

1 **The effect of different evapotranspiration methods on**  
2 **portraying soil water dynamics and ET partitioning in a**  
3 **semi-arid environment in Northwest China**

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14  
15 **Abstract**

16 Different methods for assessing evapotranspiration (ET) can significantly affect the  
17 performance of land surface models in portraying soil water dynamics and ET  
18 partitioning. An accurate understanding of the impact a method has is crucial in  
19 determining the effectiveness of an irrigation scheme. Two evapotranspiration (ET)  
20 methods are discussed: one, based on reference crop evapotranspiration ( $ET_0$ ) theory,  
21 uses leaf area index (LAI) for partitioning into soil evaporation and transpiration and  
22 is denoted as the  $ET_{ind}$  method; the other is a one-step calculation of actual soil  
23 evaporation and potential transpiration by incorporating canopy minimum resistance  
24 and actual soil resistance into the Penman-Montieth model, and is denoted as the  $ET_{dir}$   
25 method. In this study, a soil water model, considering the coupled transfer of water,  
26 vapor, and heat in the soil, was used to investigate how different ET methods could

27 affect the calculation of the soil water dynamics and ET partitioning in a crop field.  
28 Results indicate that for two different ET methods this model varied concerning the  
29 simulation of soil water content and crop evapotranspiration components, but the  
30 simulation of soil temperature agreed well with lysimeter observations. Considering  
31 aerodynamic and surface resistance terms improved the  $ET_{dir}$  method regarding  
32 simulating soil evaporation, especially after irrigation. Furthermore, the results of  
33 different crop growth scenarios indicate that the uncertainty in LAI played an  
34 important role in estimating the relative transpiration and evaporation fraction. The  
35 impact of maximum rooting depth and root growth rate on calculating ET components  
36 might increase in drying soil. The influence of maximum rooting depth was larger late  
37 in the growing season, while the influence of root growth rate dominated early in the  
38 growing season.

39

## 40 **1 Introduction**

41 Soil water movement forms the central physical process in the land surface models  
42 (LSMs), interacting with surface infiltration, evaporation, root extraction and  
43 underground water recharge. Accurate description of this process is necessary for the  
44 application of LSMs to achieve efficient and optimum water resources management.  
45 While it has been widely accepted that water vapor and heat transport should be  
46 incorporated in a soil water model, especially in arid or semi-arid environments  
47 (Bittelli et al., 2008; Saito et al., 2006; Zeng et al., 2009a, b, 2011a, b), it is still not  
48 clear how these factors affect soil water dynamics in crop fields.

49 ET plays a critical role in the process of soil water movement, as it controls the water  
50 distribution of surface and root zone soil layers through soil evaporation and  
51 transpiration. A common procedure to estimate ET is the so-called indirect ET method  
52 ( $ET_{ind}$ ), which transfers the reference crop evapotranspiration ( $ET_0$ ) into actual crop  
53 evapotranspiration ( $ET_c$ ) using a simple multiplicative crop factor. Recent theoretical  
54 developments allow the adoption of a more robust Penman-Monteith (PM) equation  
55 description of ET. The direct ET method ( $ET_{dir}$ ) is a one-step calculation procedure,

56 which expresses the stomatal and aerodynamic controls in terms of various resistances  
57 in the PM equation. Independent from land surface models (LSMs), much effort has  
58 been made to compare the performances of different approaches to estimate ET  
59 (Federer et al., 1996; Stannard, 1993). The performance of different ET equations  
60 varies with the characteristics of land cover and climate (Shuttleworth and Wallace,  
61 2009; Zhou et al., 2007). Ershadi et al. (2015) highlight the need for guidance in  
62 selecting the appropriate ET method for use in a specific region.

63 Further evaluation confirms that different ET methods can significantly affect the  
64 performance of LSMs (Anothai et al., 2013; Chen et al., 2013; Federer et al., 1996;  
65 Kemp et al., 1997; Mastrocicco et al., 2010). Vörösmarty et al. (1998) made a  
66 comparison between reference surface and surface cover-dependent potential ET  
67 (PET<sub>r</sub> and PET<sub>s</sub>, respectively) methods in a global-scale water balance model (WBM)  
68 and concluded that WBM simulations were highly sensitive to the PET method used  
69 and that the PET<sub>s</sub> method would produce quite reasonable estimates of actual ET over  
70 a broad geographic domain. Recent assessment of the HYDRUS-1D model with  
71 different ET methods indicated that using the PM equation gave a better model  
72 performance in simulating soil water content (Mastrocicco et al., 2010). However,  
73 most of this research only evaluates model performance for an individual variable (e.g.  
74 soil water content or ET) or neglects the heat or vapor transport effect (Anothai et al.,  
75 2013; Kemp et al., 1997; Vörösmarty et al., 1998).

76 In addition, uncertainties of crop growth parameters are not fully tested despite having  
77 a significant influence on model performance (Federer et al., 2003). Previous studies  
78 generally based conclusions on the combined analysis of the entire growing season  
79 (Padilla et al., 2011). However, these results could be inappropriate to some extent.  
80 Unlike soil properties, crop growth parameters are significantly affected by a  
81 changing environment during the growing season (Teuling et al., 2006). A roughly  
82 seasonal assessment would conceal the crop modulating mechanism associated with a  
83 changing environment.

84 The objectives of this study are twofold: i) comparing with observations of obtained

85 through a lysimeter experiment, we investigate how different methods for measuring  
86 ET will affect the assessment of soil water dynamics in a crop field located in a  
87 semi-arid environment in Northwest China, based on a coupled model considering  
88 transfer of water, vapor and heat in the soil; ii) with the calibrated coupled model, a  
89 sensitivity analysis is conducted to explore the influence of crop growth parameters  
90 on the ET partitioning. In the following section, the field experiment, data collection  
91 and the numerical models will be introduced. The results are discussed in section 3.  
92 The summary and conclusions are presented in section 4.

## 93 **2 Materials and methods**

### 94 **2.1 Field experiment**

95 The lysimeter experiment was conducted at the Yangling Irrigation Experiment  
96 Station located in Northwest China (34°17'N, 108°04'E, at an elevation of 521m a.s.l.).  
97 The experimental site is located in a semi-arid to sub-humid climatic region with a  
98 mean annual precipitation of 630mm and a mean annual air temperature of 12.9 °C.  
99 The soil at the location is silt clay loam with a field capacity of 23.5% and bulk  
100 density of 1.35 g cm<sup>-3</sup>. Groundwater level is at least 50m below the soil surface (Kang  
101 et al., 2001), thus the capillary rise from groundwater can be neglected in the current  
102 study.

103 The lysimeter is made of steel and is 3 by 2.2 by 3m (length, width and depth,  
104 respectively) in size. It contains a filter layer, a weighing facility and a drainage  
105 system for measuring the amount of deep percolation at the bottom of the lysimeter.  
106 Weight data generated by the weighing system and drainage system were stored in the  
107 datalogger. The data collector was programmed to record weight readings hourly with  
108 a precision of 139g (i.e. 0.021mm of water) for the weighing system and 1g for the  
109 drainage system, respectively. In order to be able to apply irrigation water, the steel  
110 wall rises 5cm above the ground surface. A detailed drawing of the lysimeter is  
111 presented in **Fig.1**. A mobile rainproof shelter was installed above the lysimeter to  
112 control precipitation. Summer maize was sown 23 June 2013 and harvested 2 October

113 2013 with a plant population of 40 plants within an area of 6.6 m<sup>2</sup>. Irrigation was  
114 applied when the soil water content dropped below a pre-set limit (i.e. 60% of the  
115 field capacity). The level of irrigation was set to replace crop water consumed since  
116 the previous irrigation, as measured by the lysimeter. Two supplemental irrigations  
117 were applied in the early growing season (DOY 178 and 184) to ensure uniform  
118 growth of the summer maize.

## 119 **2.2 Data collection**

120 Soil moisture and temperature were measured using the pre-calibrated sensors, which  
121 were installed at depths of 20, 40, 60, 80, 100, 200, 225, and 250 cm. The type of soil  
122 moisture sensors used was ThetaProbe ML2x (Delta-T Devices Ltd, Cambridge, UK),  
123 which specifies a range of 0 to 100% volumetric water content, and 1% and 2%  
124 precision for temperatures between 0-40°C and 40-70°C, respectively. Soil  
125 temperature was measured by QYWD100, made by Xi'An QingYuan Measurement &  
126 Control Technology Co. Ltd. , with a range from -30 to 50°C; and a higher than 1°C  
127 accuracy. Hourly measurements were taken throughout the growing season.  
128 Considering the possibility of damage caused by tillage and other agricultural  
129 management, soil moisture and temperature sensors were not placed in the top soil  
130 layers. Top soil water content was measured using the gravimetric method weekly.  
131 Crop ET was determined using the lysimeter weighting system (with an accuracy of  
132 0.021 mm). The ET measurements were taken hourly and summed to daily values  
133 during the growing season. The micro-lysimeter, with a diameter of 12cm, a depth of  
134 20cm, and containing a small isolated volume of bare soil, was placed between two  
135 crop rows (**Fig.1**). Soil evaporation (E) was measured by weighing the  
136 micro-lysimeter at 8:00 a.m. daily. After significant precipitation or irrigation, we  
137 replaced the soil in the micro-lysimeter to keep the soil moisture in the  
138 micro-lysimeter similar to that of surrounding field. Changes in the weight of the  
139 micro-lysimeter were assumed to be equivalent to the amount of water evaporated  
140 from the soil surface (Boast and Robertson, 1982). The source of error inherent in the  
141 micro-lysimeter method was discussed and some recommendations for the use of the

142 micro-lysimeter were made in our study area (Kang et al., 2003; Wang et al., 2007).  
143 Meteorological data were obtained from a standard weather station located inside the  
144 experimental site. The data included daily maximum and minimum air temperature,  
145 air humidity, daily precipitation, hours of sun, and wind speed at 10m height. Hourly  
146 values of air temperature, air humidity and wind speed were generated from daily  
147 measurements using a trigonometric function, of which a detailed description can be  
148 found in Saito et al. (2006).

149 Leaf stomatal conductance was measured using portable photosynthesis equipment  
150 (LI-6400, Li-Cor, USA) a few days after irrigation. Measurements were taken from  
151 three functional leaves at time intervals between 10:00-14:00 local time, when the  
152 stomatal conductance of summer maize reached its peak and remained steady (Zhang  
153 et al., 2011). Leaf area and plant height were measured, based on the average of at  
154 least 3 plant samples, at intervals of 7-10 days starting at 14 days after planting. The  
155 crop stages or phenology were assessed according the recommendations by Allen et al.  
156 (1998). Dates for each crop development phase are shown in **Table 1**.

## 157 **2.3 Numerical Model**

158 The STEMMUS (Simultaneous Transfer of Energy, Mass and Momentum in  
159 Unsaturated Soil) model was used to simulate coupled liquid water, water vapor and  
160 heat flow in unsaturated soil. In order to use STEMMUS for the lysimeter experiment,  
161 a macroscopic root water uptake module was incorporated into the STEMMUS  
162 model.

### 163 **2.3.1 STEMMUS**

164 In STEMMUS, the extended version of Richards (1931) equation with modifications  
165 made by Milly (1982) was numerically solved to consider the vertical interactive  
166 process between atmosphere and soil. The governing equation of the liquid and vapor  
167 flow can be expressed as:

$$\frac{\partial}{\partial t}(\rho_L \theta_L + \rho_V \theta_V) = -\frac{\partial q_L}{\partial z} - \frac{\partial q_V}{\partial z} - S \quad (1)$$

168 where  $\rho_L$  and  $\rho_V$  ( $\text{kg m}^{-3}$ ) are the density of liquid water and water vapor, respectively;  
 169  $\theta_L$  and  $\theta_V$  ( $\text{m}^3 \text{m}^{-3}$ ) are the volumetric water content (liquid and vapor, respectively);  $z$   
 170 (m) is the vertical space coordinate;  $q_L$  and  $q_V$  ( $\text{kg m}^{-2} \text{s}^{-1}$ ) are the soil water fluxes of  
 171 liquid water and water vapor (positive upwards), respectively; and  $S$  ( $\text{s}^{-1}$ ) is the sink  
 172 term for the root water extraction.

173 The liquid water flux, separated into isothermal  $q_{Lh}$  (pressure head driven) and  
 174 thermal  $q_{LT}$  (temperature driven), is described as:

$$q_L = q_{Lh} + q_{LT} = -\rho_L K_{Lh} \left( \frac{\partial h}{\partial z} + 1 \right) - \rho_L K_{LT} \frac{\partial T}{\partial z} \quad (2)$$

175 where  $K_{Lh}$  ( $\text{m s}^{-1}$ ) and  $K_{LT}$  ( $\text{m}^2 \text{s}^{-1} \text{ } ^\circ\text{C}^{-1}$ ) are the isothermal and thermal hydraulic  
 176 conductivities, respectively;  $h$  (m) is the pressure head; and  $T$  ( $^\circ\text{C}$ ) is the soil  
 177 temperature.

178 The water vapor flux, separated into isothermal  $q_{Vh}$  (pressure head driven) and thermal  
 179  $q_{VT}$  (temperature driven), is described as:

$$q_V = q_{Vh} + q_{VT} = -D_{Vh} \frac{\partial h}{\partial z} - D_{VT} \frac{\partial T}{\partial z} \quad (3)$$

180 where  $D_{Vh}$  ( $\text{kg m}^{-2} \text{s}^{-1}$ ) is the isothermal vapor conductivity; and  $D_{VT}$  ( $\text{kg m}^{-1} \text{s}^{-1} \text{ } ^\circ\text{C}^{-1}$ ) is  
 181 the thermal vapor diffusion coefficient, presented in Zeng et al. (2011a).

182 The root water uptake term described by Feddes et al. (1978) is

$$S(h) = \alpha(h) S_p \quad (4)$$

183 where  $\alpha(h)$  (dimensionless) is the reduction coefficient related to soil water potential;  
 184 and  $S_p$  ( $\text{s}^{-1}$ ) is the potential water uptake rate.

$$S_p = b(x) T_p \quad (5)$$

185 where  $b(x)$  is the normalized water uptake distribution, which describes the vertical  
 186 variation of the potential extraction term,  $S_p$ , over the root zone, as described in

187 Šimůnek et al. (2008).

188  $T_p$  is the potential transpiration. Following De Vries (1958)'s work, the heat transport  
189 function in unsaturated soil can be expressed as

$$\begin{aligned} & \frac{\partial}{\partial t} [(\rho_s \theta_s C_s + \rho_L \theta_L C_L + \rho_V \theta_V C_V)(T - T_r) + \rho_V \theta_V L_0] - \rho_L W \frac{\partial \theta_L}{\partial t} \\ & = \frac{\partial}{\partial z} (\lambda_{eff} \frac{\partial T}{\partial z}) - \frac{\partial q_L}{\partial z} C_L (T - T_r) - \frac{\partial q_V}{\partial z} [L_0 + C_V (T - T_r)] - C_L S (T - T_r) \end{aligned} \quad (6)$$

190 where  $C_s$ ,  $C_L$  and  $C_V$  ( $\text{J kg}^{-1} \text{ }^\circ\text{C}^{-1}$ ) are the specific heat capacities of solids, liquid and  
191 water vapor, respectively;  $\rho_s$  ( $\text{kg m}^{-3}$ ) is the density of solids;  $\theta_s$  is the volumetric  
192 fraction of solids in the soil;  $T_r$  ( $^\circ\text{C}$ ) is the arbitrary reference temperature;  $L_0$  ( $\text{J kg}^{-1}$ ) is  
193 the latent heat of vaporization of water at temperature  $T_r$ ;  $W$  ( $\text{J kg}^{-1}$ ) is the differential  
194 heat of wetting (the amount of heat released when a small amount of free water is  
195 added to the soil matrix); and  $\lambda_{eff}$  ( $\text{W m}^{-1} \text{ }^\circ\text{C}^{-1}$ ) is the effective thermal conductivity of  
196 the soil.

197 Dry air transport in unsaturated soil is originally taken into account in STEMMUS,  
198 and the balance equation can be written (Thomas and Sansom, 1995) as

$$\frac{\partial}{\partial t} [\varepsilon \rho_{da} (S_a + H_c S_L)] = \frac{\partial}{\partial t} [D_e \frac{\partial \rho_{da}}{\partial z} + \rho_{da} \frac{S_a K_g}{\mu_a} \frac{\partial P_g}{\partial z} - H_c \rho_{da} \frac{q_L}{\rho_L} + (\theta_a D_{Vg}) \frac{\partial \rho_{da}}{\partial z}] \quad (7)$$

199 where  $\varepsilon$  is the porosity;  $\rho_{da}$  ( $\text{kg m}^{-3}$ ) is the density of dry air;  $S_a$  ( $=1-S_L$ ) is the degree  
200 of air saturation in the soil;  $S_L$  ( $=\theta_L/\varepsilon$ ) is the degree of saturation in the soil;  $H_c$  is  
201 Henry's constant;  $D_e$  ( $\text{m}^2 \text{ s}^{-1}$ ) is the molecular diffusivity of water vapor in soil;  $K_g$  ( $\text{m}^2$ )  
202 is the intrinsic air permeability;  $\mu_a$  ( $\text{kg m}^{-2} \text{ s}^{-1}$ ) is the air viscosity; and  $D_{Vg}$  ( $\text{m}^2 \text{ s}^{-1}$ ) is  
203 the gas phase longitudinal dispersion coefficient. Note that the effects of dry air  
204 movement are not considered in the current study.

### 205 **2.3.2 Initial and boundary conditions**

206 In general, the soil surface water flow boundary can be characterized as a flux-type  
207 boundary controlled by atmospheric forcing, including soil evaporation, precipitation



208 and irrigation.

$$(q_L + q_V)|_{z=0} = E_s - \rho_L(P + I) \quad (8)$$

209 where  $E_s$  ( $\text{kg m}^{-2} \text{s}^{-1}$ ) is the actual soil evaporation rate;  $P$  and  $I$  ( $\text{m s}^{-1}$ ) are  
210 precipitation and irrigation rate, respectively.

211 After intense irrigation or precipitation, ponding would occur at the soil surface, with  
212 the surface boundary thus changing into a pressure-type boundary. It was assumed  
213 that surface runoff at the study site was negligible and that the maximum height of the  
214 surface ponding layer was 5cm in accordance with the lysimeter structure (**Fig.1**).  
215 Since there is a filter layer at the bottom of the soil profile (**Fig.1**), saturated water can  
216 be easily drained out of the lysimeter. The bottom boundary was considered a seepage  
217 face condition (Šimůnek et al., 2008). The soil surface temperature deduced from the  
218 in-situ measurements was used as upper boundary condition for heat transfer, and the  
219 bottom temperature was used as lower boundary condition. The initial soil moisture  
220 and temperature profile could be determined by interpolating the measured values at  
221 the starting date.

### 222 **2.3.3 Transpiration and soil evaporation**

223 (1) Calculation of the  $ET_{\text{ind}}$  method

224 Two different parameterizations of ET components are adopted in land surface  
225 models. A common procedure is based on reference crop evapotranspiration ( $ET_0$ ),  
226 which is then partitioned into soil evaporation and transpiration using crop factors  
227 (Feddes et al., 1974; Šimůnek et al., 2008; Wu et al., 1999), and noted as the  $ET_{\text{ind}}$   
228 method.

$$ET_0 = \frac{0.408(R_n - G) + \gamma \frac{900}{T_a + 273} u_2 (e_s - e_a)}{\Delta + \gamma(1 + 0.34u_2)} \quad (9)$$

229 where  $ET_0$  ( $\text{mm day}^{-1}$ ) is the reference ET;  $R_n$  ( $\text{MJ m}^{-2} \text{day}^{-1}$ ) is the net radiation at the  
230 crop surface;  $G$  ( $\text{MJ m}^{-2} \text{day}^{-1}$ ) is the soil heat flux density;  $T_a$  ( $^{\circ}\text{C}$ ) is the air

231 temperature at 2m height;  $u_2$  ( $\text{m s}^{-1}$ ) is the wind speed at 2m height (which can be  
 232 obtained from wind speed data at 10m height using a logarithmic wind profile  
 233 function);  $e_a$  and  $e_s$  (kPa) are the actual and saturation vapour pressure, respectively;  $\Delta$   
 234 ( $\text{kPa } ^\circ\text{C}^{-1}$ ) is the slope of the vapor pressure curve;  $\gamma$  ( $\text{kPa } ^\circ\text{C}^{-1}$ ) is the psychrometric  
 235 constant.

236 The potential transpiration ( $T_p$ ) can be estimated by multiplying  $ET_0$  with the crop  
 237 basal coefficient  $K_{cb}$ , describing the difference between actual and reference crop  
 238 surface.

$$T_p = K_{cb}ET_0 \quad (10)$$

239 Several research studies have related  $K_{cb}$  to the dynamics of vegetation (Er-Raki et al.,  
 240 2007; González-Dugo and Mateos, 2008; Sánchez et al., 2012). The general  
 241 expression defined by Duchemin et al. (2006) is

$$K_{cb} = K_{cb,max} (1 - \exp(-\tau LAI)) \quad (11)$$

242 where  $\tau$  is the extinction coefficient, set at 0.6 (Kemp et al., 1997). Although  $\tau$  may  
 243 change slightly in response to structural differences in crop development (Allen et al.,  
 244 1998; Tahiri et al., 2006), it is convenient to consider  $\tau$  as a constant (Allen et al.,  
 245 1998; Shuttleworth and Wallace, 1985; Zhou et al., 2006).  $K_{cb,max}$  is the basal crop  
 246 coefficient at effective full ground cover.

247 Instead of the evaporation coefficient used in FAO dual  $K_c-ET_0$ , we adopted a simple  
 248 evaporation parameterization similar to in other studies (Feddes et al., 1974; Kemp et  
 249 al., 1997; Wu et al., 1999), in which the potential soil evaporation is given by Ritchie  
 250 (1972)

$$E_p = \frac{\Delta}{\lambda(\Delta + \gamma)} R_n \exp(-0.39 LAI) \quad (12)$$

251 where  $\lambda$  ( $\text{MJ kg}^{-1}$ ) is the latent heat of vaporization. Actual soil evaporation can be  
 252 achieved using a simple relationship proposed by Linacre (1973) and verified by  
 253 Kemp et al. (1997) for bare soil. Three successive stages are arbitrarily divided into:

$$E_s = E_p \quad (\theta_1 / \theta_{1,Fc}) > (E_p / k)^{1/2}, h_1 > -100000cm$$

$$E_s = k(\theta_1 / \theta_{1,Fc})^m \quad (\theta_1 / \theta_{1,Fc}) \leq (E_p / k)^{1/2}, h_1 > -100000cm \quad (13)$$

$$E_s = k(\theta_{1+2} / \theta_{1+2,Fc})^m \quad h_1 \leq -100000cm$$

254 where  $\theta_l$  and  $\theta_{l, Fc}$  are the actual volumetric water content and water content at field  
 255 capacity of the top soil layer, respectively;  $h_l$  (cm) is the water potential of the top soil  
 256 layer;  $k$  and  $m$  are parameters primarily dependent on soil depth and soil texture,  
 257 varying from 0.8 to 1 and 2 to 2.3, respectively, for a soil depth of 10 to 20cm;  $\theta_{l+2}$   
 258 and  $\theta_{l+2, Fc}$  are the actual volumetric water content and water content at field capacity  
 259 of the top 1st and 2nd soil layers, respectively.

260 (2) Calculation of the  $ET_{dir}$  method

261 The second method used is a one-step calculation of actual soil evaporation and  
 262 potential transpiration by incorporating canopy minimum surface resistance and actual  
 263 soil resistance into the Penman-Montieth model. LAI is implicitly used to partition  
 264 available energy into canopy and soil. We call it the  $ET_{dir}$  method. Contrary to an  
 265 alternative approach proposed by Shuttleworth and Wallace (1985), the interactive  
 266 effect between canopy and soil was assumed negligible in the  $ET_{dir}$  method. This  
 267 simplification seemed reasonable, as Kemp et al. (1997) indicated that no significant  
 268 difference in simulating transpiration and soil evaporation was found for both  
 269 methods.

$$T_p = \frac{\Delta(R_n^c - G) + \rho_a c_p \frac{(e_s - e_a)}{r_a^c}}{\lambda(\Delta + \gamma(1 + \frac{r_{cmin}}{r_a^c}))} \quad (14)$$

$$E_s = \frac{\Delta(R_n^s - G) + \rho_a c_p \frac{(e_s - e_a)}{r_a^s}}{\lambda(\Delta + \gamma(1 + \frac{r_s}{r_a^s}))} \quad (15)$$

270 where  $R_n^c$  and  $R_n^s$  ( $\text{MJ m}^{-2} \text{ day}^{-1}$ ) are the net radiation at the canopy surface and soil  
 271 surface, respectively;  $\rho_a$  ( $\text{kg m}^{-3}$ ) is the air density;  $c_p$  ( $\text{J kg}^{-1} \text{ K}^{-1}$ ) is the specific  
 272 heat capacity of air;  $r_a^c$  and  $r_a^s$  ( $\text{s m}^{-1}$ ) are the aerodynamic resistance for canopy  
 273 surface and bared soil, respectively;  $r_{cmin}$  ( $\text{s m}^{-1}$ ) is the minimum canopy surface  
 274 resistance; and  $r_s$  ( $\text{s m}^{-1}$ ) is the soil surface resistance.

275 The net radiation reaching the soil surface can be calculated using the Beer's law:

$$R_n^s = R_n^c \exp(-\tau LAI) \quad (16)$$

276 And the net radiation intercepted by the canopy surface is the residual part of total net  
 277 radiation

$$R_n^c = R_n^c (1 - \exp(-\tau LAI)) \quad (17)$$

278 The minimum canopy surface resistance  $r_{cmin}$  is given by

$$r_{cmin} = r_{lmin} / LAI_{eff} \quad (18)$$

279 where  $r_{lmin}$  is the minimum leaf stomatal resistance;  $LAI_{eff}$  is the effective leaf area  
 280 index, which considers that generally the upper and sunlit leaves in the canopy  
 281 actively contribute to the heat and vapor transfer.

282 The soil surface resistance can be estimated using an exponential form proposed by  
 283 Van De Griend and Owe (1994),

$$\begin{aligned} r_s &= r_{sl} & \theta_1 > \theta_{min}, h_1 > -100000cm, \\ r_s &= r_{sl} e^{a(\theta_{min} - \theta_1)} & \theta_1 \leq \theta_{min}, h_1 > -100000cm \\ r_s &= \infty & h_1 \leq -100000cm \end{aligned} \quad (19)$$

284 where  $r_{sl}$  ( $10 \text{ s m}^{-1}$ ) is the resistance to molecular diffusion of the water surface;  $a$   
 285 ( $0.3565$ ) is the fitted parameter;  $\theta_1$  is the topsoil water content;  $\theta_{min}$  is the minimum  
 286 water content above which soil is able to deliver vapor at a potential rate.

## 287 **2.4 Model Parameters**

### 288 **2.4.1 Soil property parameters**

289 Van Genuchten's analytical model (Van Genuchten, 1980) was used to simulate the  
290 soil moisture retention curve, which describes the relationship between soil water  
291 potential and water content. Soil samples of the top 20cm were taken to obtain the  
292 parameters for the moisture retention curve.

293 Soil saturated hydraulic conductivity could be determined at the laboratory, and was  
294  $10.50 \text{ cm d}^{-1}$ . This value is lower than the value recommended by Saxton et al. (1986)  
295 value for silt clay loam ( $13.60 \text{ cm d}^{-1}$ ), but is within the range of  $10.30$  to  $14.30 \text{ cm d}^{-1}$ ,  
296 given by Wang et al. (2008) for the local soil. The soil hydraulic and thermal  
297 properties are presented in **Table 2**.

### 298 **2.4.2 Crop growth parameters**

299 LAI was determined using the measured leaf area. To simulate the seasonal dynamics  
300 in LAI, a linear interpretation was used between dates from the emergence to the first  
301 measurement and a simple quadratic function presented a good fit for the LAI  
302 measurements ( $R^2=0.96$ ) (**Fig. 2a**). The effective leaf area index ( $LAI_{eff}$ ), used in the  
303  $ET_{dir}$  method, was equal to the actual LAI where the LAI was lower than  $2 \text{ m}^2 \text{ m}^{-2}$ ,  
304 was assumed to be half the actual LAI for actual LAI values above  $4 \text{ m}^2 \text{ m}^{-2}$  and equal  
305 to  $2 \text{ m}^2 \text{ m}^{-2}$  where actual LAI values ranged between  $2$  to  $4 \text{ m}^2 \text{ m}^{-2}$  (Tahiri et al.,  
306 2006).

307 Maximum rooting depth was set to  $1.2\text{m}$ , in accordance with Allen et al. (1998). A  
308 classical logistic growth function was used to estimate root growth dynamics  
309 throughout the growing season, in which the root growth rate was determined from  
310 the assumption that 50% of the rooting depth would be reached after 50% of the  
311 growing season had elapsed, as described in Šimůnek et al. (2008) (see **Fig. 2c** for the  
312 root growth dynamics). The normalized water uptake distribution  $b(x)$ , which  
313 describes the vertical variation of the potential extraction term,  $S_p$ , over the root zone

314 was determined following Šimůnek et al. (2008).

315 A piecewise linear function, defined in Feddes et al.(1978) and Feddes and Roats  
316 (2004), was used to describe the response of root to soil water potential  $\alpha(h)$ . The  
317 input water potential parameters were: i) -15 cm for the water potential below which  
318 roots start to extract water; ii) -30 cm for the water potential below which roots extract  
319 water at the maximum possible rate; iii) higher limit -325 cm and lower limit -600 cm  
320 for the limiting water potential values below which roots can no longer extract water  
321 at the maximum rate (assuming a potential transpiration rate of 0.5 and 0.1 cm d<sup>-1</sup>,  
322 respectively); iv) -15000 cm for the water potential below which root water uptake  
323 ceases.

## 324 **2.5 Numerical Simulations and Experiments**

325 The extended STEMMUS model was run using both the ET<sub>ind</sub> method and the ET<sub>dir</sub>  
326 method. Coupled water flow and heat transport equations were numerically solved  
327 using the Galerkin's finite element method for the spatial discretization and using a  
328 fully implicit, backward difference approach for the temporal discretization. Plant root  
329 water uptake and soil water flow were fully coupled and equations were solved  
330 simultaneously at the same time step. The soil profile considered in this study had a  
331 depth of 3m, equal to that of the large lysimeter, and was divided into 38 nodes with a  
332 finer discretization in the upper soil layers (1cm) than in the lower soil layers (20cm).  
333 The large lysimeter measurements, including soil moisture, soil temperature, ET and  
334 soil evaporation were used to assess model performance. The validation of the soil  
335 water balance closure within the root zone gave an additional test of the effectiveness  
336 of the extended STEMMUS. In addition, since the estimation of crop growth  
337 parameters could harbor uncertainties, a sensitivity test was implemented to explore  
338 how the simulation results varied with fluctuating precipitation and irrigation under  
339 different crop growth scenarios.

### 340 **2.5.1 Water balance closure**

341 The water balance closure was implemented by comparing soil water storage using  
342 two different methods. The direct method was based on the summation of soil water  
343 content over the root-zone

$$V_t = \sum_{rz} \Delta x_i \frac{\theta_i + \theta_{i+1}}{2} \quad (20)$$

344 where  $V_t$  is the soil water storage in the root zone at time  $t$ ;  $\Delta x_i$  is the thickness of the  
345  $i$ th soil layer;  $\theta_i$  and  $\theta_{i+1}$  are model simulations of water content at the upper and  
346 lower surface, respectively, of the  $i$ th soil layer, at time  $t$ ;  $\sum_{rz}$  represents the  
347 summation over the root zone.

348 Soil water storage could also be derived by the inversion of the water balance  
349 equation within the root-zone

$$V_t = V_0 - \int_0^t T_c dt + \int_0^t (q_0 - q_N) dt \quad (21)$$

350 where  $V_0$  is the soil water storage in the root zone at the initial time, calculated by the  
351 integration of the initial soil moisture over the root zone;  $T_c$  is the actual crop  
352 transpiration, derived from the integration of root water uptake over the root zone;  $q_0$   
353 and  $q_N$  are the simulated water fluxes at the surface and base of the root zone,  
354 respectively.

### 355 **2.5.2 Crop growth scenarios**

356 To investigate how biological factors control shallow soil water dynamics, three  
357 additional crop growth scenarios were used: i) a changed leaf area index, ii) a changed  
358 maximum rooting depth ( $Z_{rmax}$ ), and iii) a changed root growth rate ( $R_{gr}$ ) scenario. The  
359 reference scenario (REF) was compared with these changed LAI ( $LAI/LAI_{ref}$ ),  $Z_{rmax}$ ,  
360 and  $R_{gr}$  ( $Z_r/Z_{r\_ref}$ ) scenarios to demonstrate the impact changes in biological factors  
361 may have. To select values for these three growth parameters their reference values  
362 were either increased or decreased by 20%. The influence of such a 20% increase and

363 decrease in LAI,  $Z_{rmax}$ , and  $R_{gr}$  is shown in **Fig. 2**. The influence of a 20% increase in  
364 the LAI on the relative  $LAI_{eff}$  encompassed three stages: i) a constant 1.2 times  
365 enlarged stage, ii) a constantly equal stage, and iii) a transition stage (**Fig. 2b**). The  
366 influence of a 20% decrease in the LAI depicted a similar three-stage trend. However,  
367 the 20% decreased LAI scenario (**Fig. 2b**, dash grey line) entered stage (ii), i.e. the  
368 constantly equal stage, later in the leaf growing stage and earlier in the leaf senescing  
369 stage, than the 20% increased LAI scenario (**Fig. 2b**, solid grey line) did. Compared  
370 to the reference root depth dynamics, the relative values of root depth ( $Z_r / Z_{r\_ref}$ ) of the  
371 20% increased  $Z_{rmax}$  scenario, increased gradually until it reached its maximum value  
372 late in the growing season. In the 20% increased  $R_{gr}$  scenario, the  $Z_r / Z_{r\_ref}$   
373 demonstrated a rapid increase up to a maximum value and then dropped down during  
374 the late growing season. On the other hand, a 20% decrease in  $Z_{rmax}$  and  $R_{gr}$  showed  
375 opposite trends to the 20% increase on the relative root depth dynamics. A 20%  
376 decreased  $R_{gr}$  showed a lag effect for the  $Z_r / Z_{r\_ref}$ , compared to the 20% increased  $R_{gr}$   
377 (**Fig. 2d**). In other words, the values of  $Z_r / Z_{r\_ref}$  for the 20% decreased  $R_{gr}$  scenario  
378 were lower early in the growing season (before around DOY 196) and higher late in  
379 the growing season (after around DOY 196) than for the 20% increased  $R_{gr}$  scenario.

## 380 2.6 Performance Matrixes

381 To assess the model performance, several performance matrixes were used similar to  
382 in previous studies (Wei et al., 2015; Zhao et al., 2013). The determination coefficient  
383  $R^2$ , achieved by performing a linear regression between observed and model simulated  
384 values; the root mean square error (RMSE), characterizing the variance of the model  
385 errors; as well as the index of agreement (d-index) (Willmott, 1981; Willmott et al.,  
386 1985) have been computed as follows:

$$RMSE = \sqrt{\frac{\sum_{i=1}^n (P_i - O_i)^2}{n}} \quad (22)$$



$$R^2 = \frac{\left[ \sum_{i=1}^n (P_i - \bar{P})(O_i - \bar{O}) \right]^2}{\sum_{i=1}^n (P_i - \bar{P})^2 \sum_{i=1}^n (O_i - \bar{O})^2} \quad (23)$$

$$d = 1 - \frac{\sum_{i=1}^n (P_i - O_i)^2}{\sum_{i=1}^n (|P_i - \bar{P}| + |O_i - \bar{O}|)^2} \quad (24)$$

387 where  $n$  is the number of observations,  $P_i$  and  $O_i$  are pairs of observed and model  
 388 predicted values for a specific variable (soil water content, ET, etc.),  $\bar{P}$  and  $\bar{O}$  are  
 389 the overall mean of observed and model predicted values. Good agreement between  
 390 observed and model predicted values is characterized by a high value for both the  
 391 determination coefficient and the d-index, and a low value for the RMSE.

### 392 **3 Results and discussion**

#### 393 **3.1 Soil water content**

394 Simulated soil water content, based on two ET methods, was compared with  
 395 observations at soil depths of 20cm, 40cm, 60cm, 80cm and 100cm (**Fig. 3**). The soil  
 396 water content at 20cm derived from the ET<sub>ind</sub> method was in good agreement with the  
 397 observation. Though slight underestimation occurred in the initial stage, the effects of  
 398 incoming water flux (precipitation and irrigation) on soil water dynamics were well  
 399 represented, as evidenced by a d-index of 0.81 and RMSE of 0.017 cm<sup>3</sup> cm<sup>-3</sup>. For the  
 400 deeper soil layers, however, the sensor-observed fluctuations in soil water content  
 401 were much smaller than the simulated values, thus inducing large discrepancies. The  
 402 d-index values ranged from 0.26 to 0.66 and the RMSE ranged from 0.019 to 0.025  
 403 cm<sup>3</sup> cm<sup>-3</sup> for soil depths of 40cm to 100cm.

404 The results for soil water content simulated employing the ET<sub>dir</sub> method were similar  
 405 to those based on the ET<sub>ind</sub> method (**Fig. 3**). However, owing to more  
 406 underestimation, the model based on the ET<sub>dir</sub> method performed a little worse than

407 the model based on the  $ET_{ind}$  method. The d-index values ranged from 0.20 to 0.73  
408 and the RMSE ranged from 0.020 to 0.036  $cm^3 cm^{-3}$  for the soil depths of 20cm to  
409 100cm.

410 For both ET methods, the extended STEMMUS model underestimated soil water  
411 content early in the growing season. From the point of water balance, this  
412 underestimation may be explained by more soil water consumption mainly due to  
413 topsoil evaporation, indicating that both ET methods overestimated soil evaporation  
414 early in the growing season. The other possible reason was that too little irrigation  
415 was applied during this period to obtain uniform distribution, resulting in single-point  
416 soil moisture observation losing its ability to represent the heterogeneous soil  
417 moisture variations. Such underestimation disappeared when a large amount of water  
418 was applied late in the growing season (**Fig. 3, 20cm**).

419 The discrepancies increased with soil depth for both ET methods. The reason may be  
420 twofold. On the one hand, the soil moisture observations were doubtful, as, with  
421 irrigation, no significant fluctuation occurred at the deeper soil layers, which was also  
422 inconsistent with other results for the same experimental site (Kang et al., 2001). The  
423 unreliable observations may be linked to the positioning of the soil moisture sensors  
424 (either installed at positions dominated by preferential flow or adjacent to  
425 macropores). On the other hand, the assumption of a homogeneous soil texture was  
426 inappropriate, as was discussed in previous studies (Zeng et al., 2011a). Soil hydraulic  
427 parameters controlled the liquid water flux partitioning through the soil layers. A  
428 larger infiltration rate could result in greater fluctuation in soil water content at deeper  
429 soil layers.

### 430 **3.2 Root zone water balance**

431 Applying equations (20) and (21), simulated soil water storage based on the  
432 integration of soil water content and the inversion of the water balance equation over  
433 the root-zone, using two ET methods, are compared in **Fig. 4**. Soil water storage  
434 calculated both ways agreed well for the  $ET_{ind}$  method. The value of the RMSE was

435 5.88 mm and the d-index value was 0.98. Similarly, good agreement was found using  
436 the  $ET_{dir}$  method with values for the RMSE and the d-index equaling 5.13mm and  
437 0.99, respectively. Overall, the results based on the performance matrixes and the  
438 visual comparison of soil water storage dynamics revealed that the numerical solution  
439 using both the  $ET_{ind}$  and  $ET_{dir}$  method effectively reproduced the closure of the water  
440 balance even under dramatically changed surface boundary flux conditions.

441 Simulated results using two ET methods showed similar trends in soil water storage  
442 throughout the growing season (**Fig. 4**). As expected, the greatest increases occurred  
443 after large irrigations. Using the  $ET_{dir}$  method tended to result in lower soil water  
444 storage than using the  $ET_{ind}$  method. Differences between the two ET methods  
445 generally increased with drying of the soil.

### 446 **3.3 Soil temperature**

447 **Figure 5** presents the dynamics of sensor-observed and the simulated soil temperature  
448 using two ET methods at various soil depths. Compared to the observation, the  
449 simulation started with good agreement for both ET methods, followed by a slight  
450 overestimation after the first main irrigation. Irrigation events had a significant impact  
451 on the soil temperature simulation due to the uncertainties in soil surface temperature.  
452 Nevertheless, the seasonal variations in soil temperature could be satisfactorily  
453 portrayed with both ET methods. The overall d-index values, for soil depths of 20cm  
454 to 100cm, ranged from 0.76 to 0.95 using the  $ET_{ind}$  method and from 0.78 to 0.95  
455 using the  $ET_{dir}$  method. The RMSE values ranged from 1.19 to 1.71 °C using the  $ET_{ind}$   
456 method and from 1.14 to 1.61 °C using the  $ET_{dir}$  method for these same soil depths of  
457 20cm to 100cm.

### 458 **3.4 Estimation of ET**

459 Combined with simulation results for soil water content, accurate ET estimates could  
460 help with the visualization of soil water balance, reduce deep percolation, improve  
461 irrigation efficiency and ultimately optimize water resources management. Therefore,

462 the capability of the extended STEMMUS model with different ET methods in  
463 reproducing the dynamics of ET is of great importance and requires a thorough  
464 evaluation with observed ET data.

### 465 **3.4.1 ET at hourly time scale**

466 The performance of both ET methods in estimating the diurnal pattern of ET  
467 throughout the growing season is shown in **Fig. 6** and **Table 3**. Hourly ET rates  
468 simulated using the  $ET_{dir}$  method generally agreed well with lysimeter-observed ones  
469 (**Fig. 6**). There was no significant underestimation throughout the growing season.  
470 The results summarized in **Table 3** suggest that the main disagreement for the  $ET_{dir}$   
471 method occurred during the early growing stage. The values for the d-index were 0.90,  
472 0.96, 0.98 and 0.93 and for the RMSE were 0.10 mm h<sup>-1</sup>, 0.09 mm h<sup>-1</sup>, 0.08 mm h<sup>-1</sup>,  
473 and 0.06 mm h<sup>-1</sup> for the initial, the crop development, the mid-season and the late  
474 season growing stages, respectively.

475 Compared to the  $ET_{dir}$  method, no significant difference occurred for the  $ET_{ind}$  method  
476 when the values of ET rates were small (**Fig. 6**). However, more underestimation was  
477 found when simulating higher ET values. The greatest disagreement occurred during  
478 the initial growing stage with the values of the d-index and the RMSE being 0.84 and  
479 0.10 mm h<sup>-1</sup>, respectively, compared to 0.94 and 0.11 mm h<sup>-1</sup>, 0.93 and 0.11 mm h<sup>-1</sup>,  
480 and 0.90 and 0.07 mm h<sup>-1</sup>, respectively, during other developmental stages.

### 481 **3.4.2 ET at daily time scale**

482 Compared to lysimeter observed daily ET rates, both ET methods showed similar  
483 trends over the entire growing season (**Fig. 7**). When neglecting the effects of clouds  
484 on the net radiation, large overestimation of ET rates for both schemes occurred on  
485 some cloudy days (**Fig. 7**, DOY 196, 197, 221 and 241). Daily ET rates showed more  
486 variability when simulated with the  $ET_{dir}$  method than with the  $ET_{ind}$  method.  
487 Moreover, the crop stage-specific behavior differed between the two ET methods.  
488 There was an average underestimation with the  $ET_{ind}$  method, while a slight  
489 overestimation with the  $ET_{dir}$  method, during the initial crop development stage. Daily

490 ET rates during the mid-season stage tended to be underestimated by the  $ET_{ind}$  method,  
491 while successfully described by the  $ET_{dir}$  method. Overall, with daily simulated ET  
492 rates the  $ET_{dir}$  method performed better than the  $ET_{ind}$  method, as is indicated by the  
493 d-index and RMSE values of 0.96 and 0.74 mm d<sup>-1</sup>, respectively, for the  $ET_{dir}$  method,  
494 compared to 0.89 and 1.06 mm d<sup>-1</sup>, respectively, for the  $ET_{ind}$  method.

495 Observed soil evaporation by the micro-lysimeter was used to assess the performance  
496 of both ET methods in simulating soil evaporation (**Fig. 8**). Statistical results  
497 indicated the  $ET_{dir}$  method was in closer agreement with the observations than the  
498  $ET_{ind}$  method, with RMSE and d-index values for the  $ET_{dir}$  method being 0.51mm d<sup>-1</sup>  
499 and 0.84, respectively, compared to 0.73mm d<sup>-1</sup> and 0.64, respectively, for the  $ET_{ind}$   
500 method. Unfortunately, during the period between two supplemental irrigations in the  
501 early growing season (DOY 177-183), no soil evaporation measurements by the  
502 micro-lysimeter were available. Thus, it was difficult to form a conclusion regarding  
503 model performance during this period. Late in the growing season, both ET methods  
504 tended to underestimate daily evaporation rates after main irrigation events. This  
505 underestimation may be caused by the use of the micro-lysimeter. The observed soil  
506 evaporation may have been higher than the actual soil evaporation, since the  
507 micro-lysimeter disregarded the soil water loss due to the root water extraction in the  
508 evaporative soil layer. Similar behavior was reported for maize by Zhao et al. (2013)  
509 and Wei et al. (2015) at same latitude sites. Compared to the  $ET_{dir}$  method, using the  
510  $ET_{ind}$  method resulted in much lower values for the rate of evaporation, especially  
511 after irrigation during the initial and mid-late crop development stage (see also **Table**  
512 **4**). During these periods, the local irrigation intensified the vertical vapor gradient and  
513 the relative sparse vegetation cover highlighted the importance of the aerodynamics  
514 component. Thus, larger underestimation and less fluctuation of soil evaporation  
515 using the  $ET_{ind}$  method could be partially explained by the simplification of  
516 aerodynamic and surface resistance components in the calculation.

### 517 **3.4.3 Cumulative ET**

518 A comparison between cumulative observed ET and simulated ET, using both the

519  $ET_{ind}$  and the  $ET_{dir}$  method, is shown in **Fig. 9**. The cumulative ET observed by the  
520 lysimeter, as well as simulated using the  $ET_{ind}$  and the  $ET_{dir}$  methods, were 334.18,  
521 354.89 and 369.37mm, respectively. Both ET methods overestimated seasonal ET  
522 compared to the lysimeter observations. Two periods, i.e. crop development and late  
523 season stage, contributed to the overestimation by the  $ET_{ind}$  method. While, for the  
524  $ET_{dir}$  method, the initial and crop development stage accounted for 70% of the  
525 overestimation (**Table 4**). The deviation from the observed value of total ET was  
526 greater for the  $ET_{dir}$  method than for the  $ET_{ind}$  method, i.e. 35.18mm and 20.71mm,  
527 respectively. This nearly 15mm difference is mainly attributed to the larger amount of  
528 evaporation determined by the  $ET_{dir}$  method during the initial growth stage (**Table 4**),  
529 consequently resulting in more severe soil water depletion (**Fig. 3, 20cm**).

#### 530 **3.4.4 Characteristics of ET partitioning**

531 Crop stage-specific soil evaporation (E), plant transpiration ( $T_c$ ), evapotranspiration  
532 (ET) and evaporation fraction (E/ET, EF) are presented in **Table 4**. Similar to  
533 previous studies (Kang et al., 2003; Zhao et al., 2013), the proportion of evaporation  
534 (the evaporation fraction) was largest at the initial stage, then decreased during crop  
535 development and reached its lowest value at the mid-season stage, with a significant  
536 rebound occurring during the late season. The dynamic role of evaporation was  
537 mainly attributed to crop vegetation development (Hu et al., 2009; Liu et al., 2002).  
538 The evaporation fraction of the four development stages ranged between 24.38% and  
539 86.58% for the  $ET_{dir}$  method and between 10.31% and 81.01% for the  $ET_{ind}$  method,  
540 similar to previously published results (Paredes et al., 2015; Wei et al., 2015; Zhao et  
541 al., 2013). Some differences were found in simulating individual components of crop  
542 ET when using the two different ET methods. The  $ET_{dir}$  method showed a greater  
543 evaporation and less transpiration than the  $ET_{ind}$  method throughout the growing  
544 season, resulting in an overall larger evaporation fraction.

545 The overall evaporation fractions for the two ET methods used were 24.05% ( $ET_{ind}$ )  
546 and 36.44% ( $ET_{dir}$ ). Figures that are below the range of 43.57% to 52.52% of a 4-year  
547 field observation study in the same region that saw a significantly higher frequency of

548 wetting events (Wang et al., 2007), but close to observations by Liu et al. (2002) of  
549 30.3% and Kang et al. (2003) of 33%, and within the range of 20 % to 40 %, reviewed  
550 by Kool et al. (2014) for most of row crops.

### 551 **3.5 Crop growth scenarios**

552 To investigate the uncertainty in crop growth parameters, different crop growth  
553 scenarios, introduced in section 2.5.2, were adopted to run the STEMMUS with both  
554 ET methods (**Fig. 10**). The reference scenario (REF) was compared to the changed  
555 LAI,  $Z_{\text{rmax}}$ , and  $R_{\text{gr}}$  scenarios. The relative values (i.e.  $T_c/T_{c,\text{ref}}$  &  $\text{EF}/\text{EF}_{\text{ref}}$ ) were used  
556 here to facilitate comparisons between parameters and scenarios.

557 Under the changed LAI scenario, the dynamics of seasonal relative values of  
558 transpiration ( $T_c/T_{c,\text{ref}}$ ) formed a tradeoff between increasing LAI and decreasing soil  
559 water availability, while other factors remained unchanged throughout the growing  
560 season. **Fig. 10a** shows that, for the  $\text{ET}_{\text{ind}}$  method, the sensitivity of transpiration to  
561 LAI decreased until its value approached  $2 \text{ m}^2 \text{ m}^{-2}$ , then leveled off with both factors  
562 being of equal importance and finally elevated as soil water availability was  
563 decreasing. For the  $\text{ET}_{\text{ind}}$  method, the influence of LAI was more important in the  
564 early growing season, which is consistent with previous studies. In **Fig. 10g**, the  
565 dynamics of the relative evaporation fraction ( $\text{EF}/\text{EF}_{\text{ref}}$ ) show a trend similar to the  
566 seasonal variation of the LAI (**Fig. 2a**), indicating that small differences in soil water  
567 availability appeared to have a negligible effect on the relative evaporation fraction  
568 ( $\text{EF}/\text{EF}_{\text{ref}}$ ) over the entire growing season. The LAI dynamics could explain much of  
569 the seasonal variation in the relative EF. It is worth to note that there was an  
570 asymmetric variation in the relative EF for the same LAI disturbance, indicating that  
571 the EF was nonlinearly dependent on LAI disturbance (**Fig. 10g**).

572 With the  $\text{ET}_{\text{dir}}$  method, the relative transpiration presented more complicated behavior  
573 than with the  $\text{ET}_{\text{ind}}$  method (**Fig. 10d**). Compared to the  $\text{ET}_{\text{ind}}$  method, the  $\text{ET}_{\text{dir}}$   
574 method revealed a similar trend in the sensitivity of relative transpiration to LAI in the  
575 early growing season, when LAI dominated. More fluctuation was visible in the

576 middle season. A suppression effect appeared at the end of the growing season (i.e.  
577 increasing LAI resulted in lower transpiration). This behavior could be explained by  
578 the selection of a different LAI in estimating transpiration for the two ET methods, i.e.  
579 LAI for the  $ET_{ind}$  method, and  $LAI_{eff}$  for the  $ET_{dir}$  method (**Fig. 2a**). The response of  
580 relative EF to LAI showed similar trends early in the growing season between the  
581  $ET_{ind}$  method and the  $ET_{dir}$  method, though with less sensitivity in the  $ET_{dir}$  method.  
582 Differences were found late in the growing season with a negligible effect of LAI on  
583 the relative EF in the senescing maize (**Fig. 10j**).

584 Under the changed maximum rooting depth and root growth rate scenarios, the  
585 interactive effects of root depth dynamics and soil water availability on transpiration  
586 and the evaporation fraction were explored. Seasonal transpiration ratio was an  
587 increasing function of soil water depletion until reaching a threshold in both scenarios.  
588 The effects of changed maximum rooting depth on relative transpiration and the  
589 evaporation fraction increased, as the soil was drying. Larger sensitivity was found  
590 late in the growing stage. On the contrary, the influence of the soil drying on the  
591 sensitivity of transpiration and the evaporation fraction to root growth rate decreased  
592 until no significant effects were found when the root reached its maximum depth. The  
593 period most influenced occurred early in the growing season. This behavior can be  
594 explained by the difference in root depth dynamics in both scenarios. As shown in **Fig.**  
595 **2c** and **d**, the effect of maximum rooting depth increased until reach its maximum  
596 value late in the growing season, while the effect of root growth rate primarily  
597 dominated early in the growing season. Furthermore, there was an asymmetric  
598 variation in the relative transpiration and evaporation fraction for equal disturbance of  
599 root growth rate, with a larger variation for conditions of 20% decreased root growth  
600 rate and less variation for the increased conditions (especially at DOY 225, in **Fig.**  
601 **10c, f, i, l**). Such asymmetric variation can be explained by the lag effect described in  
602 section 2.5.2. The two ET methods differed in their variation in sensitivity to root  
603 growth parameters, with higher sensitivity observed in the  $ET_{dir}$  method with equal  
604 parameter disturbance. This is probably due to the fact that the  $ET_{dir}$  method is more



605 sensitive to soil water depletion than the  $ET_{ind}$  method (**Fig. 3**), considering  
606 aerodynamic and surface resistance.

607 Based on the crop growth scenario results, some suggestions may be presented to  
608 reduce the proportion of soil evaporation in the total evapotranspiration. Under the  
609 same irrigation and atmospheric forcing conditions, the leaf area index can be  
610 increased by properly increasing the planting density (**Fig. 10g, j**). Unlike the LAI, the  
611 sensitivity of transpiration to root growth parameters depended more on soil water  
612 depletion, which indicated that the effects of dynamic root growth parameters should  
613 not be dismissed in an arid environment. In fact, a variety of maximum rooting depth  
614 values were reported for maize previously (Canadell et al., 1996; Hsiao et al., 2009;  
615 Liu et al., 1998), due to differences in genotypes and rhizosphere environment. Under  
616 conditions of soil drying, plants tend to increase root depth to maintain a certain  
617 amount of water extraction (Hund et al., 2009; Verma et al., 2014), as evidenced in  
618 **Fig. 10b-c & e-f**.

#### 619 **4 Summary and Conclusion**

620 Together with the in situ data collected in a large lysimeter experiment in a semi-arid  
621 environment, the extended STEMMUS model facilitated the investigation of how the  
622 coupling transfer of water, vapor and heat in the soil affected soil water dynamics in a  
623 crop field, using two different evapotranspiration methods ( $ET_{ind}$  &  $ET_{dir}$ ). The  
624 simulated soil water content values based on the  $ET_{ind}$  method were in closer  
625 agreement with values measured at 20cm soil depth than values based on the  $ET_{dir}$   
626 method. However, disagreement increased in deeper soil layers, with either the  
627 inaccuracy of soil moisture observations or the heterogeneity of soil hydraulic  
628 parameters being responsible for the discrepancies and requiring further investigation.  
629 The simulation of soil temperature performed relatively well for both ET methods.

630 Evaluation of the performance of the two ET methods in estimating hourly, daily and  
631 cumulative evapotranspiration demonstrated that the  $ET_{dir}$  method performed better  
632 than the  $ET_{ind}$  method, except regarding the cumulative evapotranspiration, with the  
633  $ET_{dir}$  method displaying a 15mm higher overestimation than the  $ET_{ind}$  method,

634 compared to the lysimeter observations. Caution should be exercised in partitioning  
635 ET, because individual ET components (soil evaporation, transpiration) were not fully  
636 or accurately measured. This study suggests that the  $ET_{dir}$  method provides a better  
637 simulation of soil evaporation than the  $ET_{ind}$  method, especially late in the growing  
638 season. It confirms that aerodynamic and surface resistance terms are necessary for  
639 evaporation estimation.

640 The crop growth scenario results revealed the interactive effects of LAI, maximum  
641 rooting depth and root growth rate with soil water availability on relative transpiration  
642 and the evaporation fraction. When it was less than  $2 \text{ m}^2 \text{ m}^{-2}$ , the LAI played an  
643 important role in controlling transpiration. The effects of maximum rooting depth and  
644 root growth rate only appeared in drying periods, with the first being more important  
645 late in the growing season, while the latter dominated early in the growing season. As  
646 the disturbance of crop growth parameters has a significant effect on the simulation  
647 results, further consideration of the dynamics of crop growth parameters in a changing  
648 environment is needed.

649

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845

846 **Tables and Figures**

847 **Table 1.** Crop growth stages and crop height for maize

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Crop growth stages		Date	Crop height (m)
Initial	Start	23/06 (DOY 174)	0
Crop development	Start	06/07 (DOY 187)	0.22
Mid-season	Start	14/08 (DOY 226)	1.65
Late season	Start	14/09 (DOY 257)	2.17
	Harvest	02/10 (DOY 275)	2.17

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848 DOY, day of the year

849 **Table 2.** Soil hydraulic (Van Genuchten, 1980) and thermal (De Vries, 1963)  
 850 properties including saturated ( $\theta_s$ ) and residual ( $\theta_r$ ) water content; curve-fitting  
 851 parameters ( $\alpha$  and  $n$ ); saturated hydraulic conductivity ( $K_s$ ); specific heat capacities of  
 852 the water ( $C_w$ ), air ( $C_a$ ), quartz ( $C_q$ ), clay ( $C_c$ ) and organic matter ( $C_o$ )

Soil sample	Hydraulic properties					Thermal properties				
	$\theta_s$	$\theta_r$	$\alpha$	$n$	$K_s$	$C_w$	$C_a$	$C_q$	$C_c$	$C_o$
	cm <sup>3</sup> cm <sup>-3</sup>	cm <sup>3</sup> cm <sup>-3</sup>	cm <sup>-1</sup>	/	cm d <sup>-1</sup>	J g <sup>-1</sup> K <sup>-1</sup>				
0-20cm	0.45	0.105	0.0045	1.41	10.50	4.18	1.01	0.80	0.90	1.92

853

854 **Table 3.** Statistical summary of the correlation between observed and simulated  
 855 hourly ET for each crop development stage, for both the ET<sub>dir</sub> method and the ET<sub>ind</sub>  
 856 method.

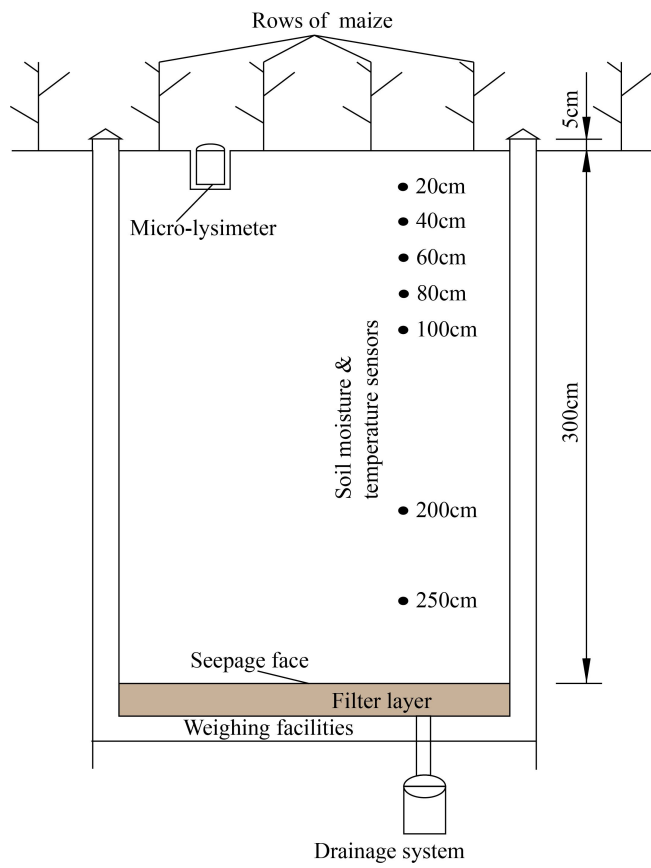
Crop stage	Number of observations	ET <sub>ind</sub> method					ET <sub>dir</sub> method				
		a	b	R <sup>2</sup>	RMSE		a	b	R <sup>2</sup>	RMSE	
					(mm h <sup>-1</sup> )	d				(mm h <sup>-1</sup> )	d
Initial	336	0.47	0.054	0.40	0.10	0.84	0.94	0.043	0.63	0.10	0.90
Crop development	936	0.69	0.064	0.70	0.10	0.94	0.81	0.041	0.78	0.09	0.96
Mid-season	744	0.62	0.055	0.80	0.11	0.93	0.89	0.027	0.90	0.08	0.98
Late season	432	0.70	0.051	0.72	0.07	0.90	0.75	0.029	0.77	0.06	0.93
<b>Total season</b>	<b>2448</b>	<b>0.65</b>	<b>0.056</b>	<b>0.72</b>	<b>0.11</b>	<b>0.90</b>	<b>0.85</b>	<b>0.035</b>	<b>0.82</b>	<b>0.09</b>	<b>0.95</b>

857 \*the regression relation is  $ET_{sim} = a \times ET_{obs} + b$ ; a is the slope and b is the intercept.

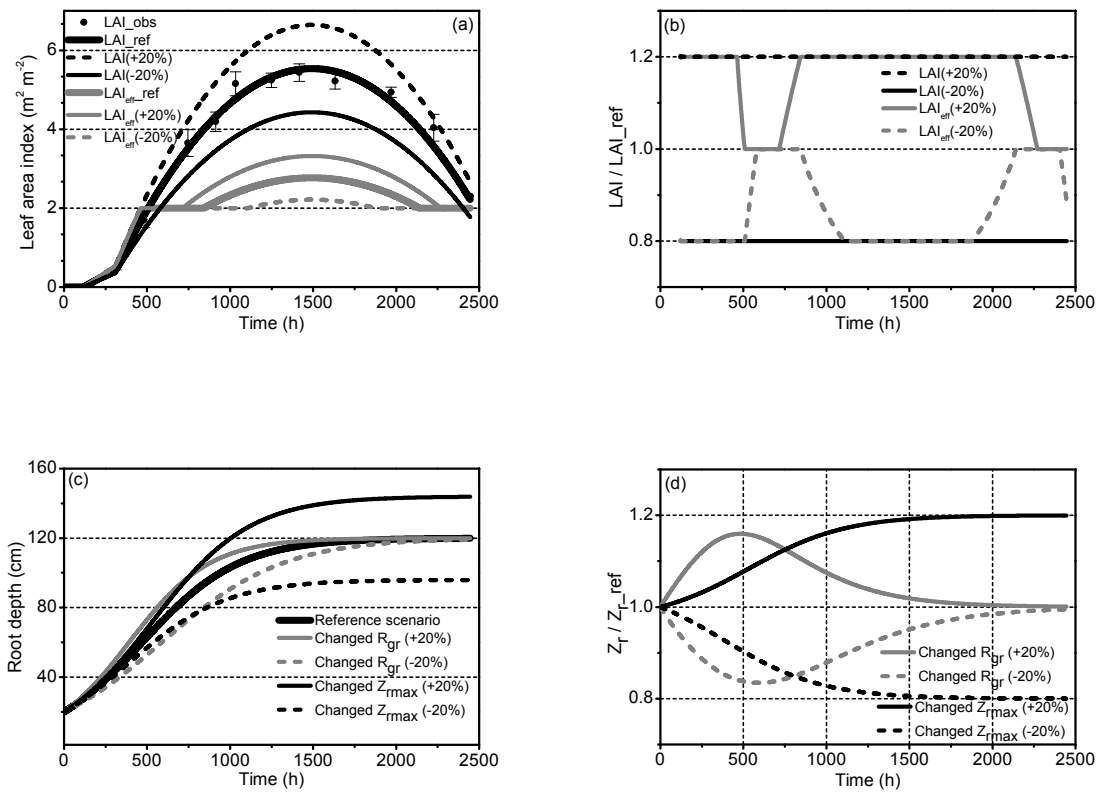
858 **Table 4.** Evaporation (E), transpiration ( $T_c$ ), evapotranspiration (ET) and evaporation  
859 fraction (E/ET, EF) for each development stage of maize, for both the  $ET_{dir}$  method  
860 and the  $ET_{ind}$  method. The actual evapotranspiration ( $ET_c$ ) is shown as well.

Crop stage	$ET_c$ (mm)	$ET_{ind}$ method				$ET_{dir}$ method			
		E	T	ET	EF	E	T	ET	EF
		(mm)	(mm)	(mm)	(%)	(mm)	(mm)	(mm)	(%)
Initial	37.72	29.13	6.83	35.96	81.01	43.32	6.71	50.03	86.58
Crop development	140.48	34.57	122.73	157.31	21.98	45.17	107.13	152.30	29.66
Mid-season	124.74	12.15	105.75	117.91	10.31	32.01	99.26	131.26	24.38
Late season	31.23	9.50	34.22	43.72	21.73	14.10	21.66	35.77	39.43
<b>Total season</b>	<b>334.18</b>	<b>85.36</b>	<b>269.53</b>	<b>354.89</b>	<b>24.05</b>	<b>134.60</b>	<b>234.76</b>	<b>369.37</b>	<b>36.44</b>

861



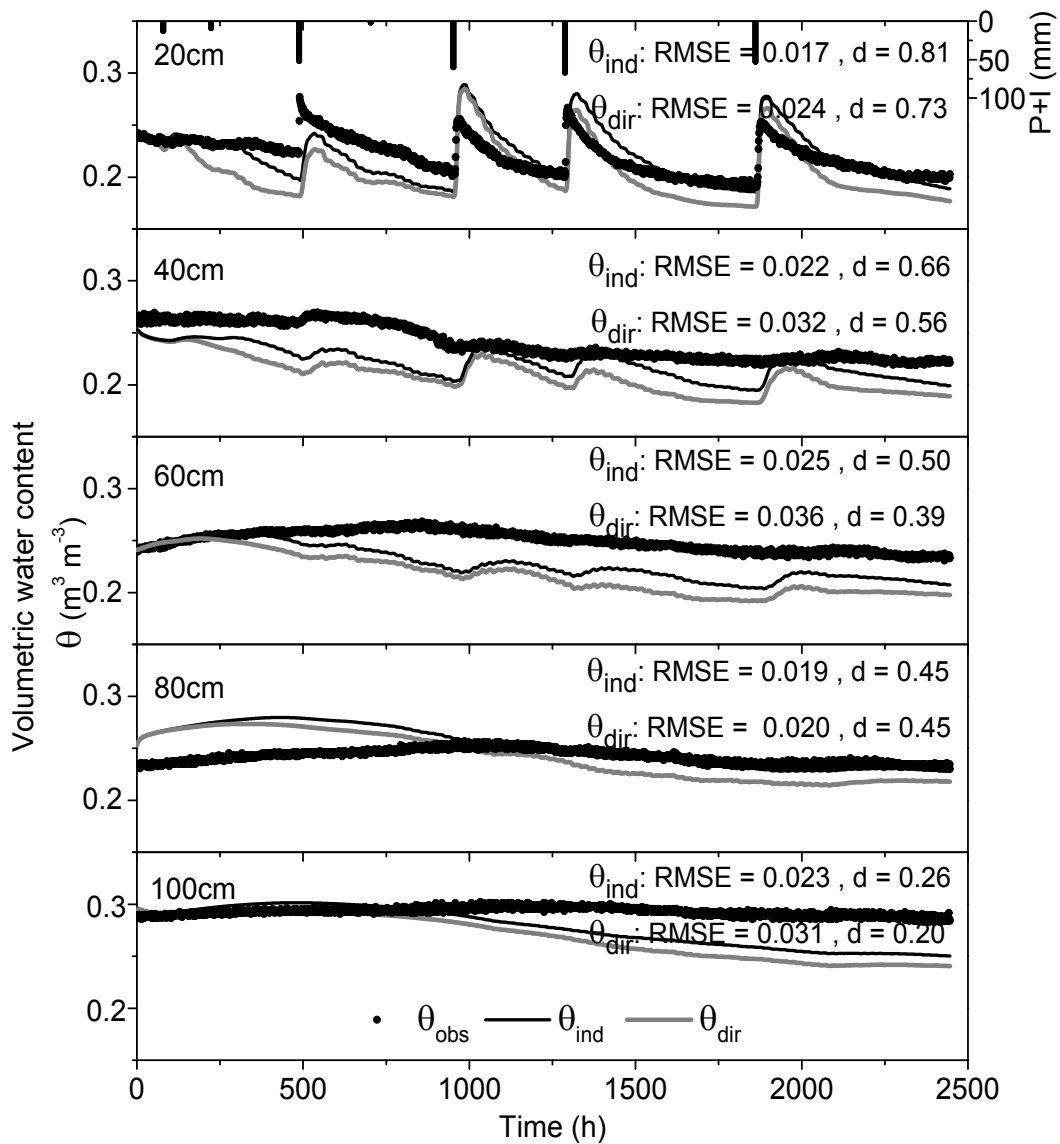
862 **Fig 1.** Schematic drawing of the large lysimeter structure



864

865 **Fig 2.** The seasonal variation in crop growth parameters used in the simulations: (a)  
 866 leaf area index (LAI), (b) relative values of LAI compared to the reference scenario,  
 867 (c) root depth ( $Z_r$ ), and (d) relative values of root depth compared to the reference  
 868 scenario. +20% and -20% indicate a 20% increase or decrease, respectively, compared  
 869 to the reference value. The vertical gridlines in (d) highlight the lag effect of the 20%  
 870 decreased  $R_{gr}$  scenario compared to the 20% increased  $R_{gr}$  scenario.

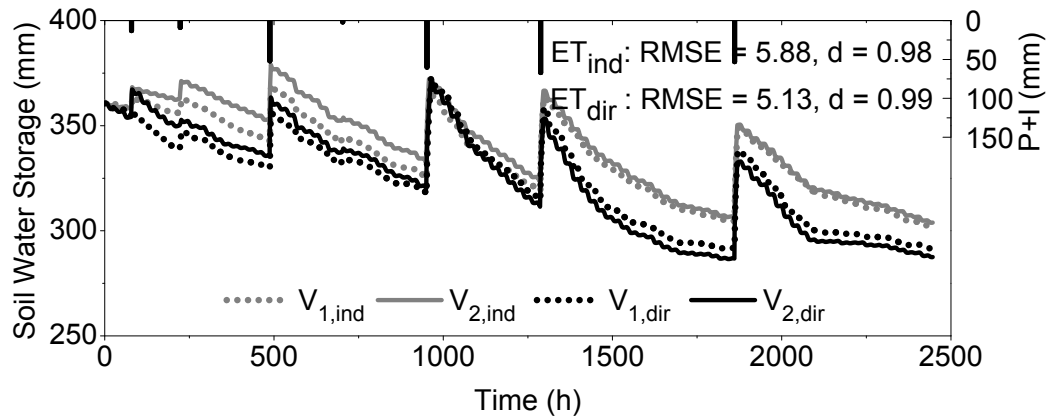
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872

873 **Fig 3.** Comparison of observed and simulated soil volumetric water content, at  
 874 selected depths: 20cm, 40cm, 60cm, 80cm and 100cm, with measured precipitation  
 875 and irrigation (the solid black bar with the right axis of “P+I (mm)”). The (connected)  
 876 black dots represent measurements, the black line depicts the simulation using the  
 877  $ET_{ind}$  method, and the gray line depicts the simulation using the  $ET_{dir}$  method.

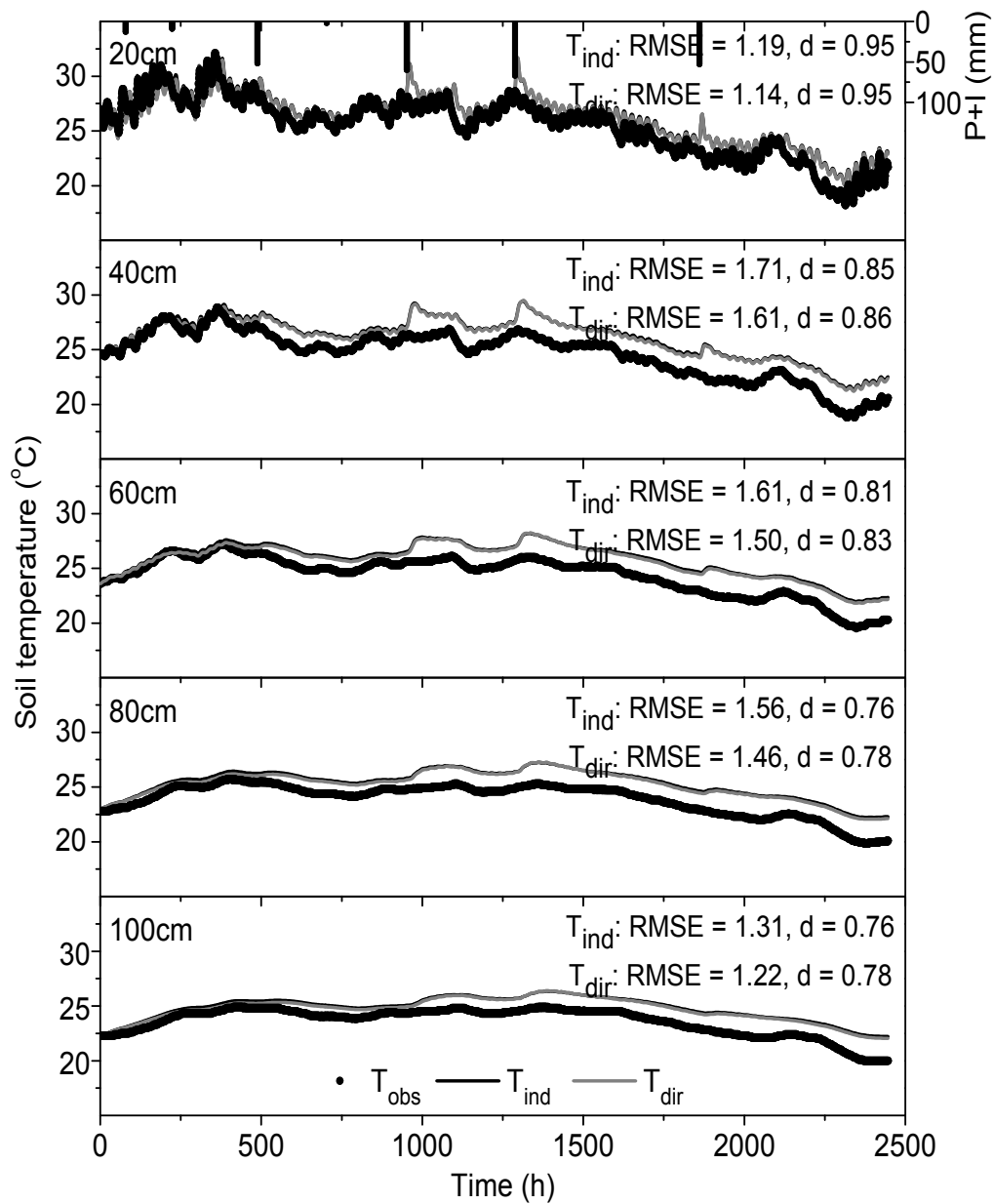




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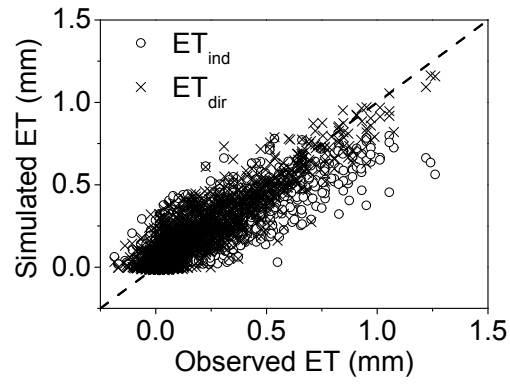
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880 **Fig 4.** Comparison between simulated root-zone water storage using different  
 881 methods (i.e.  $V_{1,ind}$ ,  $V_{2,ind}$ ,  $V_{1,dir}$ ,  $V_{2,dir}$ ), with measured precipitation and irrigation. The  
 882 grey dotted line represents water storage calculated with the integration of soil water  
 883 content over the root-zone and the grey solid line represents water storage calculated  
 884 with the inversion of the water balance equation within the root-zone, using the  $ET_{ind}$   
 885 method, i.e.  $V_{1,ind}$ ,  $V_{2,ind}$ , respectively. The black dotted and solid lines represent the  
 886  $ET_{dir}$  method.



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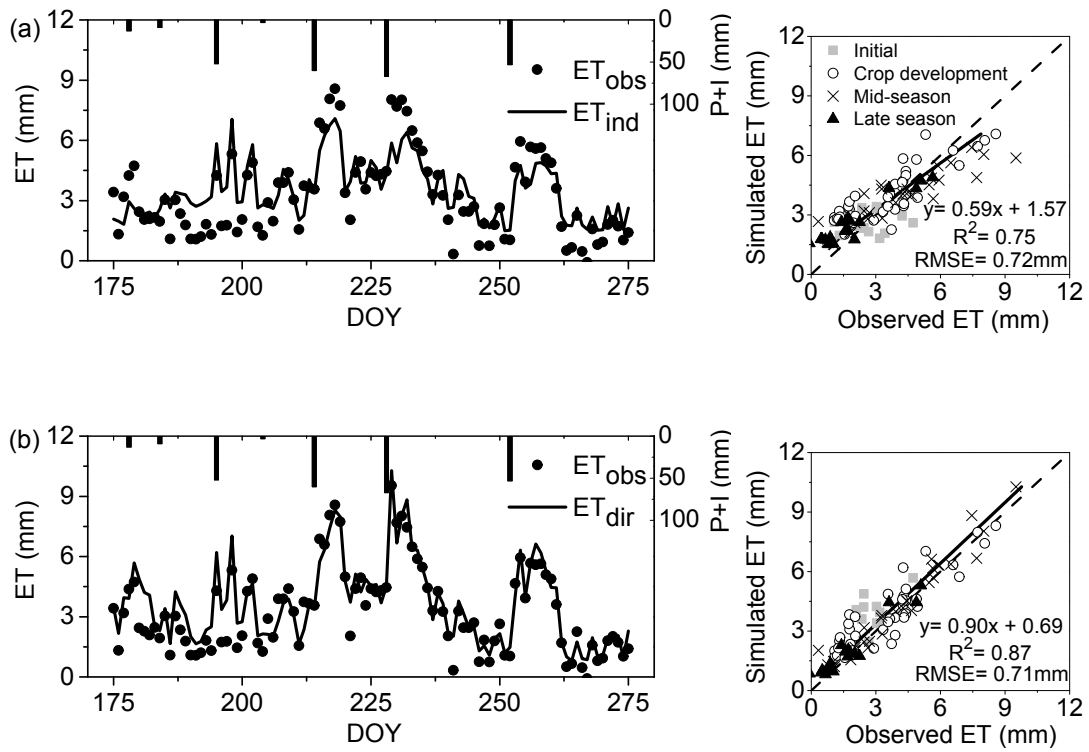
888 **Fig 5.** Comparison of observed and simulated soil temperature, at selected depths:  
 889 20cm, 40cm, 60cm, 80cm and 100cm, with measured precipitation and irrigation. The  
 890 black dots represent the observation, the solid black line shows the simulation with  
 891 the  $ET_{ind}$  method, and the solid gray line shows the simulations with the  $ET_{dir}$  method.



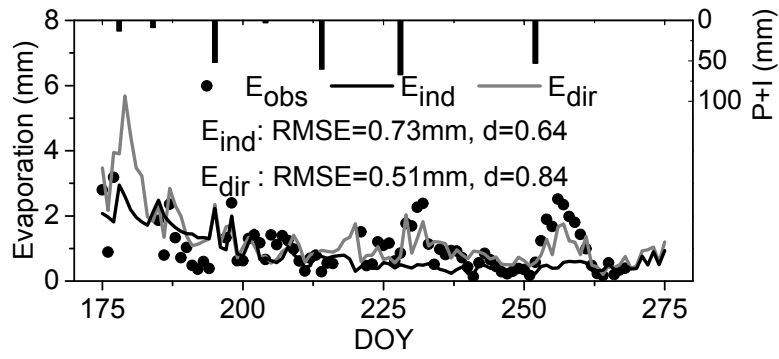
892

893 **Fig 6.** Scatter plot of hourly observed and simulated ET rates, with  $\times$  being  
894 estimations using the  $ET_{dir}$  method and  $\circ$  being estimations using the  $ET_{ind}$  method.

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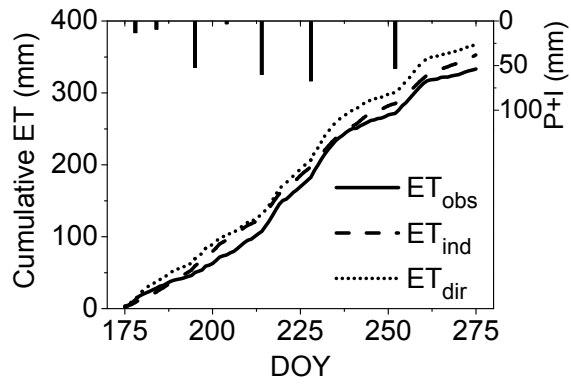


898 **Fig 7.** Daily variation in observed ET and simulated ET, based on the  $ET_{ind}$  method (a)  
 899 and the  $ET_{dir}$  method (b). On the right: the regression between observed and simulated  
 900 ET for the  $ET_{ind}$  method (above) and the  $ET_{dir}$  method (below).



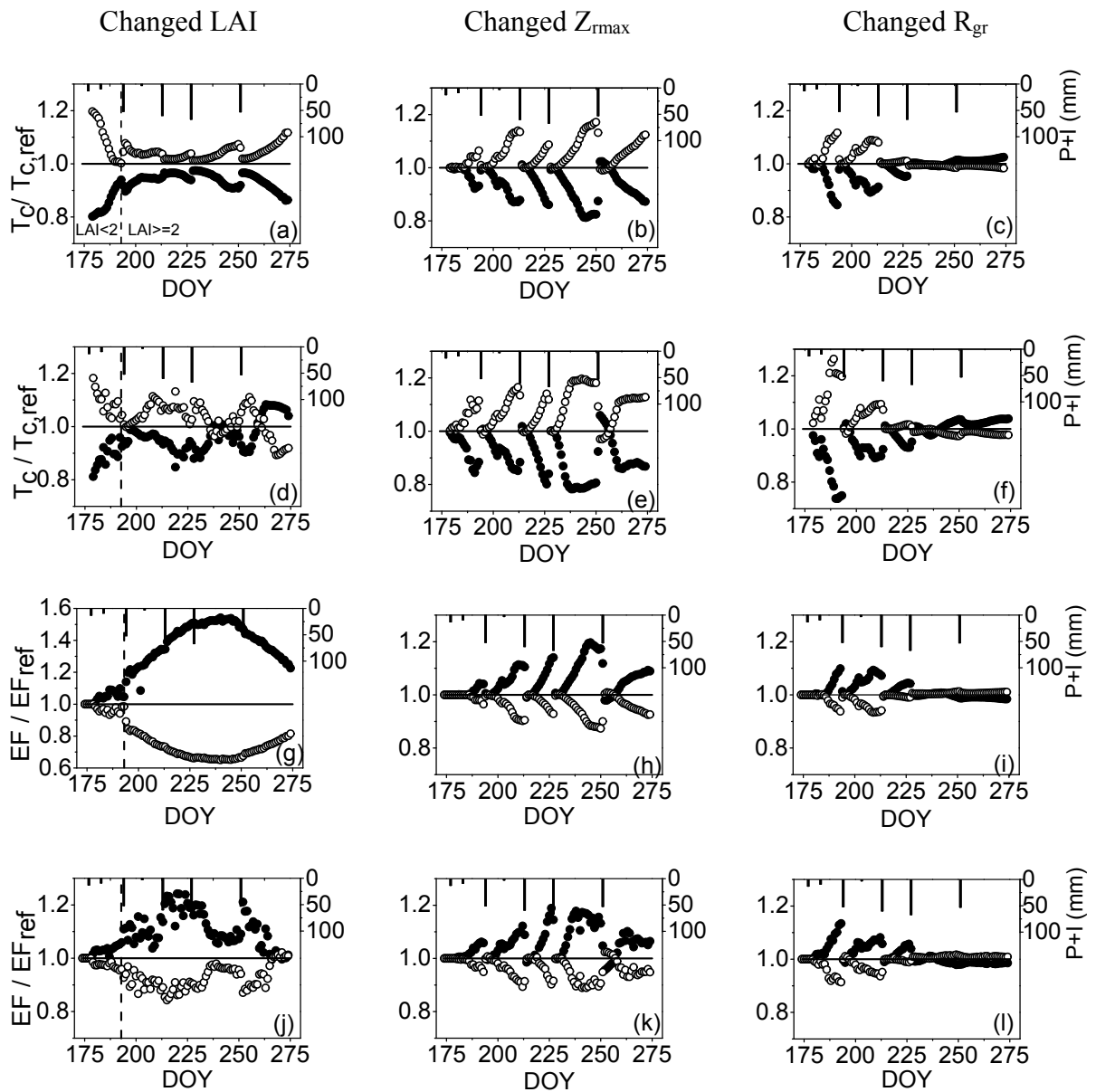
901

902 **Fig 8.** Daily variation in observed and simulated soil evaporation based on the two ET  
 903 simulation methods.



904

905 **Fig 9.** Cumulative variation in observed ET and simulated ET (as deduced from the  
 906 two ET simulation methods).



907

908 **Fig 10.** Relative daily variations, under changed leaf area index (LAI), maximum  
 909 rooting depth ( $Z_{rmax}$ ) and root growth rate ( $R_{gr}$ ), in crop transpiration: (a)-(c), using the  
 910  $ET_{ind}$  method, (d)-(f), using the  $ET_{dir}$  method; and in the evaporation fraction: (g)-(i),  
 911 using the  $ET_{ind}$  method; (j)-(l), using the  $ET_{dir}$  method, with measured precipitation  
 912 and irrigation;  $\circ$  depicting increased LAI,  $Z_{rmax}$  and  $R_{gr}$  by 20%,  $\bullet$  depicting  
 913 decreased LAI,  $Z_{rmax}$  and  $R_{gr}$  by 20%. Note that scale for (g) differs from for other  
 914 figures.

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