

1 INCREASING PARAMETER CERTAINTY AND DATA UTILITY THROUGH MULTI-
2 OBJECTIVE CALIBRATION OF A SPATIALLY DISTRIBUTED TEMPERATURE AND
3 SOLUTE MODEL

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1 **Abstract**

2 To support the goal of distributed hydrologic and instream model predictions
3 based on physical processes, we explore multi-dimensional parameterization
4 determined by a broad set of observations. We present a systematic approach to
5 using various data types at spatially distributed locations to decrease parameter
6 bounds sampled within calibration algorithms that ultimately provide information
7 regarding the extent of individual processes represented within the model structure.
8 Through the use of a simulation matrix, parameter sets are first locally optimized by
9 fitting the respective data at one or two locations and then the best results are
10 selected to resolve which parameter sets perform best at all locations, or globally.
11 This approach is illustrated using the Two-Zone Temperature and Solute (TZTS)
12 model for a case study in the Virgin River, Utah, USA, where temperature and solute
13 tracer data were collected at multiple locations and zones within the river that
14 represent the fate and transport of both heat and solute through the study reach. The
15 result was a narrowed parameter space and increased parameter certainty which
16 based on our results, would not have been as successful if only single objective
17 algorithms were used. We also found that the global optimum is best defined by
18 multiple spatially distributed local optima, which supports the hypothesis that there
19 is a discrete and narrowly bounded parameter range that represents the processes
20 controlling dominant hydrologic responses. Further, we illustrate that the
21 optimization process itself can be used to determine which observed responses and
22 locations are most useful for estimating the parameters that result in a global fit to
23 guide future data collection efforts.

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25 Index Terms: 1805, 1847, 1874, 1860, 1846
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2 **1. Introduction**

3 Typically, the calibration of models involves fitting simulations to either
4 single or multiple variables, error measures at a single location, or combining
5 information from multiple locations (Duan, 2003). Early calibration techniques were
6 notorious for converging to local optimal solutions and did not reliably find the
7 global optimum (Schaake, 2003). Additionally, many hydrological modeling
8 procedures do not make the best use of available information (Wagener et al., 2001).
9 Current research on the calibration problem primarily focuses on uncertainty analysis
10 and consideration of multiple objectives (Fu and Gomez-Hernandez, 2009; Blasone
11 et al., 2008; Ajami et al., 2007; Duan et al., 2007; and Vrugt and Robinson, 2007).
12 Rather than selecting a single preferred parameter set, equifinality of models
13 recognizes that there may be no single, correct set of parameter values for a given
14 model and that different parameter sets may give acceptable model performance
15 (Beven, 2001).

16 All calibration algorithms have basic design requirements, including the
17 selection of calibration parameters, objectives, and the a priori space within which to
18 search for an optimum solution or set of solutions. The measure of “acceptable” and
19 “optimal” is left to the design of the optimization problem, the model application,
20 and the modeler. In this study, we consider a global optimum as the solution where
21 there is acceptable tradeoff between fitting the model at all locations there is data
22 available versus just matching data at one location well; this can be accomplished by
23 using a range of multiple local optima defined by a narrowly bounded global optima.
24 Since a model is not an exact representation of reality, and observed data used for
25 verification is not perfect, the theoretical global optimum of a process based model
26 distributed in space and in time may be an unrealistic goal. However, a practical goal
27 is to resolve the multiple local optima which simultaneously perform well on a local
28 scale to narrowly bound the region surrounding the theoretical global optimum. In
29 other words, there is a need to narrowly bound the global optimum region where
30 good results exist for all data distributed throughout the system. Performing well
31 locally *and* globally, or glocalization, can be used to define an optimum in model
32 calibration which bridges scales between local and global performance. A systematic
33 approach to using various data types at spatially distributed locations to decrease
34 parameter bounds sampled within optimization algorithms is relevant to instream and
35 hydrologic models ranging in applications from the stream reach to the watershed
36 scale.

1 The Two-Zone Temperature and Solute (TZTS) model (Neilson et al., 2010a
2 and b) was developed to capture the dominant instream processes associated with
3 heat and solute fate and transport. The TZTS model separates transient storage
4 (Bencala and Walters, 1983) into two zones, (1) dead zones or the surface transient
5 storage (STS) zone that represents the eddies, recirculating zones, and side pockets
6 of water and (2) subsurface or hyporheic transient storage (HTS) zone that represents
7 the flow into or out of the stream substrate. As discussed in Neilson et al. (2010a),
8 sources and sinks of heat include fluxes across the air-water interface, bed
9 conduction, conduction between the bed and deeper ground substrate, HTS exchange,
10 and STS exchange. Solute mass is primarily influenced by HTS and STS exchange
11 (Neilson et al., 2010b). To account for each of these fluxes, the TZTS model
12 calculates energy and mass balances on the main channel, the STS zone, and the
13 HTS zone for each reach or control volume. As described further in Neilson et al.,
14 2010a,b, the model equations are:

$$\frac{\partial T_{MC}}{\partial t} = -U_{MC} \frac{\partial T_{MC}}{\partial x} + D \frac{\partial^2 T_{MC}}{\partial x^2} + \frac{J_{atm}}{\rho C_p Y_{MC}} +$$

$$16 \quad \frac{\alpha_{STS} Y_{STS}}{A_{cs,MC} \beta B_{tot}} (T_{STS} - T_{MC}) + \frac{Q_{HTS}}{V_{MC}} (T_{HTS} - T_{MC}) + \quad (1)$$

$$\frac{\rho_{sed} C_{p, sed} \alpha_{sed}}{\rho C_p Y_{MC} Y_{HTS}} (T_{HTS} - T_{MC})$$

$$17 \quad \frac{dT_{STS}}{dt} = \frac{J_{atm,STS}}{\rho C_p Y_{STS}} + \frac{\alpha_{STS}}{(\beta B_{tot})^2} (T_{MC} - T_{STS}) + \frac{\rho_{sed} C_{p, sed} \alpha_{sed}}{\rho C_p Y_{STS} Y_{HTS}} (T_{STS, sed} - T_{STS}) \quad (2)$$

$$19 \quad \frac{dT_{HTS}}{dt} = \frac{\rho C_p Q_{HTS}}{\rho_{sed} C_{p, sed} V_{HTS}} (T_{MC} - T_{HTS}) + \frac{\alpha_{sed}}{Y_{HTS}^2} (T_{MC} - T_{HTS}) + \quad (3)$$

$$\frac{\alpha_{sed}}{Y_{HTS} Y_{gr}} (T_{gr} - T_{HTS})$$

$$21 \quad \frac{dT_{STS, sed}}{dt} = \frac{\alpha_{sed}}{Y_{HTS}^2} (T_{STS} - T_{STS, sed}) + \frac{\alpha_{sed}}{Y_{HTS} Y_{gr}} (T_{gr} - T_{STS, sed}) \quad (4)$$

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$$\frac{\partial C_{MC}}{\partial t} = -U_{MC} \frac{\partial C_{MC}}{\partial x} + D \frac{\partial^2 C_{MC}}{\partial x^2} + \frac{\alpha_{STS} Y_{STS}}{A_{cs,MC} \beta B_{tot}} (C_{STS} - C_{MC}) + \frac{Q_{HTS}}{V_{MC}} (C_{HTS} - C_{MC}) \quad (5)$$

$$\frac{dC_{STS}}{dt} = \frac{\alpha_{STS}}{(\beta B_{tot})^2} (C_{MC} - C_{STS}) \quad (6)$$

$$\frac{dC_{HTS}}{dt} = \frac{Q_{HTS} (C_{MC} - C_{HTS})}{Y_{HTS} A_{S,MC}} \quad (7)$$

where T = temperature ($^{\circ}\text{C}$), Q = volumetric flow rate (m^3s^{-1}), V = zone volume (m^3), D = longitudinal dispersion (m^2d^{-1}), Δx = volume length (m), α_{STSi} = exchange between the MC and the STS (m^2d^{-1}), Q_{HTS} = HTS advective transport coefficient (m^3d^{-1}), $A_{cs,MC}$ = cross-sectional area of the MC (m^2), B_{tot} = total volume width (m), β = the STS fraction of the total channel width, Y = volume depth (m), ρ = density of the water (g cm^{-3}), C_p = specific heat capacity of the water ($\text{cal g}^{-1} \text{ } ^{\circ}\text{C}^{-1}$), ρ_{sed} = density of the sediment (g cm^{-3}), $C_{p,sed}$ = heat capacity of the sediment ($\text{cal g}^{-1} \text{ } ^{\circ}\text{C}^{-1}$), α_{sed} = coefficient of thermal diffusivity of the sediment, and J_{atm} = atmospheric heat flux ($\text{cal cm}^{-2} \text{d}^{-1}$) (consisting of net shortwave radiation (0.31 to 2.8 μm), atmospheric longwave radiation (5 to 25 μm), water longwave radiation, conduction and convection, and evaporation and condensation), and C = concentration (mg L^{-1}). The subscripts MC , STS , and HTS , STS, sed , and gr specify the main channel, surface transient storage, and the hyporheic transient storage, sediments below the STS and the deeper ground layer, respectively.

To support TZTS model applications, simultaneous data collection of temperature and solute tracer data (referred to more simply as tracer data throughout the rest of the paper) in the main channel and storage zones distributed laterally (e.g., within the main channel, HTS, and STS) at one location and longitudinally along a river segment, has created datasets that can be used to address the high dimensional problems associated with predicting heat and solute movement within streams and rivers. In recent studies, beginning with Neilson et al. (2010a,b), the TZTS model was calibrated using the Multi-Objective Shuffled Complex Evolution Metropolis algorithm (MOSCEM; see Vrugt et al., 2003a for algorithm description) and used to predict solute concentrations and temperatures in the Virgin River, Utah, USA, in two storage zones at two different locations within the study reach. Using

1 temperature and tracer observations at two different sites illustrated that using more
2 spatially distributed information and two different environmental tracers
3 (temperature and solute) in the optimization improves the overall performance of the
4 model. These studies found that even with the use of multi-objective calibration,
5 many optimal parameter sets were indistinguishable based on the objective functions,
6 fairly broad parameter ranges resulted, and parameter uncertainty was still a concern.

7 In this paper, we address these issues by presenting a systematic approach to
8 using various data types at spatially distributed locations to decrease parameter
9 bounds sampled within optimization algorithms in the context of a case study. Our
10 hypothesis is that there is a narrowly bounded parameter range that best represents
11 the hydrologic processes controlling the system, which can be determined by using
12 key data sets as multiple optimization objectives. To do investigate this, we
13 developed a simulation matrix of data types and sites that is used first to locally
14 optimize parameter sets by fitting the respective main channel data using both single
15 and multi-objective optimization algorithms. These results were then used to resolve
16 which parameter sets perform best at individual locations (distributed laterally and
17 longitudinally) or have the best local fit, and which parameter sets result in the best
18 global fit. Throughout this process we also test the utility of single and multi
19 objective optimizations and determine the most informative calibration datasets
20 resulting in global data fits.

21 22 **2. Study area and data**

23 A highly managed portion of the Virgin River, Utah, USA (Fig. 1), is
24 considered impaired due to elevated temperatures that have adversely affected two
25 endangered fish species (Virgin River Chub – *Gila seminuda* and woundfin –
26 *Plagopterus argentissimus*) and other native fishes unique to this river system. An
27 11.94 km study reach of the Virgin River (Fig. 1) was divided into two main sections
28 on the basis of bed slope (0.0039 between S1 and S2 and 0.0012 between S2 and S3)
29 and stream substrate distribution identified from a previous mapping effort (Neilson
30 et al. 2010a).

31 To support the TZTS model population, calibration, and model testing,
32 various data types were collected from 22–25 June 2007. The instream flow during
33 the study period was found to be an average of $1.06 \text{ m}^3 \text{ s}^{-1}$ at Site 1 and $1.96 \text{ m}^3 \text{ s}^{-1}$
34 at Site 3. Information regarding several lateral inflow rates and temperatures were
35 also collected during the study. The largest is the return flow from Quail Creek
36 Reservoir ($0.6 \text{ m}^3 \text{ s}^{-1}$). Groundwater exchanges were set according to Herbert (1995)
37 with a total gain $0.17 \text{ m}^3 \text{ s}^{-1}$ over the entire reach. Weather information (air
38 temperature, solar radiation, wind speed, and relative humidity) was gathered at Site
39 1 using a Davis Wireless Vantage Pro (Hayward, CA) weather station to provide the
40 data necessary to calculate the atmospheric fluxes (J_{atm} in Eqn. 1). Similar to Neilson

1 et al. (2010a,b), solute and temperature information were collected at Site 2 and Site
2 3 to support model calibration and testing. The data included solute tracer
3 experiments resulting in main channel and STS concentrations at both Site 2 and Site
4 3. Simultaneous temperatures at Site 2 and Site 3 were also collected in the main
5 channel (sensor 2), STS (sensor 1 and 3), and HTS (sensor 4, 5, and 6) (Fig. 2). The
6 temperature sensors were Hobo® Water Temp ProV1 (Onset Corporation, Bourne,
7 MA) with a $\pm 0.2\text{C}$ accuracy and resolution of 0.02C .

8 As with Neilson et al. (2010b), a 180 g instantaneous pulse of fluorescent
9 Rhodamine WT dye was injected at 02:00:00 on 6 June 2007, at the head of a riffle
10 just upstream of Site 1. A Self-Contained Underwater Fluorescence Apparatus
11 (SCUFA) (Turner Designs, Sunnyvale, CA) was deployed in the main flow of the
12 channel at both Site 2 and Site 3. Measurements were taken in situ every ten seconds
13 for approximately seven hours at Site 2 and 6 h at Site 3. Grab samples were also
14 collected at both Site 2 and 3 near the SCUFA to provide an independent measure in
15 the main channel and in two representative STS locations. The grab samples were
16 kept cool, stored in the dark in amber bottles with PTFE caps, and analyzed using a
17 Turner Model 450 fluorometer (Turner Designs, Sunnyvale, CA). As discussed in
18 Neilson et al. (2010b), loss of Rhodamine WT due to sorption to streambed
19 sediments (mineral and organic) was not a concern in this study because the organic
20 matter content in the bed sediments was extremely low (averaging 0.05% at four
21 sampling locations). Additionally, a recent sorption study within this portion of the
22 Virgin River (Bingham, 2010) provided average K_d values of 1.5mL/g , which is low
23 based on other Rhodamine WT sorption studies (Bencala and Walters, 1983; Everts
24 and Kanwar, 1994; Lin et al., 2003; Shiau et al., 1993).

26 **3. Methods**

28 **3.1. Simulation Matrix**

29 With the overall goal of iteratively reducing the size of the global search
30 space, while simultaneously investigating the information content within the
31 available data types, we established a simulation matrix (Table 1) to test the use of
32 the most commonly collected main channel data sets used in calibration of instream
33 temperature and solute models. Each row and column denotes a data type that
34 represents both heat and tracer fate and transport at Site 2 and 3 along the study
35 reach and within different zones at each location.

36 This matrix represents all possible combinations of single and two-objective
37 calibrations that use the available main channel temperature and tracer data. The
38 calibration tests were Tests 1 through 4, which are single-objective calibrations using

1 main channel temperature and tracer at Site 2 and Site 3, and Tests 5 through 10
2 which are various combinations of data resulting in two-objective optimizations. The
3 latter two objective tests include the following combinations: main channel
4 temperatures at Site 2 and Site 3 (Test 5), main channel tracer observations at Site 2
5 and Site 3 (Test 6), main channel temperature and tracer observations at Site 2 (Test
6 7), main channel temperature at Site 3 and tracer observations at Site 2 (Test 8), main
7 channel temperature at Site 2 and tracer observations at Site 3 (Test 9), and main
8 channel temperature and tracer observation at Site 3 (Test 10).

9 10 **3.2. Calibration Technique**

11 Similar to previous TZTS calibration studies (Neilson et al., 2010a,b;
12 Bingham, 2010), SCEM (for single-objective calibration) and MOSCEM (for multi-
13 objective calibration) (Vrugt et al., 2003a,b) were the optimization algorithms
14 utilized to evaluate each model test. To ensure that we were adequately searching the
15 parameter space, MOSCEM was run with a random sample of 300 parameter sets
16 that evolved using two complexes for a total of 3000 model runs for each of the ten
17 tests. In this case, a parameter set consists of a different combination of parameter
18 values for each of the 11 parameters that were calibrated and a complex is a group of
19 parameter sets within which objective function results are compared. The parameter
20 sets with the best results from each complex are selected, new randomly selected
21 parameter sets are added, and the complexes are shuffled with each search iteration.
22 We experimented with a range of sample and complex sizes (e.g., 400 samples and
23 four complexes with a total of 10 000 model runs) and we found that an increase in
24 the simulations and complexes did not significantly improve calibration results. We
25 therefore, decided to maintain the smaller number of simulations for efficiency.
26 However, we recognize that future work with extended simulations may improve the
27 search for globally optimal parameter sets, particularly with such a highly
28 dimensional parameter space.

29 In this application, measurements within the STS and HTS were withheld
30 during calibration and used to assess the predictive capacity of these components as
31 “ungauged” model outputs. As will be described in detail later, the STS data were
32 used to assist in selecting globally acceptable parameter sets. The HTS data were
33 reserved for corroboration and testing of the model calibration. Since temperature
34 and tracer data in the main channel are the most commonly collected data sets, we
35 needed to further understand whether model calibration to main channel temperature
36 and tracer data results in realistic and representative STS and HTS predictions.
37 Likewise, little was known about how single-objective model calibration at
38 individual sites controlled the resulting parameterization at other site locations and
39 for other data types. In addition to investigating how to narrow the optimization
40 parameter space, our methods are designed to test how a priori choices in study and

1 project design, as well as data availability, may affect the model calibration and
2 resulting simulation performance.

3.3 Model Parameters

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7 The a priori uniform distribution of the feasible parameter space was
8 determined primarily based on earlier work that included a sensitivity analysis using
9 Latin Hypercube sampling (Neilson et al., 2010). For this study, these ranges were
10 further expanded for some parameters based on preliminary optimization tests that
11 resulted in parameter values consistently at the upper or lower bounds of their
12 respective range (Table 2). The calibration parameters include: STS fraction of the
13 total channel width (β), cross-sectional area of the STS (m^2) ($A_{cs, STS}$), exchange
14 between the main channel and the STS ($m^2 d^{-1}$) (α_{STS}), HTS advective transport
15 coefficient ($m^3 d^{-1}$) (Q_{HTS}), and HTS depth (Y_{HTS}) for each of the two sections within
16 the study reach (resulting in 10 parameters). The depth of the ground layer below the
17 HTS (Y_{gr}) was also estimated, but was represented by one value for both sections and
18 became the eleventh calibration parameter. The total width of the main channel (B_{tot})
19 and the Manning's roughness coefficient (n) were set based on the results of
20 Bingham (2010). In this effort, multi-spectral and thermal imagery of the river
21 system were used to physically estimate the average width of the channel over each
22 section and therefore, reduced the number of parameters estimated in the calibration.
23 With B_{tot} established, n was then set to result in appropriate average travel times. The
24 longitudinal dispersion (D) coefficient was set based on the methods described in
25 Neilson et al. (2010a).

3.4 Calibration Objectives

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30 To evaluate local and global model performance, various types of statistical
31 measures were investigated. Each of the ten tests shown in Table 1 were run using
32 different statistical objectives including bias, Nash-Sutcliffe Efficiency (E), log error,
33 and root-mean square error. Similar to Neilson et al. (2010a,b), we found that E (Eq.
34 1; Nash and Sutcliffe, 1970) provided the most consistent calibration results and we
35 used this objective function throughout the remainder of the study and to quantify all
36 local calibrations.

37

$$E = 1 - \frac{\sum_{t=1}^N (T_o^t - T_m^t)^2}{\sum_{t=1}^N (T_o^t - \bar{T}_o)^2} \quad (1)$$

Where, for N timesteps: T_o^t = observations, T_m^t = modeled simulations (at time t), and \bar{T}_o is the mean of the observations. When used in calibration, the algorithm minimizes the result of $1-E$, since the bounds of E are $[1, -1]$. The normalization of the difference in error by the difference between the observed and the mean of the observed, allows comparison of results when the observations at different locations have different scales of variability, as is the case of temperature and tracer information.

To achieve an acceptable globally optimal calibration, we considered the need to match all local data regardless of the differences in optimal parameter sets associated with various calibrations. In this study, our local problem is that an acceptable parameter set must be found that results in adequately reproducing the dominant processes as measured by an individual time series. Our global problem is that we have ten time series distributed in space, six temperature and four tracer datasets, with 11 different parameters that need to be estimated based on matching both the observed temperature and tracer data in all zones and at all locations. The six locations for temperature calibration or comparisons based on available data include: Site 2 main channel ($E_{MC2 \text{ Temp}}$), STS ($E_{STS2 \text{ Temp}}$), HTS ($E_{HTS2 \text{ Temp}}$); and, Site 3 main channel ($E_{MC3 \text{ Temp}}$), STS ($E_{STS3 \text{ Temp}}$), HTS ($E_{HTS3 \text{ Temp}}$). Note that each observed time series used in these E values for the STS and HTS consists of the average of temperatures observed within the two representative STS zones and the most representative HTS time series, respectively. The appropriate HTS time series was determined based on the calibrated Y_{HTS} values: when $Y_{HTS} < 3$ cm, the 3 cm HTS data were used, when $3 \text{ cm} < Y_{HTS} < 9$ cm, an average of the 3 and 9 cm HTS time series were used, when $9 \text{ cm} < Y_{HTS} < 20$ cm, an average of the 9 and 20 cm HTS time series were used; and when $Y_{HTS} > 20$ cm, the 20 cm HTS time series was used. The four local tracer data locations used for comparison or calibration include: Site 2 main channel ($E_{MC2 \text{ Tr}}$), STS ($E_{STS2 \text{ Tr}}$); and, Site 3 main channel ($E_{MC3 \text{ Tr}}$), STS ($E_{STS3 \text{ Tr}}$). The observed STS time series used in these calibrations are the average concentrations observed within the two representative STS zones.

The first step in our calibration method was to populate the simulation matrix (Table 1) based on available observations. We then identified the a priori parameter search bounds and the most appropriate statistical objective function, E . To compare the global calibration results (i.e., matching the observations at all ten locations) for each of the tests within the simulation matrix (Table 1), we then calculated the arithmetic average (AE) of various combinations of local E values (Eq. 2).

$$AE = \frac{1}{n} \sum_{i=1}^n E_i \quad (2)$$

An AE that used only surface data (AE_s) was first defined and included the local E values for all tracer and temperature data collected in the main channel and STS, but did not include the HTS information. AE_{all} included both surface data and HTS information. AE was used to assess the global results; only E was used as the calibration objectives using the MOSCEM algorithm.

3.5 Narrowing search bounds

Using the initial a priori bounds (Table 2), we defined Level 1 results as calibrated parameter sets from the single-objective optimizations (Tests 1–4). Level 2 results represent the parameter sets from the two-objective optimizations with these same a priori bounds (Tests 5–10). The local criteria ($E > 0.8$) and global criteria ($AE_s > 0.7$) were calculated for each parameter set within each test run in the matrix. For all parameter sets that met both of criteria ($E > 0.8$ and $AE_s > 0.7$), a minimum and maximum for each individual parameter was determined. These ranges were then used to set the narrower search bounds. All simulations in Table 1 were repeated using these narrower bounds. Level 3 results represent the new parameter sets from all single-objective optimizations (Tests 1–4) and Level 4 represent the new two-objective simulation (Tests 5–10) results given the narrowed search range.

The last step was using Level 3 and 4 results to further test the model calibration. Similar to the AE_s , a new AE_{all} value was calculated for the Level 3 and 4 simulations that used all of the data including the temperatures within the HTS. Together the AE_s and AE_{all} measures were used to summarize the spatially aggregated performance of model predictions of temperature and tracer at multiple locations, and determine the ability to predict the HTS temperatures if only surface data were available. This gave an indication of the added utility of collecting subsurface data and whether the model can be calibrated sufficiently in this watershed using only surface data collected at multiple locations and within different zones.

By comparing Levels 1 and 2, a wide parameter search space, to Levels 3 and 4, a narrow parameter search space, we investigated the importance of a priori parameterization. In comparing Levels 1 and 3, single-objective calibrations, to Levels 2 and 4, two-objective calibration, we gained information about how best to utilize available calibration algorithms and various types of spatially distributed information simultaneously.

4. Results

4.1. Level 1

The AE_S , and individual E values for each calibration location and data type are presented in Table 3 for the calibrations from the simulation matrix (Table 1). The ten rows correspond to model outputs by test and shaded boxes represent the data used from that location for calibration. All other observations were used as validation data sets. Level 1 results (Table 3) provide initial information regarding how optimization at single locations can impact the model performance at ungauged locations. Of Tests 1–4, no tests with the main channel tracer data at Site 2 or Site 3 as the objective had results that met the selection criteria of $AE_S > 0.7$, with the best results ${}^2AE_S = 0.65$ and ${}^2E_{MC3, Temp} = 0.95$ and ${}^2AE_S = 0.6$ (preceding superscripts indicate Test numbers). Although the E for each of these tests meet the criteria of $E > 0.8$ and the calibration did well at fitting the dataset used as the objective, the calibration was not acceptable at other locations.

Figures 3 and 4 show the highest performing single-objective Level 1 results (Test 2) for each of the ten total data locations. The observed temperature and tracer data at Site 2 and Site 3 are shown as black circles (Figs. 3 and 4), and the E values for each location are shown within each subplot. The predicted values are shown in grey, and in this case there is a single line since a single objective calibration results in a single optimal parameter set. The calibrated Y_{HTS} value is also shown with the HTS subplots (Fig. 3d and e) since this value is used to determine the most representative HTS temperature time series for calculating E_{HTS} . Although the temperature results seem to fit the observations well (Fig. 3), the tracer results (Fig. 4) show how the model optimized to temperature at Site 3 (${}^2E_{MC3, Temp} = 0.95$) is not able to capture the timing and magnitude of the tracer pulse. This may be in part due to fixing the Manning's n parameter in calibration.

4.2. Level 2

Level 2 simulations were used to determine which parameter sets resulting from the two-objective optimizations (Tests 5–10) converge to the established criteria of $E > 0.8$ for all calibration data sets and $AE_S > 0.7$ (Table 3). The E values reported for the two-objective optimizations are based on the parameter set that represents the best compromise solution or the pareto solution (Vrugt et al., 2003a; 2003b, Boyle et al., 2000, Gupta et al., 1998; 2003, and Neilson et al. 2010a) with the smallest Euclidean distance from the origin. The best results are from Test 7 with values of ${}^7E_{MC2, Tr} = 0.94$, ${}^7E_{MC2, Temp} = 0.91$, and $AE_S = 0.81$. Figures 5 and 6 present Test 7 results where the uncertainty bounds resulting from pareto optimal parameter

1 sets are shown. The uncertainty in the temperature predictions are less at Site 2 (Fig.
 2 5) and there is a much better fit in terms of timing of the tracer curve at Site 2 (Fig.
 3 6), but there are still relatively large bounds. It should also be noted that this
 4 calibration does not capture the tail of the tracer curve at Site 2, which is critical to
 5 understand the transient storage within the study reach (Bencala and Walters, 1983).
 6 Similar to what Neilson et al. (2010a) found, comparing Level 1 and 2 results (Table
 7 3) illustrates the relative benefit of using two-objective optimization compared to
 8 single-objective optimizations. For Tests 5–10, Tests 6 and 10 did not meet the local
 9 criteria of $E > 0.8$ with tracer data used as a calibration objective, although Test 6
 10 did meet the global criteria (Table 3).

11 Since Test 7 met the local and global criteria, all the acceptable parameter
 12 sets (i.e., the pareto optimal parameter sets that also met the local and global criteria)
 13 from this test were used to define the narrowed upper and lower bounds for a new
 14 round of calibrations using the simulation matrix (Table 1). The narrowed minimum
 15 and maximum parameter range (Table 4) represent a parameter range reduction with
 16 a high of 67% for the $A_{cs, STS}$ in Sect. 1 and the least reduction of 4% for the β in Sect.
 17 2. Comparing between sections, Sect. 1 had an average of 40% reduction in bounds
 18 while Sect. 2 had an average of 17% reduction. To visually compare the a priori
 19 parameter range and the narrowed parameter range derived from Test 7 results, each
 20 of the 11 calibrated parameters were normalized or scaled between the lower bound,
 21 0, and the upper bound, 1 (Fig. 7). The thick black solid lines represents the
 22 parameter bounds if all pareto rank one sets resulting from the Test 7 calibrations are
 23 considered. The grey shaded area represents the narrowed parameter bounds for
 24 parameter sets that resulted in meeting both local and global criteria from the Test 7
 25 optimizations.

27 4.3 Level 3 and Level 4

29 Similar to Level 1 results, Tests 1 through 4 all converged to $E > 0.9$ for the
 30 data used in calibration during the Level 3 calibrations (Table 5). However, model
 31 performance at other locations was poor with the exception of Test 3, which had
 32 better AE results than Level 1: ${}^3AE_s = 0.76$, and ${}^3AE_{all} = 0.62$. While these results are
 33 promising, it is important to note that only the tracer at Site 2 (the calibration
 34 objective) fit the observations well (not shown here for brevity).

35 Level 4 had improved results when compared to Levels 1–3. The AE_{all} and
 36 AE_s values increased for most tests (Tables 3 and 5), and the maximum value
 37 increased to 0.78 and 0.9 for AE_{all} and AE_s , respectively. Although Test 6 met the
 38 global and local criteria, the temperature simulations at Site 2 overestimated the high
 39 temperatures and underestimated the low temperatures by approximately 3 C in the

1 main channel, STS, and HTS zones. Figures 8 and 9 show the best overall result for
2 Level 4 temperature and tracer predictions, Test 9: $9AE_s = 0.9$ and $9AE_{all} = 0.78$.
3 Not only are the temperature predictions more representative, but the tracer
4 responses are generally captured better in the tail of the tracer curves. As with the
5 Level 2 calibrations, both temperature and tracer objectives at different locations
6 seem to provide the information necessary to achieve an acceptable global
7 calibration.

8 Figure 10 shows the parameter ranges resulting from the Test 9 optimization
9 that met the local and global criteria and the bounds of all the pareto optimal sets.
10 The dashed line shows the narrowed parameter range within the original a priori
11 search range (normalized here [0,1]). The thick black line is the bounds of the pareto
12 optimal parameter sets. The grey area is the parameter variability given the
13 parameter sets which meet both local and global performance criteria.

14 5. Discussion

16 Comparing the results of the simulation matrix calibrations when using only
17 the main channel temperatures or tracer concentrations as an objective (Test 1–4,
18 Table 3), we see how the choice of a calibration objective effects the global
19 performance of the model by comparing the AE_s and AE_{all} values. In general, the
20 best temperature and tracer main channel result is from a single objective
21 optimization of that parameter at that location, but the corresponding model results
22 are generally inappropriate at other locations. Our results also show that when a main
23 channel temperature objective at one location results in reasonable predictions, the
24 temperature at the other location will also be reasonable. However, this is not
25 necessarily the case when using tracer data in single objective optimizations in this
26 study.

27 The best Level 2 local results at Site 2 and Site 3 for tracer are ${}^8E_{MC2, Tr} = 0.98$
28 and ${}^6E_{MC3, Tr} = 0.99$ and for temperature are ${}^5E_{MC2, Temp} = 0.96$ and ${}^{10}E_{MC3, Temp} = 0.95$
29 (Table 3). It is interesting that the best fit for tracer at Site 3 uses tracer information
30 at both Site 2 and 3 (Test 6), but the best fit at Site 2 uses tracer information at Site 2
31 and temperature information at Site 3 (Test 8). In this case, the tradeoff between
32 solute at two sites is greater than the tradeoff between solute and temperature. For
33 temperature, the best fit at Site 2 uses temperature data at both Site 2 and Site 3 (Test
34 5). However, the best temperature fit at Site 3 uses temperature and tracer data at Site
35 3 (Test 10). It should be noted that when temperature data at Site 3 and tracer data at
36 Site 2 were used (Test 8), ${}^8E_{MC2, Temp} = 0.94$ which is not significantly different than
37 Test 10. Having both main channel temperature and tracer data at two different
38 longitudinal locations provided more information about the system than just one data
39 type.

1 While these local results give insight into the utility of calibration data, it is
 2 important to acknowledge how each of these calibrations perform globally. Given a
 3 broad parameter search range (Level 2), Test 7 had the best overall results with AE_s
 4 = 0.81 and provided some corroboration of the model representing the dominant
 5 processes through an $AE_{all} = 0.75$. Most Level 2 AE_s and AE_{all} values were higher
 6 than Level 1 values. This is consistent with the findings of Neilson et al. (2010a)
 7 where they found two-objective calibrations performed better at locations not used in
 8 model calibration than did single objective calibrations. While Test 7 had the best
 9 global value, the individual results were not nearly as good as the best fits at each
 10 location for each data type. It did, however, provide the necessary information to
 11 narrow the search bounds for the Level 3 and 4 simulations.

12 With this initial understanding of the importance of single versus two-
 13 objective calibration and various data types in model calibration to narrow the search
 14 space, Level 3 and 4 results provide a more complete picture of how the system is
 15 functioning (Table 5). The majority of the Level 3 single-objective optimizations
 16 have AE_s and AE_{all} values that are higher than those in the Level 1 simulations. The
 17 actual E values for the location being used in the calibration are also higher with the
 18 exception of Test 1. This suggests that the more narrow search range was appropriate.
 19 The best Level 4 results at Site 2 and Site 3 for tracer are ${}^8E_{MC2, Tr} = {}^6E_{MC2, Tr} = 0.98$
 20 and ${}^{10}E_{MC3, Tr} = 0.99$ and for temperature are ${}^7E_{MC2, Temp} = 0.95$ and both ${}^5E_{MC3, Temp} =$
 21 0.94 and ${}^{10}E_{MC3, Temp} = 0.94$ (Table 5). The best tracer results at Site 2 are consistent
 22 with the Level 2 results where tracer information at Site 2 and temperature
 23 information at Site 3 is most appropriate (Test 8). The best Site 3 tracer results now
 24 suggest that both temperature and tracer data at Site 3 (Test 10) is better than tracer
 25 data at Site 2 and Site 3 (Test 6). Within the narrow search bounds, the best tracer
 26 results rely on temperature information at some location.

27 For Level 4 temperature results, the best fit at Site 2 uses temperature and
 28 tracer data at Site 2 (Test 7), however the Test 5 results are quite similar. The best
 29 temperature fit at Site 3 still uses temperature and tracer data at Site 3 (Test 10), but
 30 the results for Test 5 (which uses Site 2 and 3 temperatures) has the same E . These
 31 results demonstrate the need to use both temperature and solute data in two-objective
 32 TZTS calibration. The Level 4 results also showed a marked improvement in most
 33 AE_s and AE_{all} values from Level 1–3 simulations. This improvement can be related
 34 to the increased parameter certainty when comparing Level 2, Test 7 (Fig. 7) with
 35 Level 4, Test 9 (Fig. 10). These figures show the usefulness of using more
 36 information, or local data, to define a narrow range bounding the global optimum.
 37 They also highlight the importance of multi-objective calibrations to capture the
 38 spatial heterogeneity within streams and rivers and the need to determine the
 39 appropriate optimization parameter ranges.

1 To further incorporate important processes and continue advancing our
2 predictive capabilities, there is a need for a connected cycle of inquiry that includes
3 model development and refinement, identification of data types and scales of
4 measurement required to support modeling, and establishing the most effective
5 approach for calibration based on the application of interest. Inclusion of all
6 available site specific data in model calibration assists these efforts by providing
7 information that decreases the number and range of parameters, provides information
8 about model certainty, can guide the incorporation of processes missing in the
9 conceptual model, and will assist in prioritization of future data collection efforts.
10 Future work varying additional parameters or holding others constant may improve
11 overall results. Expanding the simulation matrix to examine the use of STS
12 temperature and tracer observations in the calibration would further highlight the
13 utility of these datasets.

14 **6. Conclusions**

15
16 With the overall goal of iteratively reducing the size of the global search
17 space while simultaneously investigating the information content within the available
18 data types, we established a simulation matrix to test the use of the most commonly
19 collected main channel data sets used for model calibration of instream temperature
20 and solute models. This systematic approach to using multiple types of distributed
21 information allowed us to examine the application of both single and multi-objective
22 optimization algorithms to the TZTS model using both temperature and solute data
23 available within the main channel and transient storage zones (STS and HTS).

24 In the context of a case study in the Virgin River, Utah, USA, our global
25 problem was to optimize the model given ten time series distributed in space. Our
26 local problem was that any unacceptable parameter set (i.e., the model does not
27 represent one observed time series well) signified a failure to adequately reproduce
28 the dominant processes affecting both the heat and solute response at that location.
29 Using data representing the effects of both main channel and transient storage
30 processes, we found that two-objective calibrations consistently performed better at
31 all locations where data were available within the study reach for corroboration than
32 did single objective calibrations. However, we also found neither single objective
33 results nor multiple objective pareto optimal results alone were able to produce
34 acceptable global calibrations or appropriately match all 10 data sets available. This
35 led to using parameter sets from initial calibration efforts (Level 1 and 2) to narrow
36 parameter ranges used within optimization resulting in a reduction of bounds in the
37 upstream section of the river by an average of 40%, and in the downstream section
38 by an average of 17%. In doing this, Level 3 and 4 calibrations, which used these
39 narrow parameter bounds, led to improved predictions of instream temperatures and

1 tracer concentrations at multiple locations and zones in the study area not used in
2 calibration. This global fit resulted a better representation of the dominant processes
3 controlling instream processes, where the final reduction of bounds in the upstream
4 section was by an average of 49% and the in the downstream section by an average
5 of 69%.

6 Another key finding was that, in general, using both main channel
7 temperature and solute data in calibration provided better global results. Therefore,
8 we suggest that both data types be collected at different locations, for example,
9 solute at one calibration site and temperature at another. Based on the results of this
10 study, and the need to use resources associated with data collection more efficiently,
11 we recommend future data collection focused on collecting a single tracer
12 observation time series in the main channel, with temperatures collected
13 simultaneously in multiple locations and zones to be used in model calibration and
14 testing.

15
16 *Acknowledgements.* We are indebted to those who helped collect the data that supported this
17 paper (Quin Bingham, Noah Schmadel, Jonathan D. Bingham, Andrew Hobson, Ian
18 Gowing, and Drs. Bayani Cardenas, Enrique Rosero, and Lindsey Goulden). We would also
19 like to thank the USGS and Washington County Water Conservancy District for providing
20 funding and/or support for multiple data collection efforts within the Virgin River.

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