

1 **ANSWERS TO REFEREE#1**

2

3 1) I appreciate the improvements and additions made to the manuscript. The
4 structure was improved according to the editor's recommendation. Although very
5 long and difficult to understand sentences were partially shortened, there are still
6 relatively many language-related mistakes (e.g. the use of respectively on P8LL8)
7 that could be corrected to improve readability. Please do not report significant results
8 when not supported by the statistical analysis (P1LL26; also, no uncertainty of the
9 slope estimates are provided here which could help the readers to form an opinion
10 themselves). Similar issues had been criticized in the first version of the manuscript.

11

12 *ANSWER: Slopes estimates and simulations are reported along their estimated*
13 *errors (in the form of error bars in Figure 9a).*

14

15 2) Furthermore, in that paragraph (P1LL26), the description of potential outside air
16 influences and the comparison with slopes inferred using temperatures for a local
17 weather station remains somewhat confusing and seem somewhat in reverse, with
18 overall unclear implications. I think the authors could structure their thoughts more
19 clearly here.

20

21 *ANSWER: The authors think to the contrary that the text now explains the*
22 *phenomenon well. As proposed by the editor, the following sentence was added at*
23 *the end of the paragraph:*

24 *"This also highlights the particular experimental conditions in the laboratory, where*
25 *other sources of water vapor (e.g., by opening the laboratory door) might have*
26 *influenced the isotope compositions of the air."*

27

28 3) Abstract: Although the additional information is worth reporting, the abstract may
29 be shortened.

30

31 *ANSWER: the abstract was substantially shortened (~5 lines were removed)*

32

33 4) P4L28: Consider consistent use of SI units as suggested by the editor, also later in
34 the manuscript.

35

36 *ANSWER: this is now the case in the revised manuscript.*

37

38 5) P4L29: Please consider defining „o.d.“ for a non-technical audience.

39

1 *ANSWER: “o.d” and “i.d” are now “outside diameter” “inside diameter” in the revised*
2 *manuscript.*

3

4 6) P7L16: I suggest modifying the section title since the reference is not a proper
5 reference and also unusual in a title.

6

7 *ANSWER: “Craig and Gordon model” was erased from the title*

8

9 7) P8LL8: Please correct the use of respectively.

10

11 *ANSWER: The authors rewrote the section 2.7 omitting the term “resp.”.*

12

13 8) P13L14: Since the wind velocities are not the subject of study, consider putting it
14 differently, i.e. specific wind velocities may have caused the observed differences.

15

16 *ANSWER: In an evaporation study, the aerodynamic conditions in the “atmosphere”*
17 *are crucial; therefore wind velocity profiles are important. In addition, the authors do*
18 *not understand what the reviewer means by “specific wind velocity”.*

19

20 9) P16L12: Uncertainty values should not be set just arbitrarily; please provide a
21 (brief) justification for the choice of values.

22

23 *ANSWER: Indeed. The text was modified to:*

24 *“Standard errors for the parameters θ_{res} and θ_{sat} were set to 0.01 m³ m⁻³ (i.e.,*
25 *comparable to the soil water content probes’ precision)”*

1

2 **ANSWERS TO REFEREE#2**

3

4 1) The authors have answered to my questions and I do not want to argue with that.
5 But more importantly I appreciate very much the new section about testing the Craig
6 and Gordon model. This is exactly needed and it is these kind of questions that can
7 be addressed with the new method. The results are indeed puzzling and I would
8 have loved to see a possible explanation, if possible. The authors have unfortunately
9 never explained their definition of rh . And the explanation that ϵ_K should depend
10 on $rh_{EF}-rh$ looks odd to me. rh should be e_a/e_{EF} with $e_{EF}=rh_{EF}*e_{sat}(T_{EF})$
11 and e_a the vapour pressure of ambient air. Because of the Kelvin relationship and
12 as written in the manuscript, rh_{EF} is often taken as one. T_{EF} is changing over the
13 course of the experiment. Taking ambient rh would explain, for example, the rising
14 slope in Fig. 9a.

15

16 *ANSWER: ϵ_K does not depend on rh , but the kinetic effect is, as defined by*
17 *Equations 4a and b in the precedent manuscript. The kinetic effect evaluates both*
18 *impact of the water vapor potential gradient ($rh_{EF}-rh_a$) and resistance of the air layer*
19 *opposed to water vapor flow (i.e., expressed through ϵ_K). In addition, variations of*
20 *T_{EF} are taken into account: it is the normalized rh_a that is being computed (4.3*
21 *PP14LL15)*

22

23 2) It is there that I would have loved to see a bit more explanations. rh_{EF} is just one,
24 and in my opinion an unlikely one. But then, the experimental results seem unlikely
25 as well. Would have been great to see a bit more other formulations of n or ϵ_K
26 besides Mathieu and Bariac such as the formulations in the first SiSPAT_iso paper
27 (Braud et al., J of Hydrol. 309, 277-300, 2005).

28

29 *ANSWER: Yes that would have been great! Unfortunately, we did not measure a*
30 *wind distribution profile to use the formulation of Merlivat and Coantic (1975) based*
31 *on the evaporation model of Brutsaert (1982). The other formulations (Melayah et al.,*
32 *1996 and Barnes and Allison, 1983) give α_K constant over time (n is constant in*
33 *these cases), therefore won't be able to explain a change of evaporation line slope*
34 *value through change of n .*

35

36 3) This would have sensitized the authors to the sloppy formulations they are using
37 when talking about diffusion, boundary layer and the like. For example, the
38 resistance to molecular diffusion is not dependent on the n -th power of diffusivity
39 ratio.

40

41 *ANSWER: However, this is exactly what Mathieu and Bariac (1996) say, reporting*
42 *Merlivat and Coantic (1975): "Assuming that the turbulent transport is*
43 *nonfractionating and that the molecular diffusion resistances r_M and r^*_M are*
44 *proportional to the n th power of the diffusivities d_v and d^*_v ...".*

1 *Nevertheless, this was reformulated in 2.7 following the terminology of Gat et al.*
2 *(1971).*

3

4 4) The diffusivity ratio gives directly the kinetic fractionation factor of molecular
5 diffusion ($n=1$). $n=2/3$ is taken for boundary layer resistance. Turbulent transfer
6 should have no fractionation at all, i.e. $n=0$. But there is always a boundary layer
7 even over free water surfaces, so $n=0.5$ is an effective n .

8 Also the term boundary layer over the evaporating front is misleading. If the
9 evaporative front is in the soil, then there is the soil matrix above the evaporative
10 front, which most people would not have called a boundary layer but rather a layer of
11 molecular resistance. Above the soil then comes the atmospheric boundary layer.

12

13 *ANSWER: Indeed, this term is no longer used in that way in the current manuscript.*
14 *Thank you.*

15

16 5) The data is in my opinion not a test of Craig and Gordon but rather (of the
17 formulation) of the kinetic fractionation factor. Might be different point of view.

18

19 *ANSWER: This is right, this is now reformulated in the abstract as a test of the*
20 *formulation of isotope kinetic effects and section 4.3 title is now "Isotope kinetic*
21 *effects during soil evaporation"*

22

23 6) So I would ask the authors to provide explanations about r_h , e.g. by plotting it also
24 in Fig. 9b; revisit their wording and explanations about diffusion, boundary layer and
25 the like; and perhaps also include some other formulations for ϵ_{ps_k} to find some
26 reasoning behind the unexpected results.

27

28 *ANSWER: See answers to comments 1)-4). In 4.3 is now the following § added:*

29 *"In a fourth scenario, the ratio of turbulent diffusion resistance to molecular diffusion*
30 *resistance is no more negligible, leading to n' values ranging between 0 and n*
31 *(Merlivat and Jouzel, 1979). This last scenario was however not verifiable. In any*
32 *case, only decreasing kinetic effects could provide a better model-to-data fit. Note*
33 *that the formulation of kinetic enrichments proposed by Merlivat and Coantic (1975)*
34 *and based on the evaporation model of Brutsaert (1982) was not tested due to lack*
35 *of appropriate data (i.e., unknown wind distribution profile over the soil column). The*
36 *formulations of Mélayah et al. (1996) ($n = 0$) and Barnes and Allison (1983) ($n = 1$)*
37 *were also not tested as they give kinetic enrichments constant over time and cannot*
38 *explain a change of SE_v value through change of n ."*

39

Long-term and high frequency non-destructive monitoring of water stable isotope profiles in an evaporating soil column

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Abstract

The stable isotope compositions of soil water ($\delta^2\text{H}$ and $\delta^{18}\text{O}$) carry important information about the prevailing soil hydrological conditions and for constraining ecosystem water budgets. However, they are highly dynamic, especially during and after precipitation events. ~~The classical method of determining soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ at different depths, i.e., soil sampling and cryogenic extraction of the soil water, followed by isotope ratio mass spectrometer analysis is destructive and laborious with limited temporal resolution. In this study, we present an application of~~ In this study, we present an application of a method based on gas-permeable tubing and isotope-specific infrared laser absorption spectroscopy for *in situ* determination of $\delta^2\text{H}$ and $\delta^{18}\text{O}$. We conducted a laboratory experiment ~~with an acrylic glass column filled with medium~~ where a sand ~~equipped with gas permeable tubing at eight different soil depths. The soil~~ column was initially saturated ~~from the bottom~~, exposed to evaporation for a period of 290 days, and finally rewatered. Soil water vapor $\delta^2\text{H}$ and $\delta^{18}\text{O}$ were measured daily, ~~sequentially for at~~ each ~~depth of eight available depths.~~ Soil liquid water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ were inferred from ~~the isotopic values~~ those of the vapor assuming thermodynamic equilibrium between liquid and vapor phases in the soil. The experimental setup allowed following the evolution of ~~typical exponential-shaped~~ soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ profiles with ~~unprecedentedly high~~ a daily temporal resolution. As the soil dried, we could also show for the first time the increasing influence of the isotopically depleted ambient water

1 vapor on the isotopically enriched liquid water close to the soil surface (i.e., atmospheric
2 invasion). Rewatering at the end of the experiment led to instantaneous resetting of the stable
3 isotope profiles, which could be closely followed with the new method.

4 From simple soil $\delta^2\text{H}$ and $\delta^{18}\text{O}$ gradients calculations, we showed that the gathered data
5 allowed to determinate the depth of the Evaporation Front (EF) and how it receded into the
6 soil overtime. It was inferred that after 290 days under the prevailing ~~laboratory air~~
7 ~~temperature, moisture, and aerodynamic experimental~~ conditions, ~~and given the specific~~
8 ~~hydraulic properties of the sand,~~ the EF had moved down to an approximate depth of -0.06 m.
9 Finally, data was used to calculate evaporation lines' slopes and test the
10 expression formulation for ~~the slope of evaporation lines proposed by Gat (1971) and based on~~
11 ~~the model of Craig and Gordon (1965)-isotope kinetic effects.~~ A very good agreement was
12 found between measured and simulated values (Nash and Sutcliffe Efficiency - NSE = 0.92)
13 during the first half of the experiment, i.e., until the EF reached a depth of -0.04 m. From this
14 point, calculated kinetic effects associated with the transport of isotopologues in the soil
15 surface air layer above the EF provided slopes lower than observed. Finally, values of isotope
16 kinetic effects that provided the best model-to-data fit (NSE > 0.9) were obtained from
17 inverse modelling, highlighting uncertainties associated with the determinations of isotope
18 kinetic fractionation and soil relative humidity at the EF.

20 **1 Introduction**

21 Stable isotopologues of water, namely $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ are powerful tools used in a wide
22 range of research disciplines at different and complementary temporal and spatial scales. They
23 provide ways of assessing the origin of water vapor (e.g., Craig, 1961; Liu et al., 2010),
24 solving water balances of lakes (Jasechko et al., 2013) and studying groundwater recharge
25 (Blasch and Bryson, 2007; Peng et al., 2014). Analysis of the isotope compositions ($\delta^2\text{H}$ and
26 $\delta^{18}\text{O}$) of soil surface and leaf waters allows for partitioning evapotranspiration into
27 evaporation and transpiration (e.g., Dubbert et al., 2013; Hu et al., 2014; Rothfuss et al., 2012;
28 Yopez et al., 2005).

29 Moreover, from soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ profiles, it is also possible to derive quantitative
30 information, such as soil evaporation flux, locate evaporation fronts, and root water uptake
31 depths (Rothfuss et al., 2010; Wang et al., 2010). Zimmermann et al. (1967) and later Barnes
32 and Allison (1983, 1984) and Barnes and Walker (1989) first analytically described soil

1 $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ movement at steady / non-steady state and in isothermal/ non-isothermal
2 soil profiles. Between precipitation events, the soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ profiles depend on
3 flux boundary conditions, i.e., fractionating evaporation and non-fractionating capillary rise as
4 well as on soil properties (e.g., soil tortuosity). In a saturated soil, the isotope excess at the
5 surface due to evaporation diffuses back downwards, leading to typical and well documented
6 exponential-shaped $\delta^2\text{H}$ and $\delta^{18}\text{O}$ profiles. For an unsaturated soil, assuming in a first
7 approximation that isotope movement occurs in the vapor phase above the soil “evaporation
8 front” (EF) and strictly in the liquid phase below it, the maximal $\delta^2\text{H}$ and $\delta^{18}\text{O}$ values are no
9 longer observed at the surface but at the depth of EF. Above the EF, in the so-called “vapor
10 region”, according to Fick’s law, soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ decrease towards the depleted
11 ambient atmosphere water vapor $\delta^2\text{H}$ and $\delta^{18}\text{O}$. Braud et al. (2005), Haverd and Cuntz (2010),
12 Rothfuss et al. (2012), Singleton et al. (2004), and Sutanto et al. (2012) implemented the
13 description of the transport of $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ in physically based soil-vegetation-
14 atmosphere transfer (SVAT) models (HYDRUS 1D, SiSPAT-Isotope, Soil-Litter iso,
15 TOUGHREACT). In these models, movement of soil $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ occur in both
16 phases below and above the EF, and heat and water transports are properly coupled.

17 However, these tools suffer from the comparison with other “traditional” methods developed
18 to observe and derive soil water state and transport. In contrast with soil water content and
19 tension measured by, e.g., time-domain reflectometry and tensiometry, isotope compositions
20 of soil water are determined either following destructive sampling or non-destructively but
21 with poor spatial and temporal resolution (i.e., with section cups in combination with
22 lysimeters for soil water tension higher than -600 hPa, e.g., Goldsmith et al., 2011, Litaor,
23 1988). This greatly limits their informative value. Only since recently, non-destructive
24 methodologies based on gas-permeable membrane and laser spectroscopy can be found in the
25 literature (Rothfuss et al., 2013; Herbstritt et al., 2012; Volkmann and Weiler, 2014, Gaj et
26 al., 2015).

27 The central objective of this study was to demonstrate that a direct application of the method
28 of Rothfuss et al. (2013) to a soil column would allow monitoring soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$
29 profiles in the laboratory with high temporal resolution and over a long time period. We will
30 demonstrate that the obtained isotope data can be used to locate the evaporation front as it
31 recedes into the soil during the experiment. Finally, data will be also used to test the

1 expression proposed by Gat (1971) and based on the Craig and Gordon (1965) of evaporation
2 lines' slopes.

3

4 **2 Material and methods**

5 **2.1 Isotopic analyses**

6 Isotopic analysis of liquid water and water vapor was performed using a cavity ring-down
7 spectrometer (L1102-i, Picarro, Inc., Santa Clara, CA, USA), calibrated against the
8 international primary water isotope standards V-SMOW2, GISP, and SLAP by liquid water
9 injection into the vaporizer of the analyzer. Primary and working standards' isotope
10 compositions were measured at 17,000 ppmv water vapor mixing ratio (number of replicates
11 = 4, number of injections per replicate = 8). Mean values and standard deviations were
12 calculated omitting the first three values of the first replicate to account for a potential
13 memory effect of the laser spectrometer. The laser spectrometer's dependence on water vapor
14 mixing ratio was also investigated according to the method of Schmidt et al. (2010).
15 Hydrogen and oxygen isotope ratios of water are expressed in per mil (‰) on the
16 international "delta" scale as defined by Gonfiantini (1978) and referred to as $\delta^2\text{H}$ and $\delta^{18}\text{O}$,
17 respectively.

18 **2.2 Soil column and measurements**

19 The experiment was conducted in a 0.0057 m³ acrylic glass column (0.11 m ~~i.d.~~inside
20 diameter, 0.60 m height, Fig. 1a). The bottom of the column consisted of a porous glass plate
21 (10 ~~µm~~10⁻⁶ m < pore size diameter < 16 ~~µm~~10⁻⁶ m (4th class), Robu® GmbH, Hattert,
22 Germany) connected to a two-way manual valve (VHK2-01S-06F, SMC Pneumatik GmbH,
23 Germany).

24 Three ports were available at each of eight different depths (-0.01, -0.03, -0.05, -0.07, -0.10,
25 -0.20, -0.40, and -0.60 m): one inlet for the carrier gas, i.e., synthetic dry air (20.5 % O₂ in
26 N₂, with approx. 20-30 ppmv water vapor; Air Liquide, Germany), one sample air outlet, and
27 one duct for a soil temperature (T_s) sensor (type K thermocouple, Greisinger electronic
28 GmbH, Regenstauf, Germany; precision: 0.1°C). An additional fourth port at depths -0.01, -
29 0.03, -0.05, -0.10, -0.20, and -0.60 m was used for the measurement of soil volumetric water
30 content (θ) (EC-5, Decagon Devices, USA; precision: 0.02 m³ m⁻³).

1 At each depth inside the column a 0.15 m long piece of microporous polypropylene tubing
2 (Accurel® PP V8/2HF, Membrana GmbH, Germany; ~~0.155 cm~~ $1.55 \cdot 10^{-3} \text{ m}$ wall thickness,
3 ~~0.55 cm i.d., 0.86 cm o.d.~~ $5.5 \cdot 10^{-3} \text{ m}$ inside diameter, $8.6 \cdot 10^{-3} \text{ m}$ outside diameter) was
4 connected to the gas inlet and outlet port. The tubing offers the two advantages of being gas-
5 permeable (pore size of $0.2 \cdot 10^{-6} \text{ m}$) and exhibiting strong hydrophobic properties to
6 prevent liquid water from intruding into the tubing. It allows sampling of soil water vapor
7 and, hence, the determination of the isotope composition of soil liquid water (δ_{Sliq}) in a non-
8 destructive manner considering thermodynamic equilibrium between liquid and vapor phases
9 as detailed by Rothfuss et al. (2013).

10 **2.3 Internal isotope standards**

11 Two internal standards (“st1” and “st2”) were prepared using the same procedure as described
12 by Rothfuss et al. (2013). Two closed acrylic glass vessels (0.122 m i.d., 0.22 m height), in
13 each of which a 0.15 meter long piece of tubing as well as a type K thermocouple were
14 installed, were filled with FH31 sand (porosity = $0.34 \text{ m}^3 \text{ m}^{-3}$, dry bulk density = 1.69 g
15 $\text{cm}^3 \cdot 10^3 \text{ kg m}^3$, particle size distribution: 10% ($> 0.5 \text{ mm} \cdot 10^{-3} \text{ m}$), 72% ($0.25 - 0.5 \text{ mm} \cdot 10^{-3} \text{ m}$),
16 and 18% ($< 0.25 \text{ mm} \cdot 10^{-3} \text{ m}$)) (Merz et al., 2014; Stingaciu et al., 2009). Each vessel was
17 saturated with water of two different isotope compositions: $\delta^2\text{H}_{\text{st1}} = -53.51 (\pm 0.10) \text{ ‰}$,
18 $\delta^{18}\text{O}_{\text{st1}} = -8.18 (\pm 0.06) \text{ ‰}$ and $\delta^2\text{H}_{\text{st2}} = +15.56 (\pm 0.12) \text{ ‰}$, $\delta^{18}\text{O}_{\text{st2}} = +8.37 (\pm 0.04) \text{ ‰}$. Soil
19 water vapor from each vessel was sampled eight times per day for 30 min during the whole
20 experiment.

21 **2.4 Atmospheric measurements**

22 Laboratory air was sampled passively with a 1/8” three meter-long stainless steel tubing at 2
23 m above the sand surface for isotope analysis of water vapor (δ_a). Air relative humidity (rh)
24 and temperature (T_a) were monitored at the same height with a combined rh and T_a sensor
25 (RFT-2, UMS GmbH, Germany; precision for rh and T_a were 2 % and 0.1°C , respectively).
26 Vapor pressure deficit (vpd) was calculated from rh and T_a data using the Magnus-Tetens
27 formula (Murray, 1967) for saturated vapor pressure. The laboratory was air-conditioned and
28 ventilated with seven axial fans (ETRI 148VK0281, 117 l s^{-1} airflow, ETRI/Rosenberg, USA)
29 positioned at 1.80 m height above the sand surface.

1 2.5 Sampling protocol and applied isotopic calibrations

2 The column was filled in a single step with FH31 sand and carefully shaken in order to reach
3 a dry bulk density close to *in situ* field conditions. The sand was then slowly saturated from
4 the bottom from an external water tank filled with st1 water on December 2, 2013. After
5 saturation, the column was disconnected and sealed at the bottom using the two-way manual
6 valve. It was finally installed on a balance (Miras 2 – 60EDL, Sartorius, USA), and let to
7 evaporate for a period of 290 days in a ventilated laboratory.

8 δ_{Sliq} was determined in a sequential manner at each available depth once a day following the
9 method developed by Rothfuss et al. (2013) (Fig. 1b). Dry synthetic air at a rate of 50 ml min⁻¹
10 from a mass flow controller (EL-FLOW Analog, Bronkhorst High Tech, Ruurlo, The
11 Netherlands) was directed to the permeable tubing for 30 minutes at each depth. The sampled
12 soil water vapor was diluted with dry synthetic air provided by a second mass flow controller
13 of the same type. This allowed (i) reaching a water vapor mixing ratio ranging between
14 17,000 and 23,000 ppmv (where L1102-i isotope measurements are most precise) and (ii)
15 generating an excess flow downstream of the laser analyser. By doing this, any contamination
16 of sample air with ambient air would be avoided. The excess flow was measured with a
17 digital flow meter (ADM3000, Agilent Technologies, Santa Clara, CA, USA). The last 100
18 observations (corresponding to approx. 10 minutes) at steady state (standard deviations <0.70
19 ‰ and <0.20 ‰ for $\delta^2\text{H}$ and $\delta^{18}\text{O}$, respectively) were used to calculate the raw isotope
20 compositions of soil water vapor (δ_{Svap}). The latter was corrected for the water vapor mixing
21 ratio dependence of the laser analyzer readings with 17,000 ppmv as reference level.
22 Measurements that did not fulfil the above mentioned conditions for $\delta^2\text{H}$ and $\delta^{18}\text{O}$ standard
23 deviations were not taken into account. Finally, these corrected values were used to infer the
24 corresponding δ_{Sliq} at the measured T_{S} (Eq. (1) and (2); taken from Rothfuss et al., 2013):

$$25 \quad \delta^2\text{H}_{\text{Sliq}} = 104.96 - 1.0342 \cdot T_{\text{S}} + 1.0724 \cdot \delta^2\text{H}_{\text{Svap}} \quad (1)$$

$$26 \quad \delta^{18}\text{O}_{\text{Sliq}} = 11.45 - 0.0795 \cdot T_{\text{S}} + 1.0012 \cdot \delta^{18}\text{O}_{\text{Svap}} \quad (2)$$

27 The isotope composition of laboratory water vapor (δ_{a}) was measured eight times a day. δ_{a} ,
28 δ_{Svap} , and δ_{Sliq} values were finally corrected for laser instrument drift with time, using the
29 isotope compositions of the two water standards, δ_{st1} and δ_{st2} .

30 Water vapor of the ambient air, of both standards, and from the different tubing sections in the
31 soil column were sampled sequentially in the following order: soil (0.60 m) – soil (0.40 m) –

1 atmosphere – st1 – st2 – soil (0.20 m) – soil (0.10 m) – atmosphere – st1 – st2 – soil (0.07 m)
 2 – soil (0.05 m) – atmosphere – st1 – st2 – soil (0.03 m) – soil (0.01 m). Atmosphere water
 3 vapor was sampled twice as long (i.e., one hour) as soil water vapor from the
 4 column/standards so that each sequence lasted exactly 10 hours and started each day at the
 5 same time. The remaining 14 hours were used for additional standard and atmosphere water
 6 vapor measurements (i.e., on five occasions each).

7 2.6 Irrigation event

8 On Day of Experiment (DoE) 290 at 09:30 the sand surface was irrigated with 70 mm of st1
 9 water. This was achieved over one hour in order to avoid oversaturation of the sand and avoid
 10 preferential pathways that would have affected the evaporation rate. For this, a 2 L
 11 polyethylene bottle was used. Its bottom was perforated with a set of 17 holes of 5 mm
 12 diameter and its cap with a single hole through which a PTFE bulkhead union tube fitting
 13 (Swagelok, USA) was installed. The bulkhead fitting was connected to a two-way needle
 14 valve (Swagelok, USA). Opening/closing the valve controlled the flow rate at which air
 15 entered the bottle headspace, which in turn controlled the irrigation flow rate.

16 To better observe the dynamics directly following the irrigation event, water vapor was
 17 sampled at a higher rate, i.e., 1, 3, 4, 5, 6, 9, 11, and 11 times per day at –0.60, –0.40, –0.20, –
 18 0.10, –0.07, –0.05, –0.03, and –0.01 m. Water vapor from both standards was sampled twice a
 19 day. The experiment was terminated after 299 days on September 26th, 2014.

20 2.7 Evaporation lines (~~Craig and Gordon model, 1965~~)

21 Gat et al. (1971) proposed an expression based on the model of Craig and Gordon (1965) for
 22 the slope of the so-called “evaporation line” (S_{Ev} , [-]) which quantifies the relative change in
 23 $\delta^2\text{H}\delta^2\text{H}_{\text{Sliq}}$ and $\delta^{18}\text{O}\delta^{18}\text{O}_{\text{Sliq}}$ in a water body undergoing evaporation:

$$\begin{aligned}
 24 \quad S_{Ev} &= \frac{\Delta(\delta^2\text{H}_{\text{Sliq}})}{\Delta(\delta^{18}\text{O}_{\text{Sliq}})} = \frac{rh \cdot (\delta^2\text{H}_a - \delta^2\text{H}_{\text{Sliq_ini}}) + \varepsilon_{eq}^{2\text{H}} + \Delta\varepsilon^{2\text{H}}}{rh \cdot (\delta^{18}\text{O}_a - \delta^{18}\text{O}_{\text{Sliq_ini}}) + \varepsilon_{eq}^{18\text{O}} + \Delta\varepsilon^{18\text{O}}} \\
 25 \quad S_{Ev} &= \frac{\Delta(\delta^2\text{H}_{\text{Sliq}})}{\Delta(\delta^{18}\text{O}_{\text{Sliq}})} = \frac{\left[rh \cdot (\delta_a - \delta_{\text{Sliq_ini}}) + \varepsilon_{eq} + \Delta\varepsilon \right]_{2\text{H}}}{\left[rh \cdot (\delta_a - \delta_{\text{Sliq_ini}}) + \varepsilon_{eq} + \Delta\varepsilon \right]_{18\text{O}}} \quad (3)
 \end{aligned}$$

26 ~~where $\Delta\varepsilon^{2\text{H}}$ (resp. $\Delta\varepsilon^{18\text{O}}$) is the so-called “isotope kinetic effect” associated with $^1\text{H}^2\text{H}^{16}\text{O}$~~
 27 ~~(resp. $^1\text{H}_2^{18}\text{O}$) vapor transport:~~

$$\Delta \epsilon^{2\text{H}} = (1 - rh) \cdot \epsilon_K^{2\text{H}} \quad (4a)$$

$$\Delta \epsilon^{18\text{O}} = (1 - rh) \cdot \epsilon_K^{18\text{O}} \quad (4b)$$

~~$\delta^{2\text{H}}_{\text{Sliq}}$ with $\delta_{\text{Sliq_ini}}$ (resp. $\delta^{18\text{O}}_{\text{Sliq_ini}}$) is the initial soil water (hydrogen or oxygen) liquid $\delta^{2\text{H}}$ (resp. $\delta^{18\text{O}}$) isotope composition, i.e., prior removal of water vapor by fractionating evaporation. $\epsilon_{\text{eq}}^{2\text{H}}$ (resp. $\epsilon_{\text{eq}}^{18\text{O}}$) and $\epsilon_K^{2\text{H}}$ (resp. $\epsilon_K^{18\text{O}}$) are the ϵ_{eq} [-, expressed in ‰] is the equilibrium and kinetic enrichment in either $^1\text{H}^2\text{H}^{16}\text{O}$ (resp. or $^1\text{H}_2^{18}\text{O}$) enrichments. $\epsilon_{\text{eq}}^{2\text{H}}$ (resp. $\epsilon_{\text{eq}}^{18\text{O}}$). It is defined by the deviation from unity of the ratio between water and $^1\text{H}^2\text{H}^{16}\text{O}$ (resp. $^1\text{H}_2^{18}\text{O}$) isotopologue saturated vapor pressures and can be calculated using the empirical closed-form equations proposed by, e.g., Majoube (1971). $\epsilon_K^{2\text{H}}$ (resp. $\epsilon_K^{18\text{O}}$) $\Delta \epsilon$ [-, expressed in ‰] is defined as the deviation from unity of the ratio between the resistances so-called “isotope kinetic effect” associated with the transport of $^1\text{H}^2\text{H}^{16}\text{O}$ (resp. and $^1\text{H}_2^{18}\text{O}$) vapor in the boundary air layer above the evaporating surface and that of water vapor. By assuming transports. Assuming that (i) turbulent transport is a non-fractionating process and (considering that (ii) resistance associated with the ratio of molecular diffusion of $^1\text{H}^2\text{H}^{16}\text{O}$ (resp. $^1\text{H}_2^{18}\text{O}$) vapor is inversely proportional resistance to the n^{th} power of the corresponding diffusivity ($D^{2\text{H}}$, resp. $D^{18\text{O}}$), total resistance equals one, it follows that (Gat, 2000):~~

$$\Delta \epsilon = (1 - rh) \cdot \left(\frac{D^v}{D_i^v} - 1 \right) \cdot n \quad (4)$$

~~In Equation (4), the product $\left(\frac{D^v}{D_i^v} - 1 \right) \cdot n$ is the isotope kinetic enrichment (ϵ_K , [-, expressed in ‰]). In the present study, values for ratios of diffusivities (D^v/D_i^v) were taken from Merlivat and Coantic (1975) proposed the following expressions: (1978):~~

$$\epsilon_K^{2\text{H}} = \left(\frac{D}{D^{2\text{H}}} \right)^n - 1 = (1.0251)^n - 1 \quad \begin{cases} \frac{D^v}{D^{2\text{H}}} = 0.9755 \\ \frac{D^v}{D^{18\text{O}}} = 0.9723 \end{cases} \quad (5a)$$

$$\epsilon_K^{18\text{O}} = \left(\frac{D}{D^{18\text{O}}} \right)^n - 1 = (1.0285)^n - 1 \quad (\text{and } 5b)$$

1 The ~~exponent term~~ n accounts for the aerodynamic ~~regime above the liquid-vapor interface~~
2 ~~(i.e., where the relative humidity is 100%) in the air boundary layer~~ and ranges from $n_a = 0.5$
3 ~~(fully-turbulent diffusion, i.e., atmosphere-controlled conditions)~~ to $n_s = 1$ ~~(fully~~
4 ~~diffusivemolecular diffusion, i.e., soil-controlled conditions)~~ with a value of $\frac{2}{3}$ corresponding
5 to laminar flow conditions (Dongmann et al., 1974, Brutsaert, 1975). ~~In We tested the present~~
6 ~~study, values for ratios of diffusivities (D/D^{2H} and D/D^{18O}) were taken from Merlivat (1978)~~
7 ~~and formulation proposed by Mathieu and Bariac (1996) where n was considered as a~~
8 function of soil water content ~~as proposed by Mathieu and Bariac (1996):~~

$$9 \quad n = \frac{(\theta_{\text{surf}} - \theta_{\text{res}}) \cdot n_a + (\theta_{\text{sat}} - \theta_{\text{res}}) \cdot n_s}{\theta_{\text{sat}} - \theta_{\text{res}}} \quad (6)$$

10 with θ_{res} , θ_{sat} , and θ_{surf} the residual, saturated and surface soil water contents ($[m^3 m^{-3}]$).

11 Note that Equation (3) contrasts with the expression for the slope characterizing equilibrium
12 processes (e.g., precipitation formation) and therefore strictly temperature-dependant (i.e.,
13 $S_{eq} = \varepsilon_{eq}^{2H} / \varepsilon_{eq}^{18O}$). While S_{eq} might range for instance from 7.99 to 8.94 (for temperatures
14 spanning between 5 and 30°C), a much wider spread in S_{Ev} values is possible and has been
15 measured between 2 and 6 (Barnes and Allison, 1988, Brunel et al., 1995, DePaolo et al.,
16 2004).

17 3 Results

18 3.1 Example of a measuring sequence

19 Figure 2 shows exemplarily the measuring sequence for DoE 150. Soil and standards water
20 vapor mixing ratios were stable and ranged from 17,200 to 18,200 ppmv during the last 10
21 minutes of each sampling period (Fig. 2a). δ_{Svap} was within the range spanned by δ_{st1vap} and
22 δ_{st2vap} for both 2H and ^{18}O (Fig. 2b). On DoE 150, the soil surface was sufficiently dry so that
23 atmospheric invasion of water vapor had started to significantly influence the δ_{Svap} of the
24 upper soil layers. Therefore, δ_{Svap} measured at -0.01 m was lower than at -0.03 m for both 2H
25 and ^{18}O , but less pronounced for 2H .

1 3.2 Time courses of air temperature, relative humidity and atmospheric $\delta^2\text{H}$ 2 and $\delta^{18}\text{O}$

3 During the experiment, the laboratory air temperature ranged from 15.6 to 22.5 °C (average:
4 18.7 ± 1.5 °C, Fig. 3a) and the relative humidity from 19 to 69 % (average: $40 \% \pm 0.08 \%$,
5 Fig. 3a). Lower values of δ_a were observed from DoE 0 to 125 at lower air temperatures,
6 whereas higher values occurred after DoE 125 at higher air temperatures (Fig. 3b).

7 3.3 Evolution of soil water content, temperature, evaporation flux, and δ_{Svap} 8 from DoE 0-290

9 The soil temperature ranged from 16.2 to 22.3 °C (average: 18.6 ± 1.3 °C, data not shown)
10 and closely followed that in the air, i.e., differences between daily mean soil and air
11 temperatures ranged from -0.2 to 0.2 °C during the experiment. Following the saturation of
12 the column, a strong decrease in water content was observed in the upper 10 cm, whereas
13 after 287 days the sand was still saturated at -0.60 m (Fig. 4a). Figure 4b shows the time
14 series of evaporation flux normalized by the vapor pressure deficit in the laboratory air
15 (Ev/vpd , expressed in $\text{mm day}^{-1} \text{ kPa}^{-1}$). Ev/vpd ratio was high at the beginning of the
16 experiment, i.e., ranged from 2.44 to 3.22 $\text{mm d}^{-1} \text{ kPa}^{-1}$ during the first two experimental
17 days. After DoE 180 and until the soil was irrigated, Ev/vpd stabilized to a mean value of 0.03
18 (± 0.02) $\text{mm d}^{-1} \text{ kPa}^{-1}$.

19 Due to fractionating evaporation flux, the δ_{Svap} of the topmost layer (-0.01 m) increased
20 instantaneously (i.e., from DoE 0 onward) from the equilibrium δ_{Svap} value with the input
21 water (-17.3 ‰ and -132.3 ‰ for ^{18}O and ^2H , respectively, at 16.5°C, Fig. 4c and d).
22 Through back-diffusion of the excess heavy stable isotopologues from the evaporation front,
23 δ_{Svap} measured at depths -0.03, -0.05, -0.07, -0.10, and -0.20 m departed from that same
24 equilibrium value after 2, 3, 10, 25, and 92 days of the experiment, respectively. On the other
25 hand, δ_{Svap} of the layers -0.40 and -0.60 m were constant over the entire duration of the
26 experiment. Until DoE 65, the δ_{Svap} of the first 10 cm increased. From DoE 65 to 113 δ_{Svap}
27 reached an overall stable value in the top layers -0.01 m ($\delta^2\text{H}_{\text{Svap}} = 4.82 \pm 2.06$ ‰; $\delta^{18}\text{O}_{\text{Svap}} =$
28 11.72 ± 0.67 ‰) and -0.03 m ($\delta^2\text{H}_{\text{Svap}} = 5.61 \pm 3.14$ ‰; $\delta^{18}\text{O}_{\text{Svap}} = 10.41 \pm 0.81$ ‰), whereas
29 δ_{Svap} measured at depths -0.05, -0.07, and -0.10 m still progressively increased; from DoE 72
30 onward, δ_{Svap} at -0.20 m started to increase. $\delta^2\text{H}_{\text{Svap}}$ and $\delta^{18}\text{O}_{\text{Svap}}$ values started to decrease
31 after about DoE 113 and DoE 155, respectively. $\delta^2\text{H}_{\text{Svap}}$ at -0.01, -0.03, and -0.07 m on the

1 one hand and $\delta^{18}\text{O}_{\text{Svap}}$ at -0.01 , -0.03 , and -0.07 m on the other followed similar evolutions
2 with maximum values measured below the surface down to -0.05 m.

3 **3.4 Evolution of soil water content, temperature, evaporation flux, and δ_{Svap}** 4 **from DoE 290 to 299**

5 The layers -0.01 , -0.03 , -0.05 , -0.10 , and -0.20 m showed increases in θ of 0.31, 0.22, 0.30,
6 0.23, and $0.16 \text{ m}^3 \text{ m}^{-3}$ following irrigation, whereas θ at -0.60 m remained constant (Fig. 4e).
7 $\theta_{-0.01\text{m}}$ and $\theta_{-0.03\text{m}}$ rapidly decreased down to values of 0.12 and $0.13 \text{ m}^3 \text{ m}^{-3}$. Note that when
8 $\theta_{-0.01\text{m}}$ and $\theta_{-0.03\text{m}}$ reached these values prior to irrigation, the evaporation rate was similar
9 (i.e., $E_v/vpd = 0.65 (\pm 0.12) \text{ mm d}^{-1}$, Fig. 4f).

10 Immediately after irrigation and for both isotopologues, δ_{Svap} at -0.01 , -0.03 , and -0.05 m
11 was reset to a value close to that in equilibrium with st1 water (i.e., -17.8 ‰ and -132.0 ‰
12 for ^{18}O and ^2H , respectively, at 21.8 °C soil temperature, Fig. 4g and h). At -0.07 m, δ_{Svap}
13 reached the above mentioned equilibrium values after about 3.5 days. δ_{Svap} at -0.20 m evolved
14 in a similar way, whereas at -0.10 m the equilibrium values were reached after six hours.
15 Finally, δ_{Svap} at -0.40 and -0.60 m and for both isotopologues were not affected by the water
16 addition, which was consistent with the observed θ changes.

17 **3.5 Evolution of soil temperature, water content, and δ_{Sliq} profiles**

18 In Figure 5, T_s , θ , and δ_{Sliq} profiles for both isotopologues are plotted in three different panels,
19 from DoE 0 to 100 (Fig. 5a-d, top panels), from DoE 101 to 287 (Fig. 5e-h, center panels),
20 and from DoE 288 to 299 (Fig. 5i-l, bottom panels). The represented profiles were obtained
21 from a linear interpolation of the times series of each variable. Thus, since the measuring
22 sequence started each day at 08:00 and ended at 18:00, the depicted profiles are centered on
23 13:00.

24 Even if the soil temperature fluctuated during the course of the experiment, quasi-isothermal
25 conditions were fulfilled at a given date, as the column was not isolated from its surroundings.
26 On average, T_s only varied by 0.2 °C around the profile mean temperature at a given date.
27 The δ_{Sliq} profiles showed a typical exponential shape from DoE 0 to approx. 100. Around DoE
28 100, when θ at -0.01 m reached a value of $0.090 \text{ m}^3 \text{ m}^{-3}$ (i.e., significantly greater than the
29 sand residual water content $\theta = 0.035 \text{ m}^3 \text{ m}^{-3}$, determined by Merz et al. (2014)), the maximal
30 δ_{Sliq} values were no longer observed at the surface and atmosphere water vapor started

1 invading the first centimeter of soil. Note that this happened slightly faster for $^1\text{H}^2\text{H}^{16}\text{O}$ than
2 for $^1\text{H}_2^{18}\text{O}$. On DoE 290, when the column was irrigated, the isotope profiles were partly reset
3 to their initial state, i.e., constant over depth and close to -53.5 and -8.2 ‰ for $^1\text{H}^2\text{H}^{16}\text{O}$ and
4 $^1\text{H}_2^{18}\text{O}$, respectively, with the exception of still enriched values at -0.07 m.

5 **3.6 $\delta^2\text{H}$ - $\delta^{18}\text{O}$ relationships in soil water and atmosphere water vapor**

6 Each plot of Figure 6 represents data of 50 consecutive days of the experiment. Laboratory
7 atmosphere water vapor $\delta^2\text{H}$ and $\delta^{18}\text{O}$ (gray symbols) were linearly correlated (linear
8 regression relationships in gray dotted lines) during the entire experiment (R^2 ranging
9 between 0.74 and 0.90, F-statistic p-value < 0.01), with the exception of the period DoE 125-
10 | 155 ($R^2 = 0.31$, $p < 0.001$), when atmospheric water ~~vapour~~vapor $\delta^2\text{H}$ was remarkably high in
11 the laboratory (Fig. 6c and d).

12 The linear regression slopes (LRS) between $\delta^2\text{H}_a$ and $\delta^{18}\text{O}_a$ ranged from 6.20 (DoE 50-100, p
13 < 0.01) to 8.29 (DoE 0-50, gray dotted line, $p < 0.001$). These values were significantly lower
14 than S_{eq} , the calculated ratio between the liquid-vapor equilibrium fractionations of $^1\text{H}^2\text{H}^{16}\text{O}$
15 and $^1\text{H}_2^{18}\text{O}$ (Majoube, 1971) that characterizes meteoric water bodies, which should have
16 ranged from 8.41 to 8.92 at the measured monthly mean atmosphere temperatures
17 (Forschungszentrum Jülich wheater station, $6^\circ 24' 34''$ E, $50^\circ 54' 36''$ N, 91 m.a.s.l.). Therefore,
18 it can be deduced that the laboratory air moisture was partly resulting from column
19 evaporation, typically leading to a $\delta^2\text{H}$ - $\delta^{18}\text{O}$ regression slope of lower than eight. This also
20 highlights the particular experimental conditions in the laboratory, where other sources of
21 | water ~~vapour~~vapor (e.g., by opening the laboratory door) might have influenced the isotope
22 compositions of the air.

23 Considering all soil depths, the $\delta^2\text{H}_{\text{Sliq}}\text{-}\delta^{18}\text{O}_{\text{Sliq}}$ LRS increased from 2.96 to 4.86 over the
24 course of the experiment (with $R^2 > 0.89$, $p < 0.001$). These values were much lower than that
25 of the slope of the Global Meteoric Water Line (GMWL, i.e., slope=8) also represented in
26 Figure 6. However, Figure 6 highlights the fact that in the upper three layers (-0.01 , -0.03 ,
27 and -0.05 m) $\delta^2\text{H}_{\text{Sliq}}\text{-}\delta^{18}\text{O}_{\text{Sliq}}$ LRS followed a significantly different evolution as the soil dried
28 out. Figure 7 shows average $\delta^2\text{H}$ - $\delta^{18}\text{O}$ LRS calculated for time intervals of ten consecutive
29 days for the atmosphere (gray line), the three upper layers (colored solid lines), and the
30 remaining deeper layers (-0.07 , -0.10 , -0.20 , -0.40 , and -0.60 m, black dotted line). While
31 both $\delta^2\text{H}$ - $\delta^{18}\text{O}$ LRS in the atmosphere and in the first three depths fluctuated during the

1 experiment, the LRS of the combined remaining deeper layers varied only little between 3.07
2 and 4.49 (average = 3.78 ± 0.54). From DoE 150, $\delta^2\text{H}$ - $\delta^{18}\text{O}$ LRS of the atmosphere and at –
3 0.01, –0.03, and –0.05 m were linearly correlated ($R^2 = 0.73, 0.48, \text{ and } 0.42$, with $p < 0.001, <$
4 0.01 , and < 0.05 , respectively), whereas they were not correlated before DoE 125,
5 demonstrating again the increasing influence of the atmosphere (atmosphere invasion) on the
6 soil surface layer as the EF receded in the soil. Note the negative $\delta^2\text{H}_a$ - $\delta^{18}\text{O}_a$ LRS ($R^2 = 0.26$,
7 $p < 0.001$) observed between DoE 125 and 150, due to remarkably high atmosphere vapor
8 $\delta^2\text{H}$ measured in the laboratory.

9

10 **4 Discussion**

11 **4.1 Long term reliability of the method**

12 The method proved to be reliable in the long term as the tubing sections positioned at –0.60
13 and –0.40 m (i.e., where the sand was saturated or close to saturation during the entire
14 experiment) remained watertight even after 299 days. As demonstrated by Rothfuss et al.
15 (2013), (i) the length of the gas-permeable tubing, (ii) the low synthetic dry air flow rate, and
16 (iii) the daily measurement frequency allowed removing soil water vapor which remained
17 under thermodynamic equilibrium with the soil moisture. Moreover, this was also true for the
18 upper soil layers even at low soil water content: steady values for water vapor mixing ratio
19 and isotope compositions were always reached during sampling throughout the experiment.
20 Finally, our method enabled inferring the isotope composition of tightly bound water at the
21 surface. This would be observable by the traditional vacuum distillation method with certainly
22 a lower vertical resolution due to low moisture content. As also pointed out by Rothfuss et al.
23 (2013), it can be assumed that the sand properties did not cause any fractionation of pore
24 water ^2H and ^{18}O . In contrast, this could not be the case in certain soils with high cation
25 exchange capacity (CEC) as originally described by Sofer and Gat (1972) and recently
26 investigated by Oerter et al. (2014).

27 **4.2 Locating the evaporation front depth from soil water $\delta^2\text{H}$ and $\delta^{18}\text{O}$ profiles**

28 From Figure 4b no distinct characteristic evaporation stages, i.e., stages I and II referring to
29 atmosphere-controlled and soil-controlled evaporation phases, respectively, could be
30 identified. The opposite was observed by Merz et al. (2014), who conducted an evaporation

1 study using the same sand. This indicates greater wind velocity in the air layer above the soil
2 column due to the laboratory ventilation. For higher wind velocities, the boundary layer above
3 the drying medium is thinner and the transfer resistance for vapor transfer lower than for
4 lower wind velocities. But, for thinner boundary layers, the evaporation rates depends
5 stronger on the spatial configuration of the vapor field above the partially wet evaporating
6 surface. This makes that the evaporation rate decreases and the transfer resistance in the
7 boundary layer increases more in relative terms with decreasing water content of the
8 evaporation surface for higher than for lower wind velocities (Shahraeeni et al., 2012).

9 Locating the EF in the soil is of importance for evapotranspiration partitioning purposes: from
10 the soil water isotope composition at the EF, it is possible to calculate the evaporation flux
11 isotope composition using the Craig and Gordon formula (Craig and Gordon, 1965). For a
12 uniform isotope diffusion coefficient distribution in the liquid phase, an exponential decrease
13 of the isotope composition gradient with depth is expected. However, when evaporation and
14 thus accumulation of isotopologues occur in a soil layer between two given observation
15 points, then the isotope gradient between these two points is smaller than the gradient deeper
16 in the profile. Therefore we can consider the time when the isotope composition gradient is no
17 longer the largest between these two upper observation depths as the time when the EF moves
18 into the soil layer below.

19 Figure 8a and b display the evolutions of the isotope compositions gradients $d(\delta^{18}O_s)/dz$ and
20 $d(\delta^2H_s)/dz$ calculated between two consecutive observation points in the soil (i.e., between
21 -0.01 and -0.03 m in brown solid line, between -0.03 and -0.05 m in red solid line, etc.).
22 Figure 8c translates these isotope gradients in terms of EF depths ($z^{18}O_{EF}$ and z^2H_{EF} ,
23 respectively). Each day, the maximum $d(\delta^{18}O_s)/dz$ and $d(\delta^2H_s)/dz$ define the layer where
24 evaporation occurs, e.g., when $d(\delta^{18}O_s)/dz$ is maximal between -0.01 and -0.03 m on a given
25 DoE, $z^{18}O_{EF}$ is estimated to be greater than -0.01 m and is assigned the value of 0 m.
26 When $d(\delta^{18}O_s)/dz$ is maximal between -0.03 and -0.05 m on a given DoE, $z^{18}O_{EF}$ is
27 estimated to range between -0.01 and -0.03 m and is assigned the value -0.02 m. From
28 both $d(\delta^{18}O_s)/dz$ and $d(\delta^2H_s)/dz$, a similar evolution of the depth of the evaporation front
29 was derived despite the fact that δ^2H_{Sliq} and $\delta^{18}O_{Sliq}$ time courses were different and showed
30 maxima at different times. It was inferred that after 290 days under the prevailing laboratory

1 air temperature, moisture, and aerodynamic conditions, and given the specific hydraulic
2 properties of the sand, the EF had moved down to an approximate depth of -0.06 m.

3 ~~4.3 Testing the Craig and Gordon (1965) relationship with isotope data~~

4 4.3 Isotope kinetic effects during soil evaporation

5 For each period of ten consecutive days the minimum measured $\delta^{2}\text{H}_{\text{Sliq}}$ and $\delta^{18}\text{O}_{\text{Sliq}}$ provided
6 $\delta^{2}\text{H}_{\text{Sliq_ini}}$ and $\delta^{18}\text{O}_{\text{Sliq_ini}}$ in Equation (3). $\delta^{2}\text{H}_a$ and $\delta^{18}\text{O}_a$ were obtained from the mean values
7 of their respective times series. Mean soil surface water content (θ_{surf}) measured in the layer
8 above the EF (as identified in section 4.2) provided the n parameter in Equation (6) and
9 ultimately $\varepsilon_{\text{K}}^{2\text{H}}$ and $\varepsilon_{\text{K}}^{18\text{O}}$ (Eq. (5a) and (5b)). $\varepsilon_{\text{eq}}^{2\text{H}}$ and $\varepsilon_{\text{eq}}^{18\text{O}}$ were calculated from Majoube (1971)
10 at the mean soil temperature measured at z_{EF} . Relative humidity was normalized to the soil
11 temperature measured at the EF. Finally, standard error for S_{Ev} was obtained using an
12 extension of the formula proposed by Phillips and Gregg (2001) and detailed by Rothfuss et
13 al. (2010). For this, standard errors associated with the determination of the variables in
14 Equation (3) were taken equal to their measured standard deviations for each time period.
15 Standard errors for the parameters θ_{res} and θ_{sat} were set ~~arbitrarily~~ to $0.01 \text{ m}^3 \text{ m}^{-3}$ (i.e.,
16 comparable to the soil water content probes' precision) and for the diffusivity ratios
17 $D/D^{2\text{H}}$ and $D/D^{18\text{O}}$ to zero (i.e., no uncertainty about their value was taken into account,
18 although debatable, e.g., Cappa et al., 2003).

19 Figure 9a shows the comparison between time courses of S_{Ev} and $\delta^{2}\text{H}_{\text{Sliq}}\text{-}\delta^{18}\text{O}_{\text{Sliq}}$ LRS
20 computed with data below the EF. Both ranged between 2.9 and 4.8, i.e., within the range of
21 reported values (e.g., Barnes and Allison, 1988, Brunel et al., 1995, DePaolo et al., 2004).
22 Note that both observed and simulated slopes' values increased over time, even though the
23 ~~boundary~~ air layer above the EF gradually thickened as the soil dried out. The opposite was
24 observed by e.g., Barnes and Allison (1983), who simulated isotopic profiles at steady state
25 with constant relative humidity. In the present study however the atmosphere relative
26 humidity gradually increased which in turn decreased the kinetic effects associated with
27 $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ ~~vapour~~ vapor transports and thus increased slopes over time. The general
28 observed trend was very well reproduced by the model between DoE 30 and 150 (Nash and
29 Sutcliffe Efficiency - NSE = 0.92; Nash and Sutcliffe, 1970), whereas S_{Ev} departed from data
30 from DoE 150 onwards (NSE < 0). Overall, the Craig and Gordon (1965) model could

1 explain about 62 % of the data variability with a Root Mean Square Error (RMSE) of 0.58
2 (and 76 % when data from the period DoE 0-10 is left out, p-value < 0.001, RMSE = 0.52). At
3 the beginning of the experiment (DoE 0-20), simulated values were greater than computed
4 $\delta^2\text{H}-\delta^{18}\text{O}$ LRS, even when taking into account the high S_{Ev} standard errors due to fast
5 changing θ_{surf} (Phillips and Gregg, 2001). Although S_{Ev} was equal to 3.8 for the period DoE 0-
6 10, $\delta^2\text{H}-\delta^{18}\text{O}$ LRS had already reached down a value of 2.9, meaning that the EF should have
7 been no longer at the surface (i.e., between the surface and 0.01 m depth) leading to greater n,
8 therefore lower slope value.

9 After DoE 150 and until DoE 290 when evaporation flux was lower than 0.40 mm d⁻¹,
10 difference between model and data progressively increased. For a better model-to-data fit, the
11 $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ kinetic effects should decrease, through either (i) decrease of ε_{K} (i.e.,
12 ~~decrease of n~~, n), which is from a theoretical point of view counter-intuitive and e.g.,
13 contradicts the formulation of Mathieu and Bariac (1996) or (ii) decrease of term $(1 - rh)$, or
14 else (iii) a combination of (i) and (ii). In another laboratory study where $\delta^{18}\text{O}$ of water in bare
15 soil columns was measured destructively and $\delta^{18}\text{O}$ of evaporation was estimated from
16 cryoscopic trapping of water ~~vapour~~ vapor at the outlet of the columns' headspaces, Braud et
17 al. (2009a and b) could capture $\varepsilon_{\text{K}}^{18\text{o}}$ dynamics by inverse modelling. In their case, $\varepsilon_{\text{K}}^{18\text{o}}$
18 generally reached values close to $\varepsilon_{\text{K}}^{18\text{o}} = 18.9\text{‰}$ corresponding to laminar conditions above the
19 liquid-vapor interface ($n = 2/3$). They however determined at the end of their experiments,
20 when the soil surface dry layer thickened and soil surface relative humidity was significantly
21 lower than 100%, values lower than reported in the literature (i.e., $\varepsilon_{\text{K}}^{18\text{o}} < 14.1\text{‰}$). These
22 results were partly explained by the particular experimental conditions leading to
23 uncertainties in characterizing evaporation isotope compositions when the dry soil surface
24 layer was the most developed. Nevertheless, the same observation could be made in the
25 present study while having a different soil texture (silt loam *versus* quartz sand) and
26 noticeable different atmospheric conditions ("free" laboratory atmosphere *versus* sealed
27 headspace circulated with dry air). Figure 9c displays the evolution of $\varepsilon_{\text{K}}^{2\text{H}}$ (resp. $\varepsilon_{\text{K}}^{18\text{o}}$) that
28 provided the best fit with data (NSE = 0.99) through fitting of the n parameter (shown Figure
29 9b) instead of calculating it with Equation (6). In this scenario, n decreased from one to 0.59,
30 with a mean value of 0.96 ± 0.03 during the period DoE 0-150.

1 Instead of changing the value of n over time (and therefore those of ε_K^{2H} and ε_K^{18O}), another
2 possibility is to consider that after some time the relative humidity at the EF (rh_{EF}) was
3 different from 100%, although the EF was still at thermodynamic equilibrium. In that case
4 kinetic effects would have depended on the difference ($rh_{EF} - rh$) instead of $(1 - rh)$. Figure
5 9b shows the rh_{EF} time course that provided the best model-to-data fit (NSE = 0.92), when
6 ε_K^{2H} and ε_K^{18O} were calculated (Eq. (5a-5b-6)). In this second scenario, rh_{EF} decreased from 100
7 to 81 % with a mean value of 99.5 ± 0.03 % for the period DoE 0-150, i.e., in a similar
8 fashion than fitted n values obtained in the 1st scenario. These values were significantly lower
9 than what is calculated with Kelvin's Equation linking rh_{EF} with soil water tension at the EF
10 in the case of liquid-vapor equilibrium, which for the soil retention properties (Merz et al.,
11 2014) would range between 100 and 99.6 %. In a third scenario one could consider a
12 combined decrease of n and rh_{EF} to smaller extents, for which there are no unique solutions at
13 each time step. In a fourth scenario, the ratio of turbulent diffusion resistance to molecular
14 diffusion resistance is no more negligible, leading to n' values ranging between 0 and n
15 (Merlivat and Jouzel, 1979). This last scenario was however not verifiable. In any case, only
16 decreasing kinetic effects could provide a better model-to-data fit. Note that the formulation
17 of kinetic enrichments proposed by Merlivat and Coantic (1975) and based on the evaporation
18 model of Brutsaert (1982) was not tested due to lack of appropriate data (i.e., unknown wind
19 distribution profile over the soil column). The formulations of Melayah et al. (1996) ($n = 0$)
20 and Barnes and Allison (1983) ($n = 1$) were also not tested as they give kinetic enrichments
21 constant over time and cannot explain a change of S_{Ev} value through change of n . Finally, S_{Ev}
22 calculations using diffusivity ratios determined by Cappa et al. (2003) lead to lower value of
23 S_{Ev} and less good model-to-data fit.

24 In the present study, information on δ^{2H} and δ^{18O} of the evaporation flux was missing to
25 address uncertainties in the determination of ε_K^{2H} and ε_K^{18O} . The experimental setup would also
26 have gained from the addition of appropriate sensors (e.g., micro-psychrometers) to measure
27 the soil surface relative humidity and especially rh_{EF} , although the dimensions of the column
28 would certainly be a limiting factor. ~~Finally note that S_{Ev} -calculations using diffusivity ratios~~
29 ~~determined by Cappa et al. (2003) lead to lower value of S_{Ev} and less good model-to-data fit.~~
30 A more in depth investigation of the behavior of S_{Ev} (and isotope composition gradients with
31 depth for that matter) with time could be carried out with detailed numerical simulations using
32 an isotope-enabled SVAT model such as SiSPAT-Isotope.

1 **5 Conclusion**

2 Since the initial work of Zimmermann et al. (1967), water stable isotopologues have proven
3 both theoretically and experimentally to be valuable tools for the study of water flow in the
4 soil and at the soil-atmosphere interface. In this work we present the first application of the
5 method of Rothfuss et al. (2013). This study constitutes also the very first long-term
6 application of the series of newly developed isotopic monitoring systems based on gas-
7 permeable tubing and isotope-specific infrared laser absorption spectroscopy (Herbstritt et al.,
8 2012; Volkmann and Weiler, 2014). Our method proved to be reliable over long time periods
9 and followed quantitatively the progressive isotope enrichment caused by evaporation in an
10 initially saturated soil column. Moreover, it could capture sudden variations following a
11 simulated intense rain event.

12 Simple calculations of isotope compositions' gradients made it possible to evaluate the
13 position of the Evaporation Front and observe how it progressively receded with time in the
14 soil. Confrontation of the model of Craig and Gordon (1965) with data also highlighted
15 uncertainties associated with the determinations of isotope kinetic fractionations and soil
16 relative humidity at the EF when the soil surface dry layer was the most developed and
17 evaporation flux was low.

18 Our method will allow experimentalists to measure and locate the evaporation front in a
19 dynamic and non-destructive manner and to calculate the isotope compositions of the
20 evaporation flux using the model of Craig and Gordon (1965) with much higher time
21 resolution. Provided that the isotope compositions of evapotranspiration and transpiration
22 fluxes are measured or modelled, this method will be especially useful to test hypotheses and
23 improve our understanding of root water uptake processes and the partitioning of
24 evapotranspiration fluxes.

25

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2 Technology, for providing the water isotopic analyzer for this study.
3

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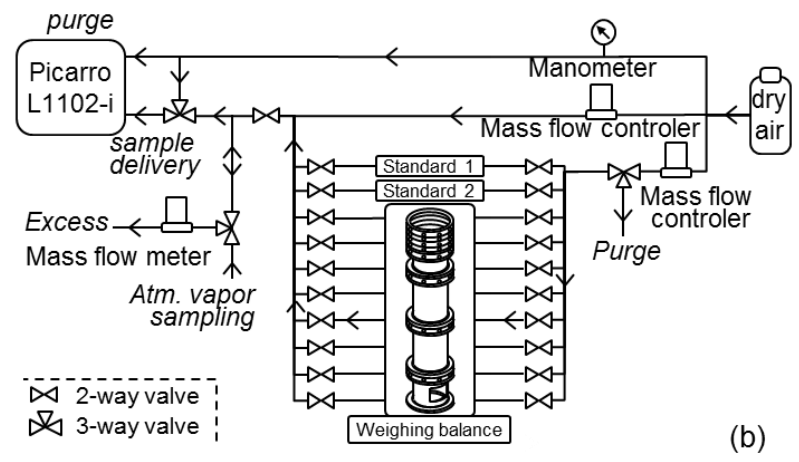
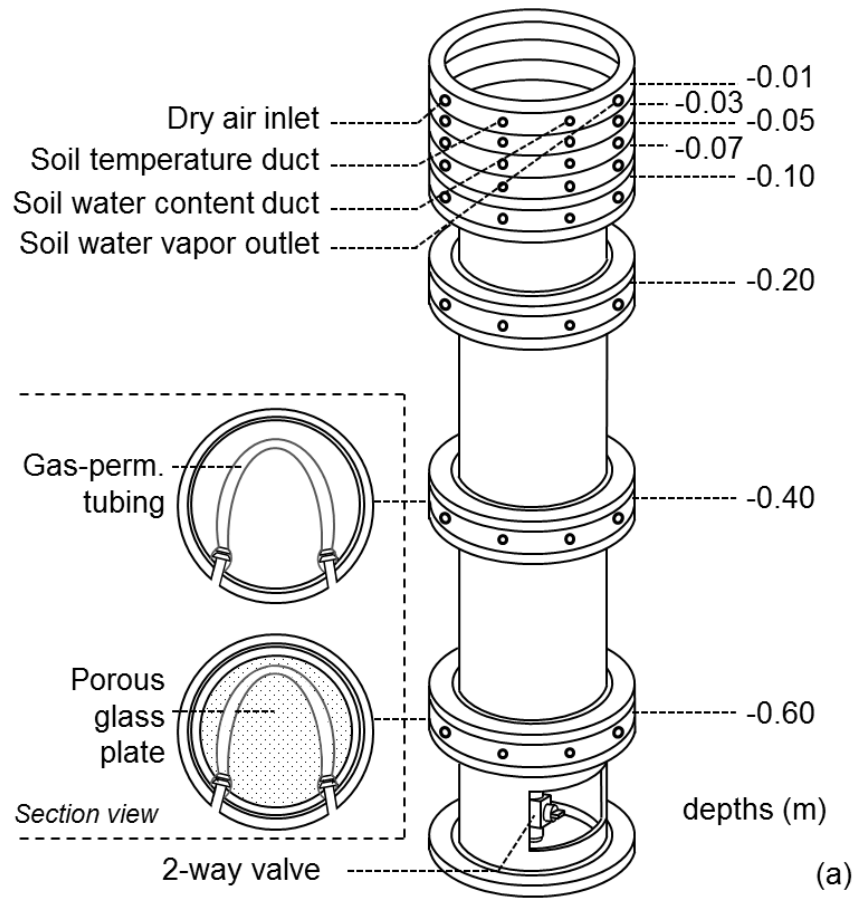
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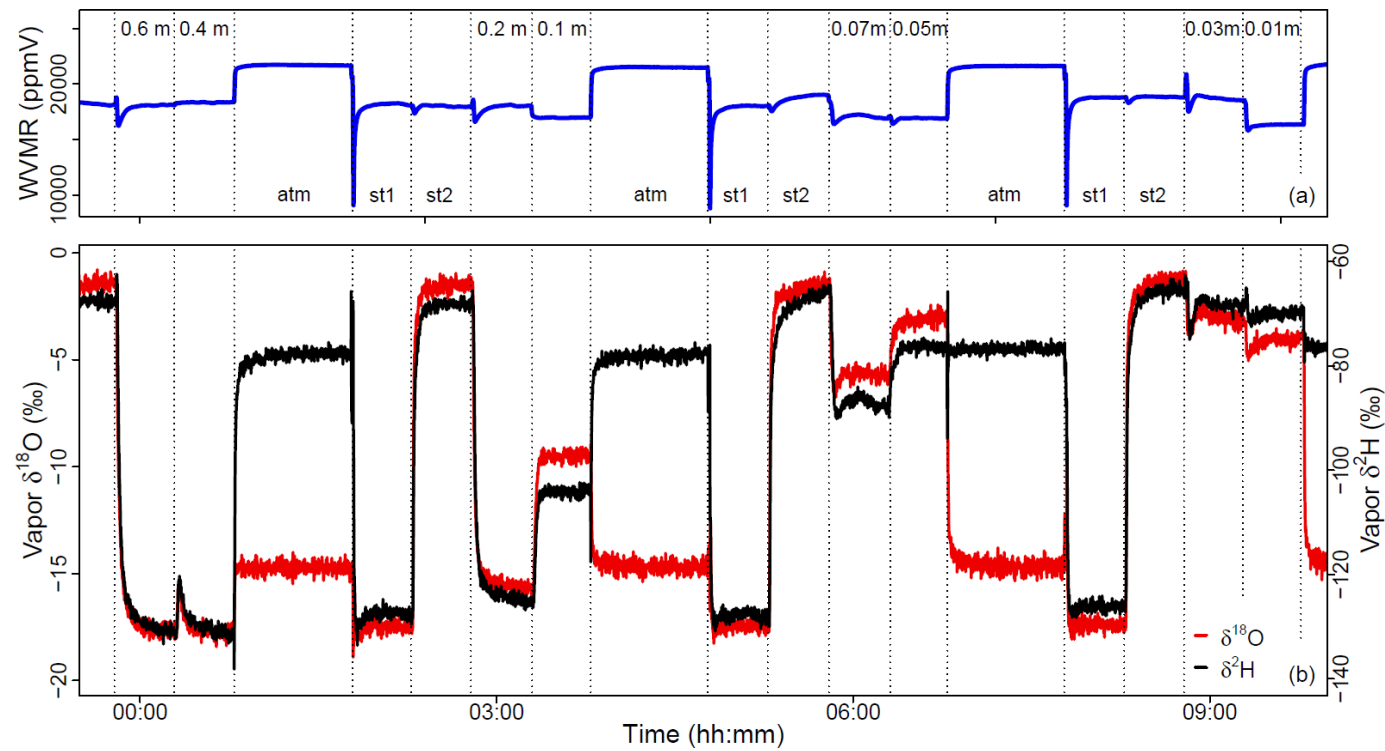
1 **Figures**



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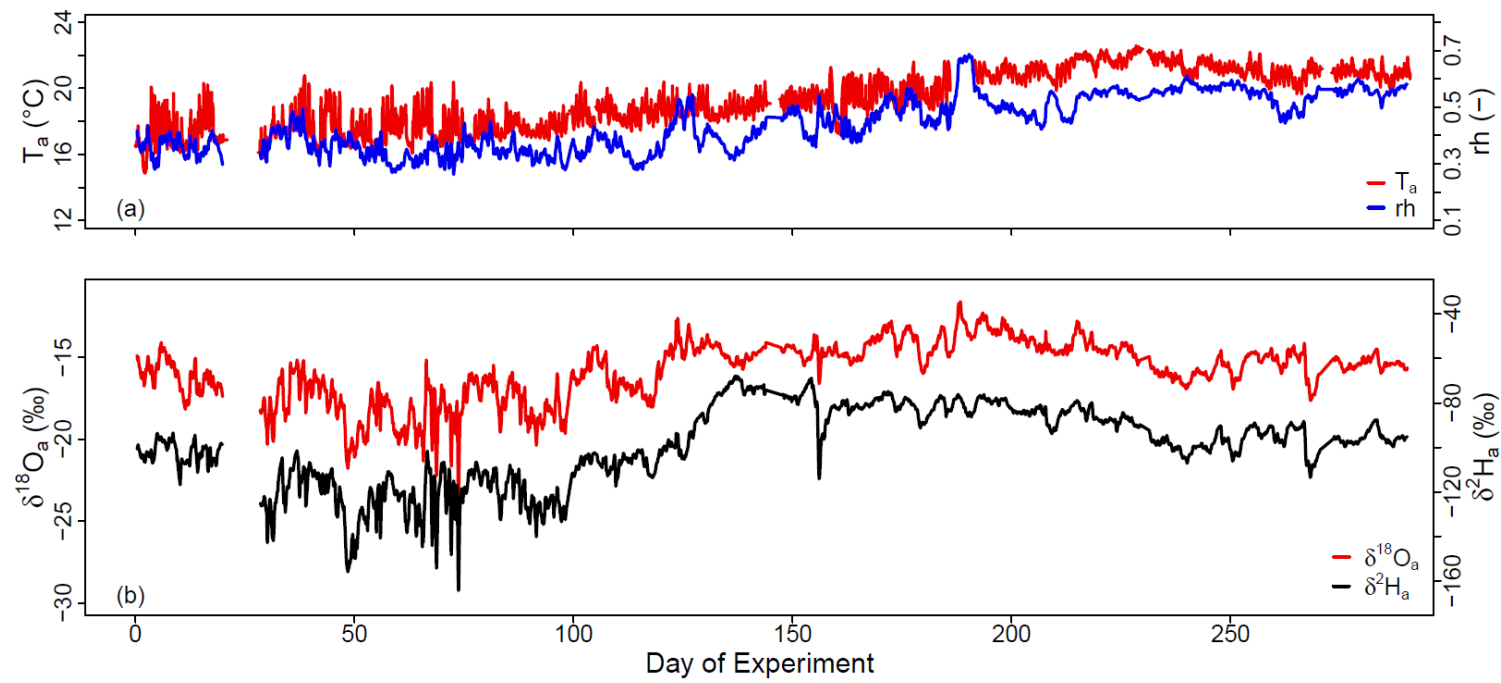
3 Figure 1. (a) Scheme of the acrylic glass column used in the experiment; (b) experimental setup for sampling water vapor at the different soil
 4 depths of the soil column, from the ambient air, and from the two soil water standards (standard 1 and 2)

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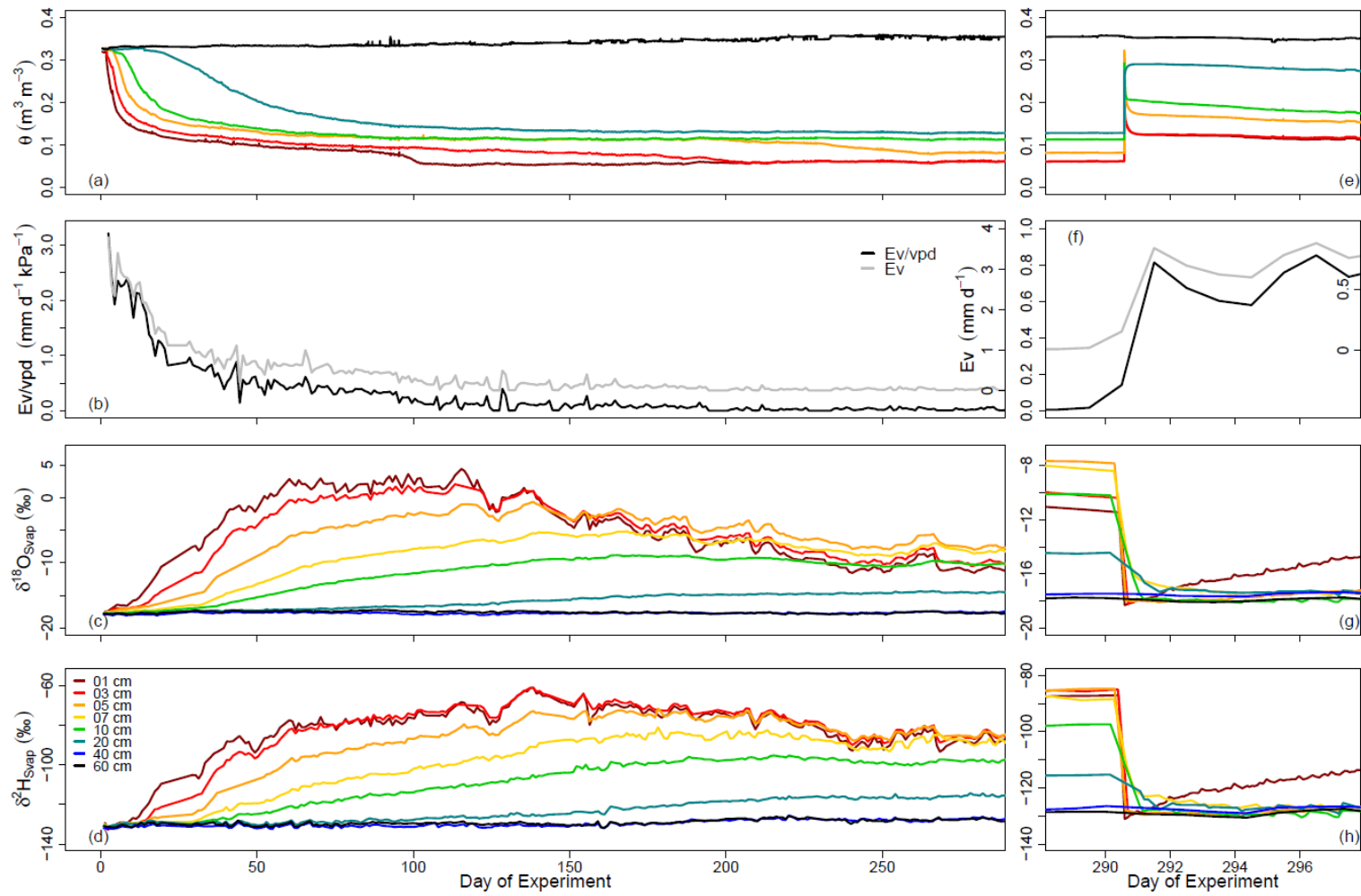
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Figure 2. Water vapor mixing ratio (*WVMR*, in ppmv) and isotope composition ($\delta^{18}\text{O}$ and $\delta^2\text{H}$, in ‰ V-SMOW) of the water vapor sampled on Day of Experiment 150 from the ambient air (“atm”), both standards (“st1” and “st2”), and from the tubing sections at soil depths 1, 3, 5, 7, 10, 20, 40, and 60 cm



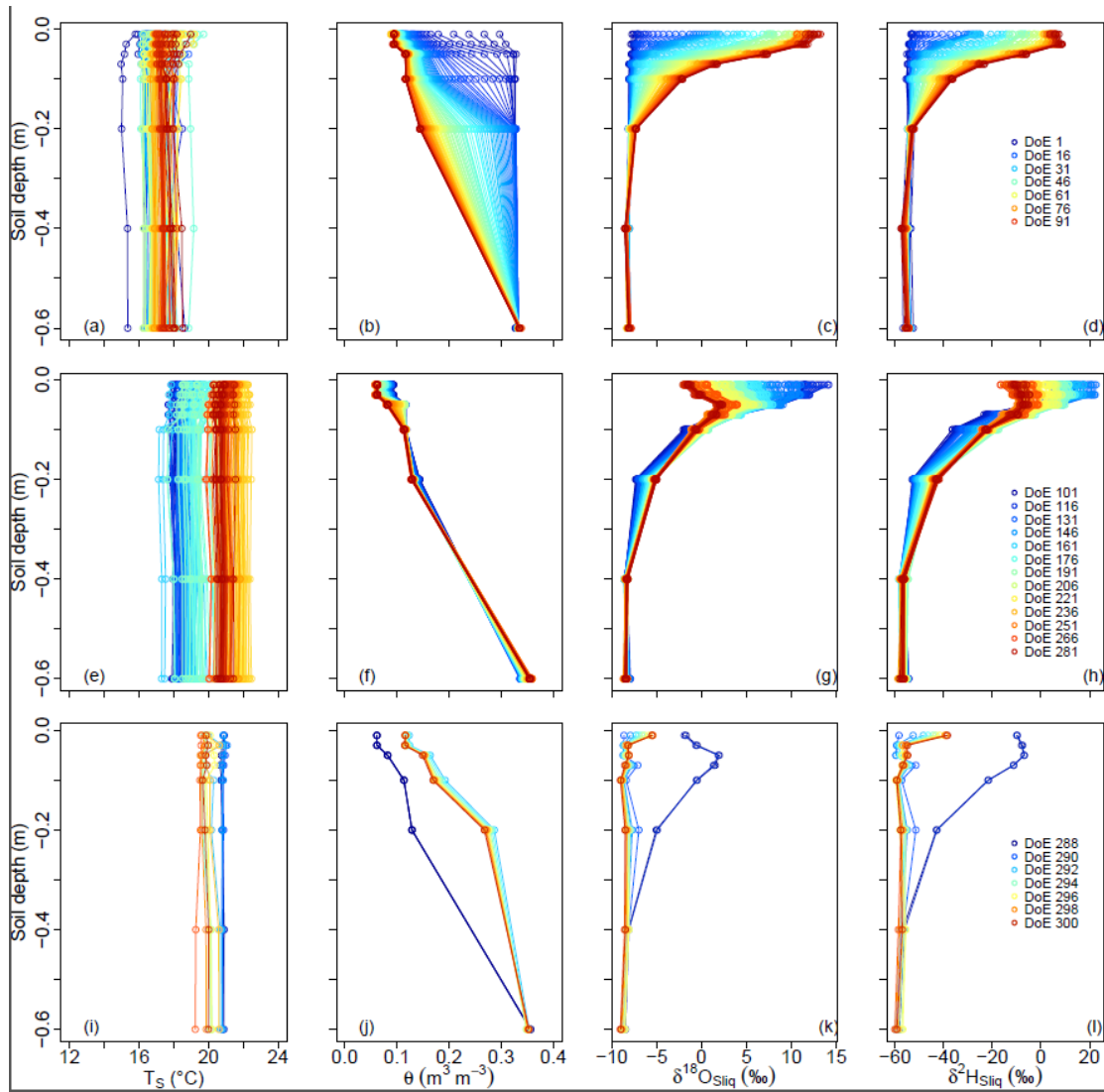
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Figure 3. Time series of the laboratory ambient air temperature (T_a , in $^{\circ}\text{C}$), relative humidity (rh , in %) and water vapor isotope compositions ($\delta^{18}\text{O}_a$ and $\delta^2\text{H}_a$, in ‰ V-SMOW) over the course of the experiment



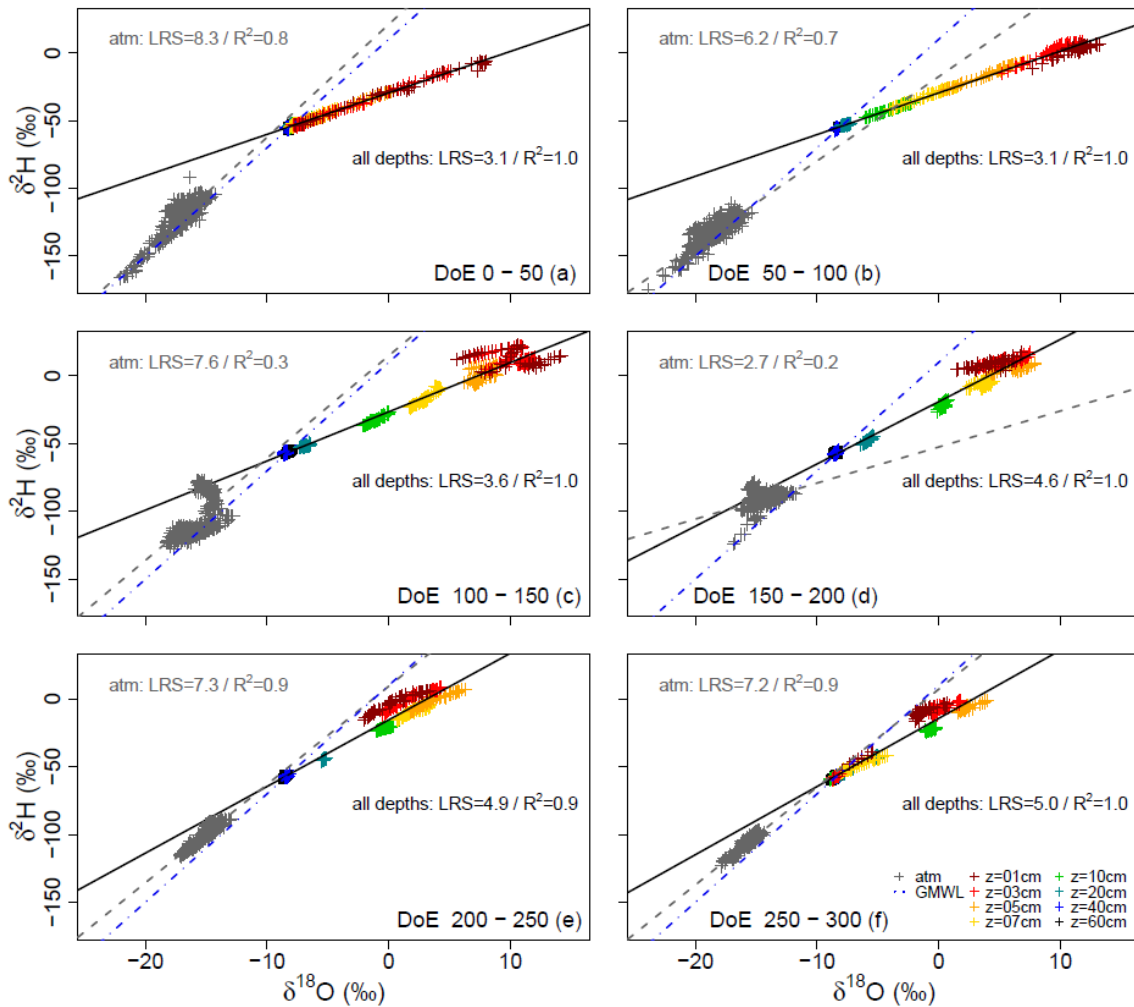
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2 Figure 4. Time series of water content (θ , in $\text{m}^3 \text{m}^{-3}$), evaporation flux (Ev , in mm d^{-1}), and water vapor isotope compositions ($\delta^{18}\text{O}_{\text{Svap}}$ and
 3 $\delta^2\text{H}_{\text{Svap}}$, in ‰ V-SMOW) during the course of the experiment



1
 2 Figure 5. Soil temperature (T_S , in $^{\circ}\text{C}$), water content (θ , in $\text{m}^3 \text{m}^{-3}$), and liquid water isotope
 3 compositions ($\delta^{18}\text{O}_{\text{Sliq}}$ and $\delta^2\text{H}_{\text{Sliq}}$, in ‰ V-SMOW) profiles from Day of Experiment (DoE) 0
 4 - 100 (top panel), from DoE 101 - 287 (middle panel), and from DoE 288 - 299 (bottom
 5 panel)

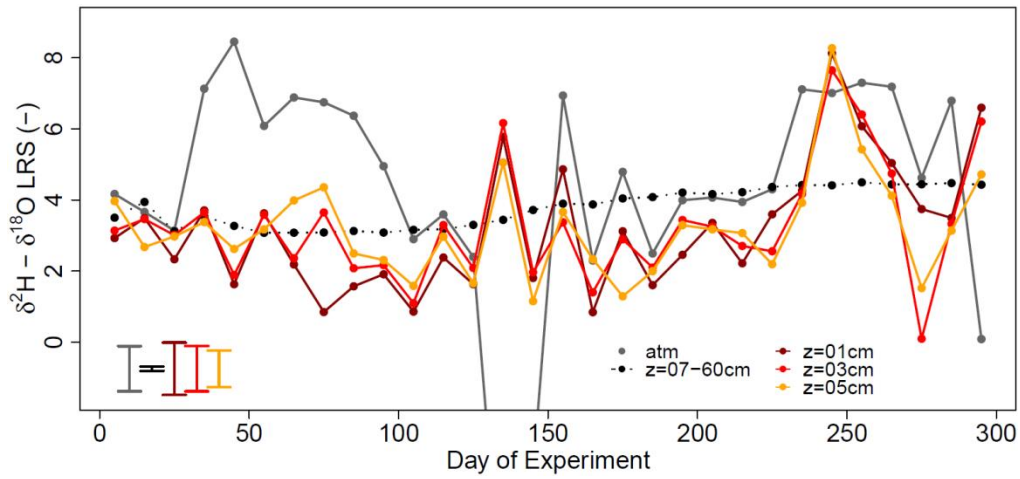
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2 Figure 6. Linear regressions (gray dotted line) between laboratory atmosphere water vapor
 3 $\delta^{18}\text{O}$ and $\delta^2\text{H}$ (in ‰ V-SMOW) and between soil water $\delta^{18}\text{O}$ and $\delta^2\text{H}$ (solid black line). Each
 4 plot represents data from 50 consecutive days of experiment (DoE). Global Meteoric Water
 5 Line (GMWL, define by $\delta^2\text{H} = 8 * \delta^{18}\text{O} + 10$, in blue dotted line) is shown on each sub-plot for
 6 comparison. Coefficient of determination (R^2) as well as the slope of the linear regressions
 7 (LRS) are reported

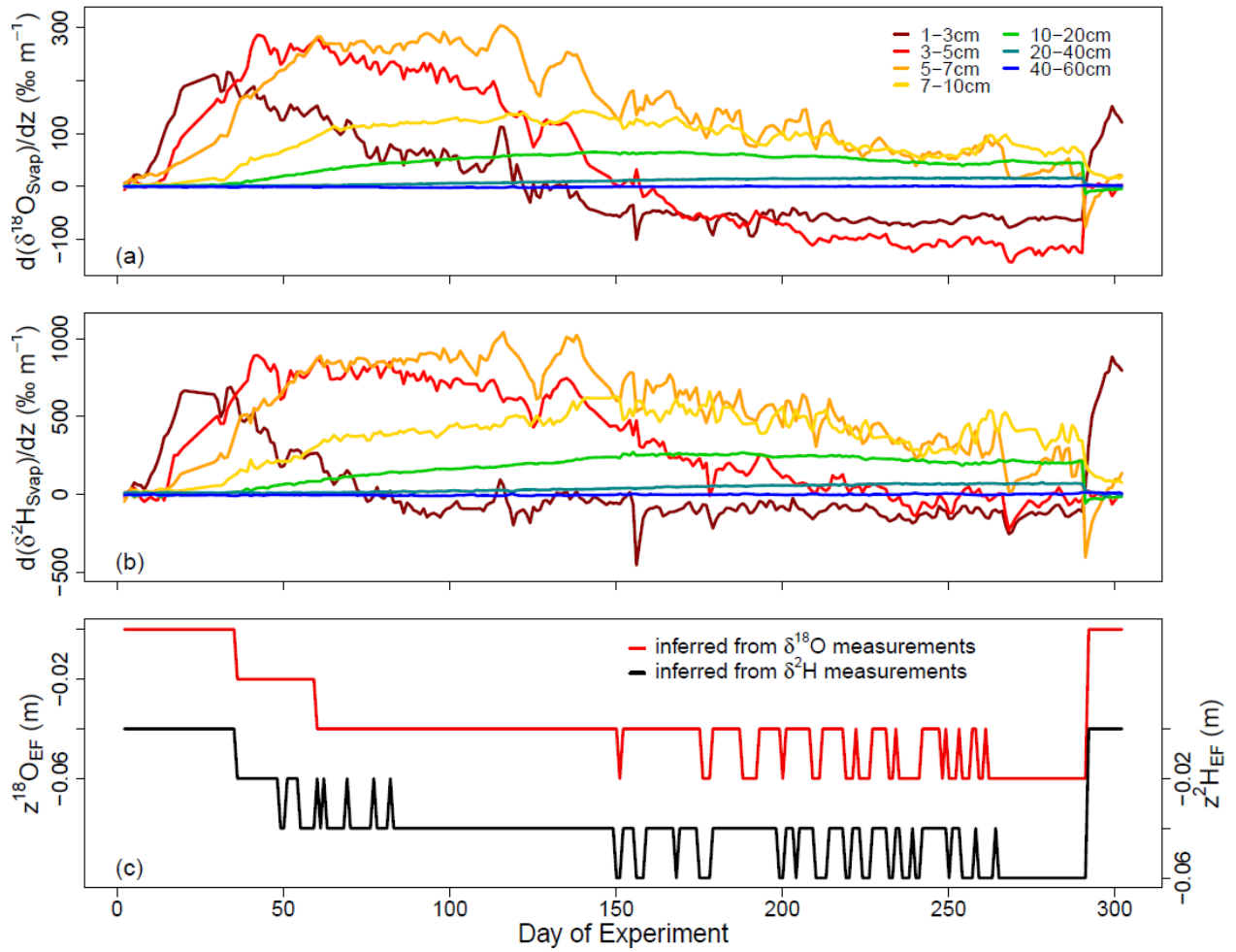
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2 Figure 7. Time course of the slopes of the $\delta^{18}\text{O}$ - $\delta^2\text{H}$ linear regressions (LRS) for time
 3 intervals of ten consecutive days of atmosphere data (gray solid line), soil data from the upper
 4 three layers (01, 03, and 05 cm, colored solid lines), and combined soil data from the
 5 remaining bottom layers (from 07 to 60 cm, black dotted line). Mean standard errors are
 6 represented by the error bars in the bottom left corner

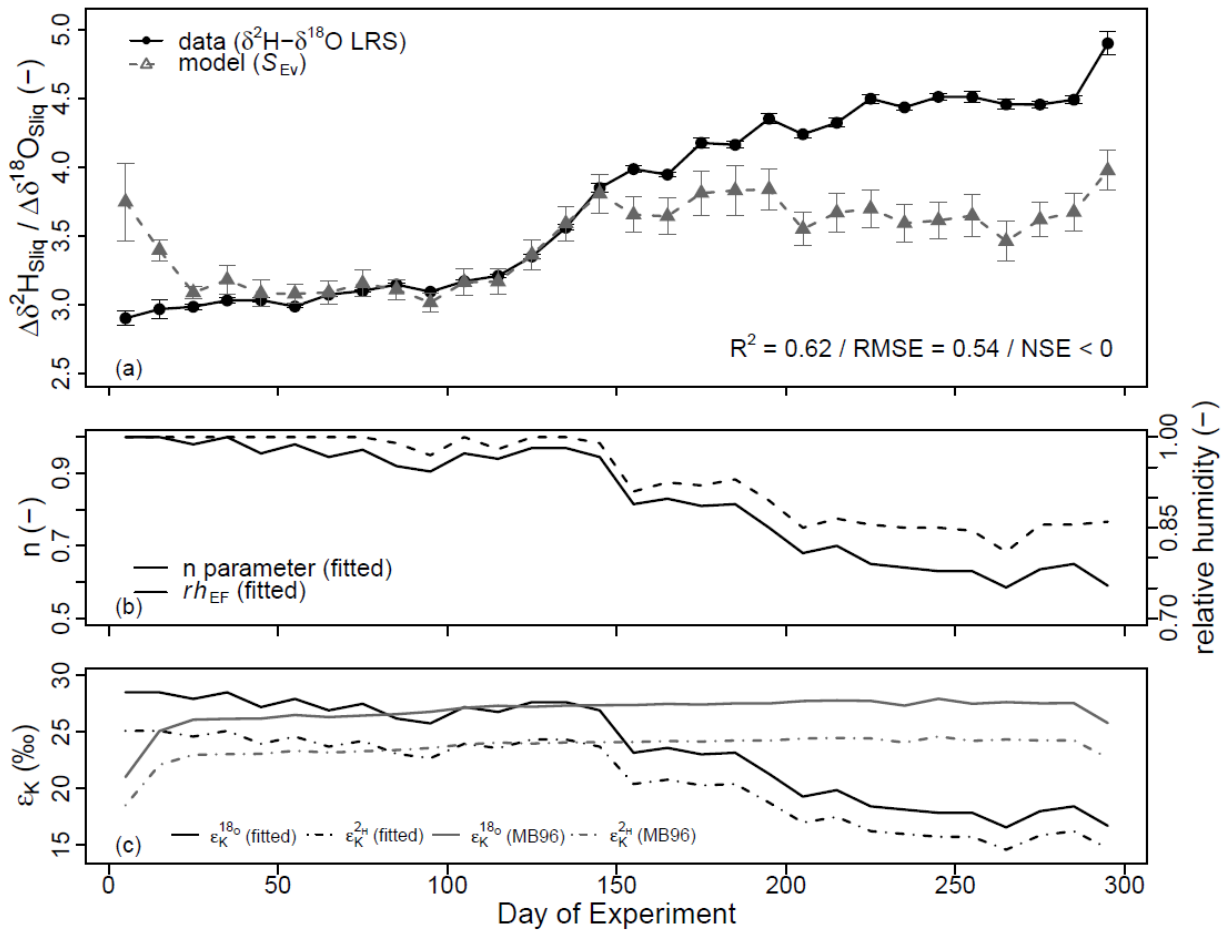
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2 Figure 8. (a) and (b) $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$ composition gradients calculated between
 3 consecutive observation points in the soil. (c) Evolution of the evaporation front depths $z^{18}\text{O}_{\text{EF}}$
 4 (red solid line) and $z^2\text{H}_{\text{EF}}$ (black solid line) inferred from the $^1\text{H}^2\text{H}^{16}\text{O}$ and $^1\text{H}_2^{18}\text{O}$
 5 composition gradients

6



1
2 Figure 9. (a) Comparison between soil liquid water $\delta^{18}\text{O}$ - $\delta^2\text{H}$ linear regressions slopes (LRS,
3 solid black line) calculated for time intervals of ten consecutive days and simulated time
4 series of evaporation line slope (S_{Ev} , dotted gray line) obtained from Equations (3-6) (Gat et
5 al., 1971, Merlivat, 1978, Mathieu and Bariac, 1996). Black error bars give the standard errors
6 of the estimated $\delta^{18}\text{O}$ - $\delta^2\text{H}$ LRS. Gray error bars are the standard errors associated with
7 calculation of S_{Ev} following Phillips and Gregg (2001). Coefficient of determination (R^2),
8 Root Mean Square Error (RMSE) and Nash and Sutcliffe Efficiency (NSE) between model
9 and data are reported. (b) Time series of n parameter (Eq. (6)) and soil relative humidity at the
10 Evaporation Front (rh_{EF}) that provided the best model-to-data fit. (c) $\varepsilon_{\text{K}}^{2\text{H}}$ and $\varepsilon_{\text{K}}^{18\text{O}}$ time series
11 obtained from fitted n values (“fitted”) and calculated following Mathieu and Bariac (1996)
12 (“MB96”)