



1 **Numerical Solution and Application of Time-Space Fractional Governing Equations**
2 **of One-Dimensional Unsteady Open Channel Flow Process**

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12 **Abstract**

13

Although fractional integration and differentiation have found many applications in various
14 fields of science, such as physics, finance, bioengineering, continuum mechanics and
15 hydrology, their engineering applications, especially in the field of fluid flow processes,
16 are rather limited. In this study, a finite difference numerical approach is proposed to solve
17 the time-space fractional governing equations of one-dimensional unsteady/non-uniform
18 open channel flow process. By numerical simulations, results of the proposed fractional
19 governing equations of the open channel flow process were compared with those of the
20 standard Saint Venant equations. Numerical simulations showed that flow discharge and
21 water depth can exhibit heavier tails in downstream locations as space and time fractional
22 derivative powers decrease from 1. The fractional governing equations under consideration
23 are generalizations of the well-known Saint Venant equations, which are written in the
24 integer differentiation framework. The new governing equations in the fractional order
25 differentiation framework have the capability of modeling nonlocal flow processes both in
26 time and in space by taking the global correlations into consideration. Furthermore, the
27 generalized flow process may shed light into understanding the theory of the anomalous



28 transport processes and observed heavy tailed distributions of particle displacements in
29 transport processes.

30

31 **Introduction**

32

33 The origin of integration and differentiation of arbitrary (non-integer) order dates back to
34 a letter of Leibniz, in which derivatives of 0.5 order was described (Oldham and Spanier,
35 1974). Especially after the first international conference (Ross, 1975), the fractional
36 calculus found many applications in various fields of science, including physics, finance,
37 bioengineering, continuum mechanics and hydrology (Caputo, 1967; Bouchaud and
38 Georges, 1990; Carpinteri and Mainardi, 1997; Podlubny, 1999; Hilfer, 2000; Barkai et al.,
39 2000; Benson et al., 2000; Scalas et al., 2000; Baeumer et al., 2001; Meerschaert et al.,
40 2002; Raberto et al., 2002; Zaslavsky, 2002; Magin, 2006; Tarasov, 2010; Benson et al.,
41 2013; Kavvas et al., 2015; Kim et al., 2015; and many others). As Tarasov (2010) stated,
42 the fractional equations are utilized to describe the fractal distributions of mass, charge and
43 probability. However, their engineering applications, especially in the field of fluid
44 dynamics, are limited (Kulish and Lage, 2002; Tarasov, 2010; Kavvas and Ercan, 2015,
45 2016; Ercan and Kavvas, 2015a).

46

47 The long-range dependence or the long memory occurs when the so called Hurst coefficient
48 (Hurst, 1951) is between 0.5 and 1 showing that the process is outside the Brownian domain
49 of finite memory processes. Slowly decaying autocorrelations and unbounded spectral
50 density near zero frequency are the characteristics of the long memory signals (Beran
51 1994). The long-range dependency or the long memory was reported for several
52 geophysical processes, for example, for river flows and velocity fluctuations by Nordin et
53 al. (1972), Montanari et al. (1997), Vogel et al. (1998), and Szolgayová et al. (2013);
54 porosity and hydraulic conductivity in sub-surface hydrology by Molz and Boman (1993);
55 climate variability by Bloomfield (1992), Stephenson et al. (2000), Koutsoyiannis (2003),
56 Franzke (2013), and Franzke et al. (2015); and sea levels by Barbosa et al. (2006), and
57 Ercan et al. (2013). Hurst phenomena or the long-range dependence is also closely related



58 to self-similarity of the geophysical processes (Pipiras and Taqqu, 2003; Beran, 1994;
59 Ercan et al., 2014; Ercan and Kavvas, 2015b, 2015c).

60

61 In order to be able to model both the long-memory behavior as well as the Brownian finite-
62 memory behavior of a flow process at various scales, Kavvas and Ercan (2016) stated that
63 a model needs to be more flexible than a purely long-memory model (such as fractional
64 Gaussian noise or Autoregressive fractionally integrated moving average model), or a
65 finite-memory model (such as the standard integer governing equations of the river flow
66 processes). Within this context, time-space fractional governing equations of
67 unsteady/non-uniform open channel flow process were developed within Caputo fractional
68 derivative framework by Kavvas and Ercan (2016). The advantage of the fractional
69 derivatives in Caputo framework is that the traditional initial and boundary conditions,
70 which are physically interpretable, can be utilized (Podlubny, 1999).

71

72 In this study, a numerical algorithm is proposed to solve the time-space fractional
73 governing equations of one-dimensional unsteady/non-uniform open channel flow process
74 and to investigate its modeling capabilities different than the standard Saint Venant
75 equations. A first-order approximation of the Caputo's fractional time derivative (Murio,
76 2008) and a second-order accurate Caputo's fractional space derivative (Odibat, 2009) are
77 coupled in the proposed numerical algorithm. When orders (or powers) of the time and
78 space fractional derivatives become one, the proposed governing equations of
79 unsteady/non-uniform open channel flow process in fractional differentiation framework
80 reduce to Saint Venant equations in integer order differentiation framework (Kavvas and
81 Ercan, 2016), and the proposed numerical algorithm reduces to the explicit finite difference
82 scheme reported in Viessman, et al. (1977). As such, utilizing the proposed numerical
83 solution, the capabilities of the proposed fractional governing equations of the
84 unsteady/nonuniform open channel flow process were investigated, comparing the results
85 of the fractional governing equations with those of the standard Saint Venant equations.

86



87 The fractional governing equations of one-dimensional unsteady/non-uniform open
88 channel flow process based on the Caputo fractional derivatives, as derived in Kavvas and
89 Ercan (2016), are presented in the next section.

90

91 **Governing Equations**

92

93 The time-space fractional mass conservation equation and the time-space fractional motion
94 equation, based on the Caputo fractional derivative framework, for one-dimensional
95 unsteady/non-uniform open channel flow in straight prismatic channels which is taking
96 place from the upstream to downstream direction, can be written as (Kavvas and Ercan,
97 2016),

$$98 \quad \frac{\Gamma(2-\alpha)}{t^{1-\alpha}} \frac{\partial^\alpha A}{\partial t^\alpha} + \frac{\Gamma(2-\beta)}{x^{1-\beta}} \frac{\partial^\beta AV}{\partial x^\beta} = q_L(x, t) \dots \quad (1)$$

$$99 \quad S_f = -\frac{\Gamma(2-\beta)}{x^{1-\beta}} \frac{\partial^\beta z}{\partial x^\beta} - \frac{\Gamma(2-\beta)}{x^{1-\beta}} \frac{\partial^\beta y}{\partial x^\beta} - \frac{V}{g} \frac{\Gamma(2-\beta)}{x^{1-\beta}} \frac{\partial^\beta V}{\partial x^\beta} - \frac{1}{g} \frac{\Gamma(2-\alpha)}{t^{1-\alpha}} \frac{\partial^\alpha V}{\partial t^\alpha} \dots \quad (2)$$

100 where $0 < \alpha, \beta \leq 1$ are the time and space fractional derivative powers, $\Gamma(\cdot)$ is the gamma
101 function, Q is the flow rate, A is the flow cross-sectional area, x is distance in the flow
102 direction, t is time, y is water depth, g is the acceleration due to gravity, z is the channel
103 bed elevation. The advantage of the utilized Caputo fractional derivative approach is that
104 the traditional initial and boundary conditions can be incorporated (Podlubny, 1999).

105

106 In the fractional continuity equation and fractional motion equation, there are three
107 unknown flow variables, while there are only two equations. Accordingly, in order to close
108 this system a resistance equation is needed. Such a resistance equation is the Manning's
109 equation, which can be expressed as

$$110 \quad S_f = \frac{n^2 V |V|}{R^{4/3}} \dots \quad (3)$$

111 The fractional mass conservation equation (1), the fractional motion equation (2) and the
112 fractional resistance equation (3) form the complete set of governing equations of
113 upstream-to-downstream one dimensional unsteady open channel flow in fractional time-



114 space. When $\alpha=\beta=1$, governing equations of one dimensional fractional open channel flow
115 reduce to classical Saint Venant equations.

116

117 A comprehensive explanation of the concepts of fractional differentiation and integration
118 could be found in Oldham and Spanier (1974), Miller and Ross (1993), Samko et al. (1993),
119 Podlubny (1999), Podlubny (2002), and Tarasov (2010).

120

121 Numerical Solution

122

123 Although a large number of physical problems are formulated by the fractional differential
124 equations, the state of art is far less developed for their solution by the numerical
125 approaches, and the analytical solutions are available for very simple linear problems
126 (Podlubny, 1999). Therefore, as pointed out by Li and Zeng (2012), it is important to
127 develop efficient and reliable numerical solutions for the problems governed by the
128 fractional differential equations. Within this context, a finite difference numerical method,
129 first order accurate in time and second order accurate in space, is introduced in this article
130 to solve time-space fractional governing equations of the one-dimensional unsteady/non-
131 uniform open channel flow process.

132

133 Dividing the time interval $[0, T]$ into N subintervals of equal width $k = T/N$ by using the
134 nodes $t_n = nk$, $n = 0, 1, 2, \dots, N$, the first-order approximation of Caputo's fractional time
135 derivative can be written as (Murio, 2008)

$$136 \quad D_t^\alpha f_i^n = \sigma_{\alpha,k} \sum_{j=1}^n w_j^{(\alpha)} (f_i^{n-j+1} - f_i^{n-j}) \dots \quad (4)$$

137 where $f_i^n = f(x_i, t_n)$, $\sigma_{\alpha,k} = \frac{1}{\Gamma(1-\alpha)} \frac{1}{(1-\alpha)} \frac{1}{k^\alpha}$ and $w_j^{(\alpha)} = j^{1-\alpha} - (j-1)^{1-\alpha}$

138 Then, the fractional continuity equation given by Eqn. (1) can be discretized as

$$139 \quad \sigma_{\alpha,k} \sum_{j=1}^{n+1} w_j^{(\alpha)} (A_i^{n-j+2} - A_i^{n-j+1}) + \frac{(t_i^n)^{1-\alpha}}{(x_i^n)^{1-\beta}} \frac{\Gamma(2-\beta)}{\Gamma(2-\alpha)} \frac{\partial^\beta A_i^n V_i^n}{\partial x^\beta} = \frac{(t_i^n)^{1-\alpha}}{\Gamma(2-\alpha)} q_{Li}^n \dots \quad (5)$$

140 where $A_i^n = A(x_i, t_n)$. Rearranging the known variables on the right hand side and the
141 unknown flow area on the left hand side results in



$$A_i^{n+1} = A_i^n - \sum_{j=2}^{n+1} w_j^{(\alpha)} (A_i^{n-j+2} - A_i^{n-j+1}) - \frac{(t_i^n)^{1-\alpha}}{(x_i^n)^{1-\beta}} \frac{\Gamma(2-\beta)}{\Gamma(2-\alpha)\sigma_{\alpha,k}} \frac{\partial^\beta A_i^n V_i^n}{\partial x^\beta} + \frac{(t_i^n)^{1-\alpha}}{\Gamma(2-\alpha)\sigma_{\alpha,k}} q_{Li}^n \quad \dots(6)$$

Fractional space derivative term $\frac{\partial^\beta}{\partial x^\beta}$ in Eqn. (6) can be obtained from the second order accurate approximation of the Caputo fractional derivatives, as proposed by Odibat (2009). Dividing the space interval $[0, a]$ into M subintervals $[x_j, x_{j+1}]$ of equal width $h = a/M$ using the nodes $x_j = jh$, for $j = 0, 1, 2, \dots, M-1$, the Caputo fractional derivative $D_x^\alpha f(x)$ at $a > 0$ can be approximated by (Odibat, 2009)

$$(D_x^\alpha f(x))(a) \approx \frac{h^{1-\alpha}}{\Gamma(3-\alpha)} \left\{ \left[(M-1)^{2-\alpha} - (M+\alpha-2)M^{1-\alpha} \right] f'(0) + f'(a) + \sum_{j=1}^{M-1} \left[(M-j+1)^{2-\alpha} - 2(M-j)^{2-\alpha} + (M-j-1)^{2-\alpha} \right] f'(x_j) \right\} \dots(7)$$

where $0 < \alpha \leq 1$ is the arbitrary order of the derivative and $f'(x_j)$ is the first order derivative at x_j , which can be estimated by the central-difference formula as

$$f'(x_j) = \frac{f(x_j+h) - f(x_j-h)}{2h} + O(h^2) \dots \quad (8)$$

The first order derivative of the function f can be estimated as $f'(0) = \frac{f(h) - f(0)}{h}$ at the upstream boundary and as $f'(a) = \frac{f(a) - f(a-h)}{h}$ at the downstream boundary when the further upstream and further downstream function values are not available, which is usually the case in open channel flow problems.

Analogous to the explicit finite difference scheme for the equation of motion in terms of integer order derivatives in Viessman, et al. (1977), and utilizing the first-order approximation of Caputo's fractional time derivative (Murio, 2008), the fractional equation of motion given by Eqn. (2) can be discretized as



$$\begin{aligned}
 165 \quad (S_f)_i^{n+1} &= -\frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta z_i^n}{\partial x^\beta} - \frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta y_i^n}{\partial x^\beta} - \frac{V_i^n}{g} \frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta V_i^n}{\partial x^\beta} \\
 166 \quad &\quad - \frac{\Gamma(2-\alpha)\sigma_{\alpha,k}}{g(t_i^n)^{1-\alpha}} \sum_{j=1}^{n+1} w_j^{(\alpha)} (V_i^{n-j+2} - V_i^{n-j+1}) \dots (9)
 \end{aligned}$$

167 When the flow is from upstream to downstream $V|V|$ in Eqn. (3) becomes V^2 and Eqn. (9)
 168 can be written as

$$\begin{aligned}
 169 \quad \frac{n^2(V_i^{n+1})^2}{(R_i^{n+1})^{4/3}} &= -\frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta z_i^n}{\partial x^\beta} - \frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta y_i^n}{\partial x^\beta} - \frac{V_i^n}{g} \frac{\Gamma(2-\beta)}{(x_i^n)^{1-\beta}} \frac{\partial^\beta V_i^n}{\partial x^\beta} \\
 170 \quad &\quad - \frac{\Gamma(2-\alpha)\sigma_{\alpha,k}}{g(t_i^n)^{1-\alpha}} \sum_{j=1}^{n+1} w_j^{(\alpha)} (V_i^{n-j+2} - V_i^{n-j+1}) \dots (10)
 \end{aligned}$$

171 Space-fractional derivative terms $\frac{\partial^\beta z_i^n}{\partial x^\beta}$, $\frac{\partial^\beta y_i^n}{\partial x^\beta}$, and $\frac{\partial^\beta V_i^n}{\partial x^\beta}$ can be estimated from Eqn. (7).

172 If bed elevation does not change through time, then the initial estimate of $\frac{\partial^\beta z_i^n}{\partial x^\beta}$ will be the
 173 same for all time steps. On the other hand, if bed elevation changes through time, such as
 174 in the case of sediment transport processes, then this term should be calculated for each
 175 time step as the bed elevation changes through time due to erosion and deposition
 176 processes.

177

178 For a known geometry, hydraulic radius R_i^{n+1} can be calculated from the known flow
 179 cross-sectional area A_i^{n+1} . For example, water depth can be calculated as $y_i^{n+1} = A_i^{n+1} / B$
 180 for a rectangular channel of width B and the hydraulic radius can be calculated as
 181 $R_i^{n+1} = A_i^{n+1} / (B + 2y_i^{n+1})$. Eqn. (10) is a quadratic equation in the form of
 182 $c_1(V_i^{n+1})^2 + c_2V_i^{n+1} + c_3 = 0$, from which V_i^{n+1} can be estimated.

183

184 **Numerical Example**

185



186 For a numerical example problem, a 3218.7-meter long, 6.1-meter wide rectangular
187 channel with a bottom slope of 0.0015 and an estimated Manning's roughness of 0.02 is
188 considered. At the upstream boundary, 1.83-meter depth initial uniform flow is subjected
189 to an increase to 56.63 m³/s in a period of 20 minutes. Then this flow decreases uniformly
190 to the initial flow depth during a subsequent period of 40 minutes duration. During the rest
191 of the simulation, the initial flow conditions are applied. In this example problem, the
192 upstream flow is routed utilizing the time-space fractional governing equations of the one-
193 dimensional unsteady/non-uniform open channel flow (Eqns 1-3, Kavvas and Ercan,
194 2016), by applying the proposed numerical solution approach given above.

195

196 A classical solution of this problem by the Saint Venant equations in integer order
197 differentiation framework was provided by Viessmann et al. (1977). In addition to the
198 above proposed numerical solution for the time-space fractional governing equations, this
199 problem was also simulated by the Viessmann et al. (1977)'s explicit numerical scheme
200 for the Saint Venant equations, with the difference that the hydraulic radius was estimated
201 by the ratio of the flow cross-sectional area to the wetted perimeter. The solutions by the
202 Saint Venant equations were depicted as Viessmann et al. (1977) in Figures 1 and 2.

203

204 Non-dimensional flow discharges (Q/Q_0) and non-dimensional water depths (y/y_0) through
205 time at the downstream boundary are depicted in Figure 1 when space and time fractional
206 powers $\beta = \alpha = 1, 0.9, 0.8, 0.7$. Here, Q_0 and y_0 are initial flow and water depths. As shown
207 in Figures 1a and 1b, when time and space derivative powers are equal to one ($\alpha=\beta=1$),
208 non-dimensional water depths and flows at the downstream location, simulated by the
209 proposed numerical scheme for the fractional governing equations of the one-dimensional



210 unsteady/non-uniform open channel flow, coincide well with those simulated by the
211 Viessmann et al. (1977)'s explicit numerical scheme for standard Saint Venant equations.
212 In order to visualize the tails better, non-dimensional flow discharges (Q/Q_0) and non-
213 dimensional water depths (y/y_0), which were depicted in Figures 1a and 1b, are zoomed
214 over the [0.9-1.1] range and presented in Figures 2a and 2b, respectively. As presented in
215 Figures 2a and 2b, non-dimensional flow discharges and non-dimensional water depths
216 exhibit heavier tails as space and time fractional derivative powers decrease from 1.

217

218 Magnitudes and occurrence times of the peak non-dimensional flows (Q/Q_0) at the
219 downstream boundary for various values of the fractional space derivative power β and of
220 the fractional time derivative power α are tabulated in Table 1. Both the magnitude and
221 the occurrence time of the peak flow decrease as the time and space fractional derivative
222 powers decrease. The magnitude of the peak flow decreases from 2.05 to 1.82 and the
223 occurrence time of the peak flow decreases from 0.59 to 0.50 hr.

224

225 Non-dimensional flow discharges through longitudinal length x at various simulation times
226 ($t=20, 30, 40, 60, 75, 90, 120, 180$ minutes) are depicted in Figure 3 when space and time
227 fractional derivative powers $\beta = \alpha = 1, 0.9, 0.8, 0.7$. Figure 3 clearly shows that non-
228 dimensional flow discharges reached the equilibrium value of 1 from upstream boundary
229 to downstream boundary (from $x=0$ to $x=3.2187$ km) after the simulation time of 120
230 minutes when space and time fractional derivative powers are 1 ($\beta = \alpha = 1$). However,
231 when the simulation time is greater than 120 minutes, the non-dimensional flow discharges
232 deviate from the value of 1 toward the downstream boundary as space and time fractional



233 derivative powers decrease from 1. In other words, the influence of the flood hydrograph
234 that enters to the channel reach from the upstream boundary, is observed for a longer
235 duration in the downstream locations when the space and time fractional derivative powers
236 are smaller than 1. This finding also explains the heavier tails at the downstream boundary
237 when the fractional derivative powers are less than 1.

238

239 **Concluding remarks**

240

241 In this study, a numerical algorithm, first order accurate in time and second order accurate
242 in space, was proposed to solve time-space fractional governing equations of one-
243 dimensional unsteady/non-uniform open channel flow process (Kavvas and Ercan, 2016)
244 and to investigate its modeling capabilities that are different from the standard Saint Venant
245 equations. The fractional governing equations under consideration are generalizations of
246 the well-known Saint Venant equations written in the integer differentiation framework.
247 When orders (powers) of the fractional time and fractional space derivatives become one,
248 the proposed fractional governing equations of open channel flow process (Kavvas and
249 Ercan, 2016) reduce to standard Saint Venant equations and the proposed numerical
250 algorithm reduces to the explicit finite difference scheme reported in Viessman, et al.
251 (1977). The new governing equations in the fractional order differentiation framework
252 have the capability of modeling nonlocal flow processes both in time and in space by taking
253 the global relations into consideration (see Eqn. 4 and Eqn. 7).

254

255 The following conclusions can be drawn from the numerical investigation:



- 256 1. When the time and space fractional derivative powers become one, the proposed
257 numerical scheme for the time-space fractional governing equations of one-
258 dimensional unsteady/non-uniform open channel flow process give similar results
259 with the explicit finite difference scheme for standard Saint Venant equations
260 (Viessman, et al., 1977).
- 261 2. Non-dimensional flow discharges and non-dimensional water depths exhibit
262 heavier tails at the downstream boundary as space and time fractional derivative
263 powers decrease from 1.
- 264 3. Both the magnitude and the occurrence time of the peak flow decrease as the
265 powers of the time and space fractional derivatives decrease from 1.
- 266 4. The influence of the flood hydrograph that enters to the channel reach from the
267 upstream boundary, is observed for a longer duration in the downstream locations
268 when the space and time fractional derivative powers are smaller than 1. This
269 finding also explains the heavier tails at the downstream boundary when the
270 fractional derivative powers are less than 1.

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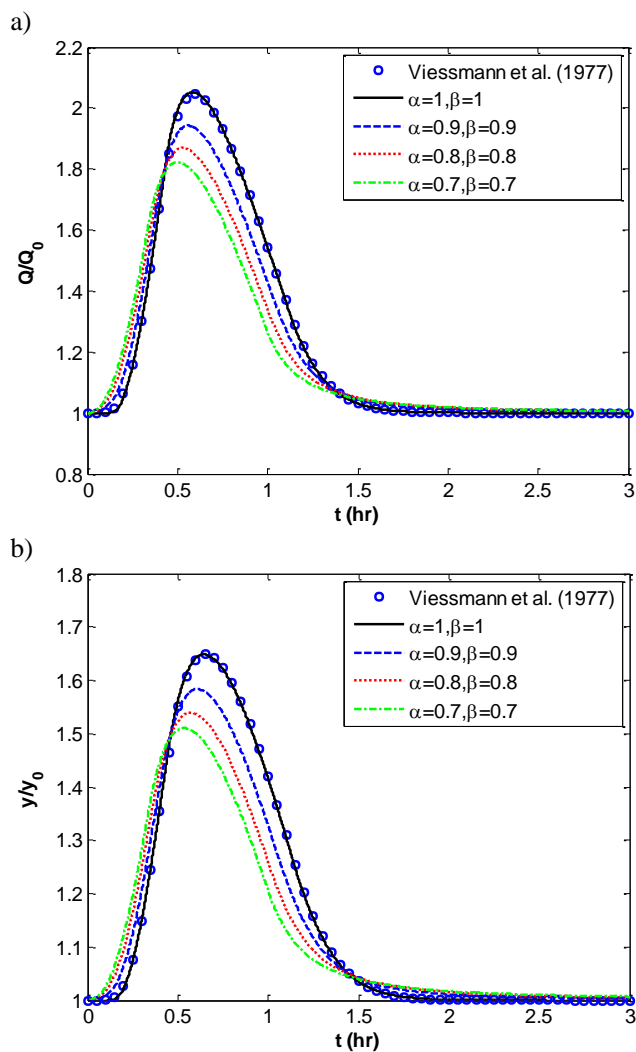


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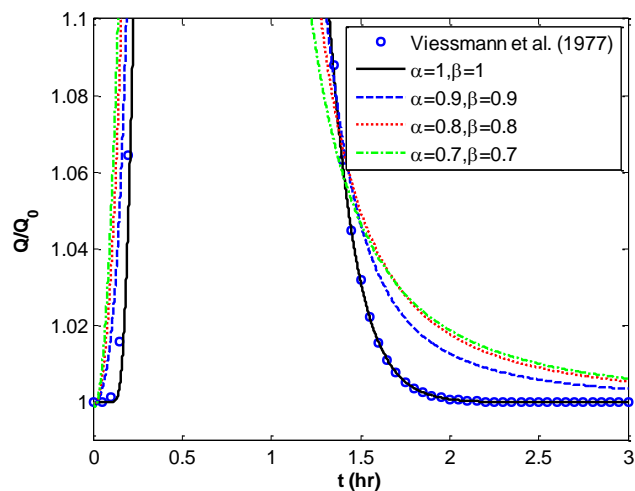
Table 1. Magnitudes and occurrence times of the peak non-dimensional flows (Q/Q_0) at the downstream boundary for various fractional space derivative power β and fractional time derivative power α

α	β	peak Q/Q_0	time of peak Q/Q_0 (hr)
$\alpha = \beta$			
1	1	2.05	0.59
0.9	0.9	1.94	0.56
0.8	0.8	1.87	0.53
0.7	0.7	1.82	0.50

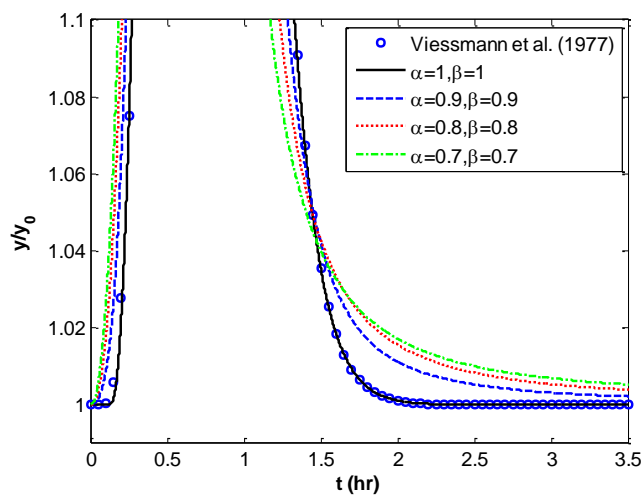
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420 **Figure 1.** a) Non-dimensional flow discharges, b) non-dimensional water depths through
421 time at the downstream boundary when space and time fractional derivative powers
422 $\beta = \alpha = 1, 0.9, 0.8, 0.7$



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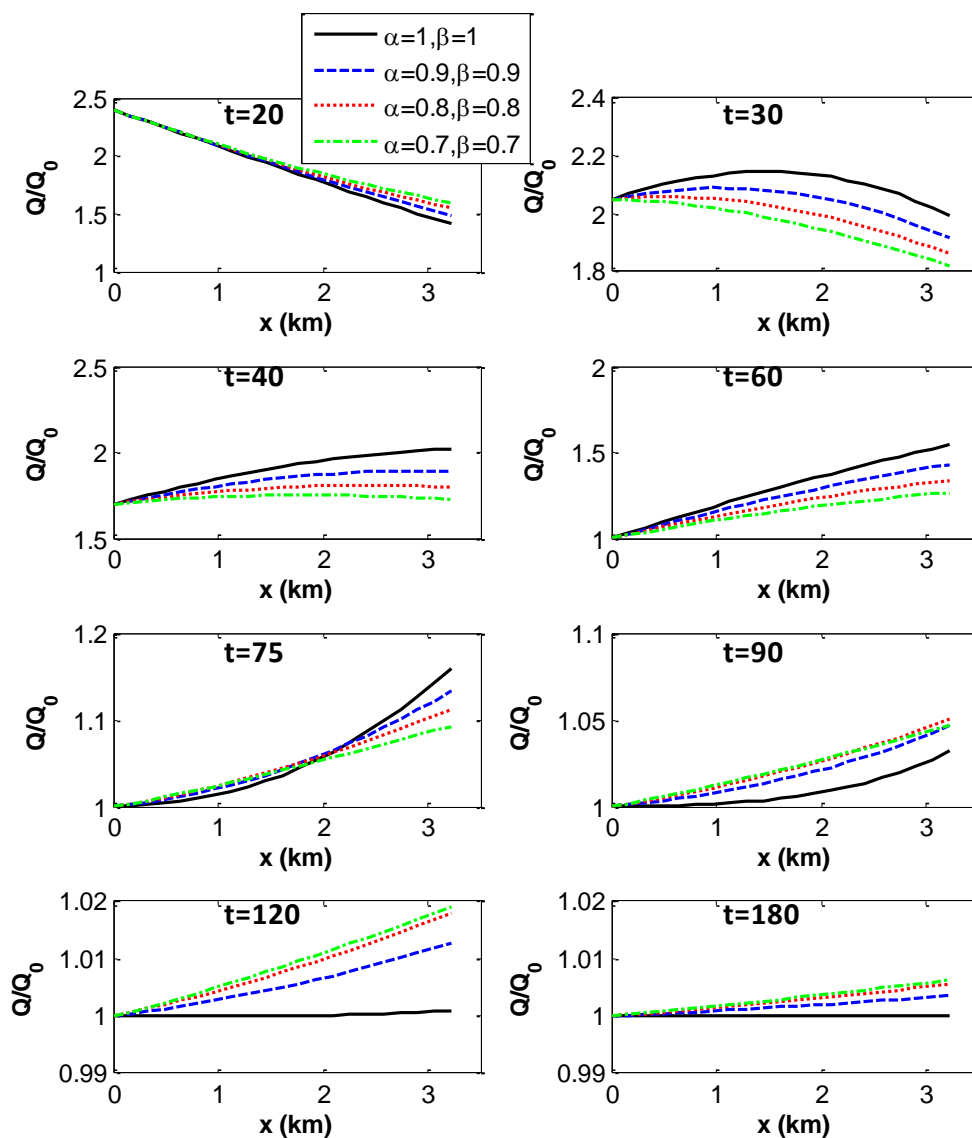
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Figure 2. **a)** Non-dimensional flow discharges (zoomed to 0.9-1.1 range), **b)** non-dimensional water depths (zoomed over 0.9-1.1 range) through time at the downstream boundary when space and time fractional derivative powers are $\beta = \alpha = 1, 0.9, 0.8, 0.7$



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Figure 3. Non-dimensional flow discharges through longitudinal length x at simulation times $t=20, 30, 40, 60, 75, 90, 120, 180$ minutes when space and time fractional derivative powers are $\beta = \alpha = 1, 0.9, 0.8, 0.7$