

1 *Soil erosion and sediment delivery in a mountain catchment under*
2 *scenarios of land use change using a spatially distributed numerical*
3 *model.*
4

5 **Abstract:** Soil erosion and sediment yield are strongly affected by land use/land cover
6 (LULC). Spatially distributed erosion models are of great interest to assess the expected
7 effect of LULC changes on soil erosion and sediment yield. However, they can only be
8 applied if spatially distributed data is available for their calibration. In this study the soil
9 erosion and sediment delivery model WATEM/SEDEM was applied to a small (2.84
10 km²) experimental catchment in the Central Spanish Pyrenees. Model calibration was
11 performed based on a dataset of soil redistribution rates derived from point ¹³⁷Cs
12 inventories, allowing capture differences per land use in the main model parameters.
13 Model calibration showed a good convergence to a global optimum in the parameter
14 space, which was not possible to attain if only external (not spatially distributed)
15 sediment yield data were available. Validation of the model results against seven years of
16 recorded sediment yield at the catchment outlet was satisfactory. Two LULC scenarios
17 were then modeled to reproduce the land use at the beginning of the twentieth Century
18 and a hypothetical future scenario, and to compare the simulation results to the current
19 LULC situation. The results show a reduction of about one order of magnitude in gross
20 erosion (3,180 to 350 Mg yr⁻¹) and sediment delivery (11.2 to 1.2 Mg yr⁻¹ ha⁻¹) during the
21 last decades as a result of the abandonment of traditional land uses (mostly agriculture)
22 and subsequent vegetation re-colonization. The simulation also allowed assessing
23 differences in the sediment sources and sinks within the catchment.

24

25 **Keywords:** soil erosion, sediment transport, sediment yield, sediment delivery ratio,
26 sediment sources, land use/land cover changes, Arnás catchment, Spanish Pyrenees.

27

28

29 **1. Introduction**

30 According to estimations one sixth of the surface land is affected by accelerated
31 water erosion (Schröter et al., 2005). Apart from the at-site problems related to loss of
32 fertile land, sediment yield to the stream network poses problems for hydraulic
33 infrastructures such as reservoirs, and for the preservation of certain fluvial ecosystems.
34 Mountain regions, where the energy relief contributes to increase soil erosion and
35 sediment redistribution rates, are among the areas at risk. It has been pointed out that land
36 use / land cover (LULC) change is among the main factors explaining the intensity of soil
37 erosion, even exceeding the importance of rainfall intensity and slope in some cases
38 (García-Ruiz, 2010). The effects of LULC change on soil erosion and sediment transport
39 have raised the attention of transnational authorities (e.g., UN, 1994; EC, 2002;
40 COST634, 2005). Many studies have demonstrated that historical LULC change has
41 affected the sediment yield in drainage basins over the World (e.g., Dearing, 1992;
42 Piégay et al., 2004; Cosandey et al., 2005; Gyozo et al., 2005).

43 The impact of LULC change on soil erosion and sediment yield are well
44 understood qualitatively, but there is still little quantitative knowledge. It has been
45 addressed in different ways: i) field suspended sediment load measurements and
46 historical sedimentary archives (sediment accumulated in lakes) showed that

47 deforestation and changes in the agricultural practices greatly influenced erosion and
48 sediment transport (e.g., Valero-Garcés et al., 2000); ii) experimental catchments have
49 been monitored worldwide in order to understand the factors that control runoff
50 generation and sediment transport (e.g., Bosch and Hewlett, 1982), and to obtain detailed
51 information on different parameters for hydrological modeling and to assess the influence
52 of LULC change on erosion rates and sediment yield (e.g., García-Ruiz et al., 2008). All
53 these studies provided a deep insight into the interaction between LULC change and
54 geomorphic processes. Experimental approaches, however, are resource-intensive and
55 very limited in their ability to address the effects of future changes in LULC or other
56 drivers such as the climate.

57 Erosion models are useful tools for comparing erosion resulting from current
58 LULC condition with a number of alternative LULC scenarios. Spatially distributed
59 models allow determining not only the variation in the total sediment exported, but also
60 assessing differences in sediment sources and the existence of sedimentation areas at
61 intermediate locations within the watershed. Although most of erosion and sedimentation
62 processes have been studied in detail using experimental devices, assessing the link
63 between on-site soil erosion and total sediment yield at the outlet of a catchment is very
64 difficult because it implies making a complete sediment budget of the catchment
65 including possible internal sedimentation areas, on which there is seldom quantitative
66 data available. Recent advances in spatially distributed erosion and sediment transport
67 models opened new possibilities to understand the complex spatial patterns of erosion
68 and deposition within a catchment (Merrit et al., 2003). However, a direct comparison of
69 predicted erosion rates with field observations, which is necessary for validating the

70 accuracy of the estimates, is usually not possible because it is not practically or
71 financially feasible to acquire long-term, spatially distributed soil erosion data. In the best
72 instances data are available only on the sediment transported by the main rivers in a
73 catchment, and these data seldom span a long time period (Alatorre et al., 2010). For
74 example, it is common to rely on catchment-aggregated soil erosion rates derived from
75 reservoir or lake sedimentation records for the calibration or validation of erosion and
76 sediment transport models (e.g., de Vente et al., 2008). This allows predicting the total
77 catchment sediment yield, but the capability to predict soil redistribution within the
78 catchment is lost. The lack of spatially distributed soil erosion data is a major problem
79 hindering the use of spatially distributed erosion models, and even makes model
80 calibration not possible (Alatorre et al., 2010).

81 In addition to modeling exercises, the difficulties associated with classical
82 techniques for estimating erosion have led to research into new methods. In the last
83 decades field measurements of fallout cesium-137 (^{137}Cs) inventories have been used to
84 determine soil redistribution rates at specific points in the landscape. Here soil
85 redistribution refers to the net result of erosion and sedimentation over a period of
86 approximately 50 years (Walling and Quine, 1990). The use of fallout radionuclides has
87 attracted increasing attention as an alternative approach for water-induced soil erosion
88 analysis, and it has been applied successfully in a wide range of environments (e.g.,
89 Ritchie and McHenry, 1990; Walling and Quine, 1991; Navas & Walling, 1992; Collins
90 et al., 2001; Bujan et al., 2003). Unlike the experimental devices described above, ^{137}Cs
91 soil redistribution estimates are related to a small sampling surface (usually a few dm^2),
92 and can be taken as point estimates when considered at the landscape scale.

93 A simple approach for studying spatial patterns of soil redistribution from point
94 ¹³⁷Cs estimates is to get a sufficiently large sample and perform a spatial interpolation.
95 ¹³⁷Cs-derived soil redistribution rates have also been used for validating the results of
96 process-based erosion models, including: i) empirical erosion models such as the Revised
97 Universal Soil Loss Equation (RUSLE) (Ferro et al., 1998; López-Vicente et al., 2008);
98 ii) spatially semi-distributed erosion models such as the Aerial Non-point Source
99 Watershed Environmental Response Simulation (ANSWERS) and the Agricultural Non-
100 point Source Pollution (AGNPS) (De Roo, 1993; Walling et al., 2003); and iii) fully
101 spatially distributed physically based models such as the Limburg Soil Erosion Model
102 (LISEM) and WATEM/SEDEM (Takken et al., 1999; Feng et al., 2010).

103 The main objective of the present study was to assess soil redistribution and
104 sediment supply to the stream network under land abandonment on a mountain
105 catchment, using a spatially distributed model (WATEM/SEDEM) combined with ¹³⁷Cs-
106 derived soil redistribution estimates. The study area (the Arnás catchment in the Spanish
107 Pyrenees) is an experimental area for which a good amount of data and process-
108 knowledge exists, including sediment yield data at the catchment outlet that could be
109 used for validation (Lana-Renault et al., 2007b). In addition, ¹³⁷Cs-derived soil
110 redistribution rates were available from a previous study (Navas et al., 2005), allowing
111 spatially distributed model calibration under the current LULC situation. Two LULC
112 scenarios were then modeled reproducing the land use at the beginning of the twentieth
113 Century and a hypothetical future scenario, and the results compared to the current
114 situation. We discuss the validity of the results and their application. The approach
115 followed is transferable to other regions of the World.

116

117 **2. Materials and methods**

118 *2.1 Hillslope sediment delivery model*

119 We used WATEM/SEDEM to model soil erosion and sediment flux from the
120 hillslopes to the stream network in a small mountain catchment under current, past and
121 hypothetical land use. WATEM/SEDEM is a spatially-distributed soil erosion and
122 sediment transport model based on the RUSLE model plus a sediment transport capacity
123 equation and a cascading transport model, for predicting sediment delivery to the stream
124 network (Van Oost et al., 2000; Van Rompaey et al., 2001; Verstraeten et al., 2002).
125 WATEM/SEDEM has been used in various types of environments in (Van Rompaey et
126 al., 2001; Verstraeten et al., 2002; Van Rompaey et al., 2003a, 2003b, 2005; Verstraeten
127 et al., 2007), including hydrological catchments in Spain (de Vente et al., 2008; Alatorre
128 et al., 2010).

129 The models starts by calculating annual soil erosion rates following the RUSLE
130 approach (Renard et al., 1991):

$$131 \quad E = R K L S_{2D} C P, \quad (1)$$

132 where E is the mean annual soil loss ($\text{kg m}^{-2} \text{y}^{-1}$), R a rainfall erosivity factor (MJ mm m^{-2}
133 $\text{h}^{-1} \text{yr}^{-1}$), K a soil erodibility factor ($\text{kg h MJ}^{-1} \text{mm}^{-1}$), $L S_{2D}$ a slope-length factor (Desmet
134 and Govers, 1996), C a dimensionless crop management factor, and P a dimensionless
135 erosion control practice factor. Next the sediment generated is routed downslope
136 according to the topography until a stream cell is reached. Sediment transport by overland
137 runoff is modeled according to a transport capacity equation (Van Rompaey et al., 2001):

$$138 \quad TC = ktc R K \left(L S_{2D} - 4.1s^{0.8} \right), \quad (2)$$

139 where TC is the transport capacity ($\text{kg m}^{-1} \text{yr}^{-1}$), s the slope gradient (m m^{-1}), and ktc (m)
140 an empirical transport capacity coefficient that depends on the land cover. A mass
141 balance approach is followed for determining the net amount of sediment in each cell: the
142 sediment transported to the cell from neighboring upslope cells is added to the sediment
143 generated in-cell by erosion, and this amount is then exported entirely to the downslope
144 cells (if it is lower than the transport capacity) or deposited in the cell (if it is greater than
145 the transport capacity). Although several equations exist for the transport capacity in
146 cases where gully erosion dominates (e.g. Verstraeten et al., 2007), we used the original
147 formulation because sheet wash erosion is the main erosion process in our study area.

148 The parameter ktc in equation (2) represents the slope length needed to produce
149 an amount of sediment equal to a bare surface with identical slope gradient, and varies
150 between extreme values of 0 and 1 (Verstraeten, 2006). It depends on the land cover, and
151 it is assumed to vary linearly between arable land highly prone to erosion where ktc is
152 highest and densely vegetated areas less prone to erosion where ktc is lowest (Van
153 Rompaey et al., 2001, 2005). This implies that ktc is site-dependent and needs to be
154 calibrated based on experimental data for each application of the model. Calibration of
155 ktc requires determining the optimum value of the two values ktc_{min} and ktc_{max} based on
156 observed erosion data. Since these values depend on the land cover, erosion data for
157 different land cover types is needed for calibrating ktc . This data is seldom available,
158 since in the best cases sediment yield data at the catchment outlet is the only data at hand.
159 It has been proposed that a fixed ratio between values ktc_{max} and ktc_{min} can be taken
160 (Verstraeten, 2006), thus reducing the problem to calibrating only one parameter, but

161 there are no easy ways to decide which is the most appropriate value for that ratio, since
162 it is site-dependent.

163 In this work we used soil redistribution rates derived from fallout cesium-137
164 (^{137}Cs) as a method for calibrating ktc_{min} and ktc_{max} . The ^{137}Cs technique is based on a
165 comparison of measured inventories (activity per unit area) at individual sampling points
166 with a measured reference inventory at stable sites in the same catchment. Soil
167 redistribution rates are estimated from the difference between those values using a mass
168 balance model and considering both the fallout rates and natural decay of the radioisotope
169 over the time span (Soto and Navas, 2004). A major advantage of the ^{137}Cs technique is
170 the potential to provide medium-term (40 to 50 years, depending on the sampling date),
171 spatially distributed information regarding net soil redistribution (erosion and
172 aggradation) rates. Additionally, and with the objective of illustrating the discussion
173 about the model calibration, we performed an alternative calibration based on seven years
174 of sediment yield recorded at the catchment outlet. Details of the ^{137}Cs and sediment
175 yield datasets and of the calibration procedure are given in the following sections.

176

177 *2.2 Study area*

178 The Arnás catchment is located in the Borau valley, central Spanish Pyrenees, in
179 the headwaters of the Aragón River (Figure 1A). The catchment is an experimental site
180 area that has been subject of many studies. It has been described in detail in several
181 works, for example in Navas et al. (2005). Here we will outline its main characteristics.

182 The catchment covers an area of 2.84 km^2 , with altitudes between 912–1339 m
183 above the sea level (Figure 1B and 1C). The climate is sub-Mediterranean with Atlantic

184 influence, with average temperature of 10 °C and average annual precipitation of 930 mm
185 for the period October 1996 to September 2009. Precipitation is slightly higher in autumn
186 and spring due to frontal activity. Nevertheless, snowfall is not rare during the winter,
187 and some storms occur in summer. Snow remains on the soil only for a few days per
188 year, since the 0 °C isotherm is located above 1600 m a.s.l. during winter.

189 The area is underlain by Eocene flysch, i.e. by alternating layers of marls and
190 sandstone. The two slopes of the catchment have contrasting physiographic
191 characteristics. On the southwest-facing slopes, poorly developed Rendzic Leptosols and
192 Calcaric Regosols on unconsolidated materials predominate (Navas et al., 2005), with an
193 average slope gradient of 0.5 m m⁻¹. On these steep slopes several ancient mass
194 movements (debris flows) are identified, disconnected from the fluvial network (Lorente
195 et al., 2000), and having a scarce influence on the sediment load at the basin scale
196 (Bathurst et al., 2007). On the gentler northeast-facing slope (average gradient of 0.28 m
197 m⁻¹), soils are haplic Kastanozems and Phaeozems. These soils are deeper (50 to >75 cm)
198 and better developed with clearly differentiated soil horizons (Navas et al., 2005). Some
199 deep mass movement (earthflows) affected the slope, resulting in an undulated
200 topography and in some small wet areas. The low slope gradient (average 0.08 m m⁻¹) on
201 the valley bottom has deep Calcaric Fluvisols developed on alluvial deposits, with
202 minimal horizon differentiation (Navas et al., 2005). The main soil properties are
203 summarized in Table 1.

204 Vegetation is composed of Mediterranean shrubs (*Buxus sempervirens*, *Genista*
205 *scorpius*) on the south-west facing slope (shrub slope), and *Juniperus communis*, *Buxus*
206 *sempervirens*, *Echynopartum horridum* and forest patches with *Pinus sylvestris* in the

207 north-east facing slope (forest slope) (Figure 1E). For centuries, land use in the Arnás
208 catchment consisted on farming both the northeast- and southwest-facing slopes, in very
209 difficult topographic conditions. Commonly, the shady aspect was not cultivated in the
210 Pyrenees, whereas the south facing slopes were cultivated up to 1600 m a.s.l. (García-
211 Ruiz and Lasanta, 1990). Exceptionally, the Arnás catchment was also farmed in the
212 north-east facing slope due to its smooth gradient, allowing a relatively high insolation
213 for cereal cropping in sloping fields. Concave slopes in the sunny slope were occupied
214 with bench terraces, while the convex and straight slopes were cultivated under shifting
215 agriculture systems with scarce practices of soil conservation (Lasanta et al., 2006). Since
216 the beginning of the 20th century, farmland abandonment firstly affected the worst fields
217 under shifting agriculture. Since the 1950's the rest of the sloping and bench terraced
218 fields were also abandoned, and the flat fields in the valley bottom were abandoned in the
219 1970's. As a consequence of land abandonment a complex process of plant colonization
220 occurred, resulting in the installation of dense shrub communities and an increasing
221 presence of trees. The fields in the valley bottom still remain as grazing meadows,
222 although *Genista scorpius* is progressively colonizing them due to very low grazing
223 pressure. The process described is similar to that observed in other European regions in
224 which re-vegetation processes are the consequence of land abandonment (Kozak, 2003;
225 Taillefumier and Piégay, 2003; Torta, 2004).

226 Since 1996 a number of studies have been carried out in the Arnás catchment
227 devoted to understanding its hydrology, soil properties and processes (Navas et al.,
228 2002a; Navas et al., 2002b; Seeger et al., 2004; García-Ruiz et al., 2005; Navas et al.,

229 | 2005; Lana-Renault et al., 2007a; Lana-Renault et al., 2007b; [Lana-Renault and Regüés,](#)
230 | 2007; Navas et al., 2008; Lana-Renault and Regüés, 2009; [López-Vicente et al., 2011](#)).

231

232 | 2.3 Data

233 | An input dataset was prepared as GIS layers with a 5x5 m horizontal resolution. A
234 | digital elevation model (DEM) was the main input, from which a drainage network map
235 | was derived [by setting a threshold upstream catchment area](#). Land use, rainfall erosivity,
236 | soil erodibility, and crop management maps were also produced [based on aerial photo](#)
237 | [interpretation, daily rainfall data, and a soil field survey \(Figure 2\)](#). Detailed information
238 | [about the development of this dataset is provided as](#) supplementary material.

239 | For calibrating the *ktc* parameter a [dataset of 19 ¹³⁷Cs inventories](#) [was used](#). They
240 | [were collected](#) along three representative transects: i) [five](#) sample points on the south-
241 | west facing slope (forest slope); ii) [four](#) sample points on the north-east facing slope
242 | (shrub slope); and, iii) [ten](#) sample points along the valley bottom (Table 3 and Figure 1).
243 | Soil redistribution rates were computed at these points by comparing these samples with
244 | a reference ¹³⁷Cs inventory for the area [taken on a flat area not affected by erosion or](#)
245 | [deposition](#). These are average values for the period between 1963 (starting of significant
246 | ¹³⁷Cs fallout in the region) and 2003 (time of sample collection and radio-isotopic
247 | analysis). We refer the interested reader to the article by Navas et al. (2005), where
248 | details of the development and interpretation of the ¹³⁷Cs dataset are given.

249 | In addition, seven years [\(from October 1999 to September 2008\)](#) of sediment
250 | yield recorded at the catchment outlet were used for validating the results of the
251 | simulation [with an independent dataset](#). Detailed information about the instrumentation

252 and data collected in the Arnás catchment is given in Lana-Renault and Regüés (2009).
253 We also used the sediment yield data to perform an exercise by comparing the calibration
254 obtained from ^{137}Cs (internal) data with a calibration based on catchment yield (external)
255 data.

256

257 **3. Results**

258 *3.1. Model calibration and validation*

259 The calibration procedure consisted in performing a high number of simulations
260 ($n=100$) corresponding to the time span 1963-2003 modifying the values of ktc_{max} and
261 ktc_{min} at discrete steps within a predefined range. For each combination of ktc_{max} and
262 ktc_{min} a soil erosion map was obtained in terms of net soil redistribution ($\text{Mg ha}^{-1} \text{y}^{-1}$),
263 allowing comparison of the point ^{137}Cs soil redistribution estimates with the model
264 simulations for the 5x5 m grid cell corresponding to the location of the ^{137}Cs
265 measurements. The Nash-Sutcliffe model efficiency statistic NS (Nash and Sutcliffe,
266 1970) was used as a likelihood metric. The relative root mean square error (*RRMSE*) was
267 used as an estimate of the model accuracy. Formulation of the two statistics is given in
268 the supplementary material section.

269 It was found that the error surfaces varied quite smoothly, allowing construction
270 of a meta-model of the NS and *RRMSE* statistics in the (ktc_{max}, ktc_{min}) space using thin
271 plate spline interpolation over the 100 simulation runs. Leave-one-out cross-validation of
272 the meta-model yielded a standard error of 0.000344, that is, around 0.1%, and the R^2 of
273 the regression line between TPS cross-validation residuals and measured NS values was
274 0. These values allow assuming that uncertainty of the meta-model did not affect the

275 estimation of the optimum parameter combination. Thus, the meta-model was analyzed to
276 determine the optimum values of ktc_{max} and ktc_{min} as those that maximized the NS
277 statistic or minimized the RRMSE.

278 The error surface topographies in the 2D (ktc_{max} , ktc_{min}) space are shown in Figure
279 3. In both cases a good convergence of the model to a global optimum point coinciding
280 with the maximum NS and the minimum RRMSE values was found, corresponding to
281 values of $ktc_{max} = 9.84$ m and $ktc_{min} = 2.05$ m (ratio = 0.208). The model efficiency
282 statistics for these parameters was NS = 0.845 and RRMSE = 0.485, which can be
283 considered very good. There were no problems in identifying the optimum parameter
284 values, since the error surfaces were smooth and converged to a single optimum value.
285 Under these conditions, it is possible to implement an automated algorithm for finding
286 the optimum parameter set in a small number of steps, up to a desired precision. The
287 results shown in Figure 3 demonstrate that the use of spatially distributed sediment yield
288 data from ^{137}Cs inventories allowed calibrating the empirical parameters of
289 WATEM/SEDEM in a satisfactory way.

290 Application of the calibrated model to the Arnás catchment allowed comparing
291 the soil redistribution rates predicted by WATEM/SEDEM and the corresponding ^{137}Cs
292 estimates (Figure 4). It must be stressed, however, that the comparison made in Figure 5
293 does not correspond to an independent test, since the ^{137}Cs redistribution rates were used
294 for calibrating the model. The results revealed a strong relationship between both erosion
295 rates ($R^2 = 0.503$, 0.818 excluding two outlier points), mainly at the points located on the
296 southwest-facing slope (shrub slope) and at the valley bottom. In general,
297 WATEM/SEDEM overestimated slightly the net erosion rates, but this was due to a few

298 influential points. Two points which corresponded to the northeast-facing slope (forest
299 slope), points 5 and 2, were located far from the perfect adjustment line. While
300 WATEM/SEDEM predicted high erosion or sedimentation rates at these points, they can
301 be considered approximately stable as derived from ^{137}Cs estimates. It was possible to
302 obtain stable results for these points by manually tuning the $k_{tc_{min}}$ parameter to a very
303 low value, but this affected negatively the overall calibration.

304 An alternative calibration was performed based on seven years of sediment yield
305 data at the Arnás catchment outlet. Contrary to the calibration based on ^{137}Cs data, the
306 results of this calibration were not conclusive, since an infinite number of possible
307 parameter combinations could be found that yield equally good results. This is shown as
308 a ‘valley’ in the RRMSE plot or a ‘ridge’ in the NS plot (Figure 5). Differences between
309 these alternative parameter combinations are related to the relative contributions of
310 different land cover types, which could not be assessed without spatially distributed soil
311 erosion data within the catchment.

312 Data from seven years of hydrological monitoring were used for validating the
313 model. Sediment yield values predicted by WATEM/SEDEM with the best parameter set
314 were compared with sediment yield values measured at the catchment outlet (Lana-
315 Renault and Regüés, 2009). In this case the two samples were independent, so a real
316 validation could be performed. Correspondence between the two values was in general
317 very good (Table 3 and Figure 6), with an overall R^2 of 0.857 (0.991 excluding the worst
318 prediction). The model was good at estimating annual sediment yields close to average,
319 but tended to underestimate high sediment yields and overestimate low sediment yields.

320 The bad results obtained for the hydrological year 2001-2002, for which the
321 measured sediment yield was abnormally low at 71 Mg y^{-1} , are attributed to changes in
322 the channel caused by accumulation of debris after the years 1999-2000 and 2000-2001,
323 which registered abnormally high sediment production due to the occurrence of severe
324 storms responsible for high rainfall erosivity values. These morphological changes
325 modified temporarily the behavior of the stream, reducing its capacity to transport
326 sediment, and were not captured by the simulation. Overall, sediment yield during the
327 measuring period 1999-2008 was 244 Mg y^{-1} , compared to 268 Mg y^{-1} predicted by
328 WATEM/SEDEM.

329

330 *3.2. Hillslope sediment delivery and major sediment sources*

331 Application of WATEM/SEDEM to the land use conditions prevailing during the
332 period 1963-2003 allowed estimation of the total sediment yield and assessment of the
333 relative contributions of each hillside. WATEM/SEDEM predicted a gross SY of 350 Mg
334 y^{-1} , which can be translated to specific sediment yield SSY of $1.23 \text{ Mg ha}^{-1} \text{ y}^{-1}$. These
335 values are slightly higher than the average values recorded during seven years at the
336 gauging station at the outlet of the Arnás catchment, which were 273 Mg y^{-1} and 0.96 Mg
337 $\text{ha}^{-1} \text{ y}^{-1}$, respectively (Lana-Renault and Regüés, 2009). This could be explained by
338 differences in rainfall erosivity (R-factor) for both periods (Table 4): while for the
339 gauging period 1999-2008 rainfall erosivity was $926 \text{ MJ mm ha}^{-1} \text{ h}^{-1} \text{ y}^{-1}$, for the period
340 1963-2003 a higher value of $1217 \text{ MJ mm ha}^{-1} \text{ h}^{-1} \text{ y}^{-1}$ was registered. This difference in
341 rainfall erosivity can explain the higher SY estimated for the long period.

342 | To assess the sediment delivery ratio ($SDR = SY/\text{gross erosion rate}$; expressed as
343 | a percentage) we calculated the gross soil erosion rate ($6,521 \text{ Mg year}^{-1}$) as the net soil
344 | erosion for the area (*i.e.*, total sediment production) before sediment was routed down the
345 | hillslopes to the Arnás ravine. The predicted SDR value at the outlet of the watershed was
346 | approximately 5%.

347 | The predicted sediment yield map was used to analyze the major sediment sources
348 | in the Arnás catchment (Figure 7). The major sediment sources were located in the south-
349 | west facing slope (scrub slope), with an average $SSY = 1.49 \text{ Mg ha}^{-1} \text{ y}^{-1}$, particularly in
350 | the straight slopes in the lowest and highest parts of the hillslope, whilst the convex and
351 | concave areas were affected by moderate erosion processes; sedimentation prevailed in
352 | some concave sectors and in the flat areas of the valley bottom. The north-east facing
353 | slope (forest slope) had a value of $SSY = 0.69 \text{ Mg ha}^{-1} \text{ y}^{-1}$, with, in general, low erosion
354 | rates and some areas in which sedimentation prevail, following the terraced borders of
355 | old cultivated fields. Apart from the land cover and physiographic differences, stoniness
356 | was clearly different between both sides of the valley, being on the south-west facing
357 | slope (mostly above 400 g kg^{-1}).

358 |

359 | 3.3. *Effect of land use change on soil redistribution patterns and on sediment yield*

360 | The robustness of the calibration of k_{tc} , with samples corresponding to different
361 | land uses gave confidence for applying the model to alternative LULC scenarios. The
362 | contemporary land use contains almost no croplands (Fig. 2B), which may result in a bad
363 | calibration of K_{tc} for this land use. However, the abundance of other land use types with
364 | a comparable C-factor (and hence similar expected values of K_{tc}) reduces the uncertainty

365 | and allows applying the model to other LULC scenarios. An analysis was made of the
366 | effects of LULC change in the Arnás catchment in soil redistribution and sediment yield
367 | by applying WATEM/SEDEM using two LULC scenarios (Figure 8):

368 | i) the first scenario corresponded to the conditions that prevailed on the catchment
369 | during the early twentieth century, when the study area was occupied by annual crops,
370 | mainly cereals; and

371 | ii) a second scenario consisting on a hypothetical LULC condition in the future,
372 | provided that land use will be almost unmanaged and that vegetation colonization will
373 | progress on the south-west facing slope (now mostly covered by dense scrub land) that
374 | would be occupied by forests.

375 | SY and SSY maps predicted by WATEM/SEDEM for these two alternative
376 | LULC scenarios allowed analyzing the effects of past and foreseen LULC changes on
377 | soil erosion patterns and total sediment yield in the Arnás catchment (Table 5 and Figure
378 | 9). For the past scenario (LULC prior to 1950) the catchment was almost entirely
379 | occupied by cereal crop fields. In fact, inspection of a vertical aerial photograph from
380 | 1956 confirms that the Arnás catchment was fully cultivated, both in the north-east and
381 | the south-west facing slopes, even on steep slope gradients, occasionally under shifting
382 | agriculture systems. The SY and SSY values ($3,180 \text{ Mg y}^{-1}$ and $11.19 \text{ Mg ha}^{-1} \text{ y}^{-1}$,
383 | respectively) obtained using that scenario were extremely high in comparison with the
384 | values obtained with the current LULC, representing an increase of approximately 810%.
385 | Consequently the SDR was higher than with the current LULC, rising up to 84% (Table
386 | 5).

387 Net erosion areas had predominance over the sedimentation areas under past
388 LULC, and erosion was intense even in the relatively gentle slopes of the northeast-
389 facing slopes (Figure 9A). A higher number of intermediate sedimentation areas also
390 appeared especially in the northeast-facing slope. These bands are related to the presence
391 of plot margins or slightly terraced slopes (now almost completely hidden by vegetation,
392 but still recognizable in the field), which helped reducing the loss of soil towards the river
393 network.

394 In the second scenario (future situation) an increment of forest and dense
395 scrubland was proposed in the northeast- and southwest-facing slopes, respectively, as a
396 consequence of land use abandonment (Table 4). The SY and SSY predicted values (255
397 Mg y^{-1} and $0.89 \text{ Mg ha}^{-1} \text{ y}^{-1}$, respectively) were approximately 38% lower with respect to
398 the current LULC condition, and 1,150% lower than the past LULC scenario. The SDR
399 was very similar to the value obtained with the current LULC (5.15 %). Nevertheless, the
400 gross erosion rate was 32% lower than the current situation. The sediment yield map
401 (Figure 9B) shows a predominance of low erosion values (less than $10 \text{ Mg ha}^{-1} \text{ y}^{-1}$), and a
402 reduction of the erosion areas. Figure 9B shows a remarkable trend towards: i) a
403 reduction in the sediment sources, even in the south-west facing slope; and ii) a trend to
404 homogenization.

405

406 **4. Discussion and conclusions**

407 A spatially distributed soil erosion and sediment transport model,
408 WATEM/SEDEM, was applied to simulate soil redistribution in a mountain catchment
409 under current, past and hypothetical future land use/land cover (LULC) conditions. A

410 dataset of soil redistribution rates derived from ^{137}Cs profiles at 19 sampling points
411 within the catchment were used to calibrate the model.

412 Calibration using ^{137}Cs data was very successful, since it was possible to
413 determine a single combination of the *ktc* parameters ($ktc_{max} = 9.84$ m, $ktc_{min} = 2.05$ m)
414 that provided a good fit to the observed soil redistribution rates within the catchment.
415 Only for two locations in the forested slope a disagreement was found between soil
416 redistribution rates obtained by the two methods, probably as a consequence of the
417 relevance in that area of soil creeping processes that are not considered by the model.
418 These results contrast with a similar study by Feng *et al.* (2010), in which they found a
419 poor convergence to a global optimum parameter set and erosion rates estimated by both
420 methods (WATEM/SEDEM and ^{137}Cs) differed considerably. The optimum values for
421 ktc_{min} and ktc_{max} in that case were 6 and 7 respectively, indicating a poor discrimination
422 between LULC types. The poor performance in this study case could be possibly
423 attributed to deficiencies in the sampling design, since farming LULCs were under-
424 represented in the calibration dataset with only 4 sites against 56 sites in well vegetated
425 LULCs, being an important source of bias against farming LULCs in the calibration
426 process. Additionally, the calibration algorithm described was far from optimal, since the
427 multi-dimensionality of the problem was eliminated by keeping the value of some
428 parameters fixed while calibrating other parameters, ignoring likely co-variances among
429 parameters.

430 An additional calibration exercise was performed based on sediment yield data at
431 the catchment outlet for comparison purposes, since most applications of
432 WATEM/SEDEM up to date have been based on catchment sediment yield data. This

433 raises a fundamental problem, since it is difficult to calibrate land-cover related
434 parameters with sediment yield alone. As a solution, some authors proposed that a fixed
435 ratio between $k_{TC_{max}}$ and $k_{TC_{min}}$ be taken, which has the effect of lumping both parameters
436 into a single one, thus allowing calibration (Verstraeten, 2006). However this raises new
437 concerns, since there is no way to decide which is the most appropriate value for that
438 ratio, which would be site-dependent. In a previous study in the Ésera watershed in the
439 Central Spanish Pyrenees (Alatorre et al., 2010) we found significant problems for
440 calibrating WATEM/SEDEM based on sediment yield data at the catchment level. The
441 results of the calibration experiment in this work confirm that it is not possible to identify
442 a single combination of k_{TC} parameters that allows optimize the objective function, hence
443 demonstrating the need for spatially- and land use-distributed soil redistribution data such
444 as that provided by ^{137}Cs data.

445 Application of WATEM/SEDEM with the optimum parameter set to the Arnás
446 catchment allowed estimating the sediment balance of the catchment. Very good
447 agreement was found between modeled and measured annual sediment yield values at the
448 catchment outlet. The simulation allowed also determining the major sediment sources
449 within the catchment, and the existence of intermediate sediment traps between the
450 hillslopes and the channel network. Mean sediment yield was determined at 350 Mg y^{-1}
451 or $1.23 \text{ Mg ha}^{-1} \text{ y}^{-1}$. These values are similar in order of magnitude to other catchments in
452 the Spanish Pyrenees. Almorox et al. (1994) obtained an estimate of $4.12 \text{ Mg ha}^{-1} \text{ year}^{-1}$
453 for the Yesa Reservoir in the Aragón River basin, $1.67 \text{ Mg ha}^{-1} \text{ year}^{-1}$ for Barasona
454 reservoir in the Ésera river basin. Similar or higher values have been estimated for small
455 experimental catchments in the French Alps (Mathys et al., 2005), the Eastern Pyrenees

456 (Gallart et al., 2005; Soler et al., 2008), and the Central Pyrenees (*García-Ruiz et al.*,
457 2008), which encompass a variety of bedrocks and climates.

458 Sediment delivery ratio (SDR) for the catchment was determined at
459 approximately 5%. This is a low value, but not extreme considering the high variability
460 of this parameter among catchments. For example, Van Rompaey et al. (2007) reported a
461 SDR of 28% for a catchment of 1,960 km² in the Czech Republic; Verstraeten et al.
462 (2007) found SDR values of 20–39% for catchments of 164–2,173 km² in Australia;
463 Fryirs and Brierley (2001) estimated an extremely high SDR of almost 70% in the Bega
464 River catchment (New South Wales, Australia), which caused dramatic changes to the
465 river morphology; Romero Díaz et al. (1992) found SDR values of 7–46% in the
466 subcatchments of the Segura River (Spain); and de Vente et al. (2008) predicted SDR
467 values ranging from 0.03% to 55% for 61 catchments in Spain. It must be noted,
468 however, that the catchments cited are of very varying size and that SDR calculation
469 methods vary between studies, so any comparison must be taken with great care.

470 The existence of a robust calibration of the model's parameters allowed
471 performing additional simulations under LULC scenarios. Simulation under past land use
472 (farming land in most of the catchment) resulted in an increase of gross erosion and
473 sediment yield of about one order of magnitude. These values coincide with the intensity
474 of erosive processes (mostly sheet wash and rill formation, but also shallow landsliding)
475 that has been described as predominant during the period of maximum agricultural
476 activity (García-Ruiz et al., 1995; García-Ruiz and Valero-Garcés, 1998), resulting in a
477 degraded landscape, surface stoniness and braiding of the stream network (Beguería et
478 al., 2006). The SDR increased up to 84%, and a much better connectivity between

479 erosion areas and the stream network was found. A second LULC cover scenario
480 reproducing an increase of the vegetation cover due to land use abandonment resulted in
481 erosion and sediment yield values approximately one third lower than under current
482 LULC. The SDR was quite similar to the current one.

483 In the absence of long-term sediment yield records, simulations with
484 WATEM/SEDEM allow quantifying the effect of recent LULC change on the reduction
485 of soil erosion and sediment source areas as a consequence of the abandonment of
486 agricultural activities and vegetation re-colonization. As our simulations suggest, this
487 process has almost reached its final stage, since further increase or densification of the
488 vegetation cover did not have a large effect on either gross erosion or sediment yield
489 values. Although these findings can be translated to other mountain areas, it must be
490 noted that in certain cases land abandonment can increase spatial connectivity and so
491 produce higher sediment yields (García-Ruiz and Lana-Renault, 2011).

492 As pointed out in previous works (Alatorre et al., 2010), ‘spatially lumped models
493 provide reasonable predictions of sediment yield but offer no insight into sediment
494 sources’. A clear advantage of spatially-distributed models is that they can be useful for
495 implementing measures to prevent soil erosion and sediment generation, since they allow
496 assessing the impacts of changes in land use or climate. However, the use of models of
497 this kind usually involves calibration of empirical parameters, so records of soil
498 redistribution rates are required. We have demonstrated that the use of catchment
499 sediment yield data alone is not enough to allow for a robust calibration of land use-
500 dependent parameters. The use of ¹³⁷Cs-derived soil redistribution rates can provide this

501 information and arises as a very promising technique for the calibration of soil erosion
502 and redistribution models.

503 In this work we have shown that a spatially-distributed soil erosion and
504 redistribution model can be used for evaluating sediment budgets with current and
505 alternative land use scenarios. We assessed variations in the amount of sediment
506 exported, but also changes in the sediment source and deposition areas as a consequence
507 of past and likely future land use change. Such an assessment has only been possible with
508 the help of internal measurements of soil redistribution such as those provided by a ¹³⁷Cs
509 survey. We demonstrate that external data such as measurements of total sediment yield
510 at the catchment outlet do not provide enough information for performing a calibration of
511 a distributed model with spatially dependent parameters. This is an important conclusion
512 that should be considered in further applications of such models.

513

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523

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751 | Walling, D.E., He, Q., and Whelan, P.A.: Using ¹³⁷Cs measurements to validate the
752 | application of the AGNPS and ANSWERS erosion and sediment yield models in
753 | two small Devon catchments, *Soil & Tillage Research*, 69, 27–43. 2003.

754

755 Table 1. Principal soil characteristics of the two valley sides in the Arnás catchment
 756 (mean \pm standard deviation over the whole soil profile), adapted from Navas et al. (2005).

	<u>Northeast-facing slope</u> <u>(forest), n=48</u>	<u>Southwest-facing slope</u> <u>(shrub), n=29</u>
pH	7.97 (\pm 0.42)	8.17(\pm 0.19)
Clay (g kg ⁻¹)	210 (\pm 31)	195 (\pm 34)
Silt (g kg ⁻¹)	660 (\pm 63)	620 (\pm 73)
Sand (g kg ⁻¹)	130 (\pm 85)	180 (\pm 103)
Organic matter (g kg ⁻¹)	59 (\pm 22)	54 (\pm 25)
Bulk density (g kg ⁻¹)	1.12 (\pm 1.22)	1.19 (\pm 0.61)
Moisture (%)	17 (\pm 6.7)	11 (\pm 7.7)
Porosity (%)	57 (\pm 5.9)	55 (\pm 6.2)

757

758

760 | Table 2. ¹³⁷Cs inventories and derived soil redistribution rates for the period 1963-2003
 761 | along three transects in the Arnás catchment (Navas et al., 2005): negative and positive
 762 | values indicate net soil erosion and aggradation, respectively. Location of the ¹³⁷Cs
 763 | inventories is shown in Fig. 1D.

Transect	Point ID	¹³⁷ Cs inventory (m Bq cm ⁻²)	Soil redistribution (Mg ha ⁻¹ year ⁻¹)
Forest	1	437	0.9
Forest	2	400	0
Forest	3	430	0.8
Forest	4	404	0.1
Forest	5	400	0
Shrub	6	175	-26.4
Shrub	7	162	-29.5
Shrub	8	280	-11.6
Shrub	9	282	-14.3
Valley	10	297	-7.4
Valley	11	367	-2.0
Valley	12	476	2.2
Valley	13	433	1.0
Valley	14	436	1.0
Valley	15	324	-4.3
Valley	16	439	1.2
Valley	17	325	-5.2
Valley	18	333	-4.7
Valley	19	248	-44.6

764

765

766 | Table 3. Values of cumulative precipitation (P), runoff coefficient (RC), rainfall erosivity
767 (R factor), measured sediment yield (Obs. SY) and specific sediment yield (Obs. SSY) in
768 the Arnás experimental catchment (adapted from Lana-Renault and Regüés, 2009),
769 rainfall erosivity (R-factor) calculated from high frequency (15 minutes) rain gauge data
770 (Angulo-Martínez and Beguería, 2009) and simulated sediment yield (Sim. SY and Sim.
771 SSY). Annual values for the hydrological years between 1999-2000 and 2007-2008, and
772 averages for the periods 1999-2008 and 1963-2003. NA (not available) indicates that no
773 data exists for a given parameter and time period.

Year (Oct-Sep)	P (mm)	RC (mm mm ⁻²)	R-factor (MJ mm ha ⁻¹ h ⁻¹ y ⁻¹)	Obs. SY (Mg y ⁻¹)	Obs. SSY (Mg ha ⁻¹ y ⁻¹)	Sim. SY (Mg y ⁻¹)	Sim. SSY (Mg ha ⁻¹ y ⁻¹)
1999-2000	881	0.42	1302	542	1.91	473	1.67
2000-2001	1353	0.35	1216	381	1.34	348	1.22
2001-2002	765	0.14	852	71	0.25	244	0.86
2002-2003	1043	0.20	792	216	0.76	227	0.80
2003-2004	958	0.33	846	253	0.89	242	0.85
2005-2006	986	0.25	715	116	0.41	155	0.55
2007-2008	922	0.30	754	129	0.45	186	0.65
1999-2008	986	0.28	926	244	0.86	268	0.94
1963-2003	925	NA	1217	NA	NA	350	1.23

774

775

776 | Table 4. Predicted gross erosion, sediment yield (SY), specific sediment yield (SSY) and
 777 | sediment delivery ratio (SDR) under current land cover / land use (LULC) conditions and
 778 | two LULC scenarios (prior to 1950 and future) in the Arnás catchment, based on the best
 779 | parameterization of ktc_{max} and ktc_{min} over the period 1963-2003.

Period	Gross erosion (Mg y ⁻¹)	SY (Mg y ⁻¹)	SSY (Mg ha ⁻¹ y ⁻¹)	SDR (%)
Current LULC	6,521	350	1.23	5.36
LULC before 1950	32,066	3,180	11.19	9.90
LULC future scenario	4,947	255	0.89	5.15

780

781

782 **Figure captions**

783

784 Figure 1. Study area: A) location of the Arnás catchment; B) map of the Arnás catchment
785 showing the sites of the main monitoring instruments and soil samples; C) Lithologic
786 map and location of the ^{137}Cs profiles (see points IDs in Table 3); D) digital terrain model
787 (DTM) and ^{137}Cs inventories (m Bq cm^{-2}); and E) current land cover/land use map
788 derived from aerial photo-interpretation.

789

790 Figure 2. Input data derived from the database of the Arnás catchment: A) drainage
791 network map derived from the DTM using threshold value of 1 km^2 contributing area
792 (continuous line); B) parcel map, derived from the current land use/land cover map; C)
793 soil erodibility map (K-factor in RUSLE, $\text{Mg h MJ}^{-1} \text{ mm}^{-1}$); and D) crop management
794 map (C-factor in RUSLE).

795

796 Figure 3. Calibration of the transport capacity parameters $k_{tc_{min}}$ and $k_{tc_{max}}$ (m) using
797 ^{137}Cs soil redistribution rates: error surface topographies as measured by the *NS* (left) and
798 the *RRMSE* (right) statistics on the two-dimensional space determined by both
799 parameters. Green colour represents the best fit.

800

801 Figure 4. Results of the calibration process: comparison of WATEM/SEDEM and ^{137}Cs
802 soil redistribution estimates for the best parameter set. The solid lines represents a perfect
803 fit, and the dashed one is the linear regression between both datasets.

804

805 | Figure 5. Calibration of the transport capacity parameters ktc_{min} and ktc_{max} (m) using
806 | seven years of sediment yield data at the Arnás catchment outlet: error surface
807 | topographies as measured by the *NS* (left) and the *RRMSE* (right) statistics on the two-
808 | dimensional space determined by both parameters. Green colour represents the best fit.

809

810 | Figure 6. Comparison of measured and predicted sediment yield at the Arnás catchment
811 | outlet between the hydrological years 1999-2000 and 2007-2008 (October to September).
812 | The line 1:1 represents a perfect fit, and the dashed line is the linear regression between
813 | both values.

814

815 | Figure 7. Predicted sediment delivery map of the Arnás catchment under current land use
816 | / land cover.

817

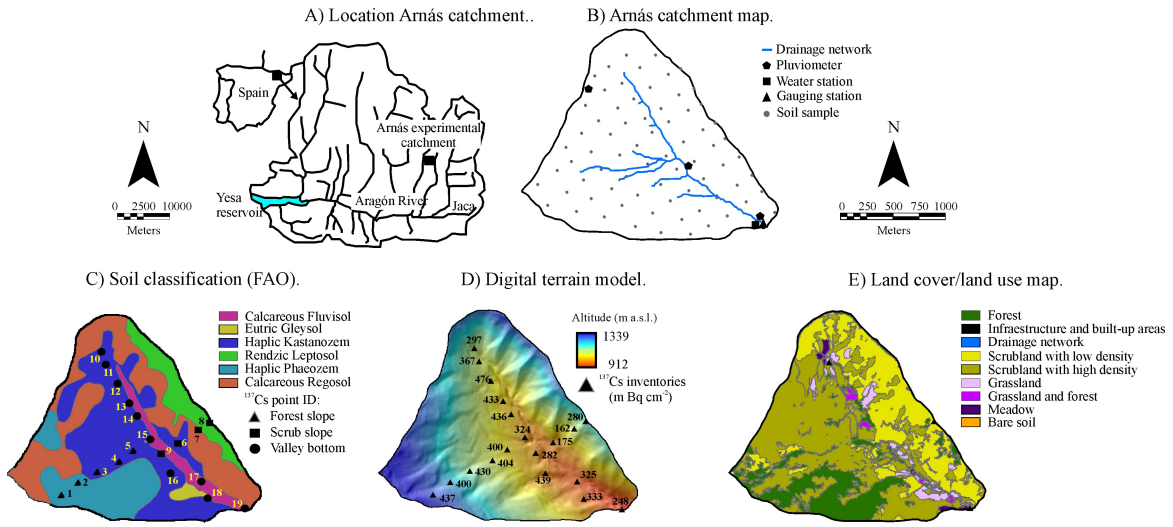
818 | Figure 8. Past (left) and future (right) land use scenarios used in the simulation.

819

820 | Figure 9. Predicted sediment delivery maps of the Arnás catchment: A) under land use /
821 | land cover system at the beginning of the 20th century; and, B) under a likely future
822 | LULC system.

823

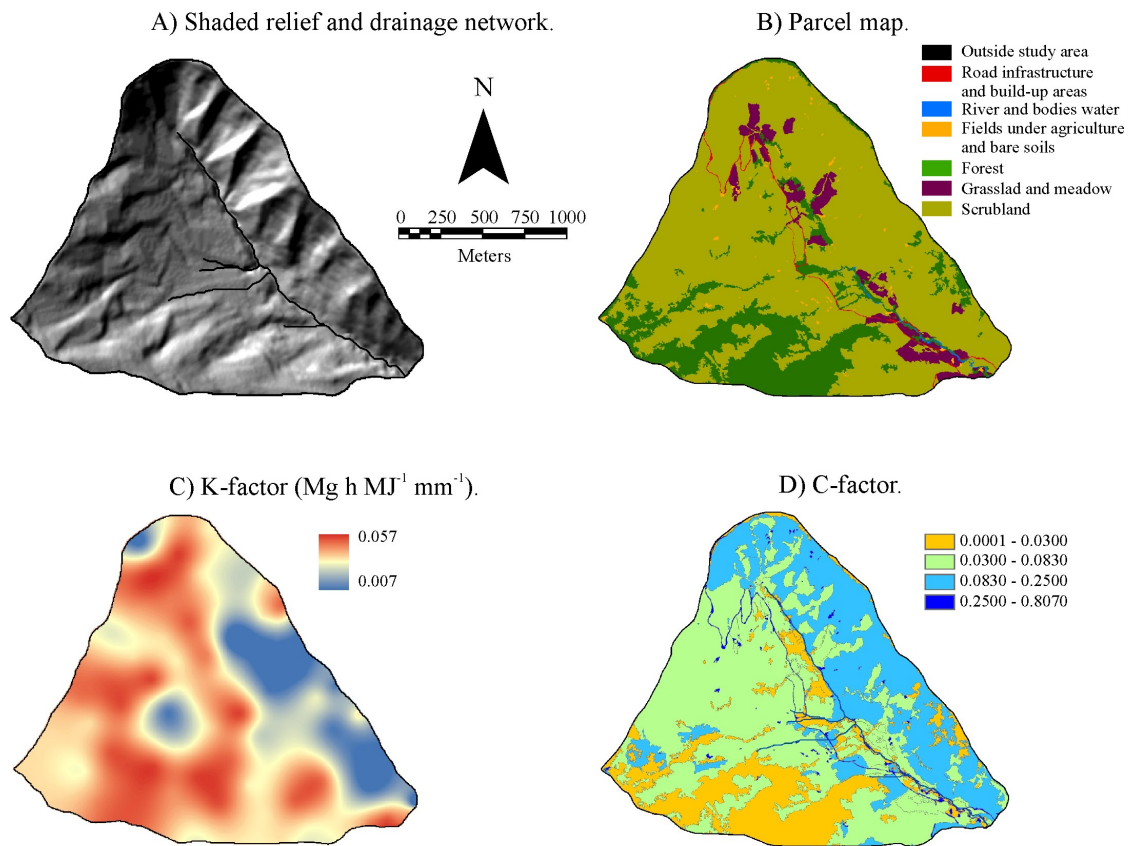
824 **Figure 1**



825

826

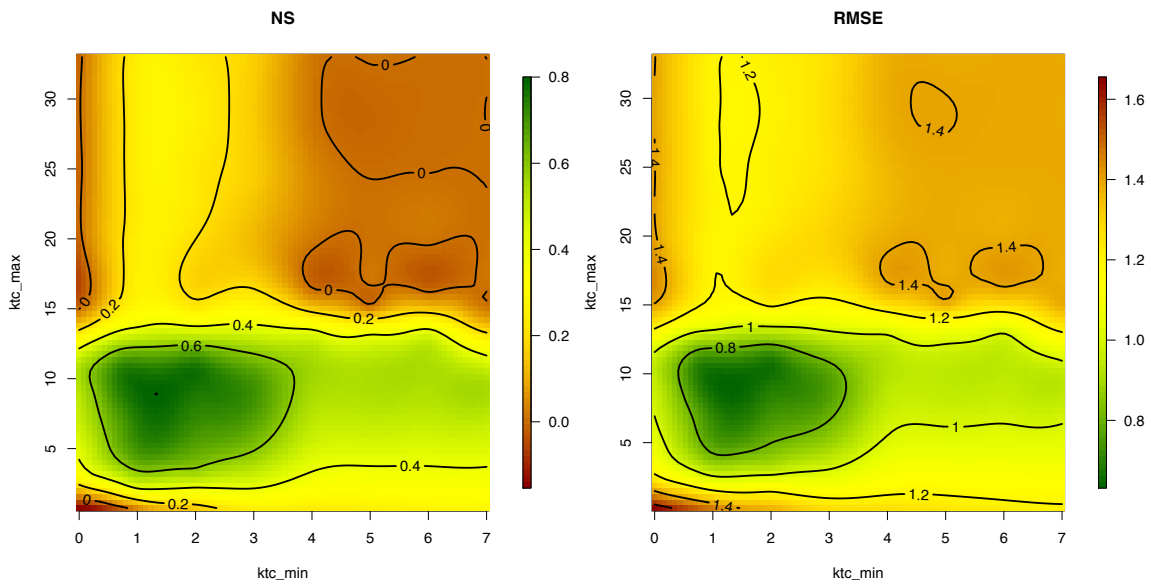
827 **Figure 2**



828

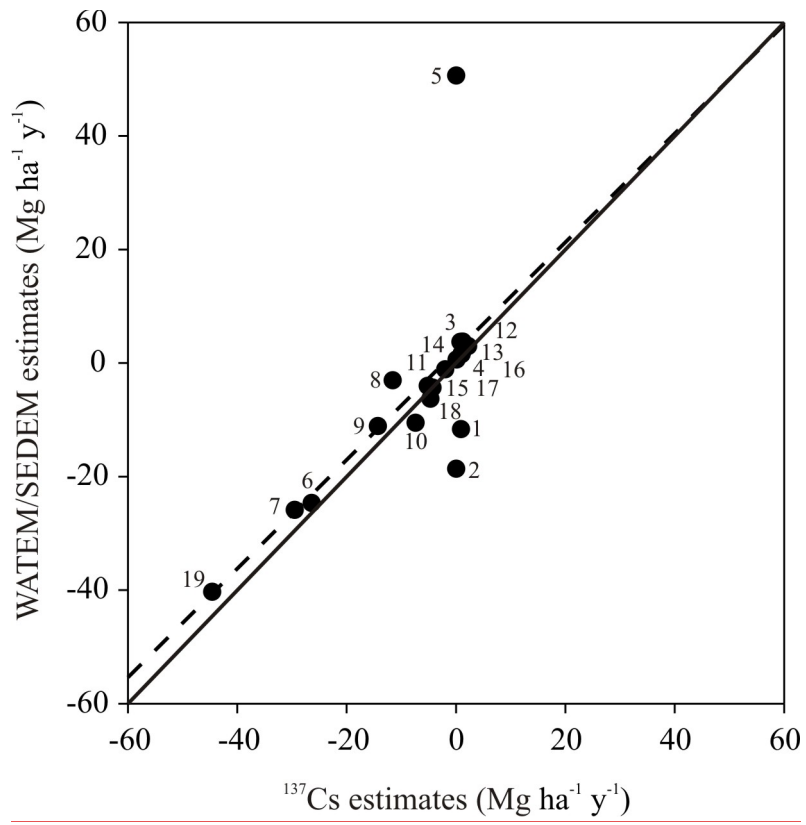
829

830 **Figure 3**



831

832 **Figure 4**

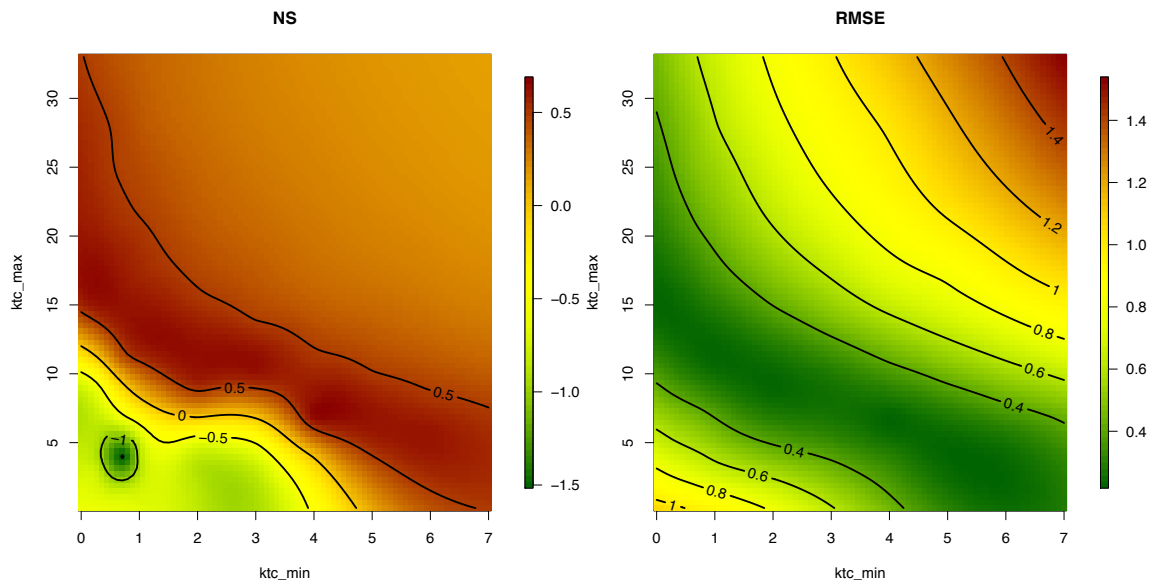


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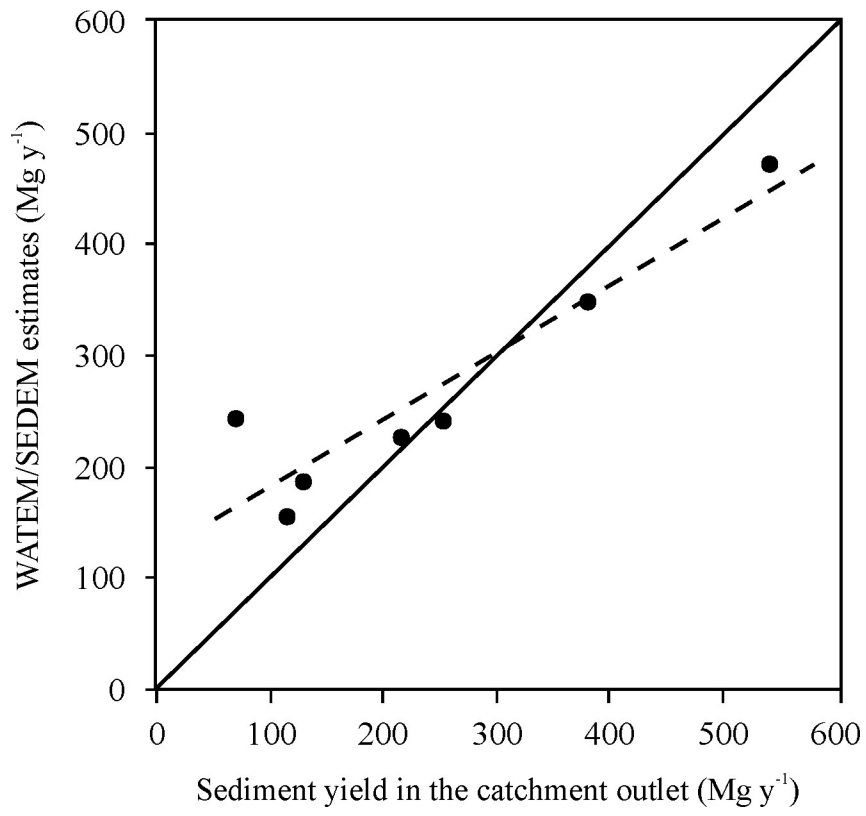
Figure 5



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837

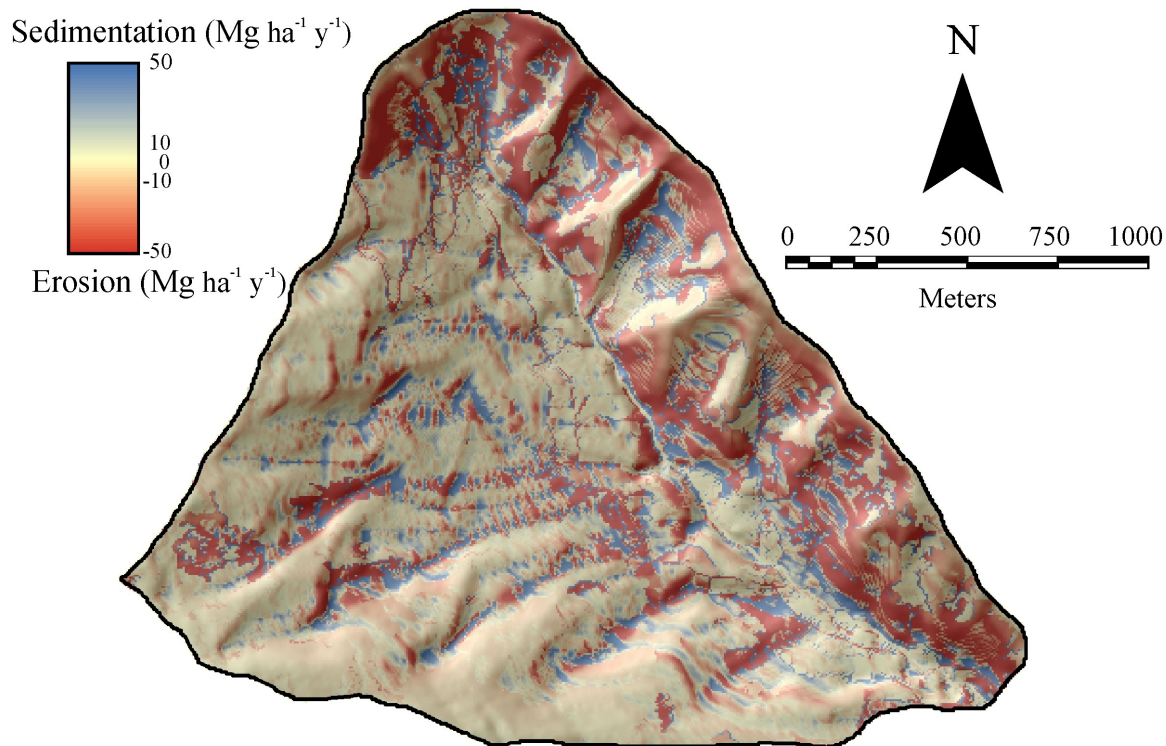
838 | **Figure 6**



839

840

841 **Figure 7**



842

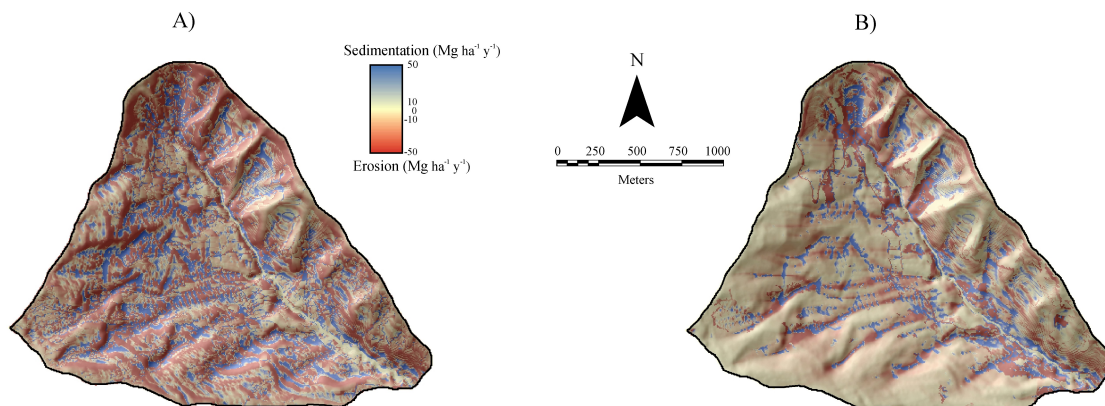
843 |

844

Figure 8.



847 | **Figure 9**



848

849

850 **Supplementary material**

851

852 **1. Generation of input maps for WATEM/SEDEM**

853 *1.1 Digital Elevation Model*

854 The DEM plays a central role in WATEM/SEDEM, since it is used to calculate
855 the slope gradient and the length–slope factor (LS_{2D}), and for routing the sediment
856 downstream. We used a DEM with a spatial resolution of 1 m elaborated by the Spanish
857 Ministry of Agriculture using photogrammetric restitution. The grid resolution of the
858 DTM was then reduced to 5×5 m grid by averaging the values on the original grid. A
859 pit-filling algorithm (Planchon and Darboux, 2001) was used to guarantee the
860 hydrological connectivity of the grid cells until the catchment outlet.

861

862 *1.2 Stream network*

863 A map of the stream network was generated using the RUNOFF module in
864 IDRISI, with the assumption that an upstream catchment area greater than a fixed value
865 defined a channel. After testing different values, we concluded that a threshold area of 1
866 km^2 constituted a good approximation, since it showed good consistency with the stream
867 network as seen in the orthophoto map of the catchment. The 1 km^2 threshold represents
868 an upper limit beyond which sediment deposition is highly unlikely because of
869 concentrated overland flow (Verstraeten et al., 2007).

870

871 *1.3 Parcel map*

872 The parcel map was a reclassification of the current land uses/land cover map
873 (Figure 2B), which was derived from aerial orthophotos (SIGPAC, 2003). The aerial
874 orthophotos were digitized and the LULC types were grouped into five major classes:
875 cultivated land, forest, grassland, infrastructure and built-up areas, and water bodies. The
876 original map was resampled to match the spatial resolution used in the study, using the
877 RESAMPLE algorithm implemented in IDRISI.

878

879 ***1.4 Soil erodibility (K-factor)***

880 The soil erodibility factor (K-factor of the RUSLE model) describes the
881 susceptibility of soil to erosion by rainfall. Because of the lack of detailed soil maps it
882 was necessary to analyze soil samples from the study area. A total of 77 bulk soil cores
883 were collected on a grid pattern at the intersections of a 200 m × 200 m grid (Figure 1B),
884 to assess the spatial distribution of physico-chemical soil properties relevant to soil
885 erosion. To provide a database for the automated land evaluation system several main soil
886 properties were analyzed in a previous study (Navas et al., 2005).

887 K-factor values were determined from soil texture data (Römken et al., 1987)
888 according to:

$$889 \quad K_{text} = 0.0034 + 0.0405 \exp \left[-0.5 \left(\frac{\log D_g + 1.659}{0.71} \right)^2 \right], \quad (1)$$

890 where K_{text} is a soil erodibility factor ($\text{Mg h MJ}^{-1} \text{ mm}^{-1}$) and D_g is the geometric mean
891 weight diameter of the primary soil particles (fraction < 2 mm). D_g was determined using
892 a Coulter laser diffraction particle size analyzer (Coulter LS 230) for the 2–2000 μm
893 fraction, following removal of organic matter (Buurman et al., 1997). K-factor values

894 were then corrected to reflect the effect of stones in the soil surface on soil erodibility
895 (Box, 1981):

$$896 \quad K = K_{text} \exp^{(-0.0278St)}, \quad (2)$$

897 where St is the weight of stones in the topsoil, expressed as a percentage of the total
898 weight of the topsoil. A K-factor map for the study area was obtained from the 77
899 selected sample points estimations by using a smoothing splines spatial interpolation
900 method (Figure 2C).

901

902 ***1.5 Rainfall erosivity (R-factor)***

903 The rainfall erosivity factor (R-factor, MJ mm ha⁻¹ h⁻¹ y⁻¹) is used to represent the
904 impact of rain on soil erosion, and is based on the rainfall amount and intensity. The R-
905 factor value was calculated for the area using a database of rainfall series from the SAIH
906 system (automatic hydrological information network) of the Ebro basin water authority
907 (Confederación Hidrográfica del Ebro). We used all available data to calculate R-factor
908 values for the period October 1963 to September 2008. No high resolution (e.g. hourly)
909 data were available, so we used an approximation based on daily rainfall data (Angulo-
910 Martínez and Beguería, 2009). This way, an average R-factor of 1217 MJ mm ha⁻¹ h⁻¹ y⁻¹
911 was used.

912

913 ***1.6 Crop management (C-factor)***

914 A crop management factor (C-factor) was used to define the susceptibility of
915 various LULC types to erosion by water. C-factor values were applied to each land use
916 category according to the values proposed by the Spanish Institute for Nature

917 Conservation, ICONA (Almorox et al., 1994): 0 for water bodies and infrastructure built-
 918 up areas (i.e. no erosion); 0.003–0.030 for forest land cover; 0.030–0.250 for scrubland;
 919 0.045–0.150 for grassland; and 0.250–0.800 for bare soil categories (Table 2). A C-factor
 920 map was constructed by applying those values to the LULC map (Figure 2D).

921

922 **1.7 Model efficiency statistics**

923

The Nash-Sutcliffe statistic was computed as:

$$924 \quad NS = 1 - \frac{\sum_{i=1}^n (O_i - P_i)^2}{\sum_{i=1}^n (O_i - O_{mean})^2}, \quad (3)$$

925 where n is the number of observations, O_i is the observed value, O_{mean} is the mean
 926 observed value, and P_i is the predicted value. The value of NS can range from $-\infty$ to 1,
 927 and represents the proportion of the initial variance accounted for by the model. The
 928 closer the value of NS is to 1, the more efficient is the model in reproducing the observed
 929 values.

930 The relative root mean square error was computed as:

$$931 \quad RRMSE = 1 - \frac{\sqrt{\frac{1}{n} \sum_{i=1}^n (O_i - P_i)^2}}{\frac{1}{n} \sum_{i=1}^n O_i}. \quad (4)$$

932