

The issues and recommendations raised by Anonymous Referee #1 are critical and profound for the improvement of this manuscript. In this regard the concerns about language, terminology and abbreviations as well as the correct use of units are currently being addressed.

However, the focus of this paper was on characterizing internal drainage and its hydraulic properties for the three soils in questions. This was pursuit in the background of infield rainwater harvesting (IRWH) as an in-situ conservational strategy developed for layered soils. Therefore, the testing of the suitability of the three soils for IRWH was objectively evaluated within the boundary conditions of internal drainage; hence monoliths were covered to keep away atmospheric elements. Hydrological processes that involved atmospheric boundary conditions including evaporation and redistribution were addressed on different papers where the van Genuchten (1980) model was used alongside the HYDRUS 2D software.

Given that internal drainage involves desorption of pores under gravitational influence, characterising the entire soil water characteristic curve for this purpose was not necessary. In this regard the hanging-column method (Dane and Hopmans, 2002) was considered appropriate to describe desorption of structural and intermediate pores under gravitational influence.

According to Ratliff et al., (1983) drainage becomes negligible after 2 to 12 days from saturation from fine textured soils and up to 20 days in clay soils. The soil water content of the root zone where the rate of drainage has reached very low levels following saturation was referred as the drainage upper limit (DUL) by Ratliff *et al.*, 1983. Shortcomings of using the concept of field capacity to characterize drainage were addressed by Hillel (2005). In this paper drainage was characterized in terms of DUL. Drainage was said to have reached DUL once instantaneous soil water content measurements showed negligible differences and Ratliff *et al.*, (1983) approximated the negligible drainage rate to about 0.1 and 0.2% per day.

The Darcian expression was used to compute the $K(\theta)$ relationships from measured data. Saturated hydraulic conductivity (K_s) was determined separately using the double ring method. Recording of the same time period for three consecutive times during the infiltration test was considered to be an indication that steady state conditions for the domain in question have been attained. The computed K_s value was then plotted as the first data point on $K(\theta)$ relationships.

Once the computed $K(\theta)$ coefficients were plotted the $K(\theta)$ relationship was described using the best fit power function. This relationship on a semi-log scale assumed the regression expression presented in Table 4. Through this best fit curve the coefficient of determination were described.