

1 4.2.1 Model concept

2 A simple daily rainfall-runoff model, the Catchment Isotope Model (CIM), was
3 developed to examine the effect of incorporating tracers and to assess associated errors
4 and uncertainties in the data (Fig. 3). The model is based on the linear storage-runoff
5 relationship $Q = S*k$ (linear scaling parameter k (s^{-1}), storage volume S (m^3) and
6 discharge Q (m^3s^{-1})). The storage volume is equivalent to a depth of water multiplied by
7 the catchment area. Two cascading reservoirs (the upper and lower active storage
8 $activeS_{up}$ (m^3) and $activeS_l$ (m^3)) are connected via a recharge flux calculated with
9 parameter R (s^{-1}) to model discharge from both reservoirs applying an upper (k_l (s^{-1})) and
10 a lower (k_2 (s^{-1})) scaling parameter. These water fluxes are used to route any conservative
11 tracer through the catchment (Hooper et al., 1988) assuming that solutes fully mix within
12 each of the two storage compartments. For each modelled water flux, the associated
13 deuterium tracer flux $Dflux$ (‰) is defined according to the following equation (Eq. 4),
14 which mathematically expresses the link of water and tracer fluxes in the applied mixing
15 cell approach (Herzer and Kinzelbach, 1987):

$$16 \quad Dflux = \frac{DS \times flow \times \Delta t}{S} \quad (4)$$

17 with S being the storage volume (m^3), $flow$ the water flux (m^3s^{-1}), DS the deuterium
18 content of the storage (‰), and Δt is the time step (s). This form of equation applies to
19 the fluxes from both storages after precipitation P and the observed tracer signature N is
20 added to the upper active storage $activeS_{up}$ (m^3). This reservoir is not restricted to a lower
21 limit; sub-zero values indicate that the active storage is emptied by evapotranspiration
22 and does not generate any lateral flow, and in this case the associated tracer loss is
23 depleted from the passive storage. This allows threshold-type behaviour to be captured by

1 the model (Fenicia et al., 2008b). Due to the high turn over of storage in the flow model,
 2 two tracer parameters $passiveS_{up}$ (upper mixing volume (m^3)), $passiveS_l$ (lower mixing
 3 volume (m^3)) are introduced into the active storage routine $activeS_{up}$ and $activeS_l$ (Barnes
 4 and Bonell, 1996) to account for an additional mixing volume (passive water) in the
 5 catchment system (Fig. 3) resulting in a **5-parameter** version of the CIM model.

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 7 The unclosed nature of the water balance in the Wemyss catchment raises the question of
 8 leakage from the superficial catchment to the deeper sub-surface, which we acknowledge
 9 by an additional loss parameter $GWloss$ (m^3s^{-1}) (Eq. 5) to account for a regional
 10 groundwater recharge $regGW$ (m^3s^{-1}) (**6-parameter** model). The value of a parameter c
 11 (s^{-1}) to conceptualize a direct runoff generation component $Q_{direct}(t)$ (m^3s^{-1}) (Leaney et al.,
 12 1993) was also explored (**7-parameter** model). This mechanism allows direct mixing of
 13 rain with stream water, even when the upper active storage is not activated, representing a
 14 type of infiltration excess runoff mechanism. A water balance is calculated at each time
 15 step for both the upper and the lower storage of the CIM model:

$$16 \Delta S_{up(t)} = activeS_{up(t-1)} + passiveS_{up(t-1)} + ((P_{(t)} - ET_{(t-1)}) \times area - R_{(t-1)} - Q_{up(t-1)} - regGW_{(t-1)}) \times \Delta t$$

$$17 \Delta S_{l(t)} = activeS_{l(t-1)} + passiveS_{l(t-1)} + (R_{(t)} - Q_{l(t-1)}) \times \Delta t \quad (5)$$

18 with ΔS_{up} (m^3) and ΔS_l (m^3) being the total upper and lower storage at time t (s),
 19 precipitation P (ms^{-1}), $area$ (m^2), recharge R (m^3s^{-1}) to the lower storage and actual
 20 evapotranspiration ET (ms^{-1}). Total discharge Q_{total} (m^3s^{-1}) is the sum of the discharge of
 21 both upper Q_{up} and lower storage Q_l , and the direct runoff Q_{direct} , whereas the simulated
 22 tracer signature in the stream DQ (‰) is calculated via a weighted mean of tracer
 23 (DQ_{direct} , DQ_{up} , DQ_l) and water (Q_{direct} , Q_{up} , Q_l) fluxes:

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$$DQ = \left[(DQ_{direct} \times Q_{direct}) + (DQ_{up} \times Q_{up}) + (DQ_l \times Q_l) \right] \div Q_{total} \quad (6)$$

2 Input time series are looped over 5 years to establish initial conditions and to verify the

3 internal water balance.

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