Responses to referees comments on "Transit times from rainfall to baseflow in headwater catchments estimated using tritium: the Ovens River, Australia"

We thank the two anonymous referees for their overall positive comments on this paper. Our original responses are below (in blue) together with a summary of changes to the manuscript (in red). The marked copy of the manuscript follows the comments.

Referee #1 stated "My only criticism lies with constraining the Tritium input function. Having a high resolution Tritium rainfall data is difficult and costly to assess, however, the paper would benefit with one or two more sentences discussing the possible uncertainties involved with a lag of a high frequency input function. I could imagine that tritium would undergo significant variability with rain event magnitudes, altitude and changes in atmospheric circulations"

We agree with this point and as with many studies there is uncertainty in the Tritium input function. In reality there are very few catchments globally where a high-resolution tritium record exists and it is not something that is able to be measured retrospectively. Since we are looking at mean transit times of more than a few years, the biggest uncertainty is probably in the long-term average Tritium activity of rainfall rather than the variability in individual seasons or events (which would probably be averaged out over several years). We have an additional annual rainfall sample from a second locality in the Ovens catchment that has a Tritium activity (2.85 TU) that we can use to estimate some of the uncertainties. For example, the MTT for a water sample with a tritium activity of 2 TU from the Exponential Piston Flow model assuming that the modern rainfall input is 3 TU is 15.2 years while assuming a rainfall value of 2.85 TU the MTT becomes ~13 years. This does not change the overall conclusions of the paper but it allows some uncertainties to be put on the calculations that are valuable. The variation in modern 3H values reported by Tadros et al. (2014) for the individual Australian stations is less than this inter-sample variation and so this calculation probably captures the spatial variability.

We carried out these modifications as indicated. Table 2 now shows the range in ages for each sample with the range calculated as the standard deviation resulting from varying the modern rainfall input from 2.85 to 2.99 TU. We have also included a discussion of this in Section 3.2. This resulted in minor changes to the mean transit times (e.g. the oldest MTT is now 30 not 31 years) and we have changes these where needed throughout the paper and in Fig. 9.

Referee #2 was also positive about the paper and its findings but had some concerns regarding the organisation of the paper, in particular what belongs in the introduction vs. the methods sections (and elsewhere such as the discussion) together with other minor points that require clarifying.

The section "sampling and analytical methods" thoroughly describes the sampling campaign and analysis. But a section describing the general approach, the choice of the particular methods to evaluate the results, and their application is missing. This makes the results and figures (e.g. the grey shading in Figs 4 and 8) difficult to understand and to evaluate for the review. I strongly recommend collecting the method descriptions provided at various parts of the manuscript (introduction, results, discussion) in a separate methods section including a description of the workflow to elaborate why the methods were chosen and why in this particular order

The locations of sections that provide the background to scientific studies vary from paper to paper. We agree that removing some of the material that describes the equations from the introduction to the methods would make the introduction more focussed and adding a short section on the mass balance in the methodology would also be useful. The discussion of how these techniques are applied to the Ovens catchment (e.g., the discussion of the input function of tritium), however, need to be in the latter sections as they rely on interpretation of data. This is a relatively minor reorganisation, and grouping both the analytical and analysis techniques into one section would certainly help the flow of the paper.

We carried out these changes. The general discussion of tritium as a tool for determining MTT remains in the Introduction; however, the presentation of the methodology and the LPM models is in the methods section. The methods section was becoming a little long as it now has sampling, analytical, and numerical methods in it and we have added subsections (the discussion of LPMs is in section 3.4).

The following are responses to comments made directly on the paper by Referee #2 (in the supplement file).

Introduction (P5249). Our comments regarding the context of the study can be clarified. We agree that there has been much hydrology carried out in headwater catchments; however, there is still considerable uncertainty over MTTs in headwater catchments, which is what we were trying to convey in this paragraph. Probably due to not being a common landform in Victoria, we'd ignored karst systems but agree that they are important elsewhere. We will reword this paragraph to more clearly convey the background to the study and to outline what our objectives are.

We clarified the material in the introduction. We never really meant to say that there hadn't been a great deal of work carried out in headwater catchments (which is clearly not the case) and were not trying to review headwater catchment hydrology in general. Our point was that MTT's were still relatively poorly understood in many catchments globally and this should now be clearer.

Section 1.1 (pages 5430-5434). The reviewer suggests moving some of this material to the methods section to shorten the introduction and to prevent the reader from losing focus. Material such as this can legitimately appear in the introduction, methods, or discussion sections (and different papers present it in different places). We consider that the more general material from this paragraph (eg the utility of tritium in the southern hemisphere) should be retained here, but that the bulk of the details of the calculations can go into the methodology. In this way we separate the important background material from the mechanics of the calculations, it will also illustrate the workflows of the study better.

As outlined above, we have done this and the discussion of LPMs now appears in section 3.4. Additionally, we have put the aims in a subsection of the introduction (section 1.3) to emphasise exactly what we were trying to achieve and how we went about it.

Section 1.2 (page 5434, line 22-23). We will reword this sentence to make it clearer.

This text now reads "Secondly, that there are first-order controls on transit times, such as catchment area, geology, landuse, catchment size, or the runoff coefficient. Finally, that the

concentration of major ions will increase with residence time in the catchment and can be used as proxies for the transit time."

Section 2 (page 5436, line 13). Late autumn and winter rain (June- September) is ~45% of the annual rainfall; however, rainfall occurs throughout most of the year (March is the driest month but still has 5-6%) of the annual total. We will add these details to this section.

The following details were added: "Approximately 45% of the annual precipitation occurs in the austral winter (June to September) with a proportion of the winter precipitation occurring as snow on the higher peaks, while March has the lowest precipitation (5 to 6% of the annual total)."

Section 3 (page 5438). The referee suggests that we add more to this section. As discussed above, it is straightforward to move the details of the calculations to the end of the methods section. However, a discussion of "how the collected data will be used to understand the varying transit times" would be out of place here. Such statement belongs where the aims of the paper are explained (section 1, page 5434, line 16 onwards) and we can integrate this material into that section.

As discussed above, we moved the discussion of LPMs to section 3.4. The discussion of the use of the data remains in section 1. However, we have separated the aims out into a small subsection (1.3), which with the removal of the material from section 1 makes them move visible and clearer.

Na and CI were the chosen as monitors of the major ion geochemistry because they are the major cation and anion in the river water and groundwater and also they are commonly measured in the routine river geochemistry monitoring programs (eg data in Fig. 8); we will explain that in this section.

We added: "While a range of major ion concentrations were measured only Cl and Na, which represent the major anion and cation in surface water and groundwater, are discussed here."

Section 5.1 (page 5442). Weighting by water volumes would be needed if one were interested in the mass flux of Na derived from weathering (eg for defining weathering rates) but not for the compositions (ie the number of mg of Na per litre of water). The mixing curves are from a mass balance calculation where the predicted Na concentration is calculated from the relative volume of surface runoff assuming all the increase in discharge over baseflow conditions is due to surface runoff. This can be better explained with the details of the mass balance going into the methods section (as also suggested by Referee #2).

We added an explanation of the mass balance and added Eq. 4 to the Methods (section 3.5), which should help clarify this calculation. We refer to Eq. 4 in this section and in the caption to Fig. 8. We have also removed the Na' vs. Q discussion here and in Fig. 8c; this representation is another way of viewing the same data that is in Fig. 8a and given that the trends are clear from Fig. 8a it was redundant and potentially confusing.

Section 5.1 (page 5443). We agree that the upstream vs. downstream categorisation is difficult to follow in the figures. However, since the samples are derived from a variety of tributaries that enter the main Ovens River at varying locations and which have different lengths, it is difficult to assign a distance to the sites. With much of the other data we have made the distinction between the

samples from the tributaries and those from the main Ovens River and that distinction would be probably useful for the stable isotope data in Fig. 6. In addition we will be more precise in our terminology in the text and refer to tributary sites vs. those on the main Ovens River rather than upstream and downstream.

We removed the upstream and downstream notation from this section and just refer to tributary sites vs. sites on the main Ovens River.

Section 5.2 (page 5445). We disagree that the discussion of the tritium input function can be part of the methods. This section requires interpretation of data and also is reliant on the measured tritium rainfall values which are not presented until Section 4.

We retained the discussion of the Tritium input function in this section.

Section 5.3 (page 5446). Morgenstern & Daughney (2012) discuss this and is a suitable reference (we reference it elsewhere in the paper).

We added this reference.

 Table 2. As discussed in response to Referee #1, it is probably most useful to assign uncertainties based on uncertainties in the input function, and this we will do. We can also add a measure of the range of the different techniques to the table.

These modifications were both made. We added uncertainties to the ages based on the variability of rainfall tritium activities and also added a column that shows the variability between the techniques. In addition, we discuss both of these aspects of the study in Section 5.2.

Figure 1. Should be "localities" not "locations".

This was changed in the figure and caption

Figure 3. The p value is 0.005 (we will add this to the figure)

This was added

Figures 4, 8. As with the tritium input function much of Figs 4 & 8 cannot be explained in the methods section as it requires discussion of data presented in Section 4 (e.g. to estimate the range of rainfall values). It is possible to add a section at the end of the methods section that explains the mass balance calculations (which we never explicitly do); this would be useful in indicating to the reader what we subsequently discuss in the paper.

We chose to retain this material in the discussion section as it requires interpretation of data which is presented in Section 4. We did, however add an explanation of the mass balance calculations to the methods and refer to that (and Eq. 4) in the figure captions and section 5.1.

Transit times from rainfall to baseflow in headwater catchments estimated using tritium: the Ovens River, Australia I. Cartwright¹ and U. Morgenstern² ¹School of Earth, Atmosphere and Environment, Monash University, Clayton, Vic. 3800, Australia ²GNS Science, Lower Hutt 5040, New Zealand

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1 Abstract

Headwater streams contribute a significant proportion of the total flow to many river systems, 2 3 especially during summer low-flow periods. However, despite their importance, the time taken for 4 water to travel through headwater catchments and into the streams (the transit time) is poorly 5 understood. Here, ³H activities of stream water are used to define transit times of water contributing to streams from the upper reaches of the Ovens River in southeast Australia at varying flow conditions. 6 7 ³H activities of the stream water varied from 1.63 to 2.45 TU, which are below the average ³H activity 8 of modern local rainfall (2.85 to 2.99 TU). The highest ³H activities were recorded following higher 9 winter flows and the lowest ³H activities were recorded at summer low-flow conditions. Variations of 10 major ion concentrations and ³H activities with streamflow imply that different stores of water from within the catchment (e.g. from the soil or regolith) are mobilised during rainfall events rather than 11 12 there being simple dilution of an older groundwater component by event water. Mean transit times 13 calculated using an exponential-piston flow model range from 4 to 30 years and are higher at summer 14 low-flow conditions. Mean transit times calculated using other flow models (e.g. exponential flow or dispersion) are similar. There are broad correlations between ³H activities and the percentage of 15 rainfall exported from each catchment and between ³H activities and Na and Cl concentrations that 16 17 allow first-order estimates of mean transit times in adjacent catchments or at different times in these 18 catchments to be made. Water from the upper Ovens River has similar mean transit times to the 19 headwater streams implying there is no significant input of old water from the alluvial gravels. The 20 observation that the water contributing to the headwater streams in the Ovens catchment has a mean transit time of years to decades implies that these streams are buffered against rainfall variations on 21 22 timescales of a few years. However, impacts of any changes to landuse in these catchments may take 23 years to decades to manifest itself in changes to streamflow or water quality.

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1 1. Introduction

Documenting the timescales over which rainfall is transmitted through catchments to streams (the transit time) is critical for understanding catchment hydrology and for the protection and management of river systems. While there has been an increasing number of studies that have estimated transit times (e.g. Kirchner et al., 2010; McDonnell et al., 2010; Morgenstern et al., 2010; Hrachowitz et al., 2013; Morgenstern et al., 2015), the time taken for water to be transformed from rainfall to stream baseflow remains poorly understood in many catchments. Likewise the factors that

8 control variations in transit times between catchments are not well documented.

9 <u>Perennial streams, especially in arid or semi-arid regions, are commonly sustained</u> by groundwater

- inflows during low-flow periods (Winter, 1999; Sophocleous, 2002). Where the lower and middle
 reaches of rivers are developed on alluvial sediments, these sediments provide a ready source of
 groundwater to sustain the river during low-flow periods. River systems in limestone terrains are
 likewise sustained by drainage through karst systems. By contrast, headwater catchments that are
- developed on indurated or crystalline rocks may not <u>be linked to</u> well-developed groundwater systems. The observation that many headwater streams continue to flow over prolonged dry periods indicates<u>, however</u>, that <u>these catchments</u> contain stores of water in soils, weathered rocks, or fractures with retention times of at least a few years (e.g., Maloszewski and Zuber, 1982; Maloszewski et al., 1992; Rice and Hornberger, 1998; Maloszewski, 2000). However, the <u>transit times</u> of <u>water</u>
- 19 within these stores and whether different stores are more active at different times, for example during
- 20 high vs. low rainfall periods, is not well known.
- 21 At times of low flow, much of the water in streams and rivers is likely derived from long-term stores
- such as groundwater (Sophocleous, 2002; McCallum et al., 2010; Cook, 2013). Less well understood is
- 23 the extent to which older water rather than event water (i.e., that derived from recent rainfall)
- 24 <u>contributes to higher streamflows</u> In some catchments at least, rainfall appears to displace water
- 25 from the soils and regolith and increase groundwater inflows to streams due to hydraulic loading. In

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1 these cases relatively old water may still contribute a significant volume of water to the river at higher

2 streamflows (Sklash and Farvolden, 1979; Rice and Hornberger, 1998; Kirchner, 2009; Hrachowitz et

3 <u>al., 2011).</u>

Understanding the timescales of water movement within headwater catchments is an essential part of water management. Headwater streams contribute a significant proportion of the total flow of many river systems (Freeman et al., 2007). Thus the water provided by headwater streams is that which may be eventually used downstream for domestic use, recreation, agriculture, and/or industry. Many headwater catchments retain native vegetation; however, increasing population growth and economic development has seen progressive changes of landuse, including plantation forestry, agriculture, and urban development. The impacts of such development on the headwater catchments,

and consequently on the river systems as a whole, is currently poorly understood.

12 Identifying first-order controls on transit times aids the prediction of likely transit times in adjacent 13 catchments. Geology, vegetation, and soil types, which influence recharge rates and groundwater fluxes, may be important controls on transit times. Catchment area and the drainage density (the 14 length of stream per unit area of catchment) may also be important controls on transit times, 15 16 (Morgenstern and Daughney, 2012). Larger catchments are likely to have longer flow paths which 17 result in longer transit times. However, if the catchment contains a higher density of streams there 18 may be numerous short flow paths between recharge areas and discharge points in the streams. 19 Additionally, transit times may correlate with the proportion of rainfall exported from the catchment 20 by the stream (the runoff coefficient). This is because catchments with low runoff coefficients are likely to have higher evapotranspiration rates which lead to low infiltration rates and relatively slow 21 22 passage of water through the catchment.

23 1.1. Determining water transit times

There are several methods that may be used to estimate the time taken for water to transit througha catchment to the stream. The temporal variation of stable isotope ratios and/or major ion

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1	concentrations in rainfall become attenuated with increasing transit times as mixing of water derived
2	from different rainfall episodes occurs within the catchment (Kirchner, 2009; Kirchner et al., 2010;
3	Hrachowitz et al., 2013). When combined with Jumped parameter models that describe the
4	distribution of residence times along flow paths in a catchment (e.g., Maloszewski and Zuber, 1982;
5	Maloszewski, 2000), the variation in geochemistry at the catchment outlet can be used to quantify
6	water transit times. While this methodology has been applied with some success, there are some
7	limitations. Firstly, it requires detailed (preferably at least weekly) stable isotope and/or major ion
8	geochemistry data for rainfall collected over a period which exceeds that of the transit times of water
9	in the catchment. Such data are not commonly available, especially where transit times are more than
10	a few years. Secondly, a single estimate of the transit time is commonly estimated for the catchment
11	whereas water with different transit times may contribute to the stream at low and higher flows (e.g.,
12	Morgenstern et al., 2010; Morgenstern and Daughney, 2012; Morgenstern et al., 2015). Seasonal
13	variations in flow within the catchment may also attenuate variations in the concentrations of these
14	tracers (Kirchner, 2015). Finally, these tracers are progressively more ineffective where transit times
15	are in excess of 4-5 years as the temporal variations are smoothed out (Stewart et al., 2010).
16	Tritium (³ H), which has a half-life of 12.32 years, may also be used to determine transit times of
17	relatively young (<100 years) groundwater into streams, using lumped parameter models. ³ H is part of
18	the water molecule and its abundance in water is only affected by initial activities and radioactive
19	decay, and not by reactions between the water and the aquifer matrix, as is the case with some solute
20	tracers such as 14 C or 32 Si. Other potential tracers such as 3 He, the chlorofluorocarbons, and SF ₆ are
21	gases that equilibrate with the atmosphere and are difficult to use in streams. The ³ H activities in
22	rainfall have been measured globally for several decades (e.g. International Atomic Energy
23	Association, 2015; Tadros et al., 2014) and these may be used to define the input of ³ H into the
24	catchment. Rainfall ³ H activities have a distinct peak in the 1950s to 1960s due to the production of
25	³ H in the atmospheric nuclear tests (the so-called "bomb pulse"). Traditionally, the propagation of the
26	bomb pulse has been used to trace the flow of water recharged during this period (Fritz et al., 1991;

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Clark and Fritz, 1997) because single measurements of ³H activities yielded non-unique estimates of 1 2 transit times. However, because ³H activities during the bomb pulse were several orders of magnitude 3 lower in the southern hemisphere than in the northern hemisphere (Clark and Fritz, 1997; 4 Morgenstern et al., 2010; Tadros et al., 2014), ³H activities of remnant bomb pulse water in the 5 southern hemisphere have decayed well below those of modern rainfall. This situation results in 6 unique transit times being estimated from single ³H measurements (Morgenstern et al., 2010; 7 Morgenstern and Daughney, 2012), which in turn permits the transit time of water contributing to 8 streams at specific flow conditions to be determined.

9 There is always uncertainty in calculating transit or residence times using Jumped parameter models 10 as they are a simplification of the flow system. However, since the bomb-pulse ³H has mostly 11 disappeared in the southern hemisphere, ³H activities reflect relative transit times that do not depend 12 on the applicability of the assumed model (i.e., water with low ³H activities has longer mean transit times than water with high ³H activities). This allows ³H activities to be readily compared with other 13 parameters (e.g. streamflow or major ion compositions). By contrast, as discussed above, for northern 14 15 hemisphere waters individual ³H activities do not yield unique residence times and comparisons can 16 only be made with transit times derived from time series of ³H activities that are inherently model dependant. 17

18 1.2. Qualitative water transit time indicators

In many catchments, including the Ovens, the concentration of major ions in groundwater increases with time (Edmunds et al., 1982; Bullen et al., 1996; Zuber et al., 2005; Morgenstern et al., 2010; Cartwright and Morgenstern, 2012). Thus, major ion concentrations in stream water can also provide an indication of the relative transit time of water that contributes to the stream. There may also be a correlation between streamflow and transit times. (Morgenstern et al., 2010). As major ion concentrations and streamflow data are easier to obtain than ³H activities and commonly already

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where τ is the transit time, t- τ is the time that the water entered the flow system, λ is the decay constant (0.0563 yr¹ for ³H), and $g(\tau)$ is the response function that describes the distribution of flow paths and transit times in the system.

The exponential flow model describes the mean transit time in homogeneous unconfined aquifers of constant thickness that receive uniform recharge and where flow paths from the entire aquifer thickness discharge to the stream. Piston flow assumes linear flow with no mixing within the aquifer, such that all water discharging to the stream at any one time has the same transit time. The exponential-piston flow model describes mean transit times in aquifers that have regions where flow paths have an exponential distribution and regions where flow paths have a linear distribution. For the exponential-piston flow model $g(\tau)$ in Eq. (1) is given by:

Moved down [7]: where τ_m is the mean transit time and f is the proportion of the aquifer volume that exhibits exponential flow. Where f = 1, Eqs (1 and 2) describe the distribution of transit times resulting from exponential flow while where f = 0, Eqs (1 and 2) describe the distribution of transit times resulting from piston flow.

Deleted: The mean transit times may be calculated using lumped parameter models (Maloszewski and Zuber, 1982, 1992; Cook and Bohlke, 2000; Maloszewski, 2000; Zuber et al., 2005) which treat the discharging water as comprising numerous aliquots each of which has followed a different flow path and thus taken a different amount of time to pass through the aquifer.

Moved down [5]: For steady-state groundwater flow, the concentration of ³H in water discharging into the stream at time *t* ($C_o(t)$) is related to the input of ³H (C) over time via the convolution integral: ¶

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$$g(\tau) = 0$$
 . . . for $\tau < \tau_m(1-f)$. (2a)¶
 $g(\tau) = (f\tau_m)^{-1}e^{-\tau/f\tau_m+1/f-1}$ for $\tau > \tau_m(1-f)$. (2b)

Moved down [8]: The dispersion model is an alternative lumped parameter model based on the one-dimensional advectiondispersion transport in a semi-infinite medium. The response function for this model is:¶

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$$g(\tau) = \frac{1}{\tau_{\lambda} \sqrt{4\pi D_{n} \tau / \tau_{m}}} e^{-\left(\frac{\left(1 - \tau / \tau_{m}\right)^{2}}{4D_{p} \tau / \tau_{m}}\right)}$$

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$$C_o(t) = \int_{0}^{\infty} C_i(t-\tau) g(\tau) e^{-\lambda \tau} d\tau$$

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1 exist, such correlations offer the possibility of providing first-order estimates of transit times in

2 adjacent catchments or to periods when no ³H activities were measured.

3 <u>1.3. Aims and objectives</u>

4 The aim of this paper is to understand the transit times of baseflow, here defined as including all non-5 surface water sources including soil water, interflow, and groundwater, contributing to headwater streams in the Ovens Catchment, southeast Australia using ³H activities and major ion concentrations. 6 7 Specifically, we use these data to test the following hypotheses. Firstly, that transit times in individual catchments vary with streamflow as different water stores in the catchments are mobilised. Secondly, 8 9 that there are first-order controls on transit times, such as catchment area, geology, landuse, catchment size, or the runoff coefficient. Finally, that the concentration of major ions will increase 10 with<u>residence time in the catchment</u> and can be used as proxies for the transit time. While this study 11 12 is based in the Ovens Catchment, understanding the first order controls on water transit times or whether there are proxies that may be used to estimate transit times has application to other 13 catchments globally. 14

15 2. Setting

The Ovens River is part of the Murray-Darling River system (Lawrence, 1988). The Ovens River is perennial with a length of approximately 200 km and its headwaters extend into the Victorian Alps (Fig. 1). It has a single channel confined within a steep-sided valley south (upstream) of Myrtleford and then develops into a network of meandering and anastomosing channels north of Wangaratta prior to its confluence with the Murray River. This study concentrates on the upper reaches of the Ovens catchment upstream of Myrtleford (Fig. 1), which includes several headwater tributaries, notably the Buckland River, Morses Creek, and the East and West Branches of the Ovens River.

The upper Ovens catchment is dominated by metamorphosed Ordovician turbidites and Silurian to
Devonian granite intrusions (Fig. 1). These rocks form fractured-rock aquifers that have hydraulic
conductivities of 0.01 to 1 m day⁻¹ with higher hydraulic conductivities occurring in weathered zones

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mainly close to the land surface (Shugg, 1987; van den Berg and Morand, 1997). The basement rocks 1 2 are overlain by sediments of the Quaternary Shepparton Formation and the Holocene Coonambidgal 3 Formation that in this area are contiguous and indistinguishable. These two formations occur in the 4 river valleys and comprise unconsolidated and generally poorly-sorted immature fluvio-lacustrine 5 sands, gravels, silts and clays (Tickell, 1978; Shugg, 1987; Lawrence, 1988). The Shepparton and 6 Coonambidgal Formations increase in thickness away from the Victorian Alps and reach a maximum 7 thickness of 170 m in the lower Ovens Valley; however, where present in the upper Ovens catchment, 8 they are <50 m thick and thin out considerably in the tributary valleys. The hydraulic conductivity of 9 the Shepparton and Coonambidgal Formations varies from 0.1 to 60 m day¹ with typical values of 0.2 to 5 m day⁻¹ (Tickell, 1978; Shugg, 1987). Alluvial fans that are locally tens of metres thick and which 10 comprise of coarse-grained poorly-sorted immature sediments commonly occur between the 11 12 basement rocks and the floodplain.

The upper reaches of the Ovens River and its tributaries are characterised by narrow steep-sided 13 valleys that are dominated by native eucalyptus forest with subordinate pine plantations. The Ovens 14 Valley broadens downstream of Harrietville (Fig. 1) and alluvial flats up to 2 km wide are developed 15 16 adjacent to the Ovens River and in the lower reaches of the tributaries. These alluvial flats together 17 with some of the alluvial fans have been cleared for agriculture, which includes cattle grazing, orchards, vineyards, hops, and fruit farms. The population of the upper Ovens Valley is ~7500, mainly 18 in the towns of Myrtleford, Bright, and Harrietville. This part of the Ovens catchment contains no 19 20 reservoirs and, while there is some use of surface and groundwater, the flow regimes in the upper 21 Ovens catchment are considered to be little impacted (Goulburn-Murray Water, 2015).

Average precipitation decreases from 1420 mm yr⁻¹ in the alpine region to 1170 mm yr⁻¹ at Bright (Bureau of Meteorology, 2015). <u>Approximately 45% of the annual precipitation occurs in the austral</u> winter (June to September) with a proportion of the winter precipitation occurring as snow on the higher peaks, <u>while March has the lowest precipitation (5 to 6% of the annual total</u>). <u>Streamflow in</u>

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1 the Ovens River at Bright (Fig. 1) between 1924 and 2014 was between 1000 and 3.28x10⁷ m³ day¹

2 with high flows occurring in winter (Department of Environment and Primary Industries, 2015).

3 3. Sampling and analytical methods

4 <u>3.1. Sampling sites</u>

5 The sampling sites in this study have been designated as being from headwater catchments or 6 floodplain areas. The headwater catchment areas are dominantly composed of basement rocks 7 covered with eucalyptus forest and subordinate plantation forest. Alluvial sediments in these 8 catchments are restricted to zones of a few metres to tens of metres wide immediately adjacent to the streams. The Ovens East Branch (catchment area of 72 km²), Ovens West Branch (catchment area 9 10 of 42 km²), and Simmons Creek (catchment area of 6 km²) were sampled at Harrietville close to where these streams enter the floodplain of the Ovens Valley. The upper Buckland River (catchment area of 11 77 km²) and upper Morses Creek (catchment area of 32 km²) are from the upper reaches of those 12 13 tributaries that are largely undeveloped. The lower Buckland River (catchment area of 435 km²) and lower Morses Creek (catchment area of 123 km²) have some land clearing on the lower parts of alluvial 14 15 fans and the floodplain. Together these streams represent the main tributaries in the upper Ovens Valley (Fig. 1). 16 17 The floodplain sites are on the main Ovens River (Fig. 1, Table 1). Here the floodplain is up to 2 km

18 wide and is underlain by coarse-grained alluvial sediments that are up to 50 m thick. The floodplain and some of the lower slopes of the alluvial fans have been cleared while the upper slopes are still 19 20 dominated by eucalyptus forests with subordinate pine plantations. The Smoko (catchment area of 267 km²) and Bright (catchment area of 302 km²) sampling sites are upstream of the junction with 21 22 Morses Creek and downstream of the Ovens East Branch, Ovens West Branch and Simmons Creek 23 tributaries. The Myrtleford sampling site (catchment area of 1240 km²) is downstream of the junction 24 with the Buckland River and upstream of the junction with the Buffalo River (not sampled in this 25 study). Sampling took place in four rounds (Table 1, Fig. 2) that represent a variety of flow conditions.

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1 <u>3.2. Streamflow measurements</u>

2 Streamflow is monitored at or close to the Myrtleford, Bright, Ovens West Branch (until 1989), 3 Simmons Creek, Lower Buckland, and Lower Morses Creek sampling sites (Department of 4 Environment and Primary Industries, 2015). A gauge at Harrietville (Fig. 1) records the combined 5 streamflow from the Ovens West Branch and Ovens East Branch tributaries. The average daily 6 combined streamflow at Harrietville and that of the Ovens West Branch are well correlated over a 7 wide range of flows (n = 1012, R² = 0.97) allowing the streamflow of the Ovens West Branch for the 8 sampling rounds in this study to be calculated from the Harrietville streamflow. In turn, this enables

9 the contribution of Ovens East Branch tributary to the combined flows to be estimated.

10 <u>3.3. Geochemical sampling</u>

11	Stream water was sampled from swiftly-flowing stream sections using a collector fixed to an
12	extendable pole. Rainfall was collected from <u>two</u> rainfall <u>collectors</u> located at Mount Buffalo (Fig. 1).
13	Cations were analysed at Monash University using a ThermoFinnigan ICP-OES or ICP-MS on samples
14	that had been filtered through 0.45 μm cellulose nitrate filters and acidified to pH <2 using double-
15	distilled 16M HNO_3 . Anions were analysed on filtered unacidified samples using a Metrohm ion
16	chromatograph at Monash University. The precision of anion and cation analyses based on replicate
17	analyses is $\pm 2\%$ and the accuracy based on analysis of certified water standards is $\pm 5\%$. While a range
18	of major ion concentrations were measured only CI and Na, which represent the major anion and
19	cation in surface water and groundwater, are discussed here. Additional major ion data is from
20	Department of Environment and Primary Industries (2015).

Stable isotopes were measured at Monash University using Finnigan MAT 252 and ThermoFinnigan DeltaPlus Advantage mass spectrometers. δ^{18} O values were determined via equilibration with He-CO₂ at 32 °C for 24–48 hours in a ThermoFinnigan Gas Bench. δ^{2} H was measured by reaction with Cr at 850 °C using an automated Finnigan MAT H/Device. δ^{18} O and δ^{2} H values were measured relative to internal standards calibrated using IAEA SMOW, GISP and SLAP. Data were normalized following Moved up [10]: Sampling took place in four rounds (Table 1, Fig. Moved up [11]: 2) that represent a variety of flow conditions. Deleted: Deleted: a Deleted: collector

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1	(Coplen, 1988) and are expressed relative to V-SMOW. Precision (1 σ) based on replicate analysis is	
2	δ^{18} O = ±0.1‰ and δ^2 H = ±1‰. ³ H activities are expressed in tritium units (TU) where 1 TU represents	
3	a 3 H/ 1 H ratio of 1×10 ⁻¹⁸ . Samples for 3 H were vacuum distilled and electrolytically enriched prior to	
4	being analysed by liquid scintillation spectrometry using Quantulus ultra-low-level counters at GNS,	
5	New Zealand. Following from Morgenstern and Taylor (2009) the sensitivity is now further increased	
6	to a lower detection limit of 0.02 TU via tritium enrichment by a factor of 95, and reproducibility of	
7	tritium enrichment of 1% is achieved via deuterium-calibration for every sample. The precision (1 σ) is	
8	~1.8% at 2 TU (Table 1).	
9	3.4. Estimating mean transit times using ³ H	
10	Water flowing through an aquifer follows flow paths of varying length, which results in the water	
11	discharging into streams having a range of transit times rather than a discrete age. The mean transit	
12	times may be calculated using the lumped parameter models described by Maloszewski and Zuber	
13	(1982, 1992), Cook and Bohlke (2000), Maloszewski (2000) and Zuber et al.(2005) that treat the	
14	discharging water as comprising numerous aliquots each of which has followed a different flow path	
15	and thus taken a different amount of time to pass through the aquifer. For steady-state groundwater	
16	flow, the concentration of ³ H in water discharging into the stream at time t ($C_{\underline{o}}(t)$) is related to the	
17	input of ³ H (C_i) over time via the convolution integral:	
18	$C_o(t) = \int_0^\infty C_i(t-\tau) g(\tau) e^{-\lambda \tau} d\tau $ (1),	
19	where τ is the transit time, t- τ is the time that the water entered the flow system, λ is the decay	
20	constant (0.0563 yr ⁻¹ for ³ H), and $g(\tau)$ is the response function that describes the distribution of flow	
21	paths and transit times in the system.	
22	The exponential flow model describes the mean transit time in homogeneous unconfined aquifers of	
23	constant thickness that receive uniform recharge and where flow paths from the entire aquifer	
24	thickness discharge to the stream. Piston flow assumes linear flow with no mixing within the aquifer.	

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1	such that all water discharging to the stream at any one time	<u>me has the same tr</u>	ansit time. The		
2	exponential-piston flow model describes mean transit times in a	quifers that have reg	ons where flow		
3	paths have an exponential distribution and regions where flow	paths have a linear of	<u>distribution. For</u>		
4	the exponential-piston flow model $g(\tau)$ in Eq. (1) is given by:				
5	$g(\tau) = 0$	for <i>τ < τ_m(1-f)</i>	<u>(2a)</u>	1	Field Code Changed
c	$a(\tau) - (f\tau)^{-\tau/f\tau} e^{-\tau/f\tau}$	for $z > z$ (1 f)	(2b)		Field Code Changed
D		$\frac{10r \tau > \tau_m (1-j)}{1-1}$	<u>(2D),</u>		
7	where $ au_m$ is the mean transit time and f is the proportion of	of the aquifer volum	<u>e that exhibits</u>		Moved (insertion) [7]
8	exponential flow. Where $f = 1$, Eqs (1 and 2) describe the distribution of the distributicating distribution of the distribu	oution of transit time	s resulting from		
9	exponential flow while where $f = 0$, Eqs (1 and 2) describe the f	distribution of transit	times resulting		
10	from piston flow. The calculations utilised the Excel workbook	TracerLPM (Jurgens e	<u>t al., 2012) that</u>		
11	specifies the ratio of exponential to piston flow as an EPM rati	o which is equivalent	to 1/f – 1. <u>The</u>		Moved (insertion) [8]
12	dispersion model is an alternative lumped parameter model base	ed on the one-dimens	onal advection-		
13	dispersion transport in a semi-infinite medium. The response fur	nction for this model	<u>s:</u>		
	$\left(\left(1-\tau/t_m\right)^2\right)$			l	Field Code Changed
14	$g(\tau) = \frac{1}{\tau \sqrt{4\pi D_n \tau / \tau}} e^{-\left(\frac{1}{4D_p \tau / \tau_m}\right)}$		(3),		
			/		
15	where <i>D_P</i> is the dispersion parameter (unitless), which is the inve	erse of the more com	monly reported		Moved (insertion) [9]
16	Peclet Number. $D_{\underline{P}} = D/(v x)$, where v is velocity (m day ⁻¹), x is o	distance (m), and D is	the dispersion		
17	coefficient (m ² day ⁻¹). While the dispersion model is considered t	to be a less realistic co	nceptualisation		
18	of flow systems, it commonly reproduces the observed distribution	tion of radioisotopes	within aquifers		
19	(Maloszewski, 2000).				
20	3.5. Mass balance calculations				
21	If groundwater and rainfall have different major ion concent	rations, stable isotor	oe ratios, or ³ H		
22	activities, variations in these parameters with streamflow, may b	e used to assess the c	egree of mixing		Moved (insertion) [12]
23	of baseflow with event water (Sklash and Farvolden, 1979; Uh	lenbrook et al., 2002	; Godsey et al.,		

1	2009). In the case where baseflow to the stream remains relatively constant and increases in
2	streamflow are due to additional event water, the proportion of baseflow in the stream (X_{bf}) is given
3	by Q_{bf}/Q where Q is the measured streamflow and Q_{bf} is the streamflow at baseflow conditions. The
4	concentration of a component in the stream (C_{st}) at higher streamflows is given by:
5	$\underline{C_{st}} = X_{bf} C_{bf} + (1 - X_{bf}) C_{ew} $ (4),
6	where and C_{bf} and C_{ew} are the concentrations in the baseflow and event water, respectively.
7	4. Results
8	4.1. Streamflow variations
9	Figure 2a summarises the variation in streamflow at Bright between 2010 and 2014 and Fig. 2b shows
10	the distribution of the sampling rounds relative to the flow frequency curve for 1980 to 2014 daily
11	streamflow at Bright. The July 2014 sampling round was during a recession period from winter high

12	flows and the streamflow of $1.57 x 10^6\ m^3\ day^{\text{-}1}$ represents the 5.5 percentile of streamflow (i.e.,
13	streamflow of this value or higher was recorded on 5.5% of days during 1980 to 2014). The December
14	2013 and October 2014 sampling rounds represent periods of intermediate streamflow of 2.69×10^5
15	and 3.19x10 ⁵ m ³ day ⁻¹ , which <u>correspond</u> to the 46.3 and 42.1 percentiles of streamflow, respectively.
16	The February 2014 sampling round represents typical late austral summer low-flow conditions. The
17	streamflow at Bright during this sampling round of $6.46 x 10^4 \text{ m}^3 \text{ day}^{-1}$ was close to the minimum
18	streamflow for the 2013 to 2014 summer of $5.44 \times 10^4 \text{ m}^3 \text{ day}^1$ (Department of Environment and
19	Primary Industries, 2015) and represents the 86.4 percentile of streamflow between 1980 and 2014.
20	The streamflow data may also be used to define the runoff coefficient (i.e., the percentage of rainfall
21	exported from each catchment) (Fig. 3). The average annual streamflow was calculated using daily
22	streamflow data between 1980 and 2014 (Department of Environment and Primary Industries, 2015).
23	Periods of no record generally due to gauge malfunction were omitted; these represent <15% of the
24	data. There is a rainfall gradient across the Ovens Catchment and insufficient rainfall stations to
25	calculate area, weighted average rainfall for individual catchments. However, it is likely that

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precipitation in the whole region is between 1170 and 1420 mm yr⁻¹, which are the annual totals at
 Bright in the north of the catchment and the Victorian Alps to the south of the Ovens catchment. Using
 an average rainfall of 1295 mm yr⁻¹, runoff coefficients range from ~7.4% for Simmons Creek to ~58%
 for the Ovens East Branch. For the range of precipitation in the Ovens Valley the relative error on these
 runoff coefficients is ~10%.

6 4.2. ³H activities

- 7 The rainfall sample from December 2013 represents a ~17 month aggregate sample from Mount
- 8 Buffalo and has a ³H activity of 2.99 TU (Table 1). A second 12 month aggregate sample collected from
- 9 <u>a different site on Mount Buffalo in March 2015 has a ³H activity of 2.85 TU (Table 1). These ³H</u>
- 10 <u>activities are</u> close to <u>those</u> expected <u>for</u> modern rainfall in southeast Australia (Tadros et al., 2014).
- 11 Shorter timescale (2 to 5 month) rainfall samples collected from Mount Buffalo in February 2014, July

2014, and October 2014 have ³H activities between 2.52 and 2.89 TU. The lowest ³H activities from
 the rainfall are from rainfall collected between February and July 2014 in the austral autumn. Autumn

14 and winter rains are commonly depleted in ³H (Morgenstern et al., 2010; Tadros et al., 2014) as the

15 main ³H injection into the troposphere occurs in early spring. Stream water samples have ³H activities

16 between 1.63 and 2.43 TU (Table 1), which are lower than all of the rainfall samples.

17 The highest ³H activities of stream water at each sampling site are generally from the high-flow conditions in July 2014, while the lowest ³H activities are from the February 2014 low-flow period 18 19 (Table 1, Figs 4, 5). The ³H activities from the three floodplain sites are similar to those of the 20 headwater streams and there are no systematic downstream trends along the main Ovens River. 21 Likewise there is little systematic variation in ³H activities downstream in the Buckland River and Morses Creek. There is also not a positive correlation between catchment area and ³H activities (Fig. 22 23 5); indeed, Simmons Creek, which is the smallest catchment, records the lowest ³H activities in each 24 sampling round. There is, however, a broad correlation between the runoff coefficient and ³H activities Deleted:), which is

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1 as illustrated for the February 2014 samples in Fig. 3, with a similar relationship apparent in the other

2 sampling campaigns (Tables 1 and 2).

3 4.3. Major ion and stable isotope geochemistry

4 The δ^{18} O and δ^{2} H values of the Ovens River from all the sampling rounds overlap (Fig. 6). Overall the 5 δ^{18} O and δ^{2} H values define an array with a slope of ~5.5 and lowest δ^{18} O and δ^{2} H values of 6 approximately -7.4 and -41‰, respectively. In common with much groundwater and surface water in 7 the Murray Basin the δ^{18} O and δ^{2} H values of the Ovens River lie to the left of the Meteoric Water Line, 8 probably due to local climatic factors (Ivkovic et al., 1998; Leaney and Herczeg, 1999; Cartwright et al., 9 2012).

Na and Cl concentrations from the rainfall sample at Mount Buffalo are 0.97 and 1.1 mg L⁻¹ respectively 10 (Table 1), which are similar to the Na concentrations of 0.9 to 1.3 mg L⁻¹ and Cl concentrations 1.2 to 11 1.4 L⁻¹ reported for rainfall in this region of southeast Australia by Blackburn and McLeod (1983). Na 12 and Cl concentrations in stream water from the Ovens catchment range from 2.4 to 5.5 mg L^{-1} and 13 14 0.82 to 3.5 mg L⁻¹, respectively (Table 1). The concentrations of these and other major ions are higher during low-flow periods (February 2014) than during periods of higher flow. Na/Cl mass ratios of the 15 stream samples are between 1.4 and 4.2 which are higher than the Na/Cl ratios of local rainfall of 0.7 16 to 0.9 (Table, 1; Blackburn and McLeod, 1983). Since ³H activities are inversely correlated with 17 18 streamflow (Figs 4, 5), there is also a broad inverse correlation between ³H activities and Cl and Na 19 concentrations (Fig. 7).

A correlation between major ion concentrations and streamflow is also apparent on a longer time scale. Fig. 8a shows the variation of streamflow and Na concentrations at Harrietville made as part of routine geochemical measurements (Department of Environment and Primary Industries, 2015). The Na concentrations range from 1.3 to 2.2 mg L⁻¹ at high flows to ~4.4 mg L⁻¹ at low flows. As noted earlier, the Harrietville gauge records the combined streamflow from the Ovens East Branch and 1 Ovens West Branch; however, the Na vs. streamflow trends for these two tributaries are similar to

2 that from the Harrietville gauge (Fig. 8a), albeit with far less data.

3 5. Discussion

4 The combination of streamflow data, major ion concentrations, stable isotope geochemistry, and ³H

5 activities allow an understanding of the hydrogeology of the upper Ovens catchment to be made.

6 5.1. Changes to water stores with streamflow

7 One fundamental question relating to catchment hydrology is the extent to which water in streams at 8 high flows is event water largely derived from recent rainfall rather than older water displaced from stores within the catchment (Sklash and Farvolden, 1979; Rice and Hornberger, 1998; Uhlenbrook et 9 10 al., 2002; Kirchner et al., 2010). Resolution of this question is important to interpreting ³H activities. If significant dilution with event water occurs, any increases in ³H activities in the stream with increasing 11 flow (e.g. Figs 4, 5) may be the result of mixing between high ${}^{3}\!H$ event water and an older baseflow 12 13 component, and the ³H activities may be used to estimate the proportions of these two components (Morgenstern et al., 2010). By contrast, if water is displaced from the catchment during high rainfall 14 events, the ³H activities will reflect the mean transit time of that water and differences in ³H activities 15 with streamflow may reflect the mobilisation of water with different residence times from different 16 17 parts of the catchment.

In the upper Ovens Valley only the Harrietville gauge, which records the combined East Branch and 18 19 West Branch streamflow, has sufficient major ion data to assess the degree of mixing of baseflow with 20 event water. Figure 8a shows the calculated Na vs. streamflow trends resulting from the mixing of event water and baseflow at the Harrietville gauge using Eq. (4) and the following assumptions: 1) Na 21 22 concentrations at the lowest streamflow represents the Na concentrations of baseflow; 2) the 23 baseflow remains constant at the value of the minimum streamflow, in this case 6600 m³ day¹; and 24 3) rainfall has a Na concentration between 0.9 and 1.3 mg L⁻¹ (Blackburn and McLeod, 1983). The 25 calculated Na vs. mixing trend underestimates the observed Na concentrations in the stream at Moved up [12]: may be used to assess the degree of mixing of baseflow with event water (Sklash and Farvolden, 1979; Uhlenbrook et al., 2002; Godsey et al., 2009).
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1 Harrietville. A similar conclusion is also made for Na concentrations at the Rocky Point gauge, which

2 is ~25 km downstream of Myrtleford (Fig. 8b).

- 3 Similar conclusions may be made from the ³H activities, albeit the datasets are much smaller. Figure <u>4</u>
- 4 shows predicted ³H activities vs. streamflow trends constructed using Eq. (4) with similar assumptions

5 to those above, namely: 1) at low-flow conditions the streams derive all their water from baseflow

6 that has ³H activities of the February 2014 sampling campaign; 2) baseflow remains constant at the

7 streamflow recorded in February 2014; and 3) rainfall has a ³H activity between 2.5 and 3.0 TU which

- 8 spans the range of activities in Table 1. For all catchments the mixing trends over-estimate the ${}^{3}H$
- 9 activities of the stream water.
- 10 That the Na/Cl ratios of all stream samples, even those at high streamflow, exceed those of rainfall

11 implies that some Na is derived from the dissolution of minerals, probably predominantly plagioclase

- 12 <u>feldspar, from the soils, regolith, or bedrock. As mineral dissolution occurs over timescales months to</u>
- 13 years (Edmunds et al., 1982; Bullen et al., 1996; Morgenstern et al., 2010; Cartwright and
- 14 Morgenstern, 2012) this observation is also consistent with the interpretation that much of the water
- 15 in the stream has been mobilised from within the catchment.

16 δ^{18} O and δ^{2} H values of stream water define arrays with slopes of 4-6 (Table 1, Fig. <u>6</u>) that most likely 17 <u>reflects</u> a combination of instream evaporation, especially in February 2014, and <u>possibly</u> the altitude 18 effect where <u>stream water derived from</u> rainfall at higher altitudes has lower δ^{18} O and δ^{2} H values (c.f., 19 Clark and Fritz, 1997). The observation that the δ^{18} O and δ^{2} H values are similar at different flows is 20 consistent with the water contributing to the stream having been resident within the catchment for 21 sufficient time that any seasonal variations in rainfall δ^{18} O and δ^{2} H values have homogenised by 22 mixing.

Taken together the ³H activities, major ion concentrations, and stable isotope values are most consistent with a significant component of water in the stream at all flow conditions being derived from stores within the catchment that have a transit time of several years. High rainfall results in Moved down [13]: Na is derived from the dissolution of minerals, probably predominantly plagioclase feldspar, from the soils, regolith, or bedrock. As mineral dissolution occurs over timescales months to years (Edmunds et al., 1982; Bullen et al., 1996; Morgenstern et al., 2010; Cartwright and Morgenstern, 2012) this observation is also consistent with the interpretation that much of the water in the stream has been mobilised from within the catchment.

Deleted: An alternative way of viewing the major ion data is to define Na' as the concentration of Na in the stream water relative to that in rainfall (i.e. Na' = Nastream - Narain). This results in the rainfall component being defined as Na' = 0. As discussed by Godsey et al. (2009), streamflow vs concentration relationships for dilution of baseflow assuming that the diluent has a concentration of 0 follow a power law relationship with an exponent of -1, which produces log streamflow vs. log concentration trends with slopes of -1 (Fig. 8c). For a Na_{rain} value of 0.9 mg L⁻¹ the log Na' vs. log streamflow trend has a slope of -0.28 (Fig. 8c), while for a Na_{rain} value of 1.3 mg $L^{\text{-}1}$ the trend has a slope of -0.38 (not shown). While there is some scatter in the data and uncertainty regarding the rainfall Na concentrations, there are no values of Na_{rain} that result in a log Na' vs. log streamflow trend with a slope of -1 and it is difficult to explain the concentration vs. streamflow relationships as simple mixing between event water and baseflow. Rather these data are most consistent with much of the water in the stream being mobilised from within the catchment¶

That the Na/Cl ratios of all stream samples, even those at high streamflow, exceed those of rainfall implies that some of the **Deleted:** 3

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1 increased recharge that displaces older water from the soils, regolith, and sediments into the stream.

2 The variation in ³H activities with streamflow (Fig. 4) probably reflects the variation in the transit times

3 (discussed below) of water within these different stores and the variations in Na and Cl concentrations

4 (Fig. 7) reflect differences in chemistry between the water stores in the catchment.

5 5.2. Transit times of stream water in the Ovens Catchment

In common with studies of shallow groundwater flow elsewhere (Maloszewski et al., 1992; Cook and 6 7 Bohlke, 2000; Morgenstern et al., 2010), the calculations of mean transit times (Table 2, Fig. 9) were made assuming that groundwater flow had both exponential and piston flow components where the 8 9 distribution transit times are described by Eqs (1 and 2). While the aquifers adjacent to the streams are unconfined and thus are likely to exhibit exponential flow, recharge through the unsaturated zone 10 will most likely resemble piston flow (Cook and Bohlke, 2000; Morgenstern et al., 2010). Initial 11 12 calculations were carried out for f = 0.75 (EPM ratio = 0.33). Based on the variations of geochemistry with streamflow (Figs 3, 8) it was assumed that the water contributing to the streams during all 13 sampling campaigns was from baseflow. If the stream contains some event water that is diluting the 14 baseflow, this approach will yield a minimum transit time for the baseflow component. 15 The ³H input function is based on the annual average ³H activities of rainfall in Melbourne collected 16 17 for the International Atomic Energy Agency Global Network of Isotopes in Precipitation program as 18 summarised by Tadros et al. (2014). The ³H <u>activities</u> of the <u>two</u> aggregated rainfall <u>samples</u> from the 19 Ovens Valley of 2.85 and 2.99 TU (Table 1) are used to bracket the present day rainfall ³H activities. 20 Rainfall ³H activities reached ~62 TU in 1965 and then declined exponentially to present day values by

21 ~1995. ³_yH <u>activities</u> of <u>2.85 and 2.99</u> TU <u>were also</u> used for the pre-atmospheric nuclear test
 22 precipitation.

The exponential-piston flow model yields unique mean transit times for the range of measured ³H activities in the Ovens catchment (Table 2, Fig. 9). The longest mean transit times at each site are from the low-flow period in February 2014 and range from <u>8</u> years at Ovens East Branch to <u>30</u> years at **Deleted:** The calculations utilised the Excel workbook TracerLPM (Jurgens et al., 2012). TracerLPM specifies the ratio of exponential to piston flow as an EPM ratio, which is equivalent to 1/f - 1 and initial **Deleted:** assuming

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			Deleted:), which is within the expected range of modern average annual ³ H activities of rainfall in southeast Australia of 2.8 to 3.2 TU (Tadros et al., 2014), was
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Simmons Creek. Stream water from the two Morses Creek sites has mean transit times of 14 to 17
years while mean transit times of stream water from the two Buckland River sites are 10 to 12 years.
Mean transit times from the high-flow period (July 2014) calculating using the same exponential-flow
model are between 4 years at Upper Buckland and 9 years at Simmons Creek (Table 2, Fig. 9). Mean
transit times in the intermediate flow periods are between $\frac{7}{2}$ and 23 years for December 2013 and $\frac{4}{2}$
and <u>16</u> years for September 2014. In both these sampling campaigns Simmons Creek recorded the
longest mean transit times while the shortest mean transit times were at Bright (December 2013) and

8 Ovens East Branch (September 2014).

13

14

9 There are several uncertainties in these calculations that need to be assessed. Firstly, the calculated

- 10 transit times vary with the choice of model (Table 2). Using the exponential-piston flow model with f
- 11 = 0.5 (EPM ratio = 1), which represents an aquifer system with equal portions of piston and exponential
- 12 flow, yields mean transit times that range from <u>8</u> to 26 years in February 2014 and <u>4</u> to <u>9</u> years in July
- 2014. Using the exponential flow model (f = 1, EPM <u>ratio</u> = 0), yields mean transit times that range
- from <u>10</u> to <u>35</u> years in February 2014 and <u>5</u> to <u>12</u> years in July 2014. The dispersion model with $D_P =$
- 0.1 yields mean transit times between <u>8</u> and 29 years in February 2014 and <u>4</u> to <u>9</u> years in July 2014. 15
- 16 The absolute difference between the results from the models increases with the mean transit time.
- 17 For the highest ³H activity of 2.45 TU (Ovens East Branch in September 2014) the average mean transit
- 18 time from the four models is 3.7±0.4 years. For the lowest ³H activity of 1.63 TU (Simmons Creek in
- February 2014) the average mean transit time from the four models is 29.9±3.8 years. 19
- 20 Allowing the ³H activity of modern rainfall to vary between 2.85 and 2.99 also results in uncertainties
- 21 in the calculated mean transit times. For the exponential-piston flow model with f = 0.75, the standard
- 22 deviation of the mean transit times decreases from ~1.0 years at 4 years to <0.1 years at >20 years,
- 23 while the standard deviation of the mean transit times for the exponential-piston flow model with f =
- 24 0.5 decreases from ~0.9 years at 4 years to <0.1 years at >10 years. The standard deviation of the
- mean transit times in the exponential flow model decreases from ~0.9 years at 4 years to ~0.3 years 25
- at 35 years but has a maximum value of ~1.1 years at 10 to 15 years, whereas the standard deviation 26

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- 1 of the mean transit times in the dispersion model decreases from ~0.9 years at 4 years to <0.1 years
- 2 at 12 years. These differences reflect differences in the exit-age frequency distribution in the various
- 3 models (e.g. Cook and Bohlke, 2000).
- 4 The analytical uncertainty of the ³H activities produces uncertainties in the calculated mean transit
- 5 <u>times. The</u> ± 0.04 TU uncertainty for a sample with <u>a ³H activity of</u> 2 TU results in an uncertainty in
- 6 mean transit time of approximately ±1.5 years. The assumptions that the ³H activity of rainfall in the
- 7 Ovens was identical to that in Melbourne and that the ³H activity of the water that recharges the
- 8 catchment is that of average rainfall are difficult to assess. However, these issues impact all of the
- 9 <u>catchments and result in uncertainties in the absolute not the relative mean transit times. Given the</u>
- 10 range of mean transit times, uncertainties in the rainfall ³H activities before and during the bomb pulse
- 11 have less impact than any uncertainties in the modern ³H activities of rainfall.
- 12 <u>Finally</u>, the lumped parameter models are only an approximation of the flow through aquifer systems
- and real flow systems will differ to a greater or lesser extent. However, while this will have little impact
- 14 on the calculated variation in mean transit times in individual catchments at different streamflows as
- 15 the flow systems within a specific catchment will likely be similar over time. Hence, while there are
- 16 <u>uncertainties in the calculated mean transit times</u>, the conclusions that the mean transit times at the
- 17 lowest flow conditions are on the order of years to decades while at higher flow conditions the mean
- 18 transit times are at least a few years remain unaffected.
- 19 5.3. Controls on transit times
- 20 The mean transit times do not increase with catchment area and the smallest catchment (Simmons
- 21 Creek) records the longest transit times (up to <u>30</u> years in February 2014). There is little difference in
- 22 the geology or topography of the headwater sites implying that these are not factors which explain
- 23 the variation in transit times between the catchments. Drainage density can influence transit times as
- 24 it controls the distance between groundwater recharge areas and the nearest point of discharge in
- the stream (Morgenstern and Daughney, 2012). In the case of the upper Ovens catchment, there is

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little difference in drainage density between the catchments, and many of the larger catchments have
areas <u>that</u> are larger than the Simmons Creek catchment (~6 km²) <u>which</u> are devoid of streams that
flow during summer. These observations imply that drainage density is not the main control on transit
times.

5 River water from the three floodplain sites along the main Ovens Valley (Smoko, Bright, and 6 Myrtleford) have mean transit times that are not appreciably different from that of many of the 7 headwater streams (Figs 3, 4), <u>implying that there is not a large store of deep older groundwater</u> 8 contributing to baseflow in this stretch of the Ovens River. This conclusion is consistent with 9 observations that the ³H activities of shallow (<40 m) groundwater from the alluvial sediments in the 10 Ovens Valley between Myrtleford and Bright are >1 TU with most having ³H activities between 1.5 and 11 2.5 TU (Cartwright and Morgenstern, 2012).

12 There is a broad correlation between transit times and the runoff coefficient (Fig. 3). 13 Evapotranspiration during recharge is a dominant hydrological process in southeast Australia and the 14 native eucalyptus vegetation in particular has very high transpiration rates (Allison et al., 1990; Herczeg et al., 2001; Cartwright et al., 2012). While the catchments are similar, subtle differences in 15 soil type which controls the rate of infiltration, vegetation density, or regolith thickness may influence 16 17 evapotranspiration rates (Cartwright et al., 2006). Infiltration rates will vary inversely with the degree 18 of evapotranspiration and catchments with high evapotranspiration rates are likely to contribute 19 smaller volumes of relatively old water to the streams draining those catchments.

20 Regardless of the cause, the correlation between the runoff coefficient and ³H activities allows a first21 order estimation of likely transit times in similar catchments to be made which is useful for
22 management purposes. The correlation between Na and Cl concentrations and ³H activities (Figs 7, 9)
23 suggests that major ion geochemistry can also provide a first-order indication of the mean transit
24 times of baseflow. That the trends in Na ion concentrations and mean transit times from the different

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1 catchments overlap (Fig. 9) indicates that this approach may be useful in adjacent catchments with

2 similar geology, topography, and vegetation.

3 6. Conclusions and implications

4 This study has demonstrated the utility of high-precision ³H measurements in determining mean

5 transit times of water in headwater <u>catchments</u>. The observation that the water contributing to the

headwater streams in the Ovens catchment has mean transit times of years to decades implies that 6 7 these streams are buffered against rainfall variations on timescales of a few years, and most of these streams continued to flow through the 1996-2010 Millennium drought (Bureau of Meteorology, 2015; 8 9 Department of Environment and Primary Industries, 2015). However, the impacts of any changes to 10 landuse in these catchments or longer-term rainfall changes may take years to decades to manifest 11 itself in changes to streamflow or water quality. If the conclusion that the mean transit times are 12 controlled by the evapotranspiration rates in the catchments is correct, large scale vegetation changes, for example replacing native forest by grassland that has lower transpiration rates, will cause 13 14 a significant change in transit times. Specifically, lower transpiration rates will increase recharge that 15 will likely result in development of shallow flow paths with short transit times and also increase the 16 flow velocities in the deeper flow paths due to increased hydraulic heads. Both of these factors will likely reduce the mean transit times. 17

18 Author contributions

Both authors were involved in the design and realisation of the sampling program. UM carried out the
 ³H analyses and IC oversaw the analysis of the other geochemical parameters. IC prepared the
 manuscript with contributions from UM.

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- 3 (M. Hrachowitz) provided encouraging and helpful comments.
- 4

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1 Figure Captions

Figure 1. Summary geological and location map of the Ovens Catchment, data from Energy and Earth 2 3 Resources (2015). Sampling sites: BR = Bright, LBK = Lower Buckland, LMC = Lower Morses Creek, MY = Myrtleford, OEB = Ovens East Branch, OWB = Ovens West Branch, SC = Simmons Creek, SM = Smoko, 4 5 UBK = Upper Buckland, UMC = Upper Morses Creek. Localities: Br = Bright, Ha = Harrietville, My = Myrtleford, Mt B = Mount Buffalo; RP = Rocky Point, Wa = Wangaratta. Inset map shows location of 6 7 Ovens Valley relative to the Murray-Darling Basin (shaded); NSW = New South Wales, QLD = 8 Queensland, SA = South Australia, VIC = Victoria. 9 Figure 2a. Flow of the Ovens River at Bright between 2009 and 2014, arrows show timing of sampling 10 campaigns. 2b. Flow duration curve for Bright. Data from Department of Environment Primary 11 Industries (2015). 12 Figure 3. Runoff coefficient vs. ³H activities for February 2014. Bars show range of runoff coefficients 13 arising from the likely range of rainfall in the catchments, line is a logarithmic fit to the data that has a R^2 of 0.83. Open symbols are sampling sites on the main Ovens River, closed symbols are from the 14 15 headwater tributaries. BR = Bright, LBK = Lower Buckland, LMC = Lower Morses Creek, OEB = Ovens 16 East Branch, OWB = Ovens West Branch, SC = Simmons Creek. Data from Tables 1 and 2; precision of 17 ³H activities (Table 1) is approximately the size of the symbols. 18 Figure 4. ³H activities vs. streamflow for the main Ovens River (open symbols) and its headwater 19 tributaries (closed symbols); data from Table 1. Shaded fields depict mixing between baseflow, which 20 is assumed to have a ³H activity of the lowest streamflow at each site, and rainfall with a ³H activity of between 2.5 and 3.0 TU, which spans the range of rainfall ³H activities in Table 1, constructed using Eq. 21 22 4. The mixing model overestimates the ³H activities recorded at higher flows at all sites. 23 Figure 5. ³H activities vs catchment area for the main Ovens River (open symbols) and its headwater tributaries (closed symbols) and the range of rainfall ³H activities (aggregated rainfall samples shown 24

by solid <u>arrows</u>, other rainfall samples by dashed arrows); data from Table 1. BR = Bright, LBK = Lower

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Buckland, LMC = Lower Morses Creek, MY = Myrtleford, OEB = Ovens East Branch, OWB = Ovens West
 Branch, SC = Simmons Creek, SM = Smoko, UBK = Upper Buckland, UMC = Upper Morses Creek.
 Precision of ³H activities (Table 1) is approximately the size of the symbols.
 Figure 6. δ¹⁸O vs δ²H values for the main Ovens River (open symbols) and its headwater tributaries

5 (closed symbols) in the four sampling rounds; GMWL = Global Meteoric Water Line. Data from Table
6 1.

7 **Figure 7.** ³H activities vs. Na (**7a**) and Cl (**7b**) concentrations for the main Ovens River (open symbols)

8 and its headwater tributaries (closed symbols) in the four sampling rounds. Data from Table 1.

9 Figure 8. Na concentrations vs. streamflow for Harrietville (8a) and Rocky Point (8b), data from

10 Department of Environment and Primary Industries (2015). Fig. <u>8a</u> also shows Na vs streamflow for

11 the Ovens East Branch (OEB) and Ovens West Branch (OWB) tributaries which join just upstream of

12 the Harrietville gauge (Fig. 1). Shaded fields depict mixing between baseflow, which is assumed to

13 have a Na concentration of the lowest streamflow at each site, and rainfall with a Na concentration of

14 0.9 to 1.3 mg L⁻¹ calculated using Eq. 4. The mixing model underestimates the Na concentration

15 recorded at higher flows at both locations,

21

16 Figure 9. Mean transit times calculated using the Exponential-Piston Flow model vs. Na concentrations

17 for the sites in the Ovens catchment (data from Tables 1 and 2). There is a broad correlation between

18 mean transit time and Na concentration. BR = Bright, LBK = Lower Buckland, LMC = Lower Morses

19 Creek, MY = Myrtleford, OEB = Ovens East Branch, OWB = Ovens West Branch, SC = Simmons Creek,

20 SM = Smoko, UBK = Upper Buckland, UMC = Upper Morses Creek.

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Deleted: 8c. Rainfall corrected Na concentrations (Na') vs streamflow at Harrietville. The trend line has a slope of -0.27 which is significantly different to the dilution trend (slope of -1). **Formatted:** Font: Bold

Table 1. Geochemistry of the Ovens River and tributaries

Site ^a	Area ^b	Streamflow ^c	³Н	δ ¹⁸ Ο	δ²Η	CI	Na
	km²	10 ³ m ³ day ⁻¹	τυ	‰ SMOW	‰ SMOW	mg L ⁻¹	mg L ^{-:}
December 2013							
Ovens East Branch	72	110	2.265±0.035 ^d	-7.5	-41	0.93	2.26
Ovens West Branch	42	44	2.168±0.037	-7.5	-40	1.94	3.23
Simmons CK	6	2.34	1.812±0.036	-7.3	-41	2.49	4.21
Bright	302	269	2.280±0.040	-7.4	-40	1.36	2.88
Upper Morses Ck	32		2.134±0.036	-6.7	-38	1.18	2.94
Lower Morses Ck	123	34.2	2.032±0.036	-6.8	-37	1.25	2.91
Upper Buckland	77		2.186±0.040	-7.2	-41	0.82	3.43
Lower Buckland	435	181	2.253±0.036	-7.0	-39	1.13	3.49
Myrtleford	1240	784	2.243±0.036	-6.7	-38	1.43	2.72
Buffalo Rain			2.986±0.046			1.10	0.87
February 2014							
Ovens East Branch	72	15.9	2.189±0.046	-7.1	-41	1.73	3.3
Ovens West Branch	42	4.2	1.974±0.037	-7.1	-41	3.44	5.4
Simmons CK	6	1.13	1.634±0.032	-7.3	-42	3.47	4.7
Smoko	267		2.088±0.042	-7.1	-40	2.61	4.6
Bright	302	64.6	1.988±0.044	-7.0	-39	1.81	3.2
Upper Morses Ck	32	5.59	1.920±0.034	-6.5	-35	1.12	4.0
Lower Morses Ck	123		1.980±0.040	-6.4	-36	1.34	4.1
Upper Buckland	77	33.7	2.097±0.036	-7.2	-41	1.36	3.4
Lower Buckland	435	85.8	2.039±0.036	-6.5	-38	1.82	3.4
Myrtleford	1240		2.074±0.036	-6.8	-39	1.97	3.4
Buffalo Rain			2.859±0.049				
July 2014							
Ovens East Branch	72	407	2.327±0.046	-7.4	-41	0.92	2.04
Ovens West Branch	42	179	2.303±0.042	-7.3	-40	1.17	2.6
Simmons CK	6	10.5	2.121±0.041	-7.4	-41	1.63	3.3
Smoko	267		2.322±0.043	-7.3	-40	0.97	2.4
Bright	302	1566	2.340±0.045	-7.2	-39	1.39	2.6
Upper Morses Ck	32		2.306±0.047	-6.9	-37	1.12	2.7
Lower Morses Ck	123	301	2.259±0.042	-7.1	-38	1.19	2.9
Upper Buckland	77		2.431±0.044	-7.3	-40	1.21	3.0
Lower Buckland	435	1111	2.381±0.039	-7.1	-39	1.53	2.9
Myrtleford	1240	3925	2.306±0.038	-7.0	-38	1.66	2.8
Buffalo Rain			2.521±0.043				
September 2014							
Ovens East Branch	72	60.6	2.446±0.045	-7.5	-41	1.14	2.4
Ovens West Branch	42	24.1	2.191±0.038	-7.3	-40	1.29	3.4

Smoko	267		2.240±0.038	-7.2	-41	1.29	2.72
Bright	302	319	2.278±0.037	-7.1	-40	1.50	3.31
Upper Morses Ck	32		2.163±0.036	-6.8	-37	1.55	3.16
Lower Morses Ck	123	48.3	2.065±0.035	-6.7	-36	1.70	3.46
Upper Buckland	77		2.226±0.038	-7.2	-40	1.63	3.14
Lower Buckland	435	255	2.314±0.037	-6.7	-39	1.61	3.19
Myrtleford	1240	747	2.272±0.038	-6.8	-39	1.89	3.28
Buffalo Rain			2.714±0.044				
Buffalo Rain 2 ^f			2.850±0.057				

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a: Localities on Fig. 1 b: Area of catchment upstream of sampling site c: River discharge. Discharge for Ovens East Branch and Ovens West Branch estimated from the Harrietville

gauge as discussed in text.

d: The tritium error is individually calibrated and calculated for each sample as described by Morgenstern and Taylor (2009).

f: 12 month aggregated sample from second rain collector, collected in March 2015

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_Table 2. Calculated mean transit times for the Ovens River baseflow

1 2

Bright

Upper Morses Ck

Site ^a	RC ^b Mean Transit Times (years) ^c						
	%	EPF (0.33) ^d	EPF (1.0)	EF	DM	Mean ^e	
December 2013							
Ovens East							
Branch	52.7-64.1	7.2±0.7	<u>6.9±0.6</u>	8.4 <u>±1.0</u>	<u>7.3±0</u> .4	<u>7.4±0.7</u>	
	45. <u>*</u> 4-						
Ovens West	52.						
Branch	6	9. <u>1±0.</u> 6	<u>9.4±0.1</u>	<u>11.3±1.0</u>	9. <u>0±0.2</u>	<u>9.7±1.1</u>	
Simmons CK	6.7-8.1	22. <u>8±0.0</u>	17.7 <u>±0.0</u>	<u>26.6±0.7</u>	16.4 <u>±0.0</u>	<u>20.9±4.8</u>	
Bright	23.2-28.1	6.9±0.7	<u>6.6±0.7</u>	8. <u>0±1.0</u>	<u>7.0±0.4</u>	<u>7.1±0.6</u>	
Upper Morses							
Ck		<u>10.0±0.5</u>	10. <u>0±0.</u> 1	<u>12.5±1.1</u>	<u>9.8±0.4</u>	10. <u>6±</u> 1 <u>.3</u>	
Ck	24,2-30,4	13.0±0.4	11.7 <mark>±0.1</mark>	16.9±1.0	11.3±0.1	13.2±2.5	
Upper Buckland	00.1	8.8±0.6	8.9+0.2	10.7+1.1	8.8±0.1	9.3±0.9	
ower Buckland	29.1-35.4	7.6+0.8	7.4+0.3	8.7+1.0	7.6+0.1	7.8+0.6	
Myrtleford	25.1.33.4	7 8+0 9	7 5+0 3	9 0+1 0	7 8+0 1 -	8 0+0 7	
	23.7-31.1	7.010.0	<u>1.3±0.3</u>	J. J. 1.U.	<u>7.020.1</u>	0,010.7	
obruggy 2014						4	
Ovens Fast							
Branch	52.7-64.1	8.3±0.7	8.0±0.5	10. <u>1±1.1</u>	<u>8</u> .2 <u>±0.3</u>	<u>8.7±0.</u> 9	
Ovens West		_					
Branch	43.4-52.6	<u>14.3±0.4</u>	12. <u>6±0.0</u>	<u>18.2±1.0</u>	12, <u>2±0.1</u>	<u>14.3±2.8</u>	
Simmons CK	6.7-8.1	30. <u>3±0.0</u>	25. <u>8±0.0</u>	<u>34.8±0.3</u>	28. <u>7±0.0</u>	<u>29.9±3.7</u>	
	23.						
	2-	10.6 <mark>+0</mark>					
Smoko	1	.6	10. <u>6±0.1</u>	<u>13.6±1.1</u>	<u>9.9±0.3</u>	<u>11.2±1.7</u>	
Bright		13.8±0.4	12. <u>3±0.0</u>	17.8±10	<u>11.9±0.1</u>	13.9±2.7	
Jpper Morses		-					
Ck		<u>16.7±0.3</u>	13.7 <u>±0.0</u>	<u>20.9±0.8</u>	13. <u>3±0.1</u>	<u>16.1±3.5</u>	
Lower Morses	24 2-30 4	14 1+0 4	12 4 + 0 0	18 2+1 0	12 0+0 1	14 2+2 8	
Inner Buckland	24.2 30.4	10 4+0 6	10 5+0 1	13 3+1 1	10 0+0 3	11 1+1 5	
ower Buckland	29 1-35 /	12 1+0 5	11 /+0 1	15 6+1 0	11 0+0 1	12 5+2 1	
Myrtleford	25.1-55.4	11 0+0 5	10 7+0 1	1/1 2+1 1	10 2+0 1	11 6+1 9	
viyiticitit	23.7-31.1	<u>41.010.5</u>	10.7.10.1	<u>14.211.1</u>	10-210.1	11.011.0	
uly 2014							
ury 2014	52.						
	7-						
Ovens East	64.						
Branch	1	<u>5.5±0.8</u>	<u>4.9±</u> 0 <u>.9</u>	<u>6.3±</u> 1 <u>.0</u>	<u>4.9±0.9</u>	<u>5.4±0.7</u>	
Jvens West Branch	13 1-52 6	5 9+0 9	5 2+0 S	6 8+1 0	5 3+0 9	5 8+0 7	
Simmons CK	67-81	9 1+0 7	8 6+0 5	11 5+1 1	8 8+0 3	9 5+1 2	
Smoko	0.7-0.1 72 7 70 1	5.110.7	5 0±0 0	6 /+0 0	E 0±0.0	5 5±0 7	
MUKU	23.2-20.1	<u>5.7±0.9</u>	<u>2.0±0.8</u>	D.410.9	5.0±0.9	<u>5.5±0.7</u>	

<u>6.1±1.0</u>

<u>6.7±1.0</u>

<u>5.3±1</u>.0 <u>4.7±0.8</u>

<u>5.8±0.8</u> <u>5.2±0.8</u>

<u>4.7±0.9</u>

<u>5.3±0.9</u>

<u>5.2±0.6</u>

<u>5.8±0.7</u>

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Lower Morses Ck 24.2-30.4 6.4±0.7 5.8±0.8 7 .5±1.0 5 .9±0.8 6.4:	<u>+0.8</u>
CK 24.2-30.4 D.4±0.7 5.8±0.8 J .5±1.0 D .9±0.8 0.4	<u>±0.8</u>
Upper Buckland <u>4.1±0.8</u> <u>3.7±0.8</u> <u>4.6±0.9</u> <u>3.6±0</u> .9 <u>4.0</u>	<u>±0.5</u>
Lower Buckland 29.1-35.4 4.7±0.8 4.2±0.8 5.4±0.9 4.2±0.9 4.2±0.9 4.2±0.9	<u>±0.6</u>
Myrtleford 25.7-31.1 <u>5.8±0.8</u> <u>5.2±0.8</u> <u>6.7±1.0</u> <u>5.3±0.9</u> <u>5.8</u>	<u>+0.7</u>
September	
2014	1
Ovens East	1
Branch 52.7-64.1 3.7±1.0 3.5±0.8 4.3±1.0 3.4±0.8 3.7±	<u>±0.4</u>
Ovens West	
Branch 43.4-52.6 <u>7.6±0.7</u> <u>7</u> .0 <u>±0.7</u> <u>9.2±1</u> .1 <u>7.2±0.6</u> <u>7.7</u> :	<u>±1.0</u>
Simmons CK 6.7-8.1 15.8±0.4 13.6±0.0 2 0.4±1.0 13 1 ±0.1 15.5	<u>±3.3</u>
Smoko 23.2-28.1 <u>6.7±0.7</u> <u>6.1±0.8</u> <u>8.0±1.0</u> <u>6.3±0.7</u> <u>6.8</u>	<u>±0.8</u>
Bright 6.2±0.8 5.5±0.8 7.2±1.0 5.6±0.8 6.1:	<u>±0.8</u>
Upper Morses 7.8±0.5	
Ck <u>8.1±0.7</u> <u>7.5±0.6</u> <u>9.9±1.1</u> <u>8.3</u> :	<u>+1.1</u>
24.	1000 C
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Lower Morses 30.	and define
Ck 4 10.3±0.6 9.7±0.3 13.2±1.1 9.7±0.2 10.7	<u>±1.7</u>
Upper Buckland 7.0±0.7 <u>6.3±0.7</u> <u>8.3±1.0</u> <u>6.6±0.7</u> <u>7.0±</u>	<u>+0.9</u> •
Lower Buckland 29.1-35.4 5.6±0.8 5.0±0.8 6.5±1.0 5.0±0.9 5.5:	<u>±0.7</u>
Myrtleford 25.7-31.1 6.3±0.8 5.6±0.8 7.3±1.0 5.7±0.8 6.2	<u>±0.8</u>

a: Sites on Fig. 1.

b: Runoff coefficient, range reflects likely rainfall range in catchments

c: Lumped parameter models: EF = Exponential flow, DM = Dispersion model, EPF = Exponential-Piston flow

with EPM ratios of 0.33 and 1.0 $\,$

d: Model discussed in text

e: Mean and standard deviation of mean transit time from the four models f: Uncertainty calculated from different values of modern rainfall input as discussed in text

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