent with the findings of Showers et al. (2008), who investigated sources of NO_3^- at an urbanized dairy farm in North Carolina, USA. The limited impact of leakage from the EMS on NO_3^- concentrations in groundwater at these sites may be partly due to the relatively shallow water table and suggests that saturation within the clay lining of the EMS may have limited the development of extensive secondary porosity that would allow rapid water percolation (Baram et al., 2012). Elevated $\text{NH}_3\text{-N}$ concentrations in the water table well at the southeast corner of the EMS at CFO1 (DMW3) indicate direct leakage from the EMS, but because nitrification within the EMS is minimal, this has not resulted in elevated $\text{NO}_3\text{-N}$ in this well. Two possibilities for the fate of $\text{NH}_3\text{-N}$ in DMW3 are attenuation by cation exchange and oxidation to $\text{NO}_3\text{-N}$ within the groundwater system. Measured $\text{NO}_3\text{-N}$ concentrations in groundwater represent only a small fraction ($\leq 10\%$) of $\text{NH}_3\text{-N}$ within the EMS (or DMW3), suggesting oxidation to NO_3^- within the aquifer may be limited. Further work is required to assess the importance of cation exchange as an attenuation mechanism for direct leakage from the EMS at this site.

The sources of manure-derived NO_3^- (manure piles vs. EMS) are distinguishable based on $\text{NO}_3\text{-N}_i/\text{Cl}_i$ ratios, provided there is also an understanding of the history of each site, local hydrogeology, and potential sources. Estimation of $\text{NO}_3\text{-N}_i/\text{Cl}_i$ assumes that background concentrations could be neglected in the mixing calculation. The error associated with this assumption increases as source concentrations and measured concentrations approach background concentrations. At these study sites, background concentrations are likely to be $< 20 \text{ mg L}^{-1}$ for Cl^- and $< 1 \text{ mg L}^{-1}$ for $\text{NO}_3\text{-N}$. Based on these values, estimated $\text{NO}_3\text{-N}_i$ values are at least 20 times background $\text{NO}_3\text{-N}$ concentrations, and over 100 times background concentrations in some wells. The estimated Cl_i values are at least three times background concentrations at CFO1 and at least 10 times background concentrations at CFO4. Measured concentrations are closer to background concentrations than initial concentrations, but neglecting background concentrations is still likely to be a small source of error relative the uncertainty in maximum concentrations. For example, well DMW13 had the lowest measured Cl^- concentration (57 mg L^{-1}); if we assume a Cl_b of 10 mg L^{-1} and a Cl_i of 100 mg L^{-1} , the error in f_m introduced by neglecting Cl_b is 9%; if Cl_b is 20 mg L^{-1} , the error is 23%. The accuracy of $\text{NO}_3\text{-N}_i/\text{Cl}_i$ is determined by the accuracy of f_a , and the uncertainty is independent of the measured concentrations of NO_3^- and Cl^- . Uncertainty in the initial concentrations (Cl_i and $\text{NO}_3\text{-N}_i$) depends on measured Cl^- and $\text{NO}_3\text{-N}$, with less uncertainty at higher measured concentrations as they approach the maximum values. Temporal variability in $\text{NO}_3\text{-N}_i/\text{Cl}_i$ for each source could not be determined based on the



snapshot isotope sampling conducted, but this could be investigated by measuring NO_3^- isotopes in conjunction with $\text{NO}_3\text{-N}$ and Cl^- at multiple times.

Nitrate isotope values in groundwater at the two CFOs studied are generally consistent with previous studies reporting denitrification of manure-derived NO_3^- at dairy farms (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008; Baily et al., 2011). However, a number of groundwater samples collected for the present study had relatively enriched $\delta^{18}\text{O}_{\text{NO}_3}$ ($> 15\text{‰}$) with depleted $\delta^{15}\text{N}_{\text{NO}_3}$ ($< 15\text{‰}$). Some of these isotopic values are within the range previously reported for NO_3^- derived from inorganic fertilizer ($\delta^{15}\text{N}_{\text{NO}_3}$ from -3 to 3‰ and $\delta^{18}\text{O}_{\text{NO}_3}$ from -5 to 25‰), with the $\delta^{18}\text{O}_{\text{NO}_3}$ depending on whether the NO_3^- is from NH_4^+ or NO_3^- in the fertilizer (Mengis et al., 2001; Wassenaar et al., 2006; Xue et al., 2009). To the best of our knowledge, however, no inorganic fertilizers have been applied at these study sites. Another potential source is NO_3^- derived from soil organic N, but this should have $\delta^{15}\text{N}_{\text{NO}_3}$ values of 0 to 10‰ and $\delta^{18}\text{O}_{\text{NO}_3}$ values of -10 to 15‰ (Durka et al., 1994; Mayer et al., 2001; Mengis et al., 2001; Xue et al., 2009; Baily et al., 2011). Incomplete nitrification of NH_4^+ can result in $\delta^{15}\text{N}_{\text{NO}_3}$ lower than the manure source (Choi et al., 2003), but as there was no measurable $\text{NH}_3\text{-N}$ in these samples this is also unlikely. These isotope values may reflect the influence of NO_3^- from precipitation, which usually has values ranging from -5 to 5‰ for $\delta^{15}\text{N}_{\text{NO}_3}$ and 40 to 60‰ for $\delta^{18}\text{O}_{\text{NO}_3}$, and has been reported to dominate NO_3^- isotope values of groundwater under forested landscapes (Durka et al., 1994). Alternatively, they may be affected by microbial immobilization and subsequent mineralization and nitrification, which can mask the source $\delta^{18}\text{O}_{\text{NO}_3}$ in aquifers with long residence times (Mengis et al., 2001; Rivett et al., 2008). The isotopic values of NO_3^- in the manure filtrate from the EMS at CFO1, were generally inconsistent with values for manure-sourced NO_3^- reported in other groundwater studies (Wassenaar, 1995; Wassenaar et al., 2006; Singleton et al., 2007; McCallum et al., 2008a; Baily et al., 2011). This is likely to be because nitrification within the EMS was negligible ($\text{NO}_3\text{-N} < 0.7 \text{ mg L}^{-1}$), such that the isotopic values of $\text{NO}_3\text{-N}$ in the manure filtrate reflect volatilization of NH_3 and partial nitrification within the EMS. $\delta^{18}\text{O}_{\text{NO}_3}$ values may also have been affected by evaporative enrichment of the $\delta^{18}\text{O}_{\text{H}_2\text{O}}$ being incorporated into NO_3^- (Showers et al., 2008).

5. Conclusions

Quantitative estimates of denitrification based on the stable isotopic value of NO_3^- in groundwater were used to constrain a binary mixing model based on Cl^- and $\text{NO}_3\text{-N}$. This approach allowed the identification of $\text{NO}_3\text{-N}$ sources and quantification of mixing and denitrification as mechanisms of NO_3^- attenuation in groundwater at two dairy farms overlying glacial sediments. Relative to leakage from the EMS, the input of NO_3^- to groundwater from temporary manure piles and pens resulted in comparable (or greater) $\text{NO}_3\text{-N}$ concentrations in groundwater at these sites. Nitrate attenuation at both sites is dominated by denitrification, which is evident even in wells directly adjacent to the NO_3^- source. On-site denitrification reduced agriculturally derived NO_3^- concentrations by at least half and, in some wells, completely. These results indicate that infiltration to groundwater systems in glacial sediments where NO_3^- can be naturally attenuated is likely to be preferable to off-farm export via runoff or drainage networks.



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Table 1. Details of groundwater monitoring wells and continuous core collection at CFO1 and CFO4 (all screens installed at bottom of the well).

Site	Well/Core hole ID	Type [†]	Lateral distance from	Ground elevation	Total depth (m below ground)	Screen length (m)	Lithology of screened interval	K (m s ⁻¹)
			EMS* (m)	(m asl)	(m)			
CFO1	DMW1	WTW	60	869.7	5.0	4.0	Sand	
	DMW2	WTW	10	867.2	6.0	4.0	Sand	1.2 × 10 ⁻⁷
	DMW3	WTW	2	867.5	3.7	2.0	Sand	
	DMW4	WTW	160		4.2	4	Sand	1.3 × 10 ⁻⁶
	DMW5	WTW	270	866.4	6.8	4.0	Clayey sand	1.7 × 10 ⁻⁵
	DMW6	WTW	310		6.7	4		
	DP10-1	Piezo	2	867.8	18.6	0.5	Clay	1.6 × 10 ⁻⁹
	DP10-2	Piezo	2	867.9	8.0	1.5	Sand	3.6 × 10 ⁻⁵
	DMW10	WTW	340	868.0	7.2	3.0	Clay	3.0 × 10 ⁻⁷
	DP11-10b	Piezo	340	868.0	20	0.5	Clay	2.2 × 10 ⁻⁸
	DMW11	WTW	470	864.8	7.0	3.0	Sand and clay	4.2 × 10 ⁻⁵
	DP11-11b	Piezo	470		20	0.5	Clay	6.3 × 10 ⁻⁹
	DMW12	WTW	50	867.6	7.0	3.0	Sand and clay	7.4 × 10 ⁻⁶
	DP11-12b	Piezo	50	867.6	20.1	1.0	Clay	1.1 × 10 ⁻⁸
	DMW13	WTW	35	867.1	7.0	3.0	Sand	8.9 × 10 ⁻⁶
	DP11-13b	Piezo + core	35	867.1	20.0	0.5	Clay	
	DMW14	WTW	105	865.7	7.0	3.0	Clay	5.7 × 10 ⁻⁶
	DP11-14b	Piezo	105	865.7	20.0	0.5	Sand	1.1 × 10 ⁻⁶
	DMW15	WTW	185		7.0	3	Clay	2.4 × 10 ⁻⁸
	DP11-15b	Piezo	185		20.0	0.5	Clay	1.4 × 10 ⁻⁷
	DMW16	WTW	320	866.0	6.0	3.0	Sand and clay	-
	DP11-16b	Piezo	320		20.0	0.5	Clay	3.2 × 10 ⁻⁹
	DC15-20	Core	76		15			
DC15-21	Core	45		10.5				
DC15-22	Core	22		12				
DC15-23	Core	9		15				
CFO4	BC1	WTW	110	857.0	6.9	3.1	Clay and sandstone	
	BC2	WTW	365	859.4	7.0	3.1	Clay and sandstone	2.2 × 10 ⁻⁷
	BC3	WTW	145	858.6	6.8	3.1	Clay and sandstone	1.3 × 10 ⁻⁶
	BC4	WTW	95	858.8	5.9	3.0	Clay and sandstone	3.4 × 10 ⁻⁶
	BC5	WTW	105	859.5	7.5	4.5	Clay and sandstone	
	BMW1	WTW	4	858.6	7.1	3.1	Clay and sandstone	4.3 × 10 ⁻⁶
	BMW2	WTW	3	857.9	7.5	4.5	Clay and sandstone	8.5 × 10 ⁻⁷
	BMW3	WTW	8	858.6	6.0	3.0	Clay and sandstone	
	BMW4	WTW	14	858.0	7.5	4.8	Clay and sandstone	1.0 × 10 ⁻⁵
	BMW5	WTW	60	858.0	7.5	4.5	Clay and sandstone	
	BP5-15	Piezo	60	858.1	15.3	1.5	Sandstone	1.0 × 10 ⁻⁷
	BMW6	WTW	150	856.9	7.5	4.5	Clay and sandstone	4.0 × 10 ⁻⁶
	BP6-15	Piezo	150	856.8	15.2	1.5	Sandstone	3.0 × 10 ⁻⁶
	BMW7	WTW	140	856.7	7.5	4.5	Clay and sandstone	1.0 × 10 ⁻⁶
	BP10-15e	Piezo	4	858.2	14.9	1.5	Sandstone	2.9 × 10 ⁻⁵
BP10-15w	Piezo	10	858.0	15.0	1.5	Sandstone	1.0 × 10 ⁻⁵	

*EMS=Earthen manure storage

[†]WTW=water table well, Piezo = piezometer, Core = continuous core

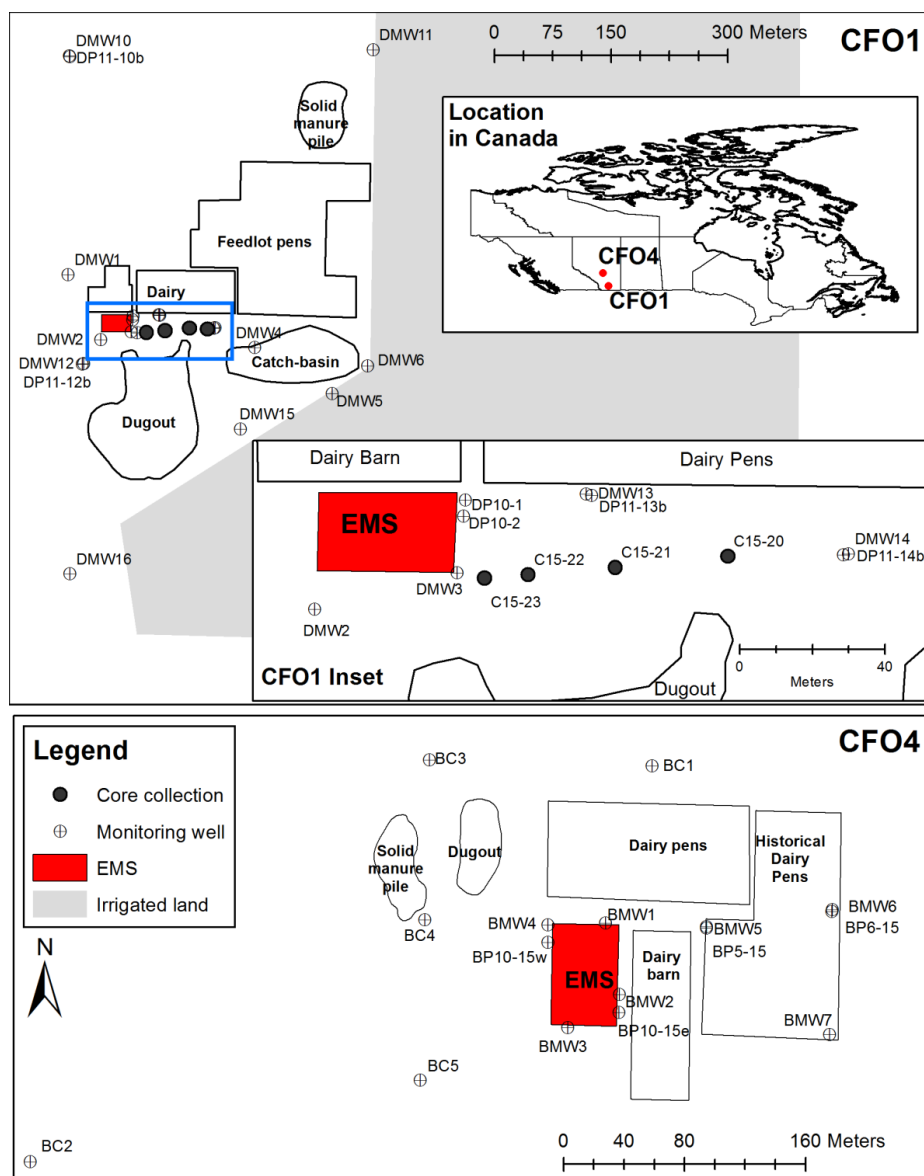


Table 2. Measured Cl⁻ and NO₃⁻ concentrations and stable isotopic values of NO₃, and estimated f_a, f_m .

Study area	Sample ID*	Cl ⁻ (mg L ⁻¹)	NO ₃ -N (mg L ⁻¹)	$\delta^{15}\text{N}_{\text{NO}_3}$ (‰)	$\delta^{18}\text{O}_{\text{NO}_3}$ (‰)	f_a (mean ± stdev)	f_m^{**} (mid-range)
CFO1	DP11-13_4.3m	28.5	7.0	30.3	9.8	0.30 ± 0.15	0.58
	DP11-13_5.2m	25.0	7.8	31.0	10.8	0.34 ± 0.13	0.58
	DP11-13_7m	72.3	12.0	31.6	10.2	0.27 ± 0.13	0.65
	DP11-13_7.9m	70.8	9.1	36.4	14.0	0.17 ± 0.09	0.68
	DP11-13_8.8m	81.7	10.9	29.6	9.9	0.32 ± 0.15	0.63
	DC15-22_6.5m	99.2	4.7	30.8	16.8	0.19 ± 0.08	0.58
	DC15-22_10m	73.0	11.0	26.1	7.4	0.47 ± 0.21	0.63
	DP10-2	74.5	11.8	24.2	4.8	0.52 ± 0.22	0.63
	DMW11	436.1	17.1	33.3	10.9	0.17 ± 0.07	0.83
	DMW12	78.0	2.57	29.8	14.3	0.23 ± 0.10	0.54
	DMW13	56.7	23.7	23.0	6.8	0.56 ± 0.22	0.65
DP11-12b	95.7	0.6	35.9	17.0	0.15 ± 0.08	0.54	
CFO4	BC4	163.1	35.1	30.6	1.6	0.37 ± 0.13	0.82
	BMW2	595.6	16.5	41.6	8.3	0.13 ± 0.06	0.92
	BMW5	131.2	12.9	28.9	6.5	0.34 ± 0.16	0.63
	BMW6	156.0	0.4	70.5	22.1	0.01 ± 0.01	0.56
	BMW7	134.7	11.6	34.0	5.9	0.21 ± 0.11	0.68

*central depth of core samples, x, indicated as SampleID_xm.

** maximum f_m is 1 for all samples, which implies no mixing.



5 **Figure 1:** Map of study sites CFO1 and CFO4, showing locations of groundwater monitoring wells, core collection, earthen manure storages (EMS), dairy and feedlot pens, manure piles, and irrigated land. Blue rectangle indicates extent of CFO1 inset.

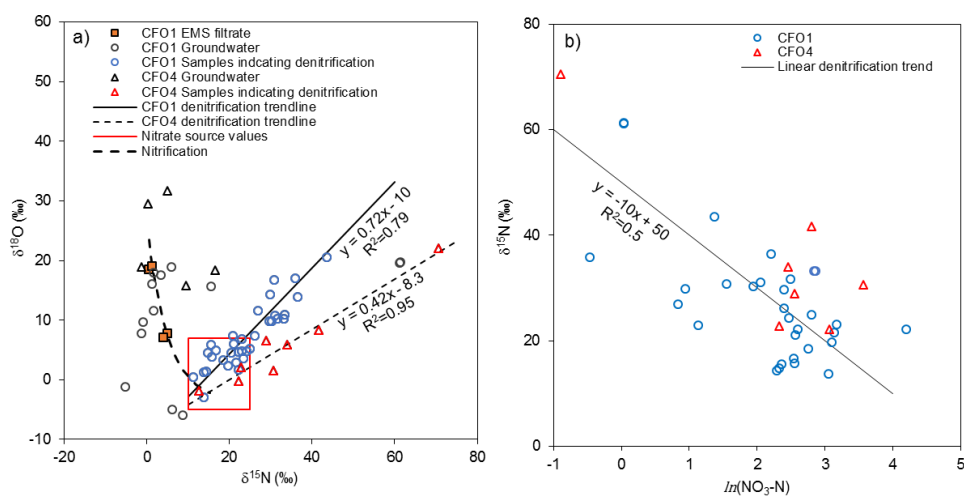


Figure 2 (a) Cross-plot of stable isotopes of nitrate at CFO1 and CFO4 showing hypothetical nitrification trend, boundary of manure-sourced NO_3^- values and linear enrichment trends associated with denitrification, (b) enrichment of $\delta^{15}\text{N}_{\text{NO}_3}$ during denitrification (only samples within source region and with evidence of denitrification are shown).

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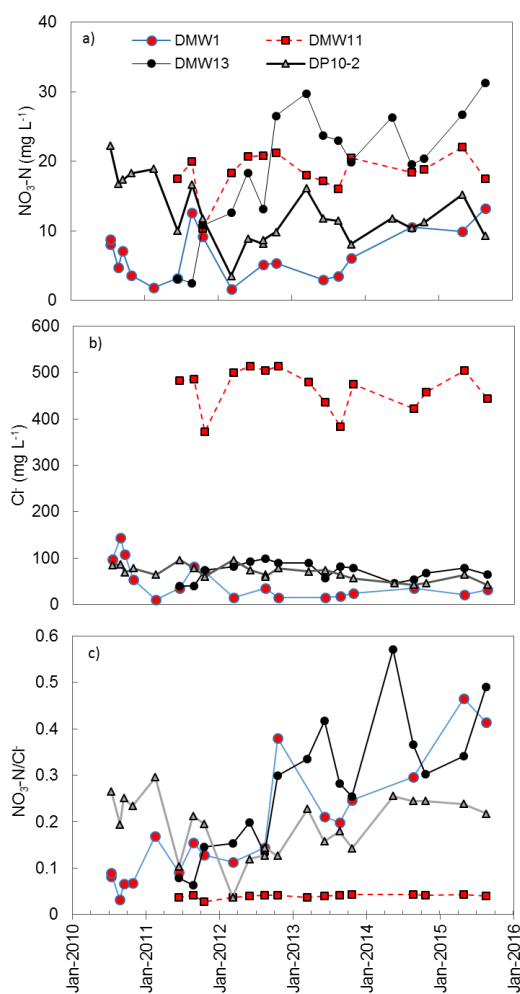


Figure 3 Temporal variations in (a) NO₃-N, (b) Cl⁻, and (c) NO₃-N/Cl⁻ at CFO1. Only wells with NO₃-N > 10 mg L⁻¹ are shown.

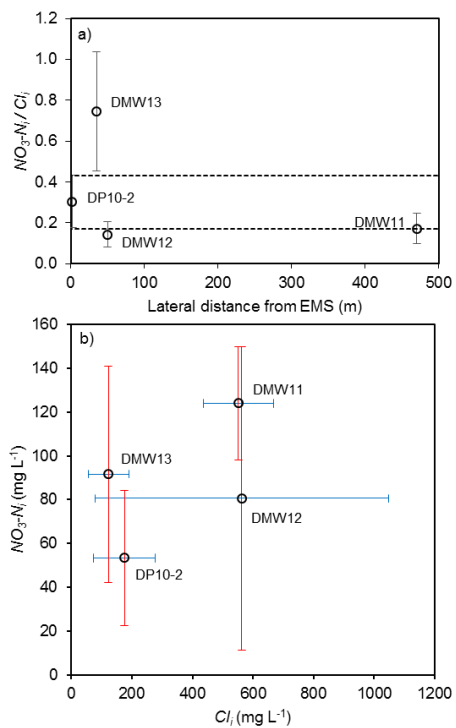


Figure 4 Estimated (a) NO_3-N_i/C_{l_i} ratios (mean and st. dev.) in water table wells with evidence of denitrification at CFO1, plotted with distance from earthen manure storage (EMS), where dashed lines are the upper and lower bounds of DP10-2 (EMS source), and (b) concentrations of NO_3-N_i and C_{l_i} at CFO1 (mid-range, error bars are max. and min. values).

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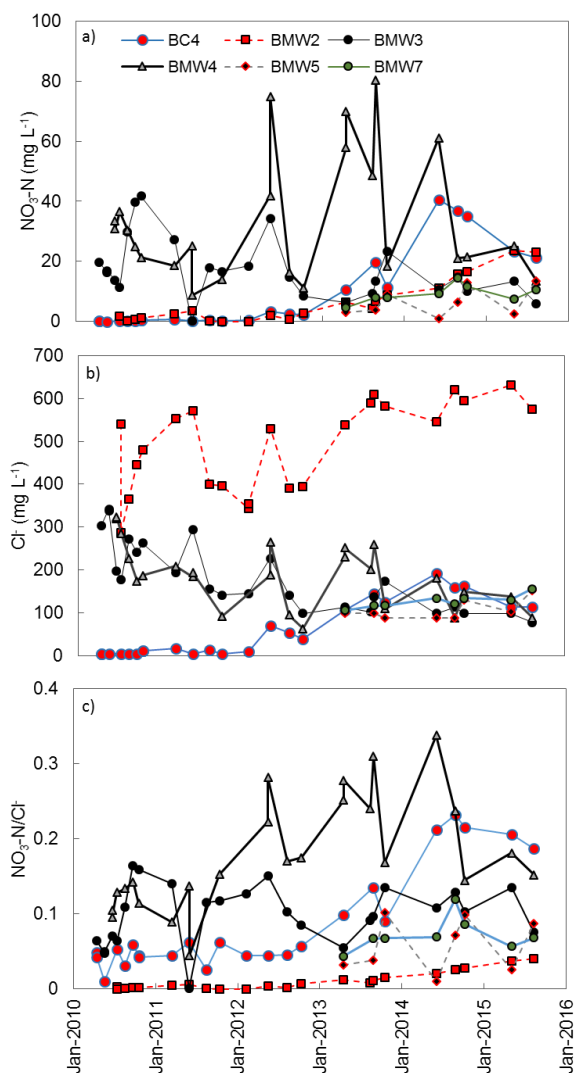
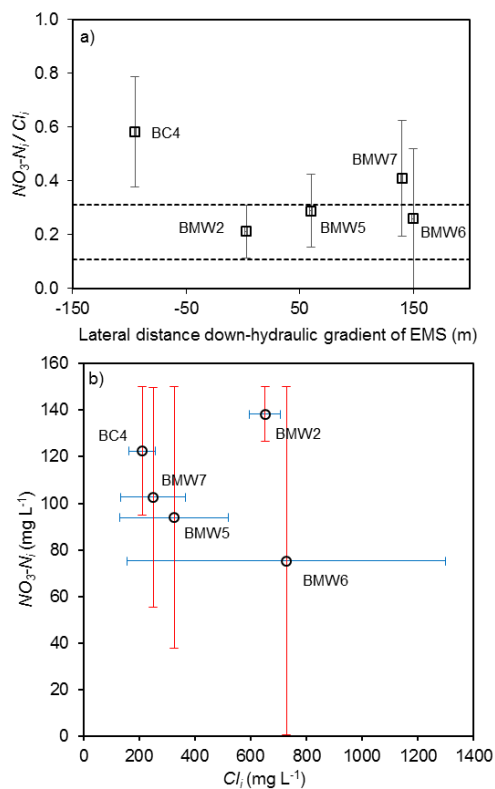


Figure 5 Temporal variations in (a) $\text{NO}_3\text{-N}$, (b) Cl^- , and (c) $\text{NO}_3\text{-N}/\text{Cl}^-$ at CFO4. Only wells with $\text{NO}_3\text{-N} > 10 \text{ mg L}^{-1}$ are shown.



5 **Figure 6** Estimated (a) NO_3-N_i/C_i ratios (mean and st. dev.) in water table wells with evidence of denitrification at CFO4, plotted with distance from earthen manure storage (EMS), where dashed lines are upper and lower bounds of BMW2 (EMS source), and (b) estimated concentrations of NO_3-N_i and C_i at CFO1 (mid-range, error bars are max. and min. values).

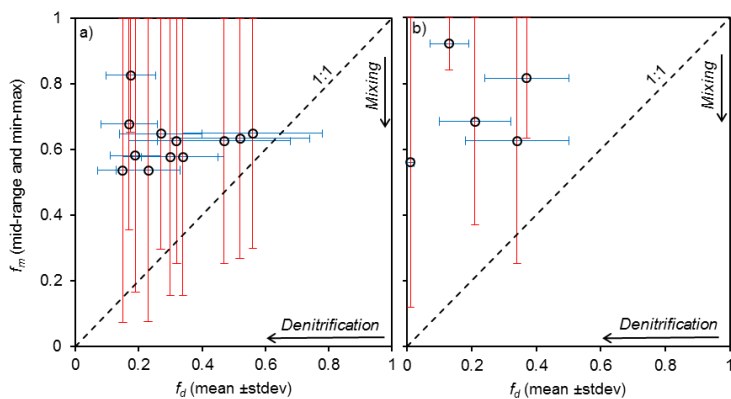


Figure 7 Relative contributions to NO_3^- attenuation by mixing and denitrification, as indicated by estimated f_m and f_d at (a) CFO1 and (b) CFO4, for groundwater samples with denitrification indicated by stable isotope values of NO_3^- .

5