

1 **Climate and hydrological variability: the catchment filtering**
2 **role**

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8 **Response to Referee Comment RC-C4407-2014 – Anonymous Referee #1**

9 The authors are extremely grateful to Anonymous Referee #1 for the time spent on our
10 research study, his/her constructive and useful comments, and relevant suggestions that will
11 greatly improve the manuscript. In particular, we would like to highlight the additional
12 analytical work done in response to comment-2 from the Referee, which substantially
13 improves and clarifies the analytical treatment of extreme flood peaks and the return period
14 estimation.

15 Here are our responses to the specific issues raised by Referee #1. Please note that point 3
16 includes additional references in the paper for a better response to the Referee's comments.

17

18 **1. On the variability of the land uses/watershed properties**

19 It is clear that certain relevant aspects in the hydrological analysis have not been addressed in
20 our study, and should guide further research on the topic.

21 As correctly indicated by anonymous Referee #1, certain dominant drivers of the hydrological
22 response, like variability of watershed properties or land use changes, have not been
23 considered in the research, although it should be noted that the proposed modelling
24 framework has the potential to incorporate the above drivers to a certain extent, and thus,
25 allow the effect of such variability to be assessed and compared. We also agree with the
26 Referee that land-use change might have a more significant impact than climate change in
27 certain hydrological conditions. However, investigating the role of land-use change would
28 require certain specific assumptions, regarding the extension of the affected area and the
29 perturbation behaviours, and therefore the general validity of our conclusions would be more

1 limited. For this reason, we decided not to include land use change impacts in the context of
 2 the present study. The latter question is beyond the scope of the present study, being
 3 modelling efforts basically centred on the role of climatic variability and its effects on
 4 catchment hydrological response, with rainfall statistical properties and its future trends
 5 representing the major factors controlling flood frequency distribution.

6 However, and following the advice by Referee #1, the scope of the study (INTRODUCTION)
 7 will be explained in more detail in the reviewed version of the manuscript. Also, emphasis
 8 will be placed on the limitations in the final conclusions, with explicit reference to future
 9 studies focusing on the effect of watershed properties and the role of land use change using a
 10 similar modelling framework.

11

12 **2. The analysis related to the number of events per year**

13 This useful comment of Referee #1 has led us to reconsider the method used for return period
 14 estimation in the study. In accordance with the main objective of the study, i.e., the analysis
 15 of maximum peak flows, we now use in the revised manuscript the analytical approach based
 16 on the classic Annual Maximum Series (AMS) method, rather than the Peak Over Threshold
 17 (POT) analysis.

18 Given the distribution function of all peak flows that is derived from the rainfall series,

$$19 \quad F_Q(q_P) = \begin{cases} 1 - (1 - \kappa I_a / \alpha)^{1/\kappa} & q_P = 0 \\ 1 - \left\{ 1 - \frac{\kappa}{\alpha} \left[I_a + \frac{t_C q_P}{2\lambda_P} \left(1 + \sqrt{1 + \frac{4\lambda_P S}{t_C q_P}} \right) \right] \right\}^{1/\kappa} & q_P > 0 \end{cases} \quad (1)$$

20 the distribution function of maximum annual floods can be expressed as (see, for instance,
 21 Viglione and Blöschl, 2009)

$$22 \quad F_{Qmax}(q_{Pmax}) = e^{-\beta(1-F_Q(q_P))} \quad (2)$$

23 where β is the annual number of rainfall events.

24 The first equation can be expressed in terms of return period (years) as:

$$25 \quad T_{Qmax} = \frac{1}{1-F_{Qmax}} \quad (3)$$

1 Combining equations (1) and (2) and replacing them in (3), we can express the T-year
2 maximum peak flow as:

$$3 \quad q_{Pmax,T} = F_Q^{-1} \left[\frac{1}{\beta} \ln \left(1 - \frac{1}{T} \right) + 1 \right] \quad (4)$$

4 Numerical results have been recalculated in the revised manuscript by using the above
5 equation (4) for the T-year maximum peak flow estimation. Figures 1, 2 and 3 have been
6 updated accordingly (see new figures at the end of this document).

7 The differences with respect to the previous analysis are not significant, and they affect low
8 return period quantiles only. Indeed, both estimation methods (POT and AMS) converge for
9 large return periods.

10 For the purpose of this study, the AMS method seems to be more illustrative and robust. On
11 the other hand, it yields the same results. In the revised version of the manuscript, the end of
12 section 2.3 will be modified to replace the estimation method for the return period.

13 To reply to the Referee, in section 3 of the paper the sentence “*According to Eq. (8), a 20%
14 increase in β implies a 16.7% decrease in the flood return period*” has been replaced. After
15 the proposed incorporation of the AMS estimation method for T, a 20% increase in β implies
16 a decrease in the flood return period ranging from 0% (for low T values) to 16.7% (for high T
17 values). In the revised version of the manuscript, this issue will be better addressed as
18 suggested by Referee #1.

19

20 **3. On the variability induced by initial abstraction and concentration time**

21 The initial abstraction value is directly obtained using a factor $k=0.2$, which is taken from
22 practical recommendations (Ferrer Polo, 1993). Concentration time value has been
23 determined based on a wide hydrological experience in many small catchments of rapid
24 response in the Mediterranean East and South East coast of Spain (Olivares Guillem, 2004;
25 Camarasa Belmonte, 1990). It can be considered a realistic, representative value for a typical
26 ephemeral river of the region. The main idea is to define a set of parameters to be kept
27 constant for the given hydrological conditions, which can essentially be representative and
28 typical of fast responding catchments in semi-arid Mediterranean regions. As stated before,
29 studying the effect of the variability of such parameters is beyond the scope of the paper,
30 although it will be underlined in the revised version of the manuscript as a main research line

1 to be pursued using the proposed modelling framework, following the suggestion by Referee
2 #1.

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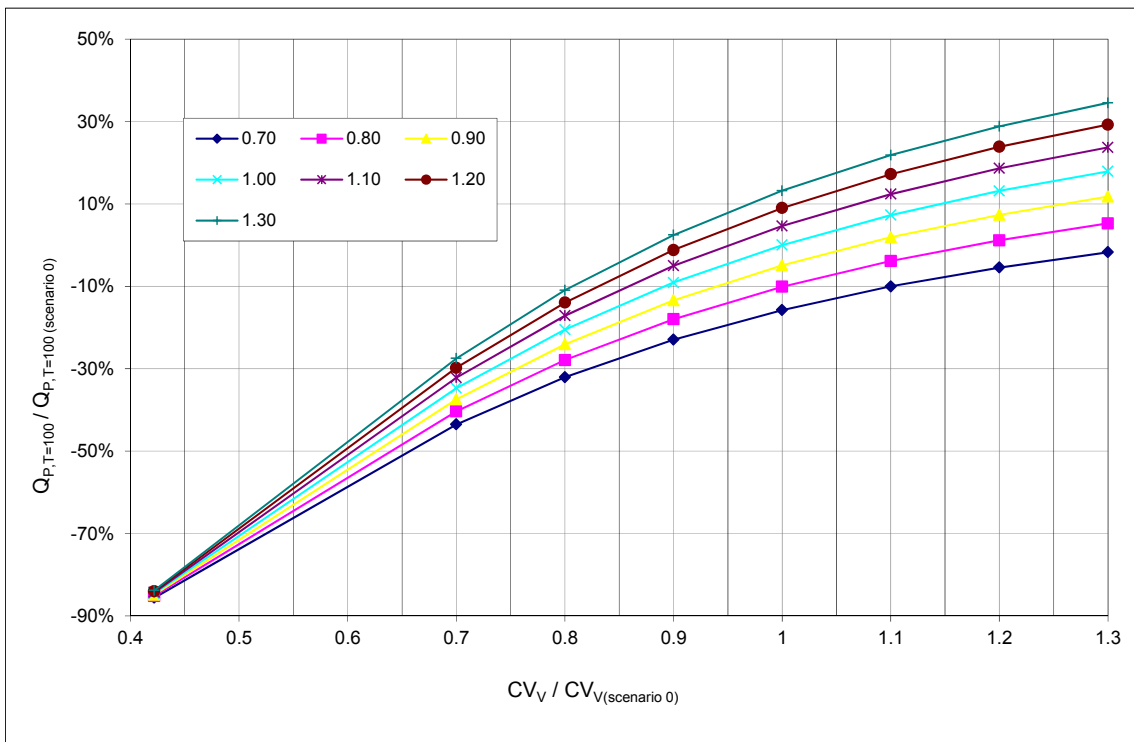
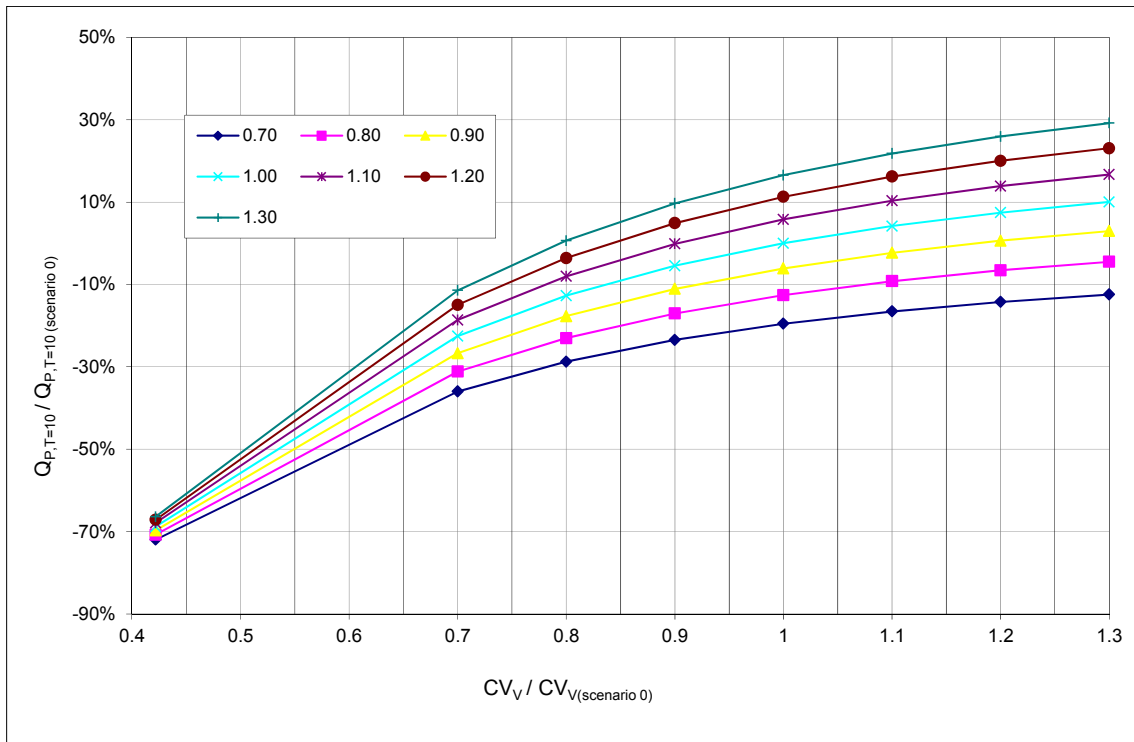
4 **Additional references**

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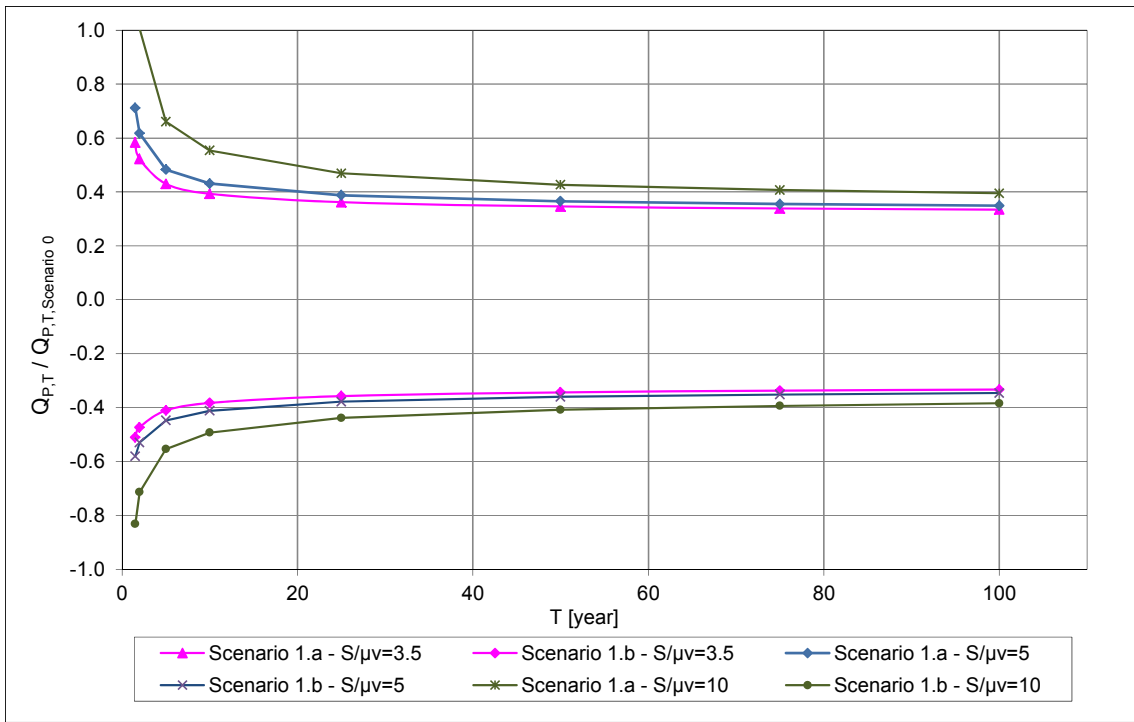
7 Ferrer Polo, J.: Recomendaciones para el cálculo hidrometeorológico de avenidas, Centro de
8 Estudios y Experimentación de Obras Públicas, Madrid, 1993.

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10 aplicación al episodio de octubre de 2000, Cuad. De Geogr., 76, 155-182, 2004.

11 Viglione, A., Blöschl, G.: On the role of storm duration in the mapping of rainfall to flood
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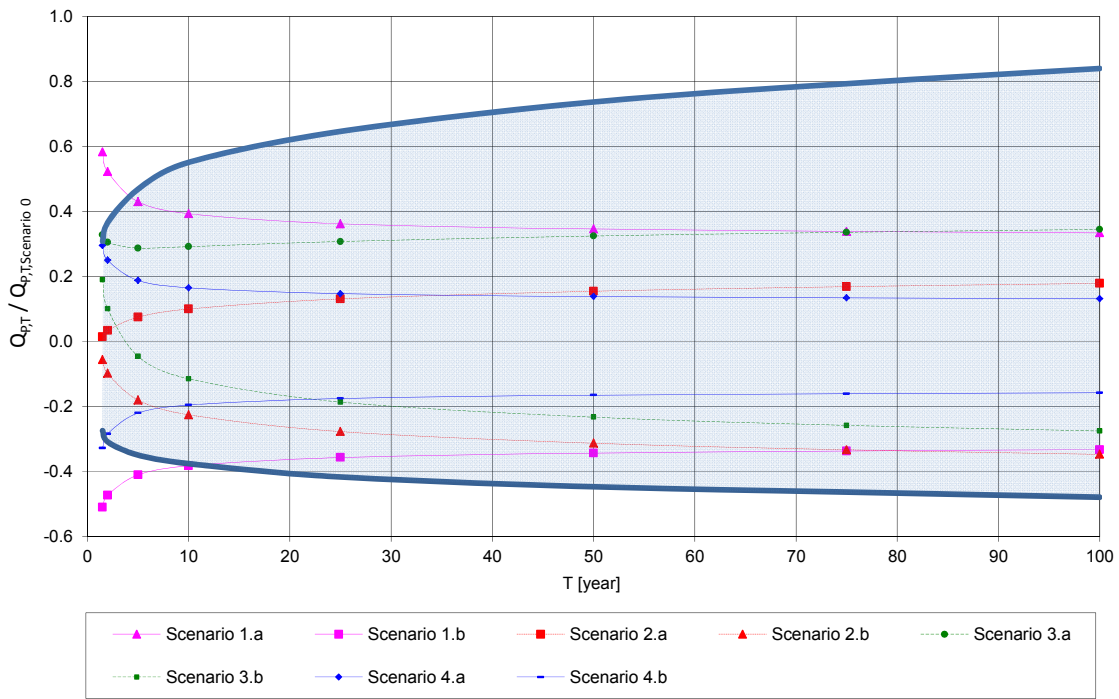


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 2 **Figure 1.** Flood quantile variations for changes in β and CV_V . Catchment parameters are set
 3 to $S/\mu_V=3.5$ and $t_C=1$ h. Cases $T=10$ years (top) and $T=100$ years (bottom).



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2 **Figure 2.** Flood quantile variations for scenarios 1.a (+30% μ_V) and 1.b (-30% μ_V) and for
 3 $S/\mu_V=3.5, 5$ and 10 .



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2 **Figure 3.** Flood quantile variations for scenarios defined in Table 1 and $\xi=0.05$ confidence
 3 interval for scenario 0 peak flow distribution (shaded area). Catchment parameters are set to
 4 $S/\mu_V=3.5$ and $t_C=1$ h.