

1 **Is Annual Recharge Coefficient a Valid Concept in Arid and Semi-Arid Region?**

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21 **Abstract.** Deep soil recharge (DSR) (at depth more than 200 cm) is an important part of water
22 circulation in arid and semi-arid regions. Quantitative monitoring of DSR is of great importance
23 to assess water resources and to study water balance in arid and semi-arid regions. This study
24 used a typical bare land on the Eastern margin of Mu Us Sandy Land in the Ordos basin of China
25 as an example to illustrate a new lysimeter method of measuring DSR to examine if the annual
26 recharge coefficient is valid or not in the study site, where the annual recharge efficient is the
27 ratio of annual DSR over annual total precipitation. Positioning monitoring was done on
28 precipitation and DSR measurements underneath mobile sand dunes from 2013 to 2015 in the
29 study area. Results showed that use of an annual recharge coefficient for estimating DSR in bare
30 sand land in arid and semi-arid regions is questionable and could lead to considerable errors. It
31 appeared that DSR in those regions was influenced by precipitation pattern, and was closely
32 correlated with spontaneous strong precipitation events (with precipitation greater than 10 mm)
33 other than the total precipitation. This study showed that as much as 42% of precipitation in a
34 single strong precipitation event can be transformed into DSR. During the observation period,
35 the maximum annual DSR could make up 24.33% of the annual precipitation. This study
36 provided a reliable method of estimating DSR in sandy area of arid and semi-arid regions, which
37 is valuable for managing groundwater resources and ecological restoration in those regions. It
38 also provided strong evidence that the annual recharge coefficient was invalid for calculating
39 DSR in arid and semi-arid regions. This study shows that DSR is closely related to the strong
40 precipitation events, rather than to the average annual precipitation, as well as the precipitation
41 patterns.

42 **Key words:** Deep soil recharge, deep soil infiltrometer, sandy land, new apparatus, rainfall,
43 lysimeter

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47 **Introduction**

48 Recharge is an important source of groundwater budget and it is also a fundamental process
49 that links the surface hydrological processes (e.g. precipitation), vadose zone process (e.g.
50 infiltration and soil moisture dynamics), and the saturated zone process (e.g. groundwater flow)
51 (Sanford, 2002;McWhorter and Sunada, 1977). How to accurately estimate recharge remains a
52 persistent challenge and an active research topic in the hydrological science community over
53 many decades (Gee and Hillel, 1988;Scanlon, 2013;Sanford, 2002). It is generally accepted that
54 recharge is correlated to the precipitation in some fashions, and many studies adopt the concept
55 of a recharge coefficient (Turkeltaub et al., 2015;Kalbus et al., 2006;Allocca et al., 2014), which
56 is the ratio of the actual recharge to the precipitation, to estimate the recharge (Fiorillo et al.,
57 2015;Allocca et al., 2014). The magnitude of such a recharge coefficient is controlled by a
58 complex interplay of multiple factors such as moisture dynamics in the vadose zone
59 (Schymanski et al., 2008), depth to water table, vegetation, etc., and the recharge coefficient is
60 often regarded as a temporally invariant value at a given location (Fiorillo et al., 2015;Min et al.,
61 2017;Vauclin et al., 1979). Specifically, it is assumed to be primarily controlled by the total
62 precipitation, not too much by the temporal fluctuation of precipitation events (Hickel and Zhang,
63 2006;Acworth et al., 2016). In this study, we will challenge the concept of using a constant
64 recharge coefficient to estimate the recharge in arid and semi-arid regions based on a multi-year
65 field investigation.

66 As water tables in many arid and semi-arid regions are relatively deep (greater than 2
67 meters below ground surface) (Williams, 1999;Soylu et al., 2011), recharge in those regions is
68 named Deep Soil Recharge (DSR), which will be the concern of this study. DSR could ease the
69 demand of sand-fixing vegetation on moisture during extremely dry seasons (Zhang et al.,

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71 2001;Shou et al., 2016) , and it reduces water deficit, sustains life activities, and helps the
72 vegetation live through extreme droughts (Zhang et al., 2004). In this sense, DSR is an important
73 factor of water cycle in arid and semi-arid regions (Adolph, 1947), and it could also provide
74 much needed references for the stability analysis of sand-fixing vegetation (Li et al., 2004;Li et
75 al., 2014). In the following, we will briefly review the existing methods of estimating DSR.

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76 In general, there are three methods of measuring DSR in arid and semi-arid regions. The
77 first is an empirical approach which assigns a constant recharge coefficient associated with a
78 certain precipitation event (Allison et al., 1994;Jiménez-Martínez et al., 2010). The empirical
79 approach is simple to use but it lacks a rigorous theoretical base, and the recharge coefficient has
80 to be calibrated through a groundwater flow model in the region, which is often not available.

81 The second is a modeling approach involving numerical models such as HYDRUS
82 (Šimůnek et al., 2012), SWAT (Arnold et al., 2012), UNSATH (Fayer, 2000), SWIM
83 (Krysanova et al., 2005), SWAP (van Dam, 2000) to calculate DSR. Modeling is an efficient
84 way to test different hypothetical scenarios and it may be used to predict DSR in the future if the
85 model is calibrated carefully. Detailed water balance models can be used for irrigated

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86 agriculture, but they usually cannot predict evapotranspiration accurately, especially when plants
87 suffer seasonal water stress and plants cover is sparse (Gee and Hillel, 1988). When recharge is
88 estimated as residual in water balance models, it can cause miscalculation as much as an order of
89 magnitude (Scanlon, 2013;Voeckler et al., 2014). When using soil water flow models with
90 measured or estimated soil hydraulic conductivities and tension gradients, similar miscalculation
91 can also occur (Nyman et al., 2014;Gee and Hillel, 1988). In addition, the modeling usually
92 involves upscaling of parameter values over a spatially and temporally discretized mesh from
93 measurements which are made on specific moments and locations. Such an upscaling process is

97 not always easy to execute and it could sometimes lead to serious errors. This is particularly true
98 for arid and semi-arid regions where most precipitation may be episodic (occurring in short and
99 unpredictable events) (Modarres and da Silva, 2007;Zhou et al., 2016), and may be confined to
100 restricted portions of the area (Gee and Hillel, 1988).

101 The third includes a cluster of experimental techniques such as isotopic tracer (Klaus and
102 McDonnell, 2013), water flux (Katz et al., 2016), and lysimeter (Scanlon, 2013). Among them,
103 lysimeters are instruments that directly measure the hydrological cycle in infiltration, runoff and
104 evaporation. Generally, this instrument is located in an open observation field or as a controlled
105 device, working either solely or in groups (Good et al., 2015). In a typical lysimeter, soil are
106 filled into a column surrounded by impermeable lateral boundaries thus water can only enter or
107 leave the column from upper or lower boundaries (Duncan et al., 2016;Fritzsche et al., 2016). A
108 drainage system is usually placed at the bottom (Glenn et al., 2013). The depth of soil in the
109 column depends on the experimental purpose. Experiments can be done with the same type of
110 soil at different depths in a single column, or in different columns but at the same depth. The soil
111 surface can be cultivated with different crops or left as bare land. Observation can be recorded
112 with weight or volume of water.

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113 Application of above-mentioned methods for assessing DSR in arid and semi-arid regions
114 has met a variety of challenges, primarily due to the fact that precipitation events often happen in
115 the form of short pulses with highly variable intensity (Collins et al., 2014). The intermittent and
116 unpredictable characteristics of precipitation events lead to highly variable moisture and nutrient
117 levels in the soils (Beatley, 1974;Huxman et al., 2004). It is unclear how the precipitation
118 amount, time, and interval will affect the water moisture of arid and semi-arid regions, especially
119 the change of deep soil water storage.

122 In this study, a new type of lysimeter is designed to accurately measure the amount of DSR
123 in arid and semi-arid regions. With the help of a three-year (2013-2015) field investigation with
124 this new lysimeter, one can answer the following question: Is the concept of an annual recharge
125 coefficient valid or not for estimating DSR at a given location in an arid and semi-arid region?
126 Before the introduction of this new type of lysimeter, it is necessary to briefly explain the
127 challenges faced by the conventional lysimeter for studying DSR in arid and semi-arid regions.

128 2. Design of the new lysimeter for DSR measurement

129 2.1. Problems with the conventional lysimeter methods in arid and semi-arid regions

130 Lysimeters have been used to access the amount of water consumed by vegetation for more
131 than three hundred years (Howell et al., 1991). The type of lysimeter that is specifically designed
132 to measure evapotranspiration (ET), called precision weighing lysimeter, has been developed
133 within the past six decades. In order to satisfy different requirements and needs, there are various
134 designs of weighing lysimeters, with surface areas ranging from 1.0 m² to over 29 m² (Howell et
135 al., 1991). The stored media mass and the type of scale such as diameter and height are factors
136 on which the accuracy of ET measurement depends, and many lysimeters have accuracy better
137 than 0.05 mm (Howell et al., 1991). Figure 1A shows the schematic diagram of a conventional
138 lysimeter installation in the field. It is basically a weight meter of soil with an open upper
139 boundary at ground surface and a perforated bottom boundary and impermeable vertical side
140 walls. The typical depth of lysimeters varies from 0.2 m to 2 m, but is rarely greater than 2.5 m
141 (Howell et al., 1991). The horizontal cross-section area is usually in the range of 1 m² to 29 m².
142 Precipitated water can freely infiltrate into the soil from the top and downward flow of water at
143 the bottom of the lysimeter is collected (through the perforation) as a function of time to
144 calculate the recharge. Alternatively, the weight of combined water and soil inside the lysimeter

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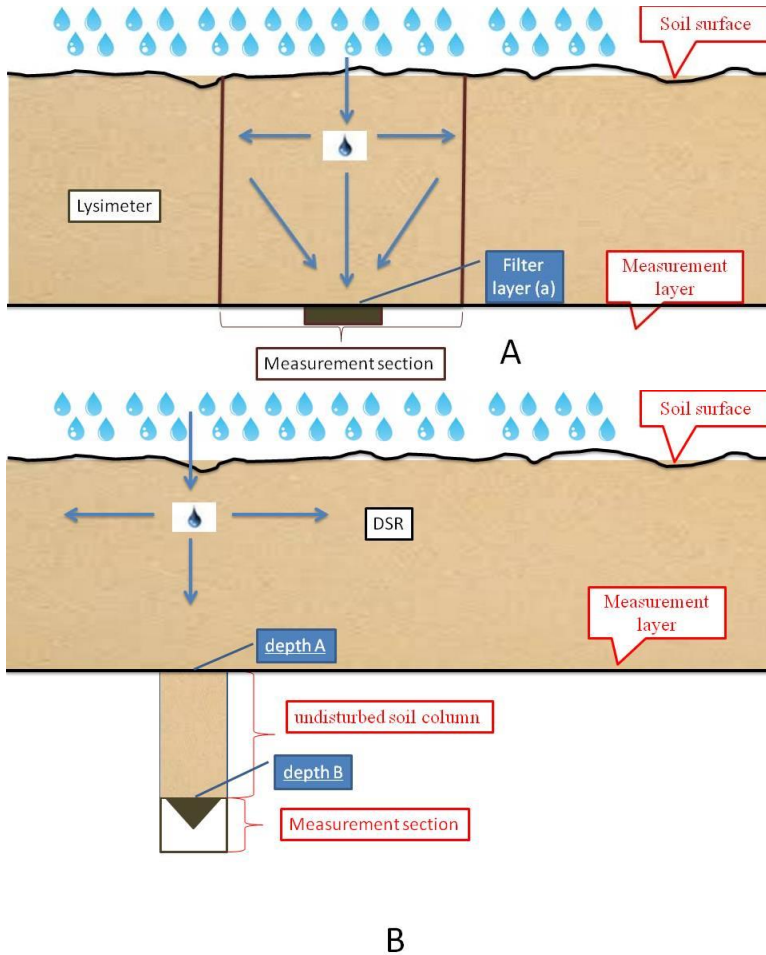
148 can be accurately measured using a weight gauge to reflect any soil moisture change. Such
149 information, combined with infiltration or evaporation at the surface, can yield the information
150 of downward water flux at the depth of lysimeter.

151 The following issues deserve special attention when applying the conventional lysimeter for
152 measuring recharge. Firstly, soil layers are inevitably disturbed when installing the instrument,
153 so the result may not reflect the actual recharge in native (undisturbed) soils (Weihermüller et al.,
154 2007) . Secondly, the cost is too high to use multiple lysimeters to observe large-scale infiltration
155 (Stessel and Murphy, 1992). Thirdly, when precipitation strength is relatively light and
156 concentrated, a large lysimeter cannot sensitively and rapidly measure DSR (Goldhamer et al.,
157 1999;Farahani et al., 2007). The conventional lysimeter often cannot answer the following
158 questions: To what soil layer can different levels of precipitations infiltrate? How much is the
159 infiltration amount under different levels of precipitation? (Gee and Hillel, 1988;Ogle and
160 Reynolds, 2004).

161 The conventional lysimeter as shown in Figure 1A may meet additional challenges when
162 applied to arid and semi-arid regions. Firstly, the water table depths in arid and semi-arid regions
163 may be much greater than the maximal depth of a conventional lysimeter (2.5 m). For instance,
164 in Chagan Nur, southeast of Mu Us sandy land in the Ordos basin of China, the water table depth
165 was found to be greater than 4 m. In the Gobi desert, the water table was reported to be at least
166 2.8 m deep (Ma et al., 2009). Therefore, the infiltration measured at the base of a conventional
167 lysimeter may not represent the actual recharge that eventually enters the groundwater system.
168 Secondly, the measurement accuracy of lysimeter often declines for soils with deep plant roots
169 because the depth of lysimeter installation is limited and it may be less than the depth of those
170 roots at site, which by itself can be important pathways for water migration. Consequently, the

171 measured recharge of such disturbed soil by lysimeter may not represent the in-situ recharge of
172 the native (undisturbed) soil.

173 To resolve the above-mentioned issues faced by the conventional lysimeter, a new type of
174 lysimeter is designed with specific considerations of the unique precipitation patterns and soil
175 characteristics in arid and semi-arid regions. This new lysimeter is illustrated schematically in
176 Figure 1(B).



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179 Figure 1. Schematic diagram of conventional lysimeter (A) and the new lysimeter (B).

180 **2.2 Design of a new lysimeter for measuring DSR in arid and semi-arid regions**

181 This new lysimeter has a few innovations (see Figure 1B) that can be outlined as follows.

182 Instead of setting the upper boundary of the lysimeter at ground surface, the new design has its

183 upper boundary at a designed depth (denoted as depth-A in Figure 1B) where infiltration will be

184 measured. A cylindrical container with a diameter of 20 cm to 40 cm with impermeable walls is
185 installed from depth-A downward to a deeper depth-B. The length of AB is determined
186 according to the capillary rise of the in-situ soil, which can be calculated using the average grain
187 size of soils within AB. More specifically, the length of AB is greater than the capillary rise of
188 soils within AB and it is usually great than 0.6 m (Liu et al., 2014). [At the soil surface there is a](#)
189 [device to measure the amount of the precipitation and at](#) the base of the instrument (depth B), a
190 water collection device is used to measure the amount of water exit the base.

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191 Before the measurement, one necessary preparation is to inject water from the top of the
192 instrument at depth-A using water pumps, the injection will stop until water starts to drip out
193 from the base at depth-B. One usually has to wait 10 days to allow the water profile in column
194 AB to become equilibrium. When water stops flowing out from depth-B, the soil water in the
195 column is regarded as reaching its equilibrium state, in which the soil moisture at depth-B
196 reaches the maximum field capacity. Under such an equilibrium status, the amount of infiltration
197 entering the upper surface of the lysimeter will be discharged (with the same amount) from the
198 base of the lysimeter after a certain delay time.

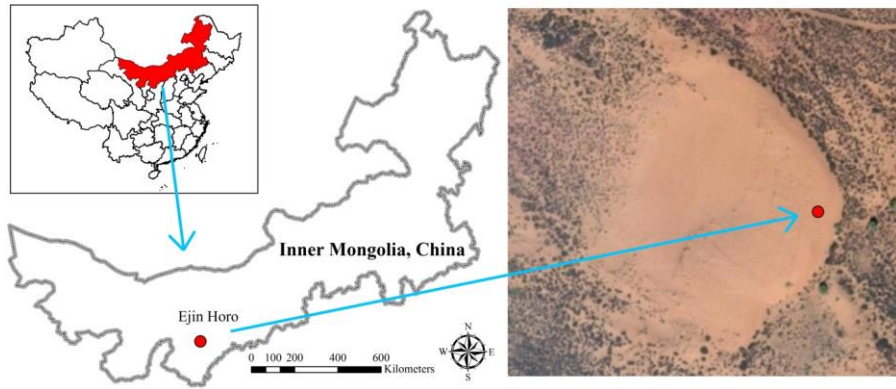
199 The proposed new method has a few innovative features that have not been considered in
200 previous studies. Firstly, it can measure DSR at any given layer of a multi-layer soil system
201 using a single apparatus installed in the field. Secondly, continuous real-time measurements can
202 be recorded over any given time period, thus a time-series of DSR can be obtained, which will be
203 very useful to understand the soil water dynamics at sandy area of arid and semi-arid regions.
204 Thirdly, the apparatus is portable and easy to install, thus a large amount of data can be collected
205 in various locations of a study area using multiple lysimeters, and spatial recharge distribution
206 can also be obtained straightforwardly. This method is field tested in arid and semi-arid sandy

209 regions of western China. It provides key references for the evaluation of water resources, water
210 balance, and the stability assessment of sand-fixing vegetation in arid and semi-arid areas. It also
211 provides data that are much needed for evaluating soil water contents and groundwater resources
212 of those areas. An important feature of this new lysimeter is that it can provide reliable DSR data
213 to examine the concept of annual recharge coefficient when comparing with the precipitation
214 data.

215 **3. Field testing of the new apparatus**

216 **3.1 Description of the study area**

217 Figure 2 shows the location of the study which is located in Ejin Horo Banner, on the
218 Eastern margin of Mu Us Sandy Land in the Ordos basin of China (geographic location: 39°05'
219 N, 109°36' E; altitude: 1070-1556 m above mean sea level). The groundwater table between
220 dunes are 5.3-6.8 m below ground surface. The climate is semi-arid continental monsoon climate
221 zone. Precipitation concentrates from July to September, with relatively concentrated rainstorm.
222 The average annual precipitation from 1960 to 2010 is 296.01 mm. The average annual
223 temperature of this area is 6.5°C, with about 151 days of frost-free season, 1809 mm total
224 evaporation, an average of 2900 hours of sunshine, and an average wind speed of 3.24 m/s (Wu
225 and Ci, 2002; Karnieli et al., 2014). The study area is located in relatively gentle mobile dunes,
226 and the soil type is Aeolian sandy soil.



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Figure 2. Geographic location of the experimental area.

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In term of geological structure, Mu Us Sandy Land is in the Ordos basin, a large-scale syncline sedimentary basin with nearly north-south striking axis, and is of Mesozoic and Paleozoic ages. The basin covers an area of 640 km from north to south, and 400 km from east to west. The axis of syncline is off west, and the east and west wings are asymmetric. The east wing is Monoclinic of westward tilt with a width of more than 300 km. The west wing is made of

235 many fault-fold belts striking along the north-south direction and thrusting eastward with a width
236 of less than 100 km. The southern boundary of the basin is Weibei plateau uplift. The southern
237 part of this plateau uplift is descending in ladder-shape with blocks to Fenwei rift-subsidence
238 basin. The northern boundary of this basin is Yimeng plateau uplift, with a lack of Lower
239 Paleozoic, and its edge-fault is connected to Hetao fault basin. The basement of Ordos basin is of
240 Precambrian crystalline metamorphic rocks.

241 Deposited in the basin are, in turn, Lower Paleozoic carbonate rocks, Upper Paleozoic-
242 Mesozoic clastic rocks, and Cenozoic sedimentary rocks with a total depth of more than 6000 m.
243 The discontinuous Cenozoic sediment is on top of the Mesozoic and Paleozoic layers, mainly of
244 the Quaternary and partially of the Tertiary sediments. The Quaternary layer is mainly made of
245 Aeolian sand and loess. Generally divided by a line along the Great Wall, the northwest land
246 surface is mainly covered by wind-blown sand layers of varying thickness and a 40-120 m thick
247 layer of alluvial-lacustrine; the southeast land surface is mainly covered by loess with various
248 thickness from tens of meters to more than 200 m. Below the loess layers, there is Tertiary
249 Pliocene mud rock with thickness of a few meters to tens of meters.

250 The hydro-stratigraphic units of the Ordos basin is quite complex, consisting of multiple
251 connected aquifers. Following the order from bottom to top, the multiple aquifers are primarily
252 made from various rock types of a karst aquifer consisting of Precambrian and Ordovician
253 limestone, a fractured aquifer consisting of Carboniferous and Jurassic clastic rocks, a porous-
254 fractured aquifer of Cretaceous clastic rocks, and a porous aquifer consisting of unconsolidated
255 Cenozoic and Quaternary sediments. Generally speaking, Mu Us Sandy Land has relatively rich
256 groundwater resources. The shallow groundwater reservoir is estimated to hold about 120.3
257 billion metric tons of freshwater. Groundwater is mainly recharged by precipitation with an

258 annual average recharge amount of 1.4 billion metric tons. Fine sands are the dominating
259 sediments observed in the experimental site. In the upper 200 cm soil layer in the experiment
260 area, the percentage of fine sand (0.5-0.1 mm) are 88.56%, 77.88%, 88.23%, 88.89%, 90.28%,
261 83.90%, and 84.21% at depths of 0 cm, 10 cm, 30 cm, 60 cm, 90 cm, 150 cm, and 200 cm,
262 respectively. The rest parts of the soil are primarily coarse sands. It is evident that the soil at the
263 upper 200 cm is relatively homogeneous.

264 3.2 Statistical analysis of data

265 Research on the relationship between precipitation and DSR of bare sand land in arid and
266 semi-arid regions is beneficial to understand the soil-water dynamics of those regions. Because
267 vegetation is absent, complexity related to transpiration process by plants is not a concern.
268 Based on two time series of real-time data of precipitation and DSR, one can examine the
269 relationship between DSR and precipitation. This study can serve as a basis for further study of
270 DSR in semi-fixed and fixed sand lands with different fractional vegetation covers.

271 In September 1, 2012, mobile sand dune within the study site was set as the monitoring plot
272 (geographic location: 39°05' N, 109°36' E; altitude: 1310 m) with the upper 300 cm soil profile
273 excavated. The lysimeter as shown in Figure 1B was installed following the procedure described
274 in section 2.2, and then backfilled using the excavated soil. Infiltration passing through the upper
275 200 cm depth is generally regarded as DSR in this study. It is worthwhile to point out that some
276 other investigators may use a more or less different depth threshold for defining DSR. For
277 instance, (Zhang et al., 2008) used 140 cm instead of 200 cm depth as the threshold to define
278 DSR. It was found that the water table depth was greater than 5 m in 2012-2015 at the study site,
279 so its influence to DSR was negligible. A precipitation sensor (AV-3665R, AVALON, United
280 States; precision: 0.2 mm) was placed above ground at the site. Data acquirer (CR200X,

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290 [Campbell, USA](#)) was used to record DSR, of which DSR data were recorded every one hour, and
 291 [the precipitation data were recorded every half hour. In order to avoid the effect of freeze-and-](#)
 292 [thaw action, the experiment was conducted between April 1, 2013 and November 30, 2015.](#)
 293 ~~[During such a three-year period, no runoff occurs at the studied area.](#)~~

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294 The statistics of precipitation and DSR are shown in Table 1, which reveals that there is an
 295 obvious difference of precipitation at the experimental plot from 2013 to 2015. The annual
 296 precipitation is 83 mm in 2013, 205.6 mm in 2014, and 186.4 mm in 2015. This is to say, the
 297 annual precipitations in 2014 and 2015 are 2.48 and 2.25 times of that in 2013, respectively.
 298 Such a dramatic fluctuation and uneven distribution of annual precipitation is typical of arid and
 299 semi-arid regions. The corresponding annual DSR is 20.2 mm in 2013, 20.6 mm in 2014, and 9.2
 300 mm in 2015. This is to say that the annual DSR values in 2014 and 2015 are 1.02 and 0.46 of that
 301 in 2013. The annual DSR/precipitation ratios (or the so-called annual recharge coefficient) for
 302 2013, 2014, and 2015 are 24.33%, 10%, and 4.94%, respectively.

303 It appears that there is no clear correlation between the annual DSR and the annual
 304 precipitation according to the data of 2013-2015. In another word, use of the annual recharge
 305 coefficient for the study site becomes questionable as such a coefficient implies that there is a
 306 close correlation between the annual DSR and the annual precipitation, which is not supported
 307 by the data of 2013-2015 [here](#). Therefore, we will scrutinize the precipitation pattern and
 308 intensity more closely to decipher the connection of precipitation and DSR in the following.

309 Table 1: The annual precipitation-DSR relationship from 2013-2015.

Year	Precipitation (mm)	DSR (mm)	DSR/precipitation*100%
2013	83	20.2	24.33%
2014	205.6	20.6	10%
2015	186.4	9.2	4.94%

2013	83	20.2	24.33%
2014	205.6	20.6	10%
2015	186.4	9.2	4.94%

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315 3.2.1 The relationship between precipitation pattern and DSR

316 Research on bare sandy soil water dynamic process usually focuses on temporal and vertical
317 differences (Ritsema and Dekker, 1994; Postma et al., 1991). In term of temporal soil moisture
318 variation over an annual cycle, the process could be divided as soil moisture replenishment,
319 depletion, and relatively stable periods. In term of vertical soil moisture variation, soil water
320 content usually first increases with depth and then decreases based on an interplay of mutual
321 infiltration and evaporation processes. In general, soil could be divided as a surface dry sand
322 layer, a layer with drastic moisture change, and a layer with relatively stable moisture content.
323 Specifically, the soil deeper than 160 cm in arid and semi-arid regions would have a relatively
324 stable moisture content. This is because of two reasons. Firstly, soil water will not be up-taken to
325 the surface by capillary force at such depths; secondly, ground water table in arid and semi-arid
326 regions is usually much lower than 160 cm.

327 In our study site, 2013 is an especially dry year with only 83 mm precipitation compared to
328 296.01 mm of average annual rainfall calculated over a period from 1960 to 2010. The
329 precipitation and DSR patterns of 2013 are shown in Figure 3. The measurement accuracy of the
330 lysimeter is 0.2 mm. During the observation period from April 1 to November 30, there are
331 totally 25 recorded precipitation events, mostly concentrated in the period from May to August.

332 There is a one-time strongest precipitation event with a 24-hour precipitation amount reaching 32
333 mm in August 3. The DSR correlated to this event can be identified from September 21 to
334 November 30 and reaches 17.2 mm. The delay time from precipitation event to the start of DSR
335 is approximately 48 days. The DSR/precipitation ratio for this particular event is as high as
336 53.75%. Such a DSR/precipitation ratio appears to be the highest in 2013. It is ~~notable~~, that
337 although the strongest precipitation event at August 3 contributes the greatest to DSR observed
338 from September 21 to November 30, a few precipitation events with amount of 6.6 mm prior to
339 this strongest precipitation event also contribute a minor part for DSR from July 27 to August 1.
340 It is also notable that the DSR/precipitation ratio for the strongest precipitation event is
341 substantially higher than the average annual recharge coefficient of 24.33% in 2013. This leads
342 to the conclusion that DSR is closely related to the strong precipitation events, rather than to the
343 average annual precipitation.

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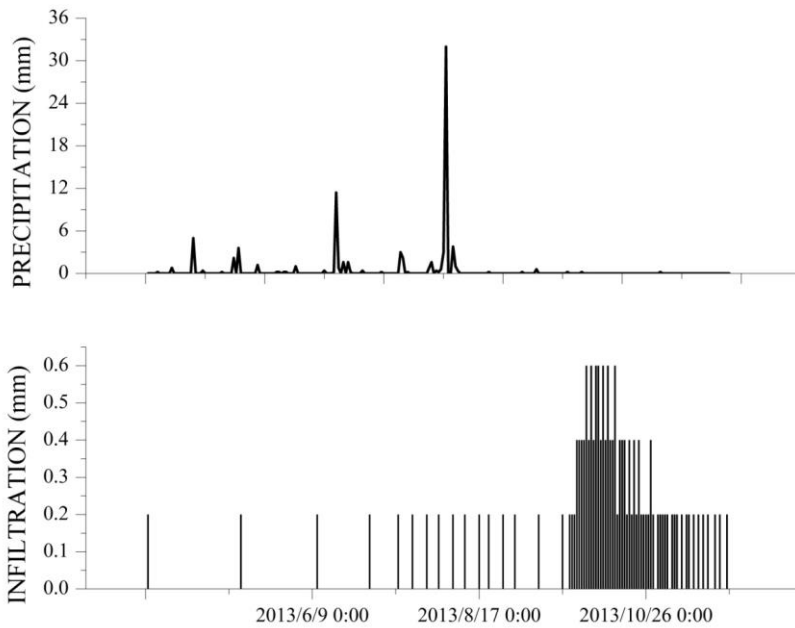


Figure 3: Precipitation and DSR patterns in 2013.

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348 In 2014, the annual precipitation is 205.6 mm, and DSR is 20.6 mm, leading to a 10%
 349 annual average recharge coefficient, which is less than half of that in 2013. As shown in Figure 4,
 350 the frequency of precipitation events in 2014 is obviously higher than that of 2013. From April 1
 351 to November 30, there are total 68 times of precipitation events, compared to 41 times in 2013.
 352 Furthermore, the precipitation distribution in 2014 is more uniform than that in 2013.
 353 Specifically, precipitation events are concentrated in the period from June to August, with the
 354 highest 24-hour accumulative precipitation of 15 mm on July 30. As shown in Figure 4, recorded
 355 DSR data cover a period from April 1 to November 30, and the maximum DSR occurs in
 356 October 1. Because the experimental plot is located in a transition zone between arid and semi-
 357 arid regions, summer evaporation is strong, leading to relatively less DSR during the summer

358 season. While during the period from September 1 to November 30, atmospheric temperature
359 drops and sunshine duration becomes shorter, which results in less surface evaporation and
360 greater DSR during this period. Comparing with 2013, there are more summer precipitation
361 events in 2014. That is [one reason](#) why precipitation in 2014 (205.6 mm) is greater than 2013 (83
362 mm) but the overall DSR in 2014 is less than that in 2013.

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363 The strongest single-day precipitation in 2014 is 15 mm (occurred in July 30), which is less
364 than half of the strongest single-day precipitation event of 32 mm occurred in 2013 (August 3),
365 annual DSR/precipitation ratio [is 24.33% in 2013 but drops to 10% in 2014](#). This once again
366 supports the conclusion that the strong precipitation events rather than the average annual
367 precipitation are mostly responsible for the average annual DSR. [This is the other reason why](#)
368 [precipitation in 2014 \(205.6 mm\) is greater than 2013 \(83 mm\) but the overall DSR in 2014 is](#)
369 [less than that in 2013](#).

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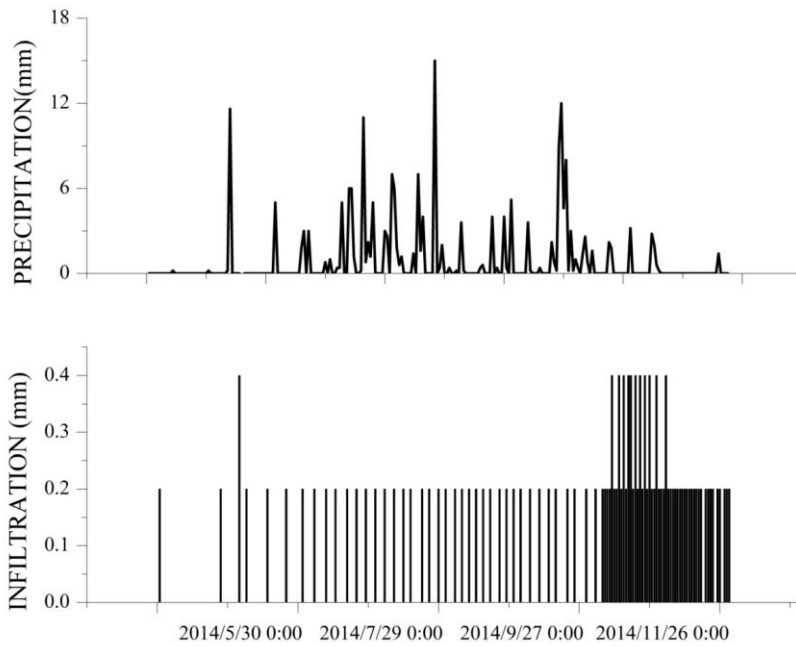


Figure 4: Precipitation and DSR patterns in 2014.

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As shown in Figure 5, the total annual precipitation of 2015 is 186.4 mm, and DSR is 9.2 mm, leading to a 4.94% annual average recharge coefficient, which is significantly smaller than of 2013 (24.33%) and 2014 (10%). There are total 66 observable precipitation events in 2015. Such precipitation events are mostly concentrated from April 4 to July 6, with a total precipitation of 155 mm during this period, which represents 83.15% of the total precipitation in 2015. The measured DSR from April 4 to July 6 is only 7 mm, representing 77.78% of the total DSR in 2015. Throughout 2015, two strongest precipitation events happens on April 4 and June 5, both 24-hour precipitation events reach 17.2 mm. We observe a single-day DSR peak of 0.8 mm, 36 days after April 4, one of the two greatest single-day DSR values observed in 2015, but

389 no peak value of DSR response to the strong precipitation on June 5. As explained before,
 390 summer stronger evaporation leads to relatively less DSR during the summer season compared
 391 with other seasons. The third greatest precipitation is 16.8 mm on October 5, which leads to a
 392 peak value of 0.8 mm of DSR on October 21, with a 16-day delay time. If comparing the
 393 precipitation events occurred on April 4 (17.2 mm) and October 5 (16.8 mm), one can see that
 394 these two precipitation events are similar in strength (17.2 mm for April 4 and 16.8 mm for
 395 October 5) but different in the DSR delay time (36 days for April 4 and 16 days for October 5).
 396 [Comparing two precipitation events which are similar in strength but different in the DSR delay](#)
 397 [time. temperature is the most likely factor responsible for such delay, so this leads](#) to a
 398 conclusion that temperature influences the DSR rate. To investigate how the soil temperature
 399 affects the DSR rate, further field experiments are needed in the future study.

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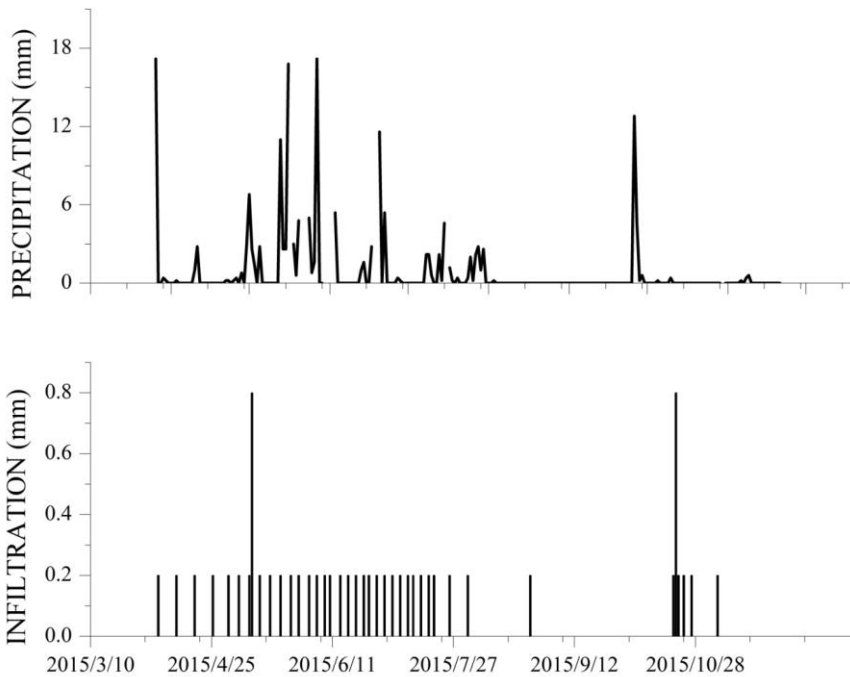
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408 Figure 5: Precipitation and DSR patterns in 2015.

409 **3.2.2 Relationship between precipitation intensity and DSR**

410 Based on observational data and analysis in 3.2.1, one can see that precipitation intensity, to
411 some extent, influences DSR. For the sake of illustration, the precipitation intensity for bare sand
412 land is roughly classified into light, moderate, and strong events with precipitation amount less
413 than 6 mm, between 6 mm to 10 mm, and greater than 10 mm, respectively. In general, light
414 precipitation rarely can reach the soil zone deeper than 40 cm because of evaporation, thus it
415 makes almost no contribution to DSR (Zhang et al., 2016). Such a classification may be revised
416 under different vegetation covering conditions in different regions (Kosmas et al., 2000).

417 According to this classification, statistics of moderate to strong precipitation events and
418 their percentage shares in the annual precipitation from 2013 to 2015 are shown in Table 2. In
419 2013, there are only two precipitation events with intensity greater than 6 mm. The total amount
420 of these two precipitation events is 43.4 mm, which represents 52.29% of the annual
421 precipitation in 2013. In 2014, there are 11 precipitation events with intensity greater than 6 mm,
422 much more frequent than that of 2013 (2 times) and moderately more frequent than that of 2015
423 (8 times). The total moderate to strong precipitation in 2014 is 98.6 mm, representing 47.96% of
424 the annual precipitation in 2014. In 2015, there are 8 precipitation events with intensity greater
425 than 6 mm, accounting for 53.54% of the annual precipitation in 2015.

426 Among these three years, 2015 has the largest percentage of moderate to strong
427 precipitation over the annual precipitation. However, at this same year, one has seen the smallest
428 ratio of annual DSR/precipitation ratio or annual recharge coefficient (see Table 1). This implies
429 that the annual DSR does not seem to be positively correlated to the annual total precipitation.
430 This finding has a few profound consequences. It basically states that assigning a constant annual

431 recharge coefficient for a particular soil regardless of precipitation patterns is not a good practice,
 432 because annual DSR is not always proportional to the total annual precipitation. Instead, it
 433 appears to be more closely related to individual precipitation events stronger than 10 mm.

434 Table 2: Percentage of valid precipitation in total precipitation amount.

Year	Number of precipitation >6mm (24 hr cumulative)	Amount of precipitation >6mm (mm)	Valid precipitation /annual precipitation (%)
2013	2	43.4	52.29
2014	11	98.6	47.96
2015	8	99.8	53.54

435
 436 Table 3 lists the number of strong precipitation (with amount greater than 10 mm) and also
 437 the strongest precipitation amount for each of 2013, 2014 and 2015. In 2013, there are only 2
 438 strong precipitation events, but the maximum single-day precipitation amount reaches 32 mm
 439 (August 3). The accumulative strong precipitation of 2013 is 43.4 mm, which is 52.28% of the
 440 annual precipitation in 2013. In 2014, there are 4 strong precipitation events and the maximum
 441 single-day precipitation amount is 15 mm. The accumulative strong precipitation of 2014 is 49.6
 442 mm, which is 24.12% of the annual precipitation in 2014. In 2015, there are 6 strong
 443 precipitation events, and the maximum single-day precipitation amount is 17.2 mm. The
 444 accumulative strong precipitation of 2015 is 86.6 mm, which represents 46.46% of the annual

445 precipitation in 2015. The annual DSR versus annual precipitation ratios are 24.33%, 10%, and
 446 4.94% for 2013, 2014, and 2015, respectively.

447 As shown in Table 3, the strongest single-day precipitation (32 mm in 2013) appears to
 448 affect DSR the most in 2013. For 2014 and 2015, as the strongest precipitation events in these
 449 two years are significantly smaller than that in 2013. Such a positive correlation is particularly
 450 strong for 2013 which has the largest maximum precipitation event of 32 mm, showing that the
 451 strong single-day precipitation affects DSR. This positive correlation is weaker for 2014 and
 452 2015 which have moderate and somewhat similar maximum precipitation events (15 mm and
 453 17.2 mm, respectively). As shown in Figures 4 and 5, precipitation patterns in 2014 and 2015 are
 454 quite different despite the fact that the maximum precipitation events are similar to each other.
 455 The precipitation in 2014 is somewhat uniformly distributed from April to November, while the
 456 precipitation in 2015 is mostly concentrated from May to June. This observation suggests that
 457 DSRs for these two years are related to the precipitation pattern as well as the precipitation
 458 strength. However, precisely quantifying such a correlation between DSR and the precipitation
 459 pattern and precipitation strength requires further investigations.

460 In summary, one may conclude that annual DSR in arid and semi-arid regions mainly rely
 461 on strong precipitation events, but the determination of the threshold for strong precipitation
 462 events that directly contribute to DSR is still unclear and requires further investigation.

463 Table 3: Inter-annual statistics of strong precipitation and its percentage in total annual
 464 precipitation amount.

Year	Number of strong precipitation	Maximum precipitation	Annual DSR (mm)	Annual DSR /annual precipitation (%)
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 2013 年单次强降雨达到 32mm，2013 年总渗漏量最大，对比 2013 年与 2014,2015 年数据，显示强降雨与渗漏量正相关，虽然 2014,2015 年最大单次降雨相近（15mm，17.2mm），但是 2014 年和 2015 年最大降雨量和渗漏量并不相关，因为 2014,2015 年降雨格局不同，如图 4，5 所示，2014 年降雨平均分布在 4 月到 11 月之间，2015 年降雨比较集中分布在 5 到 6 月，这就解释为什么单次最大降雨强度相似但是渗漏量却不同。¶

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event(mm)				
2013	2	32	20.2	24.33
2014	4	15	20.6	10
2015	6	17.2	9.2	4.94

484

485 Under the condition of continuous precipitation, it may be difficult to discretize
486 precipitation into individual events. The following example illustrates a procedure to deal with
487 this situation. As shown in Figure 6, there is a 13-days continuous precipitation process in 2013
488 from July 27 to August 8, and the accumulative precipitation is 43.8 mm. The start of a
489 continuous DSR distribution corresponding to this 13-day continuous precipitation event is
490 observed 3 days after the end of this precipitation process, and the peak value of DSR occurs 46
491 days after the end of this precipitation process. The DSR distribution gradually recedes to zero
492 around 78 days after the end of the precipitation process. The accumulative DSR amount over a
493 75-day period is 18.4 mm. The ratio of the 75-day cumulative DSR over the 13-day precipitation
494 event is 42%.

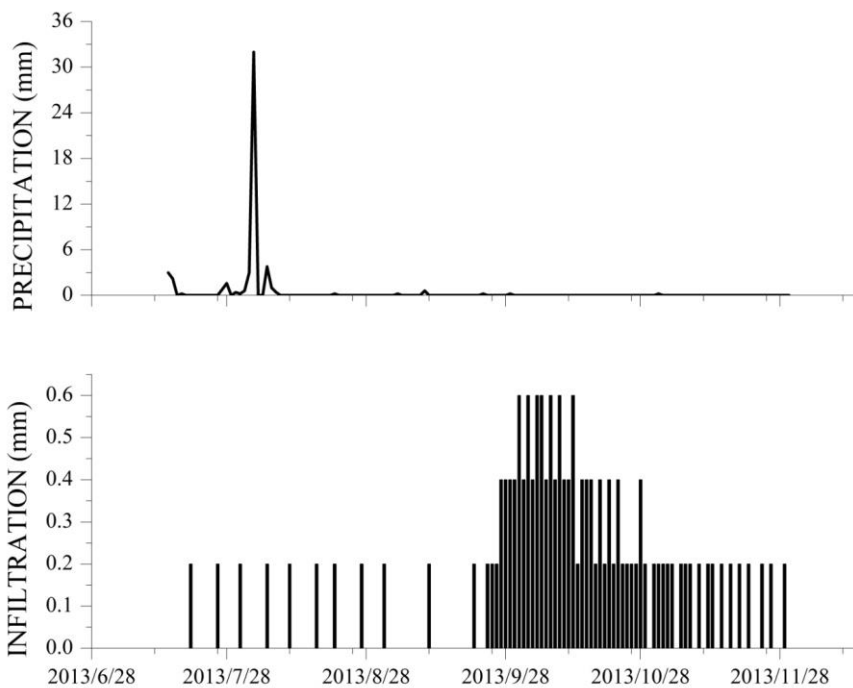


Figure 6: One-day intensive precipitation's contribution to DSR in 2013.

495
496

497 **4. Discussion**

498 This improved lysimeter is on the real-time dynamic monitoring of DSR, and it provides
 499 reliable evidence for an accurate evaluation of precipitation-related recharging capability of bare
 500 sand lands in arid and semi-arid regions. However, there are a number of issues that deserves
 501 further attention and requires additional investigations in the future. The moisture evaporation,
 502 the soil absorption of moisture, and the water infiltration of post-evaporative redistribution, are
 503 all very complex processes, especially in arid and semi-arid regions. It is sometimes difficult to
 504 clearly distinguish the amount of evaporation and DSR with conventional methods as outlined in
 505 the introduction. This study selects precipitation and infiltration data during the period from
 506 April 1 to November 30, so the influence of freeze-thaw process during winter is avoided, and

507 the experimental design and data analysis is simplified. For this reasons, the next steps should be
508 a full-term monitoring, a systematic study on DSR, as well as a study on the soil temperature and
509 daily temperature influences on DSR.

510 Although this experiment does not address the issue of soil temperature effect on DSR in
511 great details, the relationship between DSR and soil temperature is evident. In general, a higher
512 temperature means a stronger evaporation demand, thus an often smaller DSR.

513 Through the analysis of this study, one can see that the use of an annual recharge coefficient
514 for the study area is not supported by the data collected from the new lysimeter, as the annual
515 recharge is not positively correlated with the annual total precipitation. Instead, we find that the
516 recharge is somewhat positively correlated with a few strong precipitation events (greater than
517 10 mm), and is closely correlated with the strongest precipitation event (considerably greater
518 than 10 mm), as well as the precipitation patterns. It is probably reasonable to assign different
519 weighting factors for different precipitation strengths to calculate DSR. However, the threshold
520 to define a strong precipitation event that makes direct contribution to DSR is not precisely
521 quantified, and this is a subject that should be investigated in more details in the future. The
522 determination of weighting factors for different precipitation strengths is also a subject requires
523 further investigation.

524 This investigation is based on detailed analysis of precipitation and DSR data at the study
525 site without involving modeling effort which certainly will be explored in the future as well. This
526 study represents our first attempt of questioning the application of recharge coefficient concept
527 in arid and semi-arid regions.

528

529 **5. Conclusions**

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531 This study uses a newly designed lysimeter to study three consecutive years (2013-2015) of DSR
532 underneath bare sand land on the Eastern margin of Mu Us Sandy Land in the Ordos basin of
533 China. The objective is to identify the characteristics of the DSR distribution and the factors
534 affecting the DSR distribution. Specifically, we like to examine if the commonly used recharge
535 coefficient concept can be applied for arid and semi-arid regions such as the Eastern margin of
536 Mu Us Sandy Land of China. The following conclusions can be drawn from this study:

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- 537 (1) The annual recharge coefficient concept is generally inapplicable for estimating DSR in the
538 study site.
- 539 (2) Precipitation pattern including precipitation intensity and precipitation season significantly
540 influences DSR.
- 541 (3) The temperature influences the DSR/precipitation ratio, which is less in summer as in other
542 seasons, given the similar precipitation intensity.
- 543 (4) DSR is not correlated with the annual precipitation. Instead, it is correlated with the strong
544 precipitation (greater than 10 mm) events at the site. However, quantitative determination of
545 the thresholds for such strong precipitation events that makes direct contribution to DSR is
546 not entirely understood. Further investigation is needed on this subject.

547

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549 Science and Technology of the People's Republic of China (2013CB429901).

550

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