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On selection of the optimal data time interval for real-time hydrological forecasting

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Abstract

With the advancement in modern telemetry and communication technologies, hydrological data can be collected with an increasingly higher sampling rate. An important issue deserving attention from the hydrological community is what suitable time interval

- ⁵ of the model input data should be chosen in hydrological forecasting. Such a problem has long been recognised in the control engineering community but is a largely ignored topic in operational applications of hydrological forecasting. In this study, the intrinsic properties of rainfall-runoff data with different time intervals are first investigated from the perspectives of the sampling theorem and the information loss using
- the discrete wavelet decomposition tool. It is found that rainfall signals with very high sampling rates may not always improve the accuracy of rainfall-runoff modelling due to the catchment low-pass filtering effect. To further investigate the impact of data time interval in real-time forecasting, a real-time forecasting system is constructed by incorporating the Probability Distributed Model (PDM) with a real-time updating scheme,
- the autoregressive-moving average (ARMA) model. Case studies are then carried out on four UK catchments with different concentration times for real-time flow forecasting using data with different time intervals of 15 min, 30 min, 45 min, 60 min, 90 min and 120 min. A positive relation is found between the forecast lead time and the optimal choice of the data time interval, which is also highly dependent on the catchment con-
- ²⁰ centration time. Finally, based on the conclusions from the case studies, a hypothetical pattern is proposed in three-dimensional coordinates to describe the general impact of the data time interval and to provide implications on the selection of the optimal time interval in real-time hydrological forecasting. Although nowadays most operational hydrological systems still have low data sampling rates (daily or hourly), the trend in
- the future is that higher sampling rates will become widespread and there is an urgent need for both academic and practising hydrologists to realise the significance of the data time interval issue. It is important that more case studies in different catchments





with various hydrological forecasting models should be explored in the future to further verify and improve the proposed hypothetical pattern.

1 Introduction

Hydrological forecasting has always been a dominant and challenging field in operational hydrology. Owing to the spatial and temporal variability of catchment characteristics and rainfall patterns, together with a number of associated hydrological components which are highly nonlinear, time-dependent and spatially varying (Cluckie and Han, 2000; Tokar and Markus, 2000), the rainfall-runoff transformation is always a complex hydrological process for modelling and there still exist inevitably various uncertainties in the hydrological forecasting (Mantovan and Todini, 2006; Han et al., 2007). In

- ties in the hydrological forecasting (Mantovan and Todini, 2006; Han et al., 2007). In the last decade, increased scientific interests have been shown in the topics of the real-time updating schemes and data assimilation methods (Refsgaard, 1997; Madsen and Skotner, 2005; Moradkhani et al., 2005; Weerts and El Serafy, 2006; Komma et al., 2007; Clark et al., 2008), the probabilistic forecasting with either physical or data-driven
- ¹⁵ models (Freer et al., 1996; Krzysztofowicz, 1999, 2002; Tamea et al., 2005; Mantovan and Todini, 2006; Chen and Yu, 2007), as well as the numerical weather prediction (NWP) which provides precipitation forecasts as the input of the forecasting model and allows for an extension of the forecast lead time (Cloke and Pappenberger, 2009; Wood and Schaake, 2008; Lin et al., 2002, 2006, 2010). However, no matter how advanced
- these methods are and how much they can improve the forecasting results, they all depend on a reliable hydrological forecasting model, which normally consists of a hydrological model (either lumped, distributed or semi-distributed) together with a real-time updating scheme. When constructing the forecasting model, there is an important issue that cannot be avoided, i.e. the selection of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of the model input state (a sthe with a transition of the time interval of
- ²⁵ data (e.g. the rainfall, streamflow and evaporation, etc.) used to drive the model, which is, however, mostly ignored by the hydrological community in operational applications.





First of all, a distinction should be made between the sampling interval of the hydrological measurements and the time interval of the input data for the hydrological forecasting model. A sampling interval is determined by the instruments (e.g. the rain gauge and the flow gauge) and could be as frequent as the instrument can afford;
⁵ while the time interval of the model input data mentioned in this study refers to the time interval of the hydrological data (e.g. rainfall and streamflow) used to construct the forecasting model, or in other words, it can be comprehended as the time interval" thereafter to refer to the interval of the model input data and use "sampling interval" to describe the raw hydrological measurements.

Traditionally, hydrological measurements have been manually carried out with very low sampling rates (e.g. monthly, weekly and daily). However, modern telemetry systems have been developed to increase the hydrological sampling rate to hourly, minutely or even in seconds (e.g. weather radar is able to measure rainfall once every one minute and optical rain gauge can do it in seconds). One burning question

- ¹⁵ ery one minute and optical rain gauge can do it in seconds). One burning question for hydrologists would be how to select the optimal time interval in the hydrological forecasting. If the modern telemetry system keeps advancing in its current pace, will our hydrological forecasting model be able to cope with this "data rich" environment? It is interesting to note such a problem has already concerned modern control engi-
- neers. Unlike the "slow" sampling rate in hydrology, control engineers need to deal with very fast sampling, e.g. hundreds or even thousands of samples per second in rocket trajectory control. In the work of Åström (1969), a simple Gauss-Markov process was analysed using a parametric model, with the parameters completely describing the stochastic process. It was found that there was an optimal choice of the time interval
- and that the variance of parameter estimates would increase rapidly when the time interval increased or decreased from the optimal value. This is the first time the "optimal time interval" has been proposed with regard to the data used for model construction. Later on, Ljung (1987, 1999) pointed out that data with too large intervals would bear little information about the dynamics of the sampled signal; while too fast sampling would





involve more measurement noise and lead to numerical problems in a model, as the model could only fit in high-frequency bands with poor performances for extra work. It was further proposed by Ljung that the optimal choices of the time interval would lie in the range of the time constant of the system, which measures how quickly the system responses. However, the system time constant is not exactly known for highly nonlinear systems, but overestimating it might lead to a dramatic increase in the variance of the model parameter estimates.

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In the past decade, this issue begins to gain attention from the academic hydrologists. A general consensus has been reached that the parameters, simulation results and process representations of the hydrological models are inherently and strongly time-step dependent (e.g. Duan et al., 2006; Merz et al., 2009, 2010). More than a decade ago, Schaake et al. (1996) developed a simple water balance model and tested its sensibility for operating at time steps different from what it was calibrated at. It was recommended that to obtain the best performance, the model should be cali-

- ¹⁵ brated at the same time step as the one used for operation. Following this, a number of studies have been carried out on the time-step dependency of the hydrological model parameters (Finnerty et al., 1997; Tang et al., 2007; Littlewood and Croke, 2008; Wang et al., 2009; Cho et al., 2009; Kavetski et al., 2011), for its implications in regionalisation at ungauged catchments or climate impact analysis, etc. However, the impact of the
- ²⁰ model time step, or using the equivalent expression in this study, the time interval of the model input data, on the inference of the catchment structure, model parameters, and more generally the catchment behaviour remains poorly understood (Kavetski et al., 2011). Further, in operational applications, people care more about the improvement of the model accuracy and the appropriate use of the observational data, rather than
- reducing the time dependency of the model parameters. Albeit the utilisation of hydrological observations at appropriately fine resolutions is advocated by Wagener et al. (2010), there still remains a lack of general guidance for hydrologists to easily cope with this time interval issue in operational applications. Moreover, most of the previous studies are focused on using the hydrological models for simulation. With respect to





the hydrological forecasting, this issue becomes more complicated by the involvement of another temporal concept, the forecast lead time. In such cases, a suitable choice of the time interval of the model input data is more important and deserves further considerations.

- In the area of hydrological forecasting, it has been firstly addressed in the work of Remesan et al. (2010), when the artificial neural network (ANN) is used for real-time flood forecasting, that there is an optimal time interval for the input data. It is found that the 30 min interval can produce more accurate forecast results than the 15 min, 60 min and 120 min intervals in the Brue catchment of the UK, and the significance
- ¹⁰ of the time interval impact on the forecasting accuracy is more prominent to longer lead times than shorter ones. The results are quite meaningful to data-driven models, the performances of which are highly time dependent and improper data inputs could easily lead to overfitting (a serious weakness associated with such models). However, a question might arise: will this "optimal time interval" still exist for forecasting made
- ¹⁵ by using the more widely applied conceptual rainfall-runoff models? The conceptual rainfall-runoff models encompass a broad spectrum of plausible descriptions of the physical rainfall-runoff processes, which are found to be both reliable and effective in various situations, especially for real-time hydrological forecasting (Bell et al., 2001). The purpose of this study is to explore the general impact of the data time interval on bydrological forecasting using the conceptual rainfall runoff models are not the study of the data time interval.
- ²⁰ on hydrological forecasting using the conceptual rainfall-runoff model and a real-time updating scheme.

The rest of the paper is organised as followed. In Sect. 2, the intrinsic properties of observed rainfall-runoff data with different sampling intervals are investigated from the perspective of the sampling theorem and the information loss using the wavelet tool.

Section 3 examines the impact of data time interval on the forecast accuracy through case studies. A real-time forecasting system is built up by incorporating the Probability Distributed Model (PDM) with a real-time updating scheme, the autoregressive-moving average (ARMA) model. Rainfall-runoff data from four UK catchments of different sizes with time intervals of 15 min, 30 min, 45 min, 60 min, 90 min and 120 min are used to





drive the forecasting system. Forecasts are then made using different time-interval data for the four catchments with the forecast lead time ranging from 1 to 12 h. Finally, based on the forecasting results from the case studies, a hypothetical pattern is proposed in Sect. 4 to describe the general pattern of the time interval effect and to provide some implications on the selection of the optimal time interval in real-time hydrological forecasting.

2 Observed rainfall-runoff data with different time intervals

2.1 Sampling methods for observed rainfall-runoff data

Sampling refers to the process of converting a signal (e.g. a function of continuous time or space) into a numerical sequence (a function of discrete time or space) (Shannon, 1949, 1998). The hydrological processes are continuous in the time domain. However, most of the observed hydrological measurements are only available at discrete time intervals. There are two methods by which a continuous time function can be represented in a discrete time domain. One is to use a sampling data function where the value of the continuous function Q(t) in the *j*th time interval Q_j is given simply by the instantaneous value of Q(t) at time $j\Delta t$:

$$Q_i = Q(t_i) = Q(j\Delta t)$$

The other way is to adopt a pulse data function, in which the value of the discrete time function Q_i is given by the area under the continuous function Q(t):

²⁰
$$Q_j = \int_{(j-1)\Delta t}^{j\Delta t} Q(t) dt$$

5

The two principal variables of interest in hydrology, streamflow and rainfall, are measured as sampled data series and pulse data series, respectively (Chow et al., 1988).



(1)

(2)



When the values of streamflow and rainfall are recorded by gauges at a given instant, the flow gauge value represents the flow rate at that instant (in dimension of (L^3/T)), while the rainfall gauge value is the accumulated depth of rainfall (in dimension of (L) standing for the volume of rainfall (L³)) which has occurred up to that instant.

- ⁵ For example, if a rain gauge measures rainfall every 30 min then at an instantaneous time of 08:00 a.m. LT its value of 15 mm represents the total rainfall accumulated from 07:30 a.m. to 08:00 a.m. On the other hand, $15 \text{ m}^3 \text{ s}^{-1}$ at 08:00 a.m. from a river gauge represents the instantaneous stream flow at 08:00 a.m. (neither the average flow from 07:30 a.m. to 08:00 a.m., nor the accumulated flow volume during that period). It should
- be clarified that here we are only talking about how the rainfall and flow data are collected at site. When forcing the rainfall into the rainfall-runoff model to produce the flow, the model output can be either sampled or pulse data series.

By representing a continuous signal using discrete measurements, the sampling process always results in some kind of information loss. Figure 1 shows the rainfall-runoff measurements with sampling intervals of 15 min, 30 min, 60 min and 120 min. It can be

- seen that as the sampling interval increases from 15 min to 120 min, the flow curve is less smooth and the shape of the columns representing the rainfall volume becomes more approximate. Slower sampling leads to subsets of the data sets produced by fast sampling, and hence is less informative (Ljung, 1991). However, from the theoreti-
- cal aspect of the signal reconstruction, downsampled data can also result in a perfect reconstruction of the original signal by choosing an appropriate interpolation method and more importantly, complying with the sufficient condition of the Nyquist-Shannon sampling theorem (Nyquist, 1928, 2002). The theorem, often known as the sampling theorem, provides a lower boundary of the sampling frequency thus an upper bound-
- ²⁵ ary of the sampling interval as a sufficient condition for a perfect reconstruction of the original signal:

 $f_{\rm s}>2B$

15

or equivalently:





$B < f_{\rm s}/2$

5

where f_s is the sampling frequency and *B* is the one-sided baseband bandwidth of the band-limited original signal. $f_s/2$ is defined as the Nyquist frequency, which is a property of the sampled system. If the condition is not satisfied, the part of information of the original signal with frequencies beyond the Nyquist interval $[-f_s/2, f_s/2]$ will be lost

- during sampling, and the spectral density inside the interval can be distorted in the process of signal reconstruction, which will lead to the phenomenon of aliasing (Mitchell et al., 1988). On the other hand, if the frequency of the downsampled data is higher than twice of the bandwidth of the original signal, the information loss can be neglected and the original signal can also be successfully reconstructed. This has, at least from
- and the original signal can also be successfully reconstructed. This has, at least from the theoretical aspect of the signal reconstruction, refuted the intuition of many modellers and demonstrated that choosing a relatively larger time interval will not always deteriorate the modelling results.

2.2 Spectral analysis for observed data with different time intervals

In order to further investigate the information content of the observed rainfall-runoff data with different sampling intervals, the discrete wavelet transform (DWT) is applied to investigate the energy distribution of the observed rainfall-runoff data in different frequency domains. DWT is a powerful mathematical tool for the spectral analysis of discrete signals, which is more efficient than the Fourier transform in studying nonstationary time series (Meyer, 1993; Polikar, 1999). A most popular and efficient way to implement DWT is the Mallat decomposition algorithm (Mallat, 1989), the process of

The decomposition level *j* is associated with a frequency band ΔF calculated based on the sampling frequency f_s :

 $2^{5} \quad 2^{-j-1}f_{\rm s} \le \Delta F \le 2^{-j}f_{\rm s}$

which is illustrated in Fig. 2.

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(4)

(5)



The original signal is first decomposed into an approximation and an accompanying detail. The detail contains the high-frequency components of the signal within the frequency band ΔF while the approximation represents the low-frequency components below the band. Table 1 gives the corresponding frequency bands of the six wavelet decomposition levels for a 15 min data series, obtained by using Eq. (5). The decom-

- position process is iterated, with successive approximations being decomposed in turn so that the original signal is broken down into many lower-resolution components. In this study, the decomposition is carried out by decomposing one-year observed rainfallrunoff data into six decomposition levels using the Daubechies wavelet of order 10, 12
- and 20 (Daubechies, 1990; Labat et al., 2000, 2004). Since we are only interested in the general frequency profile instead of the frequency distribution details, the six wavelet decomposition levels are sufficient for this purpose. The observed rainfall-runoff data are first obtained with a sampling interval of 15 min, and then downsampled to 30 min, 45 min, 60 min, 90 min and 120 min data series according to different sampling methods are prior for the sampling methods.
- of rainfall and streamflow. The decomposition results are shown in Table 2. Since the results from the Daubechies wavelet of order 10, 12 and 20 have very similar patterns, only those from the Daubechies wavelet of order 20 are presented.

The energies shown in Table 2 can be interpreted as the magnitudes of information content of the one-year data in different frequency bands. For the flow, the majority of energy is distributed in the lower bands, with little energy in the higher bands of

- ²⁰ of energy is distributed in the lower bands, with little energy in the higher bands of level 1 to level 4. As for the rainfall, the energy distribution is relatively balanced, with considerable amounts in all frequency bands. It has been pointed out by some studies (Bras, 1979; Bras and Rodriguez-Iturbe, 1976; Storm, 1989) that the catchment behaves like a low-pass filter to the climatic input data, e.g. rainfall and evapotran-
- ²⁵ spiration, by absorbing their subtle time variability. To further investigate the energy variance in a certain frequency band caused by the flow and rainfall data with different time intervals, it can be noticed that the variances for the flow series are not obvious, considering the relatively large amounts of the total energies; while with respect to the rainfall, the variances are more outstanding, which are on an increasing trend





from the approximation to lower decomposition levels. In the low frequency band of (0.35×10^{-6}) Hz (approximation + level 6 + level 5), where most energy of the flow data is distributed, the energy variance of the rainfall series is less obvious compared to that in higher frequency bands. Moreover, the energies of approximations are exactly the same for all the rainfall series. The difference of energy distribution for the flow and

the same for all the rainfall series. The difference of energy distribution for the flow and rainfall data with different intervals might be caused by the intrinsic characteristics of the two different hydrological processes, and also the different sampling methods.

Similar to the low-pass filtering function of the catchment, the high-frequency variances of the rainfall inputs can be absorbed by the soil moisture reservoirs in the

- rainfall-runoff model (Oudin et al., 2004). As a consequence, the information content of the rainfall input in the higher frequency bands, which can show large variances with regard to a different time interval, is not likely to be transformed into the simulated flow through the rainfall-runoff model. As discussed above, since the energy variances of the rainfall data in low frequency bands are not obvious, the transformed flow will not
- ¹⁵ have much difference when using rainfall data with different intervals as the input of the rainfall-runoff model. This indicates that the increased sampling rate for the rainfall data may not necessarily improve the performance of the rainfall-runoff model. This has been verified by many studies, e.g. Schaake et al. (1996) found that using 6-h, 12-h, 1-day, 2-day and 4-day rainfall data could generate similar simulation results of flow as
- ²⁰ long as the model was calibrated and operated at the same time intervals. However, this conclusion may be only true for pure simulation using the rainfall-runoff model. The energy distribution from the wavelet analysis is not enough to provide a general pattern about the impact of time interval on real-time forecasting, where the existence of the real-time updating scheme involves the historical flow data as another system
- input together with the rainfall. In the following section, the impact of data time interval in real-time forecasting is trying to be explored through case studies by constructing a real-time forecasting system and applying it to four UK catchments of different sizes.





3 Case studies

3.1 A real-time hydrological forecasting system

The real-time forecasting system in this study consists of a conceptual rainfall-runoff model, the Probability Distributed Model (PDM) and a commonly used updating scheme for real-time error correction, the autoregressive-moving average (ARMA) model.

3.1.1 Rainfall-runoff model

The PDM (Probability Distributed Model) (Moore, 1985) is a lumped conceptual rainfall-runoff model which has been widely applied in various catchments in the UK and
 ¹⁰ abroad. It could be viewed as a representative of the conceptual saturation-excess models used for the runoff simulation in humid and semi-humid regions. The PDM model is developed based on the scheme of the Xinanjiang model with a soil moisture storage capacity that varies over the catchment and is described by a simple probability distribution curve. Inputs to the model are the rainfall and the potential evaporation. Actual evaporation depletes the soil moisture storage, the rate of which depends

- on the soil moisture deficit and the potential evaporation. Further loss as recharge to the groundwater is defined by assuming that the rate of draining depends linearly on the current soil moisture conditions. The groundwater recharge is then routed through a "slow response system" which can be best represented by a cubic form of a nonlinear
- storage model (Dooge, 1973). The direct flow, defined as the difference between the soil moisture storage at the beginning and the end of a time interval, is routed through "a fast response system" which is often described by a cascade of two linear reservoirs (O'Connor, 1982). Further details of the model equations are presented by Moore (2007). Figure 3 shows the conceptual structure of the PDM model. Table 3 lists the 13 parameters to be calibrated in the model.





3.1.2 Real-time updating scheme

Error prediction is now a well established technique for forecast updating in real time (Box and Jenkins, 1970; Moore, 1982). The real-time updating scheme used in this study is wholly external to the deterministic model operation thus can be easily ap-

- ⁵ plied in combination with any kind of rainfall-runoff models. A feature of errors from a conceptual rainfall-runoff model is that there is a tendency for errors to persist so that sequences of positive errors (underestimation) or negative errors (overestimation) are common (Moore, 2007). This dependent structure in the error sequence may be exploited by developing an error predictor which incorporates the error structure and
- ¹⁰ allows future errors to be predicted. In this updating scheme, the structure of errors is analysed and the predictions of future errors are added to the deterministic model prediction to obtain the updated and improved forecasts of flow. With q_{t+l} representing the modelling result of the observed flow Q_{t+l} at some time t + l, directly obtained from the PDM model without incorporating the observed flow data, the error η_{t+l} is defined
- as $Q_{t+l} q_{t+l}$. Let $\eta_{t+l|t}$ denote a prediction of the error η_{t+l} , made *l* steps ahead from a forecast origin at time *t* using an error predictor. Then a real-time forecast, $q_{t+l|t}$, can be expressed as the sum of the predicted error and the original modelling result:

 $q_{t+/|t} = q_{t+/} + \eta_{t+/|t}$

Among various forms of error predictors, the autoregressive-moving average (ARMA) ²⁰ model is considered to be most appropriate and parsimonious (Moore, 2007). The equations of the error predictions $\eta_{t+/|t}$ expressed by the ARMA model can be written as follows:

$$\begin{split} \eta_{t+/|t} &= -\phi_1 \eta_{t+/-1|t} - \phi_2 \eta_{t+/-2|t} - \dots - \phi_p \eta_{t+/-p|t} + \theta_1 a_{t+/-1|t} + \theta_2 a_{t+/-2|t} \\ &+ \dots + \theta_q a_{t+/-q|t}, \qquad l = 1, 2, \dots \end{split}$$



(6)

(7)



25

where $\phi_1, \phi_2, ..., \phi_p$ and $\theta_1, \theta_2, ..., \theta_q$ are autoregressive and moving average parameters, respectively with

$$a_{t+l-i|t} = \begin{cases} 0 & l-i > 0 \\ a_{t+l-i} & \text{otherwise} \end{cases}$$

and a_{t+l-i} is the one-step ahead prediction error defined as:

5
$$a_{t+i} \equiv a_{t+i} = a_{t+i} = \eta_{t+i-1} = \eta_{t+i} - \eta_{t+i} = Q_{t+i-1} = Q_{t+i-1} - q_{t+i-1}$$

and

$$\eta_{t+1-i|t} = \eta_{t+1-i} = Q_{t+1-i} - q_{t+1-i}$$
 for $1 - i \le 0$

- ¹⁰ Equation (7) together with the related Eqs. (8)–(10) is used recursively to produce the error predictions of $\eta_{t+1|t}, \eta_{t+2|t}, ..., \eta_{t+/|t}$, from the available values of $a_t, a_{t-1}, ...$ and $\eta_t, \eta_{t-1}, ...$ Using this error prediction methodology, the PDM model original modelling results, $q_{t+/}$, can be updated using the error prediction $\eta_{t+/|t}$, to calculate the required real-time forecast, $q_{t+/|t}$, according to Eq. (6).
- As for the number of parameters in the ARMA structure, i.e. $\phi_1, \phi_2, ..., \phi_p$ and $\theta_1, \theta_2, ..., \theta_p$ in Eq. (7), a third order autoregressive with dependence on three past model errors has been proved to be an appropriate choice for UK conditions (Moore, 2007). Thus the ARMA structure containing three autoregressive parameters and one moving average parameters (with p = 3 and q = 1) is chosen as the updating scheme
- ²⁰ in this study. It should be noted that for the forecasts made from an origin *t*, by calculating the error predictor $\eta_{t+l|t}$, the real-time observations of flow are assimilated into the forecasting results. For instance, with the structure of ARMA (3, 1), the observed flows at *t*, *t* – 1 and *t* – 2 are involved in the calculation of the error predictor $\eta_{t+l|t}$, which are then added to the original model prediction q_{t+l} to derive the updated result of $q_{t+l|t}$
- ²⁵ according to Eq. (6). For the obtaining of $q_{t+/}$, we assume the perfect knowledge of the future rainfall and potential evaporation, i.e. the observed catchment average rainfall and the MOSES potential evaporation are used as the model inputs after the origin *t*.



(8)

(9)

(10)



An automatic calibration procedure utilising an efficient population based evolutionary optimisation technique, i.e. the Particle Swarm Optimisation (PSO) algorithm (Eberhart and Kennedy, 1995, 2001), is adopted to estimate the 4 error-prediction parameters of the ARMA model and the 13 parameters of the PDM model.

5 3.2 Study catchments and experiment design

Four catchments are selected from southwest England, which are Bellever, Halsewater, Brue and Bishop_Hull. They have different sizes of the catchment area, varying from 20 to 200 km², as shown in Fig. 4. Except for the Bellever catchment which is in the Devon area with a maximum altitude of 604 m above the sea level, the other three catchments are located in the area of North Wessex, with an average altitude of 119 m. All the catchments are predominantly rural areas with the main land-use types being the moorland, low grade agriculture or wood land. Catchment descriptors are obtained from the Flood Estimation Handbook (FEH) (Bayliss, 1999) produced by the Centre of Ecology and Hydrology (CEH) in the UK. Meanings of the descriptors are explained in Table 4 and values of the respective descriptors for the four catchments are listed in Table 5. It can be seen from Table 5 that the average annual rainfall (SAAR) is 2095 mm for the Bellever catchment with the percentage runoff (SPRHOST) being 47.5%, while the other three catchments have less rainfall (about 850 ~ 1000 mm per year) and slightly lower percentage runoff, i.e. 30.6%, 36.4% and 32.9%. From the descriptors of the catchment size and configuration, it can be noticed that the increase 20 of the catchment area (AREA) corresponds to an increase of LDP and DPLBAR representing the longest and average length of the drainage path, which thus suggests an

 increasing travel time of the streamflow before it routes to the catchment outlet. Seven years' rainfall-runoff data are collected from the four catchments with a sam pling interval of 15 min. The period is from October 1998 to September 2005 for Bellever, Halsewater, and Bishop_Hull. Data from the HYREX (Hydrological Radar Experiment) project funded by the NERC (Natural Environment Research Council) are used for the Brue catchment from September 1993 to May 2000. All the data are





downsampled into other sequences with time intervals of 30 min, 45 min, 60 min, 90 min and 120 min. Daily potential evaporation data are obtained from the MOSES (Met Office Surface Exchange Scheme) and then disaggregated into the same time steps as the rainfall.

- ⁵ For each catchment, one-year data are selected for the validation of the calibrated parameters of the rainfall-runoff model and the real-time updating scheme. Another one-year is used for independent evaluation of the model performance (i.e. the forecast accuracy). The rest data of nearly five years are used for calibration. It is widely accepted that the information quality of the calibration data is of more importance in desiding the performance of the calibrated model, rather than the data length (Curte
- deciding the performance of the calibrated model, rather than the data length (Gupta and Sorooshian, 1985a,b). According to the conclusions of Liu and Han (2010), a calibration data set of 12 months contains sufficient information of hydrological variability to result in a reliable and stable model in the Brue catchment. In order to reduce the burden of the calculation work and improve the efficiency of data utilisation, in this
- study the most appropriate one-year data are selected from the calibration data sets for calibration using an effective selection index named the Information Cost Function (ICF). More detailed information of the ICF index can be found in the work of Liu and Han (2010).

The 5-yr calibration data are first split into a group of calibration scenarios with the fixed length of 12 months, using a moving-window of one month. As a result, up to 50 calibration scenarios are resulted for each catchment. With the one-year validation data determined beforehand, the ICF index is used to select the most appropriate 10 calibration scenarios with sufficient hydrological information for calibration. Since the ICF index can only identify the relatively better calibration scenarios rather than the absolutely best one, the 10 scenarios initially selected by ICF are used to carry out the calibration procedure. The best three calibrated models which have the best

performances on the validation data are chosen to perform the real-time forecasting $1 \sim 12$ h ahead using the testing data, an independent 1-yr dataset of the calibration and validation data. Finally, the forecasting performances of the best three models are





averaged. This is to present more stable results and in that way the uncertainty of calibration data can be involved in the final results which are unavoidable in practice.

It should be mentioned that the whole process described above is carried out for all the four catchments and repeated using data with different time intervals of 15 min,

⁵ 30 min, 45 min, 60 min, 90 min and 120 min. That is to say, for each data sequence with a certain time interval, the calibration and validation procedures are carried out to construct a forecasting system that is suitable to perform with future data of the same time interval, and real-time forecasting is made with the constructed system functioning at the same time step.

3.3 Relation between the optimal data time interval and the forecast lead time

Analyses and comparisons are based on the forecasting results (i.e. performances of the forecasting system on the one-year testing data) with lead times of $1 \sim 6$, 9 and 12 h. The lead steps of the forecasting system constructed from data with different time intervals are shown in Table 6. It can be noticed that for some forecast lead times such as 1, 2, 3, 4, 5, 9 h, these are no integers for the time intervals of 45 min, 90 min and 120 min. Therefore, forecasts are not made for such lead times by the forecasting systems constructed from the 45 min, 90 min and 120 min data.

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The forecasting results for the four catchments are shown in Table 7, evaluated by the root mean square error (RMSE). Example hydrographs resulted from the best calibra-

- tion scenario for the 4h-ahead forecasts using the 30 min data are shown in Fig. 5. By examining each row of Table 7, it can be seen that for a forecasting system built on data with a certain time interval, the RMSE value increases as the increase of the forecast lead time. This trend is more obviously in Fig. 6 shown by the slopes of curves for the Nash-Sutcliffe efficiency (NSE) statistics (Nash and Sutcliffe, 1977). For each catch-
- ment in the subfigure of Fig. 6, all the six curves revealing the relationship between the performance of the forecasting system and the forecast lead time are on decreasing trends. Moreover, when comparing the differences between the six curves, it can be found as the lead time increases, the distance of the curves becomes increasingly





larger and finally the curves are clearly distinct from each other. This means that when the lead time is small, e.g. from 1 to 6 h, the variance of the forecasts resulted from data with different time intervals is also subtle; while as the increase of the lead time, e.g. when exceeding 6 h, the variance becomes more and more significant. This proves that the choice of the time interval does have a considerable impact on the forecast-

ing results, which is even more prominent with longer forecast lead times than shorter ones.

5

The lowest RMSE values for the forecasts made with a certain lead time are highlighted in Table 7 to show the optimal choice of the time interval for a certain lead time forecast. It can be seen that there is an increase of the optimal time interval for all four catchments when the lead time increases from 1 to 12 h. To further illustrate this, the rankings of the time intervals according to the RMSE values are listed in Table 8. An interesting phenomenon is revealed by the rankings, i.e. the optimal time interval is replaced gradually by longer ones as the increase of the forecast lead time. Taking the

- ¹⁵ Brue catchment for example, the optimal intervals is 15 min for 1 h to 3 h-ahead forecasts, while it is replaced by 30 min and 60 min for forecasting made with lead times of 4 and 5 h; later the 90 min interval replaces 60 min to be the best one when the lead time is longer than 6 h. Moreover, it should be pointed out that for the 15 min interval, although it is the optimal choice for the 1 h, 2 h and 3 h-ahead forecasting, it appears to
- ²⁰ be at the bottom of the ranking when the lead time is 12 h. This again indicates the importance of selecting the appropriate time interval in real-time forecasting, rather than simply build the model using data as what they are originally measured.

To make the patterns shown by Table 7 more obvious, the forecasting results are plotted in three-dimensional coordinates for the four catchments, as shown in Fig. 7.

The x-axis stands for the data time interval (15 min, 30 min, 45 min, 60 min, 90 min and 120 min); the y-axis represents the eight forecast lead times (1, 2, 3, 4, 5, 6, 9, 12 h); and the values on the vertical axis z show the forecasting results in RMSE. In each subfigure, each of the eight suspended curves indicates the variance of the forecast accuracy with respect to different time intervals for forecasts made with a certain lead





time. The lowest points of the eight curves (representing the optimal time intervals which result in the least forecasting errors) are projected onto the X-Y plane and then connected together. The projection curve (in blue) thus reveals the relationship between the optimal time interval and the forecast lead time. It can be seen that all the

- four projection curves for the four catchments are on increasing trends, which indicates the increase of the optimal time interval with the increase of the forecast lead time. This is consistent with the previous conclusions made by examining the rankings in Table 8. However, besides the positive relation between the optimal time interval and the forecast lead time, it can also be noted that the increasing patterns of the projection our reason with different for the four establements. The reason of this uprises increasing
- 10 curves are quite different for the four catchments. The reason of this various increasing pattern will be fully discussed in the next section.

3.4 Implication of the catchment concentration time

By examining the increasing pattern of the projection curves in Fig. 7, it is interesting to note that the sharpest curve is generated by the catchment of Bishop_Hull in Fig. 7d, which has the largest drainage area of 202.0 km^2 with the largest LDP (longest

- ¹⁵ Fig. 7d, which has the largest drainage area of 202.0 km⁻ with the largest LDP (longest drainage path) value of 40.21 km (see Table 5). Further, when comparing the projection curves in Fig. 7a and c produced by Bellever and Brue, it can be found the two curves start at the same values of the optimal time interval (both at 15 min) when the lead time is within 2 h, and become stable after the lead time exceeds 6 h. However,
- the middle section of the curve in Fig. 7c, which rises to 90 min at the lead time of 6 h, is much steeper than that of the curve in Fig. 7a, which only increases to 45 min at the same lead time. This may also be explained by the concentration times of the two catchments. From Table 5, it can be seen that Brue has a larger area of 135.2 km² with higher indices of LDP and DPLBAR suggesting a longer concentration time compared
- to Bellever, which has an area of only 21.5 km². A further comparison of DPSBAR which reflects the average steepness of the catchment can also lead to the same conclusion. For the catchment of Brue, DPSBAR shows a lower value representing a lower catchment steepness, which thus indicates a longer concentration time compared to





Bellever. All these facts imply that a longer concentration time might result in a sharper increase of the projection curve; while on the other hand, a flatter curve might be resulted from a catchment with a quicker response.

FEH provides a simple method to calculate the catchment concentration time using a generalised model of the catchment descriptors derived by regression analysis (Houghton-Carr, 1999), as shown by Eq. (11):

 $T_{\rm p} = 4.270 \times \text{DPSBAR}^{-0.35} \times \text{PROPWET}^{-0.80} \times \text{DPLBAR}^{0.54} \times (1 + \text{URBEXT})^{-5.77}$ (11)

where *T*_p stands for the time-to-peak of the instantaneous unit hydrograph. The advantage of this equation is that it is theoretically independent of the time interval, which
enables an independent evaluation of catchment concentration time other than those normally derived by using rainfall-runoff data sampled with a certain time interval (Littlewood and Croke, 2008). The calculated results of the four catchments are 4.36, 6.81, 8.37 and 8.82 h, respectively for Bellever, Halsewater, Brue and Bishop_Hull. This is in agreement with the above conclusion made by simply examining the values of the catchment descriptors of LDP, DPLBAR and DPSBAR. It should be mentioned that results from the Eq. (11) also can only provide a provisional comparison of the concentration times, which may not be treated as the realistic response times of the catchment (Houghton-Carr, 1999).

By a further check of the correlations between the concentration times and the in-²⁰ creasing patterns of the projection curves in Fig. 7, it can be noticed that the projection curve in Fig. 7b for the Halsewater catchment seems to be much flatter than the one in Fig. 7a produced by Bellever, although Halsewater has a larger catchment area together with larger values of LDP, DPLBAR and *T*_p, and a lower average steepness (DPSBAR), compared to Bellever. Nevertheless, this might be explained to some ex-²⁵ tent by another index, ASPVAR (see Tables 4 and 5), which reveals the invariability of the slope directions in every grid of the catchment. Halsewater has the largest ASP-





VAR value among the four catchments, which indicates the highest consistency of the

directions of all catchment grids and thus might result in a better concentration of the surface and underground flow.

All the above analyses indicate that the concentration time might play a considerable role in influencing the selection of the optimal time interval when the forecast lead time is determined. It is known that a steeper, naturally wetter and more urbanised catch-5 ment tends to have a faster response; whilst the larger and longer the catchment is, the slower the response will be. However, besides the descriptors presented in Table 4 and used in Eq. (11), the concentration time is also affected by many other factors (Akan, 1989), e.g. the density of the watercourse, the consistency of the flow directions, the soil infiltration conditions, the rainfall intensity and the storm path, etc. As 10 a consequence, although it can be deduced from the above analyses that the longer the concentration time is, the steeper the projection curve tends to be, the various influencing factors make it difficult to figure out how exactly the selection of the optimal time interval is affected by the concentration time. And it is far too early to say that the concentration time is definitely the principal factor determining the increasing pattern 15 of the optimal time interval with respect to the increase of the forecast lead time. More research with various catchments bearing different response characteristics is needed to explore the underlying factors and their functions in determining the optimal time

interval.

20 4 Discussion: hypothetical pattern for the selection of the optimal data time interval

Based on the analyses of the forecasting results in the case studies, it is interesting to note that the conclusions from the four catchments are consistent with the findings in modern control engineering as mentioned in the Introduction part, i.e. the best fore-

casts with a certain lead time are not always produced by the finest time interval or the largest one. Conversely, in hydrological forecasting, the optimal choice of the time interval is found to be increased with the extension of the forecast lead time. Following





this, a generalised pattern for the selection of the optimal time interval in real-time hydrological forecasting can be proposed, as shown in Fig. 8, in similar three-dimensional coordinates as that in Fig. 7.

- In Fig. 8, the axes of X, Y and Z represent the time interval, the forecast lead time and the forecasting error in the three subfigures. Two U-shape curves are used to describe the relations between the forecasting error and the time interval in two cases when forecasts are made with a small forecast lead time and a long lead time, as shown, respectively in Fig. 8a and b. The lowest points of the two U-shape curves, (X_1, Z_1) and (X_N, Z_N) , thus represent the optimal choices of the time interval in the two cases. As concluded from the case studies, with the increase of the forecast lead time,
- the forecasting accuracy is decreasing and the optimal time interval is on an increase. Consequently, the two lowest points have the relations of $Z_1 < Z_N$ and $X_1 < X_N$. This trend is more obvious when the two curves are represented in the three-dimensional coordinates in Fig. 8c. A connection of the projections of the two lowest points on the
- $_{15}$ X-Y plane (i.e. the red dotted line) reveals a positive relation between the optimal time interval and the forecast lead time, which is, the longer the lead time is, the larger should the optimal time interval be. Although this projection curve is found to be positive by the case studies, the exact increasing pattern cannot be easily determined. The increasing rate can be either a constant or an accelerating/ decelerating value, or even
- ²⁰ a non-monotonic rate, which is found to be highly related to the characteristics of the catchment, such as the concentration time as discussed in the case studies.

It should be emphasised that this hypothetical pattern of the optimal time interval is especially proposed for real-time forecasting, rather than simulation with only the rainfall-runoff model. When making forecasts using either the data-driven model (e.g.

²⁵ ANN and TF model, etc.) or the physically-based rainfall-runoff model together with a real-time updating scheme, an extrapolation is made based on the historical data to the future. Too dense data will result in a worse extrapolation further into the future, while too sparse data can also make the extrapolation fail in very near future. This is why in substance the data time interval makes differences to the forecasting results.





On the other hand, as discussed by using the wavelet decomposition in Sect. 2.2, for pure simulations with only the rainfall-runoff model, the simulated flow may not vary too much when the model is driven by rainfall data with different time intervals. This is true to some extent due to the low-pass filtering function of the rainfall-runoff model,

- ⁵ which filtering out the high-frequency variances of the rainfall inputs with different time intervals. However, in real-time forecasting, the involvement of the flow data as another input of the modelling system by the updating scheme (e.g. the ARMA model) makes the case very different. This may to some extent explain why the optimal time interval exists for real-time forecasting but not in the case of pure simulation (at least for the commonly used time intervals as these exemined in this study). Nevertheless, it is
- commonly-used time intervals as those examined in this study). Nevertheless, it is believed that with an infinitely small or large time interval, the simulation results can also get deteriorated due to the involvement of measurement noises or the lack of an efficient representation of the original signals of rainfall.
- The forecasting results in the case studies are to some extent subject to the specific structure of the forecasting system (i.e. the PDM model integrated with the ARMA updating scheme) and the characteristics of the selected catchments. Therefore it is important that more case studies are explored by in different geographical and climatic regions with various forecasting systems, i.e. various combinations of the hydrological models and the real-time updating schemes. In that case the proposed hypothetical
- ²⁰ pattern can be further verified, improved or on the contrary refuted, e.g. is the proposed curve universal or only applicable to a certain types of catchments or forecasting systems? Besides these, another question that might be raised is when different error measurement statistics are used, will the hypothetical pattern remain the same? Hall (2001) addressed the error measurement issue and analysed 10 commonly used
- indices to evaluate the goodness-of-fit of a model to a set of observations, and it was found that not a single error measurement method was perfect. Here we chose the two square error based statistics, NSE and RMSE, in this study since they are the most widely used error measurements in hydrological forecasting. However, other error





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evaluation methods are worth trying, to testify whether the hypothetical pattern is limited to a certain type of error statistics or not.

5 Conclusions

- This paper explores the time interval of the model input data and its impact on the ⁵ hydrological forecasting system, consisted of a conceptual rainfall-runoff model and a real-time updating scheme. Modern telemetry system is able to measure and record hydrological variables with increasingly higher sampling rates, e.g. nowadays rainfall data can be collected once a second by the optical rain gauge. An important problem deserves attention from hydrologists would be what suitable time interval should be ¹⁰ used, i.e. should our hydrological forecasting system take in rainfall and flow data measured in seconds? Such a problem has long been recognised in control engineering
- (albeit mainly in linear systems), but is a largely ignored topic in operational hydrological forecasting area. In the beginning of this paper, discrete wavelet decomposition is used to examine the spectral variances of rainfall-runoff data with different time in-
- tervals in the frequency domain. It is found that the rainfall signal has energy spread more widely than the flow; but due to the low-pass filtering function of the rainfall-runoff model, the high-frequency variances of the rainfall signal with different time intervals are not likely to be transformed into the flow. This indicates that higher sampling rates may not always help improve the results of rainfall-runoff modelling. To further investi-
- gate the impact of time interval in real-time forecasting, which is more complicated by involving the flow data as the system inputs by the real-time updating scheme, case studies are carried out in four catchments with different sizes and concentration times. Main findings from the case studies can be concluded as: (1) the data time interval does have a considerable impact on the performance of the forecasting system, which
- is more prominent to longer lead times than shorter ones; (2) there exists an optimal time interval for forecasts made with a certain lead time, and the length of the optimal time interval is increasing as the increase of the forecast lead time; (3) the positive





relation between the optimal time interval and the forecast lead time can show various patterns, which is found to be highly related to the catchment concentration time; and (4) the longer the concentration time is, the more sharply the optimal time interval tends to increase as the increase of the forecast lead time. Finally, according to the results of the case studies, a hypothetical pattern is proposed in three-dimensional coordinates.

the case studies, a hypothetical pattern is proposed in three-dimensional coordinates for the selection of the optimal time interval in real-time hydrological forecasting.

It should be recognised that the data time interval issue addressed in this study has not yet been completely solved by the control engineers, albeit they have many decades of experience with this problem. According to Ljung (1999), it is impossible to deduce a mathematical expression for the identification of the optimal time interval for

- ¹⁰ deduce a mathematical expression for the identification of the optimal time interval for highly nonlinear systems. Only for very simple models, e.g. the Gauss-Markov process, the problem may be addressed by a deductive approach. Hydrological models together with the real-time updating schemes are highly nonlinear and diverse, which militate a deductive derivation and favour an inductive approach. Although nowadays most
- operational hydrological forecasting systems still have low data sampling rates (daily or hourly), the trend in the future is that higher sampling rates will become widespread and there is an urgent need for both academic and practising hydrologists to realise the significance of the time interval issue. The main purpose of this paper is to draw attentions of hydrologists to this problem at an early stage when they are dealing with
- the "data-rich environment", rather than providing a general mathematical formula in selecting the most appropriate data time interval. Therefore, the best way to identify the optimal time interval is to explore various forecasting models with different catchments and eventually a more general pattern applicable to a wide range of cases could be found.

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Table 1. Frequency bands of the wavelet decomposition levels for data with a sampling intervalof 15 min.

Level j	2 ^{-j-1}	2 ^{-j}	Sampling rate <i>f</i> _s (Hz)	Frequency band $\Delta F(\times 10^{-6} \text{ Hz})$
1	0.25	0.5	1/900s	[278, 556]
2	0.125	0.25	1/900s	[139, 278]
3	0.0625	0.125	1/900s	[69, 139]
4	0.03125	0.0625	1/900s	[35, 69]
5	0.015625	0.03125	1/900s	[17, 35]
6	0.007813	0.015625	1/900s	[9, 17]

Note: For a certain decomposition level of the wavelet analysis, the detail contains the components of the original signal within the relevant frequency band, while the approximation represents the components below the frequency band.

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Table 2. Energy distributions in different frequency bands for one-year rainfall-runoff observations with different sampling intervals of 15 min, 30 min, 45 min, 60 min, 90 min and 120 min.

Details						Total			
Frequ	ency band	Approx.	Level 6	Level 5	Level 4	Level 3	Level 2	Level 1	energy
(10 ⁻⁶	Hz)	[0, 9]	[9, 17]	[17, 35]	[35, 69]	[69, 139]	[139, 278]	[278, 566]	[0, 566]
Flow	15 min	356 196	18422	6848	543	39	3	1	382 052
	30 min	356 176	18375	6795	529	35	2	1	381 913
	45 min	356 115	18298	6705	504	29	2	1	381 654
	60 min	356 026	18 175	6573	471	22	2	2	381 271
	90 min	355 880	17892	6253	395	18	7	2	380 447
	120 min	355718	17 477	5804	311	35	6	2	379 353
Rain	15 min	112	56	71	80	86	78	43	526
	30 min	112	56	71	77	73	41	30	460
	45 min	112	56	70	71	57	33	16	415
	60 min	112	55	68	66	50	15	13	379
	90 min	112	55	63	50	29	8	10	327
	120 min	112	54	59	42	18	7	7	299

Note: The observed data are taken from the Brue catchment of the UK with a sampling interval of 15 min. Four-year rainfall-runoff data (19 September 1993–19 July 1997) are used to form 47 sets of one-year data with a moving window of one month. With the data collection methods of streamflow and rainfall described by Eqs. (1) and (2), each data set is downsampled into another five series with time intervals of 30 min, 45 min, 60 min, 90 min and 120 min. For a comparable analysis and a convenient calculation of the wavelet decomposition, extra data are added into the 30 min, 45 min, 60 min, 90 min and 120 min data series in order to make them have the same amount of data as the 15 min series, by either using a simple linear interpolation for the streamflow series or interpolating constant values for the rainfall. In that case, all the data series have the same sampling interval of 15 min, thus a sampling frequency of 1/900 Hz. The 47 pairs of data series of streamflow and rainfall with a certain time interval are used to perform the wavelet decomposition on 6 levels, which refer to the frequency bands of [278, 566] × 10⁻⁶ Hz, [139, 278] × 10⁻⁶ Hz, [69, 139] × 10⁻⁶ Hz, [35, 69] × 10⁻⁶ Hz, [17, 35] × 10⁻⁶ Hz and [9, 17] × 10⁻⁶ Hz from level 1 to level 6. Finally, the decomposition results are averaged for the 47 pairs of data series with a certain time interval and the energy values are calculated for each frequency band based on the wavelet coefficients.





Table 3. Para	ameters in th	ne PDM mode	l (Moore, 2007).	Discussion Paper Discus	HE 9, 10829– Optimal interval fo hydro forec	data time or real-time logical asting
Parameter	Unit	Suggested value	Description	sion	J. Liu ar	nd D. Han
f _c	none	1	Rainfall factor	Pap		
$ au_{d}$	h	0	Time delay	ber	Title	Page
c _{min} , c _{max}	mm	0	Minimum and maximum soil moisture store capacity			
b	none	0.5	Exponent of the soil moisture distribution	_	Abstract	Introduction
b _e	none	2.5	Exponent in the actual evaporation function		Conclusions	References
k _g	h mm ^{bg-1}	10 [°]	Groundwater recharge time constant	SCU	Conclusions	
b _g	none	1.5	Exponent of the groundwater recharge function	SS.	Tables	Figures
S _t	mm	0	Soil tension storage capacity in the recharge function	on		_
K_1, K_2	n , 2	1-20	lime constants of the surface routing	Pa	14	►L
k _b	h mm ⁻ 3 -1	5-100	I me constant of the groundwater storage routing	per		
q _c	m° s '	0	Constant flow representing returns/abstractions			•
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Table 4. Definitions of the FEH catchment descriptors (Bayliss, 1999).

Catchment descriptors	Unit	Definitions
AREA	km ²	Catchment area
ALBAR	m	Mean altitude of the catchment above the sea level
LDP	km	Longest drainage path, defined by recording the greatest distance from a catchment node (50 m gird) to the catchment outlet
DPLBAR	km	Mean drainage path length, calculated as the mean distances between each catchment node and the outlet
DPSBAR	m km ⁻¹	Mean drainage path slope, calculated as the mean of all the inter-nodal slopes which characterises the overall steepness of the catchment
ASPVAR	none	Invariability of the inter-nodal slope directions, where values near to zero indicate there is considerable variability in the aspect of catchment slopes. Values approaching one indicate that catchment slopes tend to face one particular direction.
SAAR	mm	Standard average annual rainfall (1961–1990)
QMED	m ³ s	Median annual maximum flood (1961–2008)
PROPWET	none	Proportion of time when SMD (Soil Moisture Deficit) was equal to or below 6 mm during the period 1961–1990
SPRHOST	%	Standard percentage runoff derived by using the HOST (Hydrology Of Soil Types) soil classification
URBEXT	none	Extent of urban and suburban land cover (1990)

Table 5. Flow gauge locations and values of the FEH catchment descriptors for the four catchments in the case studies.

		(A) Bellever	(B) Halsewater	(C) Brue	(D) Bishop₋Hull
Flow gauge location Catchment descriptors	Latitude Longitude AREA (km ²) ALBAR (m) DPLBAR (km) DPSBAR (mkm ⁻¹) ASPVAR SAAR (mm) QMED (m ³ s ⁻¹) PROPWET SPRHOST (%) URBEXT	50.582° N 3.898° W 21.5 459 13.46 6.28 94.9 0.25 2095 37.4 0.46 47.5 0	51.022° N 3.133° W 87.8 109 19.40 9.57 85.7 0.30 851 12.2 0.35 30.6 0.006	51.075° N 2.587° W 135.2 104 22.61 13.62 71.1 0.16 857 36.2 0.37 36.4 0.007	51.019° N 3.134° W 202.0 144 40.21 17.75 98.0 0.17 964 43.7 0.36 32.9 0.007

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Table 6. Lead steps c	f the forecasting	system with	different time intervals.
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	1 h (00 min)	2h (100 min)	3h (100 main)	4 h	5 h (200 min)	6 h	9 h (5 40 min)	12h (700 min)
	(60 min)	(120 min)	(180 min)	(240 min)	(300 min)	(360 min)	(540 min)	(720 min)
15 min	4	8	12	16	20	24	36	48
30 min	2	4	6	8	10	12	18	24
45 min	_	-	4	-	-	8	12	16
60 min	1	2	3	4	5	6	9	12
90 min	_	-	2	-	-	4	6	8
120 min	-	1	-	2	-	3	-	6

Table 7. Forecasting results shown in RMSE $(m^3 s^{-1})$ for the four catchments using data with different time intervals. The lowest RMSE value for a certain lead time forecasting is highlighted to show the optimal time interval.

	Forecast lead time (h)											
	1	2	3	4	5	6	9	12				
(A) Bellever (21.5 km ²)												
15 min	0.2099	0.4870	0.7232	0.8915	1.0039	1.0754	1.1530	1.1593				
30 min	0.2359	0.4851	0.6699	0.7955	0.8801	0.9378	1.0200	1.0448				
45 min	-	-	0.6754	-	-	0.9218	0.9981	1.0231				
60 min	0.2938	0.5359	0.7073	0.8175	0.8907	0.9401	1.0143	1.0395				
90 min	-	-	0.7942	-	-	1.0489	1.1083	1.1260				
120 min	-	0.5833	-	0.9042	-	1.0189	-	1.0832				
(B) Halsewater (87.8 km ²)												
15 min	0.0555	0.1177	0.1859	0.2516	0.3111	0.3638	0.4863	0.5672				
30 min	0.0570	0.1211	0.1883	0.2510	0.3061	0.3535	0.4585	0.5238				
45 min	-	-	0.1896	-	-	0.3626	0.4827	0.5635				
60 min	0.0605	0.1243	0.1930	0.2578	0.3161	0.3668	0.4842	0.5623				
90 min	-	-	0.1905	-	-	0.3644	0.4802	0.5568				
120 min	-	0.1246	-	0.2600	-	0.3668	-	0.5441				
(C) Brue	(C) Brue (135.2 km ²)											
15 min	0.2641	0.7190	1.1873	1.5767	1.8617	2.0583	2.3422	2.3939				
30 min	0.3172	0.7824	1.2185	1.5671	1.8263	2.0157	2.3155	2.3867				
45 min	-	-	1.2121	-	-	1.9803	2.2150	2.2654				
60 min	0.3208	0.8044	1.2549	1.5896	1.8114	1.9554	2.1539	2.1984				
90 min	-	-	1.2584	-	-	1.9229	2.0934	2.1395				
120 min	-	0.9306	-	1.7574	-	2.1469	-	2.3157				
(D) Bishop_Hull (202.0 km ²)												
15 min	0.1496	0.3849	0.6502	0.9099	1.1468	1.3567	1.8314	2.1099				
30 min	0.1447	0.3677	0.6210	0.8713	1.1007	1.3048	1.7792	2.0676				
45 min	-	-	0.7068	-	-	1.4327	1.8736	2.1137				
60 min	0.1644	0.4088	0.6783	0.9291	1.1436	1.3213	1.6848	1.8869				
90 min	-	-	0.7190	-	-	1.3865	1.7814	2.0101				
120 min	-	0.4576	-	0.9703	-	1.3422	-	1.8412				





Table 8. Rankings of different time intervals according to the forecasting results (RMSE) with a certain lead time (from the lowest to the highest RMSE). The optimal time intervals (ranked as the 1st) are highlighted.

	1 h	2h	Зh	4 h	5 h	6 h	9 h	12 h			
(A) Bellever (21.5 km ²)											
1st	15	30	30	30	30	45	45	45			
2nd	30	15	45	60	60	30	60	60			
3rd	60	60	60	15	15	60	30	30			
4th	_	120	15	120	-	90	90	120			
5th	_	_	90	_	_	120	15	90			
6th	-	_	-	_	-	15	-	15			
optimal	15	30	30	30	30	45	45	45			
(B) Halsewater (87.8 km ²)											
1st	15	15	15	30	30	30	30	30			
2nd	30	30	30	15	15	45	90	120			
3rd	60	60	45	60	60	15	45	90			
4th	-	120	60	120	-	90	60	60			
5th	-	-	90	-	-	60	15	45			
6th	-	-	-	-	-	120	-	15			
optimal	15	15	15	30	30	30	30	30			
(C) Brue (135.2 km ²)											
1st	15	15	15	30	60	90	90	90			
2nd	30	30	45	15	30	60	60	60			
3rd	60	60	30	60	15	45	45	45			
4th	-	120	60	120	-	30	30	120			
5th	-	-	90	-	-	15	15	30			
6th	-	-	-	-	-	120	-	15			
optimal	15	15	15	30	60	90	90	90			
(D) Bishop_Hull (202.0 km ²)											
1st	30	30	30	30	30	30	60	120			
2nd	15	15	15	15	60	60	30	60			
3rd	60	60	60	60	15	120	90	90			
4th	-	120	45	120	-	15	15	30			
5th	-	-	90	-	-	90	45	15			
6th	-	-	-	-	-	45	-	45			
optimal	30	30	30	30	30	30	60	120			

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Fig. 2. Process of the discrete wavelet decomposition following the Mallat decomposition algorithm. X(n) is a discrete signal with *n* samples, passing though a low-pass filter *G* and a high-pass filter *H* with impulse responses of G(n) and H(n), respectively. A1, A2, A3 and D1, D2, D3 are the decomposed approximations and details on level j = 1, 2, 3, ...







Fig. 3. Conceptual structure of the PDM model. The 13 model parameters to be calibrated are in the brackets.







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Fig. 4. Locations and configurations of the four UK catchments in case studies with river networks and the flow gauging stations at the catchment outlets: (a) Bellever, (b) Halsewater, (c) Brue and (d) Bishop_Hull.



Fig. 5. Six-month length hydrographs of the observed rainfall-runoff data versus the best results of the 4 h-ahead forecasts using the 30 min data. The NSE values calculated between the observed and the forecasted flows are 0.8932, 0.9544, 0.9167 and 0.9420, respectively for the four catchments in panels (a), (b), (c) and (d).







Fig. 6. Decreasing performance of the forecasting system constructed using data with different time intervals as the increase of the forecast lead time, for the catchments of Bellever, Halsewater, Brue and Bishop_Hull, respectively in (a), (b), (c) and (d).







Fig. 7. Forecasting results in three-dimensional coordinates for the four catchments, of Bellever, Halsewater, Brue and Bishop_Hull, respectively in panels (a), (b), (c) and (d).







Fig. 8. Hypothetical pattern for the general impact of data time interval on forecasting accuracy and the selection of the optimal time interval in real-time hydrological forecasting. The axes of X, Y and Z, respectively stand for the time interval of the model input data, the forecast lead time and the forecasting error.



