

Interactive comment on “Uniform flow formulas for irregular sections” by E. Spada et al.

P. Rameshwaran (Referee)

ponr@ceh.ac.uk

Received and published: 30 March 2015

Title: Uniform flow formulas for irregular sections By E. Spada, T. Tucciarelli, M. Sinagra, V. Sammartano, and G. Corato

In this paper, the authors presented two new methods for calculating flow discharge. However, it does need further clarification.

1. The title - Uniform flow formulas for irregular sections - suggests that the new methods are applicable to all planform rivers (i.e. straight, meander and skewed simple or compound rivers) but the sections up to 4 are only deals with straight simple (K4 case?) or compound channels (other cases). Are these methods applicable to all planform rivers?

2. The SKM or similar methods can be numerically solved (see our paper with Rameshwaran & Shiono 2007) i.e. for irregular sections. You only need to discretized into linear elements for analytical solution only (lines 101 to 102).

C750

3. In SKM papers, the friction factor is defined as $f=8gRS/U^2$ but some other papers including Huthoff et al. 2008, it is defined as $f=gRS/U^2$. The authors need to state their friction factor equation.

4. Looking at 13 km Alzette study reach in Figure 4, It got variety of planform (straight, bend/curve, meander etc). In such cases, the energy losses not only form bed roughness elements but also from secondary flows due to planform and expansions and contractions in meandering. Are these methods applicable to the Alzette study reach? The authors need to clarify this.

5. Line 400, the length of the reach is about four times the top width of the section. Line 450, in the inlet section a constant velocity, normal to the section, is applied, and the pressure is left unknown. Is the length (i.e. using constant velocity inlet) enough for flow to develop within 3D model? The authors need to provide evidence.

6. Lines 460 to 462: CFX allows the use, inside the boundary layer, of a velocity logarithmic law, according to an equivalent granular size. What is the logarithmic d_{50} relationship used in CFX?

7. What is the d_{50} value used? Is the logarithmic relationship and first (i.e. boundary mesh size) valid (see papers Nicholas, 2005; Lane et al., 2004; Carney et al., 2006, Rameshwaran et al. 2011)?

References

References

Carney SK, Bledsoe BP, Gessler D. 2006. Representing the bed roughness of coarse grained streams in computational fluid dynamics. *Earth Surface Processes and Landforms* 31: 736–749.

Lane SN, Hardy RJ, Elliott L, Ingham DB. 2004. Numerical modeling of flow processes over gravelly surfaces using structured grids and a numerical porosity treatment. *Water*

Resources Research 40: W01302.

Nicholas AP. 2005. Roughness parameterization in CFD modelling of gravel-bed rivers. In *Computational Fluid Dynamics: Applications in Environmental Hydraulics*, Bates PD, Lane SN, Ferguson RI (eds). John Wiley and Sons: Chichester; 329–355.

Rameshwaran, Ponnambalam; Naden, Pamela S.; Lawless, Mark. 2011 Flow modelling in gravel-bed rivers: rethinking the bottom boundary condition. *Earth Surface Processes and Landforms*, 36 (10). 1350-1366.

Rameshwaran, P.; Shiono, K.. 2007 Quasi two-dimensional model for straight overbank flows through emergent vegetation on floodplains. *Journal of Hydraulic Research*, 45 (3). 302-315.

Interactive comment on Hydrol. Earth Syst. Sci. Discuss., 12, 2607, 2015.