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# Hydrogeology of an alpine rockfall aquifer system and its role in flood attenuation and maintaining baseflow

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## Abstract

The frequency and intensity of extreme hydrological events in alpine regions is projected to increase with climate change. The goal of this study was to better understand the functioning of aquifers composed of complex alluvial and rockfall deposits in alpine valleys and to quantify the role of these natural storage spaces in flood attenuation and baseflow maintenance. Geomorphological and hydrogeological mapping, tracer tests, and continuous flow measurements were conducted in the Reintal valley (German Alps), where runoff from a karst spring infiltrates into a series of postglacial alluvial/rockfall aquifers. During high-flow conditions, groundwater velocities of 30 m h<sup>-1</sup> were determined along 500 m; hydrograph analyses revealed short lag times (5 h) between discharge peaks upstream and downstream from the aquifer series; the maximum discharge ratio downstream (22) and the peak recession coefficient (0.196 d<sup>-1</sup>) are low compared with other alpine catchments. During low-flow conditions, the underground flow path length increased to 2 km and groundwater velocities decreased to 13 m h<sup>-1</sup>. Downstream hydrographs revealed a delayed discharge response after 101 h and peaks dampened by a factor of 1.5. These results indicate that alluvial/rockfall aquifers might play an important role in the flow regime and attenuation of floods in alpine regions.

## 1 Introduction

Snowmelt is a major hydrologic component of flow regimes in alpine regions, and these regimes therefore are particularly sensitive to climate change (Barnett et al., 2005). The temperature in the Alps has increased 2 °C since 1901, which is twice the average warming of the Northern Hemisphere (Auer et al., 2007). A shift of snow and precipitation pattern accompanied by higher precipitation in winter and poor snow storage is likely to substantially affect the timing and magnitude of summer discharge. Extreme events, such as floods and droughts, are expected to increase in frequency and

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intensity/magnitude (Bogataj, 2007). Because of the high contribution of alpine runoff to the total discharge of major streams in Europe, climate change will affect hydrology at lower elevations as well as in alpine regions.

The assessment of potential effects of climate change on alpine water resources requires an understanding of recharge and drainage processes. Although numerous studies have used numerical climate models to predict future amounts of recharge and water budgets (Huss et al., 2008; Bavay et al., 2009), there also is a need to investigate the hydrogeology of alpine aquifers and their drainage systems. The geological and lithological setting is often complex and has a major influence on recharge, storage, and discharge processes (Goldscheider, 2011). A thorough knowledge of the geologic framework and a conceptual model of the recharge area provide the basis for characterizing alpine groundwater systems (Plan et al., 2009). To assess underground drainage properties in high-elevated catchments, hydrochemical classification and spring monitoring methods are applicable. Such methods allow characterization of flow components and spring response to precipitation events, so that transit times can be estimated and the presence of preferential flow paths determined (Maloszewski et al., 2002; Wetzel, 2004; Mueller et al., 2013). Artificial tracer tests enable determination of flow velocities, water volumes, and storage capacities within the alpine aquifer (Gremaud et al., 2009; Goldscheider and Neukum, 2010; Finger et al., 2013). These parameters control the amount of quickflow and baseflow and thus have a large influence on flood generation and baseflow maintenance.

To investigate discharge properties in alpine headwaters, spring hydrograph studies have been conducted. It has been demonstrated that soil thickness and soil moisture (Haga et al., 2005), topography (Merz and Blöschl, 2009), and subsurface flow components (Zillgens et al., 2007) have a major control on discharge response in individual headwater catchments. Discharge properties that often are used include the discharge response as the ratio between direct discharge and precipitation intensity (Onda et al., 2006; Zillgens et al., 2007), the discharge ratio, defined here as the ratio between peak discharge and initial discharge, and the time lag between precipitation

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and the discharge peak at springs and streams (Haga et al., 2005). Stormflow and baseflow recession characteristics can further help to characterize fast and slow discharge components (Millares et al., 2009). The presence of low permeability bedrock, sparse vegetation, and high topographic gradients are likely to cause large amounts of surface runoff, which leads to high peak discharge of alpine streams and a rapid stormflow recession (Wetzel, 2003). However, a steady amount of base flow, indicated by low baseflow recession, is particularly important for baseflow maintenance in dry periods and depends greatly on the geologic structure of the aquifer, e.g., the presence of permeable structures, a high effective porosity, or triple-porosity such as occur in karst aquifers (Geyer et al., 2008). Detailed understanding of hydrogeological settings and discharge properties is necessary to construct vulnerability maps of alpine regions, which are particularly affected by floods and droughts. For maintaining and protecting natural retention zones and for developing water management strategies, natural groundwater reservoirs in the Alps need to be known. Furthermore, the feasibility of engineering works, e.g., dams, river channels, large-scale irrigation schemes, and energy production projects, is determined on the basis of the hydrogeological data. Such knowledge is required for effective flood management and creation of increased water-storage capacity (Viviroli and Weingartner, 2008; Beniston et al., 2011).

Information about hydrogeologic settings of high-alpine catchments remains incomplete because of the poor accessibility of alpine areas and the great effort required to obtain data. Applicable methods are limited and collection of data often is restricted to summer months. As a contribution to a better understanding of alpine aquifers, this study focuses on the hydrogeology of a rockfall aquifer system in the Reintal valley (Wetterstein Mountains, Germany). Alluvial and rockfall deposits are often found in steep high-alpine valleys and apparently influence discharge pattern by a strong interaction between surface flow and underground drainage. Detailed geomorphologic investigations of the sedimentary filling of the Reintal valley (Hoffmann and Schrott, 2003; Schrott et al., 2006; Morche et al., 2007, 2008; Sass et al., 2007) provided the

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basis for this hydrogeological research, which includes a combination of tracer tests and hydrograph analyses.

The study had five major goals: (1) to develop a conceptual model and to identify discharge components, (2) to characterize discharge pattern under different flow conditions, (3) to determine drainage parameters of the alluvial/rockfall aquifer, (4) to quantify discharge characteristics of the system, and (5) to evaluate effects on flood-buffering and baseflow maintenance of the alluvial/rockfall aquifer system.

## 2 Field site

### 2.1 Geography and geology

The Wetterstein Mountains are located in the Bavarian Alps near the border between Germany and Austria (Fig. 1). They consist of three mountain ridges that form some of the highest summits in Germany, including Mt. Zugspitze (2962 m a.s.l.). The deeply incised Reintal valley has steep mountain slopes and topographic relief of up to 2000 m between the valley floor and the summits. Above 2000 m a.s.l., vegetation is sparse and bare rocks dominate the landscape. The two cirques are still partially covered by vestigial glaciers with a total extent of about 55 ha.

The geological and lithological setting of the Wetterstein Mountains is dominated by the thick Triassic Wetterstein limestone, which is as much as 1000 m thick and forms the main karst aquifer (Fig. 2). The underlying strata comprise a sequence of marl and well-bedded limestone, the Partnach and Alpine Muschelkalk formations. The folded strata form two large synclines and one anticline, which appear as valleys and ridges. The fold axes trend W–E and plunge to the east (20–35°).

Since the Eocene, the region has been uplifted almost steadily to a high mountain massif. The exposure of the limestone established the basis for karstification and intense weathering, including gravitational erosion. Karstification is particularly high at cirques, where topographic gradients are lower and underground drainage dominates.

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However, only small surface karst structures, such as karren and rillenkarren, are developed along steep mountain ridges as gravitational erosion and frost wedging occur along numerous fissures and fractures.

During the glaciation in the Quaternary period, strong glacial erosion caused the present shape of the valleys, including sequences of cirques. After the retreat of glaciers and the melting of permafrost, several rockslides occurred during the Holocene along the steepened alpine valley slopes (Haeberli and Beniston, 1998). Two major rockslides occurred about 200 and 500 years ago in the Reintal valley (Schmidt and Morche, 2006). Mountain lakes formed upstream of the natural rockfall dams, but were gradually filled by sediment. The last remnant of the lower lake disappeared during a high-flow event with associated sedimentation in 2005 (Fig. 3). The alluvial plains and rockfall deposits thus have created a series of two alluvial/rockfall aquifers about 2 km long down the valley (Figs. 2 and 4). The Quaternary sediments comprise talus sheets and cones, debris cones, rockfall deposits, alluvial fans, avalanche deposits, moraines, and fluvial gravel (Schrott et al., 2006) (Fig. 2).

As a result of gravitational mass movement, the grain-size spectrum of the rockfall deposits, talus sheets, and cones covers a wide range, including large blocks with edge lengths of several meters. The coarse-grained sediments consist mainly of Wetterstein limestone, and the unsorted components form well-drained parts of the alluvial/rockfall aquifer system (Fig. 2).

The alluvial plains consist of fluvial gravel, transported by the alpine stream and surface runoff from steep slopes along the valley. Because of the reduced flow velocity and transport force, the gravel was deposited behind the rockfall dams (Morche and Schmidt, 2005). The sediments contain coarse-grained delta sediments and fine limnic sediments developed in proximity to the rockfall deposits. At the surface of the alluvial plain, braided river systems have developed, the location of which shifts following flood events. The unconsolidated alluvial deposits are part of the well-drained alluvial/rockfall aquifer and surface streams infiltrate as a result of the high permeability.

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## 2.2 Hydrology and hydrogeology

The headwaters Partnach stream in the Reintal valley forms a tributary of the Loisach river north of the Wetterstein Mountains (Fig. 1). Discharge comprises melt water from the glaciers, snow, and precipitation. Glacial and snow meltwater contribute about 30 %  
5 to the annual spring discharge (Wetzel, 2004).

In the upper valley, the stream is fed mainly by the Partnach spring (Fig. 1). With a mean discharge of  $1.2 \text{ m}^3 \text{ s}^{-1}$  between May and November (2005–2011) and a recorded maximum discharge of  $17 \text{ m}^3 \text{ s}^{-1}$  (2005), this karst springs is among the largest in the German Alps. In the lower valley, the hydrology is largely controlled by  
10 Quaternary deposits at the bottom of the valley (Fig. 2). As surface water crosses the alluvial plains, it infiltrates into the alluvial sediments and rockfall deposits. Downstream from each alluvial/rockfall deposit is a spring that drains the alluvial/rockfall aquifer system: one spring is intermittent (SP-R1) and one is perennial (SP-R2) (Fig. 4). Several  
15 more springs discharge from the river bed downstream from the rockfall deposits. The presence of these springs is attributed to the decrease in the thickness of the Quaternary deposits and the narrowing of the river bed. As a result, stream discharge increases substantially in this part of the valley. The total discharge from the Reintal valley is measured at the downstream end of the valley (gauging station GS-RD, Fig. 1). The mean annual discharge associated with the  $28 \text{ km}^2$  catchment area during  
20 2005–2011 is about  $1.8 \text{ m}^3 \text{ s}^{-1}$ .


## 3 Methods

### 3.1 Artificial tracer tests



To investigate the alluvial/rockfall aquifer system in the valley, a tracer test with 5 kg  
25  sodium-naphthionate (CAS 130-13-2) was conducted on 19 July 2011. The injection was performed after several days of rain, which resulted in high discharge at all springs

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in the valley. Where the stream flows through the upper alluvial plain, it forms a braided river system that infiltrates completely into the coarse-grained alluvial/rockfall deposits at several swallow holes (Fig. 2). The tracer was injected in one of the numerous swallow holes near the lower end of the alluvial plain, where the infiltration rate into the rockfall  
5 deposits was about  $6 \text{ L s}^{-1}$ . The dye was dissolved in a 20-L canister at the injection site and the tracer solution was injected instantaneously. Observation points were located downstream in the valley: at the springs draining the alluvial/rockfall masses (SP-R1 and SP-R2) and further downstream at the outlet of the valley (SP-R3) (Fig. 4). At the spring closest to the injection point (SP-R1), water samples were collected  
10 every 30 min during the first 10 h following tracer injection. As many as six water samples a day were collected during the following days. The final samples were collected three weeks after injection.

Two spectro-fluorimeters (Perkin Elmer, LS 50 B and LS 55) in the hydrogeology laboratory of the Karlsruhe Institute of Technology were used to measure tracer concentration in water samples, using the synchronous-scan-method. Tracer recovery was  
15 calculated using data from  salt-dilution measurements at springs and gauging stations.

### 3.2 Discharge measurements

The two principal gauging stations in the valley are located at the Partnach karst spring upstream from the alluvial/rockfall deposits (site GS-RU) and at the outlet of the alluvial/rockfall aquifer system (site GS-RD) (Fig. 1). Water levels were measured every 15  
20 min during observation periods with dataloggers DL 8.4 (EBRU), Orphimedes, and Orpheus K (Ott Hydrometrie) (Schmidt and Morche, 2006). Measurements were collected from late spring until late autumn, as snow, ice, and avalanches inhibit measurement in the winter season. Data from 2002–2011 were evaluated, but no measurements were  
25 conducted at GS-RU in 2009. Discharge was measured using a current meter (Ott C2) for a range of flow conditions. At other observation points in the valley, e.g., SP-R1 and SP-R2, discharge was measured manually by the  salt-dilution method. 

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### 3.3 Data analysis

All breakthrough curves (BTCs) from the tracer tests were analysed quantitatively. The time of first detection ( $t_0$ ), maximum flow velocity ( $v_{\max}$ ), peak transit time ( $t_{\text{peak}}$ ), and peak flow velocity ( $v_{\text{peak}}$ ) were directly determined from the BTCs. Mean flow velocities ( $v$ ) and dispersion coefficients ( $D$ ) were quantified using the analytical advection-dispersion model (ADM) implemented in the CXTFIT software (Toride et al., 1999) (Eq. 1).

$$\frac{\delta c}{\delta t} = D \frac{\delta^2 c}{\delta x^2} - v \frac{\delta c}{\delta x} \quad (1)$$

The model calculates one-dimensional flow of the tracer indicated by its concentration ( $c$ ) at a given distance ( $x$ ) in the direction of flow. The analytical equation is solved by assuming homogeneous profiles, a uniform and unidirectional flow field that is constant in time and space, and constant flow parameters. An inverse modelling tool of the ADM provides best estimates of the two flow parameters ( $v, D$ ) by fitting a modelled BTC to measured values.

Using additional information from discharge measurements, recovery was calculated according to (Käss, 2004). Water volume ( $V$ ) was estimated by multiplying the mean discharge ( $Q_{\text{mean}}$ ) and the mean transit time of the tracer ( $t_{\text{mean}}$ ) (Field and Nash, 1997).

In analysing hydrographs, the best correlation of water level ( $h$ ) and discharge ( $Q$ ) is determined by fitting an exponential regression function with the two adjusting variables  $a$  and  $b$  (Eq. 2):

$$Q = a \cdot e^{bh} \quad (2)$$

Coefficients of determination are greater than 0.91 and the standard error is about  $0.3 \text{ m}^3 \text{ s}^{-1}$  (Morche et al., 2008). With more than 56 measurements, the calibration covers a wide range of discharges. To compare discharge characteristics from upstream and downstream of the series of alluvial/rockfall aquifers, hydrographs of the

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years 2006 and 2011 are presented in this paper, as they have the most continuous records. The year 2006 is further characterized by extreme flow conditions. Annual discharge of the catchment is lowest of all observed years and an extreme precipitation event causes extreme high-flow conditions in August.

Discharge was analysed for selected precipitation events that caused clear discharge peaks at the gauging stations. Because of the strong influence of snowmelt, which results in a more diffuse discharge response, most events analysed occurred during summer and autumn. Precipitation data with a sampling interval of 6 h were obtained by Deutscher Wetterdienst (DWD) at the summit of Mt. Zugspitze. As a consequence, the lag time between peak rainfall and peak discharge cannot be quantified at a higher resolution than 6 h. Initial discharge for an event ( $Q_i$ ) is defined as the discharge rate before the increase began and peak discharge ( $Q_p$ ) is defined as the discharge maximum. The discharge response is calculated by dividing the amount of direct discharge ( $Q_p - Q_i$ ) by the precipitation intensity ( $P_{\text{peak}}$ ), a unit conversion factor and the catchment area ( $A$ ) (Blume et al., 2007). The increase of discharge after a precipitation event is described by the discharge ratio  $Q_p/Q_i$ . Additionally, the lag time between discharge peaks upstream (site GS-RU) and at the outlet of the catchment (site GS-RD) was determined to assess discharge characteristics of the aquifer system.

Discharge response characteristics were described quantitatively by transfer functions (Asmuth and Knotters, 2004). This method can be applied to input signals that are transferred through a system and that result in distinctive output signals dispersed in time. In this case, the transferred signal can be described by an impulse-response-function with a lognormal distribution (Eq. 3) (Long and Mahler, 2013).

$$Q_t = Q_i + \frac{A_{\text{out}}}{t \omega \sqrt{2\pi}} e^{-\frac{\left[\ln \frac{t}{t_m}\right]^2}{2\omega^2}} \quad (3)$$

where  $A_{\text{out}}$  is a scaling coefficient that quantifies the area under the curve, and  $t_m$  and  $\omega$  describe mean transit time and its variance. In this study, discharge peak upstream from the alluvial/rockfall aquifer system (GS-RU) was used as the input impulse ( $t = 0$ ).

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The output signal downstream from the alluvial/rockfall deposits (GS-RD) occurring at time  $t$  after the input impulse was fitted with the function ( $Q_t$ , Eq. 3). Because additional surface runoff from steep slopes that occurs under mean- to high-flow conditions can interfere with the original input signal, only selected discharge responses under low-flow conditions with one clear input and one clear output signal were analysed.

To quantify aquifer properties under stormflow and baseflow conditions, recession coefficients ( $\alpha$ ) were determined from hydrographs upstream (karst drainage) and downstream from the alluvial/rockfall aquifers. The falling limb of the hydrographs represents drainage of groundwater reservoirs that exhibit distinct exponential flow rates for each groundwater reservoir (Bonacci, 1993; Bailly-Comte et al., 2010). Recession curve analyses were done using an exponential function (Eq. 4):

$$Q_t = Q_0 \cdot e^{-\alpha t} \quad (4)$$

where  $Q_0$  is the initial spring discharge and  $t$  is the time step following the decline of spring discharge ( $Q_t$ ). Each falling limb was divided into up to three sections to obtain the recession coefficient  $\alpha$ . Because of the strong linear correlation on a semi-logarithmic plot ( $r^2 > 0.9$ ), the use of Eq. (4) was justified (Zillgens et al., 2007).

## 4 Results and discussions

### 4.1 Conceptual model

The conceptual model of the alpine valley consists of one karst aquifer and a series of two alluvial/rockfall aquifers. In the upper valley, the karst spring is the principal contributor to stream discharge (Fig. 5). All meltwater from glacial ice, snowmelt, and all precipitation in the highly karstified cirque drain through subsurface flow paths to the Partnach karst spring. Tracer tests have shown fast drainage along well-developed karst conduits with linear mean flow velocities of up to  $104 \text{ m h}^{-1}$  (Rappl et al., 2010).

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The lower valley comprises two alluvial/rockfall aquifers in series (Fig. 5), each consisting of an alluvial plain and a rockfall deposit. The alluvial/rockfall aquifers are linked and characterized by a substantial thickness of Quaternary sediments. All discharge from the karst spring infiltrates into the first alluvial/rockfall aquifer because of the high permeability of the rockfall deposits (Fig. 6). Several sinks and sources, including SP-R1 and SP-R2, exist in the area of the aquifers; the number and location depend on flow conditions and water levels. Total discharge increases towards the outlet of the valley because of the decreasing thickness of the Quaternary fill.

Here we define low-flow conditions as those under which all discharge from the Partnach karst spring infiltrates into the alluvial/rockfall aquifer and follows a 2 km long subsurface flow path until it discharges at SP-R2 at the lower end of the alluvial/rockfall aquifer system (Fig. 6). Low-flow conditions generally occur when baseflow is less than  $0.8 \text{ m}^3 \text{ s}^{-1}$  at site GS-RU and  $1.8 \text{ m}^3 \text{ s}^{-1}$  at site GS-RD. Peak discharge after precipitation events at GS-RU rarely exceeds  $2.3 \text{ m}^3 \text{ s}^{-1}$ . Because the water table is low, there is no flow from spring SP-R1. At low water levels, spring SP-R2 is situated in the river bed as much as 600 m downstream from the alluvial/rockfall deposits (Morche et al., 2007) (Fig. 6). There is no surface runoff from steep slopes of the valley. Low-flow conditions generally occur in late summer, autumn, and winter, when there is little precipitation and no meltwater.

Moderate-flow conditions are characterized mainly as a transition between low- and high-flow and therefore often occur only for a short period of a few hours to a few days. Because the water table is higher than during low-flow conditions, some part of the water discharges directly downstream from the first alluvial/rockfall deposits at spring SP-R1 after traveling along a short subsurface flow path of about 500 m (Fig. 6). Until 2005, there was a small ephemeral mountain lake on the second alluvial plain, which functioned as a water reservoir and sediment trap (Schmidt and Morche, 2006) (Fig. 3). Today, discharge from SP-R1 infiltrates into the second alluvial/rockfall aquifer after traveling along a short surface flow path, and drains underground to spring SP-R2 (Fig. 6). Because the water level is higher than during low-flow conditions, spring SP-R2

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discharges directly downstream from the alluvial/rockfall deposits. During moderate-flow conditions, the steep slopes along the valley contribute a few tens of  $\text{L s}^{-1}$  surface runoff, which is only a small proportion of total stream flow.

High-flow conditions occur after intense or prolonged precipitation events and during peak snow melt in early summer. Because the water table is high, a substantial proportion of the groundwater discharges directly downstream from the first alluvial/rockfall deposits at spring SP-R1, where discharge can exceed  $1 \text{ m}^3 \text{ s}^{-1}$ . While some of the water infiltrates into the second alluvial/rockfall aquifer, there is also surface flow over the second alluvial/rockfall deposits (Fig. 6). Surface flow and subsurface drainage converge and mix at spring SP-R2. After large precipitation events, fast-flowing streams and torrents from steep slopes along the valley deliver surface runoff. Most high-flow conditions have been observed when peak discharge rates exceed  $2.3 \pm 0.2 \text{ m}^3 \text{ s}^{-1}$  at site GS-RD.

## 4.2 Drainage properties

The overall results of the tracer test enabled insights into drainage properties of different parts of the alluvial/rockfall system and proportions of flow paths to the total discharge along the valley. The naphthionate was detected at all three sampling points: the two springs SP-R1 and SP-R2 and the outlet of the aquifer system SP-R3 (Fig. 4, Table 1). High-flow conditions occurred during the first three days after the injection (Fig. 6).

The tracer breakthrough curve (BTC) at SP-R1, 500 m downgradient from the injection site, has one clear peak and a short tail (Fig. 7a). The tracer was first observed 8 h after the injection, and the tracer peak concentration of  $52.1 \mu\text{g L}^{-1}$  was measured 16 h after the injection. The linear peak flow velocity was about  $31 \text{ m h}^{-1}$ . A discharge of  $440 \text{ L s}^{-1}$  was measured during the first three days, resulting in a recovery of 30% of the tracer.

At spring SP-R2, the tracer was first detected after 23 h (Fig. 7b) and the tracer peak concentration of  $21.8 \mu\text{g L}^{-1}$  was measured 28 h after injection. The linear peak flow

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velocity was  $53 \text{ m h}^{-1}$ . During the first 75 h, the BTC had one sharp peak followed by a decrease of concentration down to  $0.6 \mu\text{g L}^{-1}$ . 117 h after injection, the concentration rose slightly to  $1.5 \mu\text{g L}^{-1}$ , forming a second, small peak (Fig. 7b, Table 1). During the first half of the tracer breakthrough (about the first 75 h), flow conditions were high and surface flow occurred downstream from SP-R1 (Fig. 6). However, after 75 h, moderate-flow conditions were reached and all water from SP-R1 infiltrated (Fig. 6). We therefore interpret the second increase in tracer concentration as a separate peak related to the peak in subsurface flow. The linear subsurface flow velocity of  $13 \text{ m h}^{-1}$  was substantially less than the linear surface-flow velocity of  $53 \text{ m h}^{-1}$ . During the main part of the tracer breakthrough, mean discharge at this sampling point was about  $580 \text{ L s}^{-1}$ , and tracer recovery was about 21%.

At site SP-R3, the outlet of the system, the maximum tracer concentrations of  $4 \mu\text{g L}^{-1}$  was measured 66 h after injection (Fig. 7c). The linear peak flow velocity was  $48 \text{ m h}^{-1}$ . The shape of the tail at SP-R3 indicates the presence of the second peak at this site as well (Fig. 7c). Because of high dilution and high dispersion along the surface flow path, the second peak is small but recognizable. The sampling point is about 3.1 km from the injection point. The mean discharge at this site was about  $2500 \text{ L s}^{-1}$ , and tracer recovery was 59%.

Hydraulic parameters of the system were determined by ADM modelling of the observed BTCs at the observation points. A dispersion of  $630 \text{ m}^2 \text{ h}^{-1}$  was obtained from data for spring SP-R1 and applies to flow through the high-permeability part of the rockfall aquifer. Results from sites SP-R2 and SP-R3 are influenced by surface flow and are not further discussed. However, high dispersion values for site SP-R3 indicate highly turbulent flow of the stream.

The obtained flow velocities are attributed to different parts within the aquifer system and tracer recovery demonstrates discharge proportions of flow paths. The flow velocities of  $30 \text{ m h}^{-1}$  along the short flow path from IP-2011 to SP-R1 are very high for a porous aquifer and are attributable to flow through very coarse-grained rockfall deposits with numerous large limestone blocks. The tracer recovery of 30% at site SP-R1

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indicates that only about 1/3 of spring infiltration discharges directly downgradient from the first alluvial/rockfall deposits. Along the long subsurface flow path to SP-R2, substantially lower flow velocities of  $13 \text{ m h}^{-1}$  occur because flow is through alluvial gravel. The decreased recovery of 21 % at SP-R2 in comparison with recovery at SP-R1 is related to infiltration processes upstream at the alluvial/rockfall aquifer under moderate- to high-flow conditions (Fig. 6). The total recovery of the tracer downstream at SP-R3 reaches 59 %, because stream discharge increases steadily in a downstream direction to the outlet and there are further inflows from the Quaternary sediments into the stream. The tracer test thus demonstrated that there is a large amount of water draining underground.

The total tracer recovery of 59 % indicates the relatively large storage capacity of the series of alpine alluvial/rockfall aquifers. As all of the water from the upper valley drains towards SP-R3, a recovery of almost 100 % can be estimated as a best case. The difference of about 41 % indicates intermediate storage in the aquifer system.



### 4.3 Discharge characteristics

The hydrographs in the Reintal valley show distinct annual patterns because of the snowmelt-controlled discharge regime. In 2006, discharge begins to increase in mid-April and reaches a characteristic discharge maximum of about  $7 \text{ m}^3 \text{ s}^{-1}$  at the end of June, corresponding to the period of maximum snowmelt (Fig. 8). Daily discharge fluctuations of about  $100 \text{ L s}^{-1}$  are attributed to diurnal temperature changes and meltwater production from the glacier and snow fields (Figs. 8 and 9). There are several discharge peaks related to moderate to large precipitation events. Maximum discharge rates of  $8 \text{ m}^3 \text{ s}^{-1}$  at GS-RU and  $16 \text{ m}^3 \text{ s}^{-1}$  at GS-RD were measured after an extreme precipitation event in 2006. With decreasing snowmelt contribution, discharge decreased gradually to  $0.5 \text{ m}^3 \text{ s}^{-1}$  during the second half of 2006 and 2011. As the valley is largely inaccessible during winter months, there has been only one observation (March 2007) that the karst spring is not perennial. The stream at the outlet of the system (site GS-RD) has not been observed to run dry during winter months.

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Hydrologic flow conditions and water levels in the alluvial/rockfall aquifer have a substantial influence on discharge characteristics in the valley. Differences between the hydrographs upstream and downstream from the alluvial/rockfall aquifers depend on surface and subsurface drainage between the two sites. The input signal at the karst spring shows that sharp discharge peaks occur less than 6 h following precipitation events reflecting concentrated drainage through a well-developed karst system. On the basis of 38 discharge events that occurred during 2002–2011, lag times of about 5, 35, and 101 h between the input at GS-RU and output signal at GS-RD are dominant (Table 2, Fig. 11, Table S1 in the Supplement). There is no direct correlation between lag times and individual hydrometeorological parameters; instead, lag times are related to the hydrologic flow conditions in the alluvial/rockfall aquifer system. In summer (May–August), the sharp input signal at site GS-RU results in rapid and marked discharge responses downstream from the alluvial/rockfall aquifer systems (site GS-RD) (peaks 1–3 and peaks 7–9, Figs. 8 and 9). Short lag times of a few hours are associated with precipitation events occurring at high water levels, when subsurface flow paths are short and surface discharge downstream from the upgradient rockfall deposits results in rapid transit of the flood wave (Figs. 6 and 8). An extremely fast response of less than 5 h also can be attributed to surface runoff and torrents from steep slopes along the valley (Fig. 6).

Recharge events occurring during low-flow conditions result in distinctive wide discharge peaks downstream from the alluvial/rockfall deposits. In spring and autumn, sharp discharge peaks upstream cause delayed flood waves downstream that span several days (peaks 4–6 and 10–11, Fig. 8–10). The mean lag time between maximum discharge at the karst spring (GS-RU) and the outlet of the valley (GS-RD) determined from the impulse-response analyses is 101 h (Table 3). Substantial flood dampening is indicated by a decrease in maximum discharge of a factor of 1.5 (Fig. 10). The strong dampening effects are attributable to infiltration associated with low water levels, resulting in a long subsurface flow path of up to 2 km and storage within the aquifer (Fig. 6). During prolonged periods of low-flow conditions, e.g., during dry periods or in late





autumn, flow velocities are expected to decrease as groundwater levels fall and discharge decreases. Lag times determined from the hydrographs can increase to values of as much as 190 h in extreme dry years, e.g., 2003 (Table S1 in the Supplement).

The discharge ratio downstream from the alluvial/rockfall aquifers is less than that of the Partnach spring, indicating flow dampening along the subsurface flow path between the two sites. While the discharge ratio at GS-RU has a mean value of 2.7, the ratio downstream from the aquifer system at site GS-RD has only a mean value of 1.9 (Table 2). The mean values exclude the extreme event in August 2006, which resulted in discharge ratios of 8 at GS-RU and 22 at GS-RD. A substantially higher discharge ratio downstream at GS-RD is the result of a high proportion of surface runoff relative to groundwater discharge. Extreme precipitation intensity followed by a high volume of surface runoff likely causes this discharge response. Nevertheless, the discharge ratio for the Reintal valley is much less than that for other alpine catchments, e.g., the Lahnwiesgraben, where a discharge variability of up to 2500 was reported by Schmidt and Morche (2006). The Lahnwiesgraben catchment is largely covered by glacial sediment and the bedrock is dominated by diverse lithologies, including marls and mudstones. The results from the Reintal valley thus demonstrate that the flood-buffering potential is related to karst drainage and flow through the permeable alluvial/rockfall deposits.

The much larger recession coefficients upstream relative to downstream is evidence of the strong flood-buffering effects of the alluvial/rockfall deposits and demonstrates that they act as a natural retention zone. Analyses of 15 recession events demonstrate that flood recession coefficients at the karst spring (GS-RU) are generally about a factor of 2 to 5 higher than those downstream the alluvial/rockfall deposits (GS-RD) (Fig. 10). The highest flood recession coefficient at the karst spring ( $1.04 \text{ d}^{-1}$ ) was determined for the extreme precipitation event in August 2006 and is attributed to concentrated recharge and drainage through the karst conduit network. For the same event, the flood recession coefficient downstream at GS-RD was about  $0.20 \text{ d}^{-1}$ , while the falling limb is gentler and the base of the peak downstream (site GS-RD) generally is broader than at the Partnach spring upstream (site GS-RU). Baseflow recession coefficients at

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the karst spring and downstream from the alluvial/rockfall aquifer show lowest values of about  $0.005 \text{ d}^{-1}$  after a long period (45 days) in 2005, at which time the discharge decreased to the lowest values measured ( $0.56 \text{ m}^3 \text{ s}^{-1}$  at GS-RU and  $0.84 \text{ m}^3 \text{ s}^{-1}$  at GS-RD). Water storage properties of the alluvial/rockfall aquifer maintain baseflow and perennial discharge at the outlet. In the Lainbachtal valley in the German Alps, substantially higher flood recession coefficients in the range of  $7.2$  to  $84 \text{ d}^{-1}$  indicate very rapid drainage of the underground reservoir (Wetzel, 2003). The steep area is dominated by moraine sediments with a low hydraulic permeability resulting in a rapid discharge response.

Infiltration and storage processes are related to water levels in the aquifer system and are highest at low water levels. During low-flow conditions, flood-buffering of recharge events play an important role because of the high infiltration of water into the series of alluvial/rockfall deposits and because of long subsurface flow paths (Fig. 6). This is shown by the long lag times and the dampened discharge ratio at GS-RD. Substantial infiltration was also observed during early summer in 2006, when discharge downstream from the alluvial/rockfall aquifers (site GS-RD) was about  $0.4 \text{ m}^3 \text{ s}^{-1}$  lower than that upstream, at the karst spring (site GS-RU) (Fig. 8). The observations in 2006 indicate replenishment of the aquifer after low-flow conditions during the winter. At high water levels, when infiltration and subsurface flow paths are shortest, flood-buffering effects are at a minimum because of the high proportion of overland flow. This is indicated by rapid transit of the flood wave but, nevertheless, moderate flood recession

High magnitude rockfall deposits (bergsturz, rockslide) have a long persistence and an impact on sediment transfer and ecosystems in high mountain basins. The interaction between surface and subsurface flow inhibits large sediment output in the catchment; sediment deposition occurs at the alluvial plains (Schmidt and Morche, 2006; Morche et al., 2007). Braided-river systems on the alluvial plains and infiltration and storage in the alluvial/rockfall aquifer system enable the development of unique alpine ecosystems in the Reintal valley. Because the flood-buffering properties of the aquifer system prevent abrasive fluvial erosion, vegetation can grow close to the stream bed.

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## 5 Conclusions and outlook

The alluvial/rockfall aquifer system of the Reintal valley has a substantial influence on the discharge and water storage in the high-alpine valley. The valley is characterized by a series of karst and alluvial/rockfall aquifers that affect discharge from the alpine catchment. Depending on the hydrologic flow conditions, the surface and underground flow patterns change substantially in the valley. Under high-flow conditions, discharge peaks at the outlet of the valley occurred about 5 h after discharge peaks in the upper part of the valley. Flood recession curves were substantially wider downstream than upstream, indicating that the strong interaction of surface and subsurface flow along the alluvial/rockfall aquifer system buffers flood flow. The greatest flood-dampening effects were observed in response to recharge events that occurred under low-flow conditions during the autumn. Dominant lag times of 101 h occurred together with a decrease in peak discharge by a factor of 1.5. The storage properties of the aquifer enable replenishment and a slow release of water and thus provide baseflow during periods of low flow.

The presence of such natural retention zones might be important with regard to climate change, i.e., floods and droughts. Other high alpine valleys also might have hydrogeologic settings conducive to flood dampening and baseflow maintenance. Better understanding of the hydrogeology of alpine headwaters could be a useful tool for improved water management and the development of risk maps.

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**Table 1.** Results of the 2011 tracer test in the Reintal valley.

|                              |                                | SP-R1  | SP-R2 | SP-R3  |
|------------------------------|--------------------------------|--------|-------|--------|
| Linear distance              | m                              | 500    | 1500  | 3150   |
| Mean discharge <sup>a</sup>  | L s <sup>-1</sup>              | 440    | 580   | 2500   |
| First detection              | h                              | 8.4    | 23.0  | 22.5   |
| Max. flow velocity           | m h <sup>-1</sup>              | 59.7   | 65.2  | 140    |
| Peak transit time (1st peak) | h                              | 16.3   | 28.4  | 65.8   |
| Peak flow velocity (1st)     | m h <sup>-1</sup>              | 30.6   | 52.8  | 47.8   |
| Max. concentration (1st)     | µg L <sup>-1</sup>             | 52.1   | 21.8  | 4.1    |
| Peak transit time (2nd peak) | h                              | –      | 116.8 | 262.2  |
| Peak flow velocity (2nd)     | m h <sup>-1</sup>              | –      | 12.8  | 12.0   |
| Concentration (2nd)          | µg L <sup>-1</sup>             | –      | 1.5   | 0.3    |
| Recovery                     | %                              | 30.0   | 20.5  | 58.7   |
| Water volume                 | m <sup>3</sup>                 | 25 883 | –     | –      |
| Mean transit time (1st peak) | h                              | 21.3   | 33.7  | 85.6   |
| Mean flow velocity (1st)     | m h <sup>-1</sup>              | 23.5   | 44.5  | 36.8   |
| Dispersion (1st)             | m <sup>2</sup> h <sup>-1</sup> | 630    | 806   | 15 700 |
| R <sup>2</sup>               | –                              | 0.966  | 0.945 | 0.916  |

<sup>a</sup> mean discharge during main tracer breakthrough.

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**Table 2.** Discharge characteristics of selected precipitation events in 2006 and 2011. All events with a peak discharge  $Q_P > 2.3 \pm 0.2 \text{ m}^3 \text{ s}^{-1}$  are high-flow events ( $Q_i$ : initial discharge;  $Q_P$ : peak discharge; discharge response: ratio between direct discharge ( $Q_P - Q_i$ ) and precipitation ( $P_{\text{peak}} \cdot A$ ); discharge ratio: quotient between  $Q_P$  and  $Q_i$ ; lag time: time difference between discharge peak upstream (GS-RU) and downstream (GS-RD) from the rockfall aquifers; flow conditions indicate high-flow (HF) and low- to moderate flow conditions (LF/MF) of the individual events).

| Event   | Gauging station | $P_{\text{SUM}}^a$<br>mm | Peak rainfall <sup>b</sup><br>mm | Rainfall duration<br>h | $Q_i$<br>$\text{m}^3 \text{ s}^{-1}$ | $Q_P$<br>$\text{m}^3 \text{ s}^{-1}$ | Discharge response | Discharge ratio | Lag time<br>h    | Flow conditions <sup>d</sup> |
|---|-----------------|--------------------------|----------------------------------|------------------------|--------------------------------------|--------------------------------------|--------------------|-----------------|------------------|------------------------------|
| 20 May 2006   | GS-RU           | 37                       | 8                                | 6                      | 0.97                                 | 3.52                                 | 0.604              | 3.63            | 38               | HF                           |
|   | GS-RD           |                          |                                  |                        | 0.53                                 | 3.11                                 | 0.611              | 5.87            |                  |                              |
| 28 May 2006   | GS-RU           | 148                      | 80                               | 18                     | 1.14                                 | 6.03                                 | 0.116              | 5.29            | 33               | HF                           |
|   | GS-RD           |                          |                                  |                        | 0.51                                 | 2.63                                 | 0.050              | 5.16            |                  |                              |
| 7 Aug 2006  | GS-RU           | 487                      | 100                              | 12                     | 0.96                                 | 8.09                                 | 0.135              | 8.43            | 3.8              | HF                           |
|   | GS-RD           |                          |                                  |                        | 0.64                                 | 14.40                                | 0.261              | 22.50           |                  |                              |
| 18 Sep 2006   | GS-RU           | 171                      | 80                               | 18                     | 0.65                                 | 1.25                                 | 0.014              | 1.92            | 101 <sup>c</sup> | LF/MF                        |
|   | GS-RD           |                          |                                  |                        | 0.74                                 | 1.06                                 | 0.008              | 1.43            |                  |                              |
| 27 Sep 2006   | GS-RU           | 264                      | 90                               | 30                     | 0.65                                 | 1.22                                 | 0.012              | 1.88            | 93 <sup>c</sup>  | LF/MF                        |
|   | GS-RD           |                          |                                  |                        | 0.67                                 | 0.93                                 | 0.005              | 1.39            |                  |                              |
| 4 Oct 2006  | GS-RU           | 292                      | 150                              | 18                     | 0.67                                 | 2.84                                 | 0.027              | 4.24            | 106 <sup>c</sup> | LF/MF                        |
|   | GS-RD           |                          |                                  |                        | 0.77                                 | 1.80                                 | 0.013              | 2.34            |                  |                              |
| 18 Jun 2011   | GS-RU           | 391                      | 200                              | 18                     | 1.65                                 | 3.77                                 | 0.020              | 2.28            | 9.5              | HF                           |
|   | GS-RD           |                          |                                  |                        | 2.58                                 | 4.96                                 | 0.023              | 1.92            |                  |                              |
| 30 Jun 2011   | GS-RU           | 300                      | 160                              | 12                     | 1.34                                 | 4.02                                 | 0.032              | 3.00            | 29               | HF                           |
|   | GS-RD           |                          |                                  |                        | 2.04                                 | 3.08                                 | 0.012              | 1.51            |                  |                              |
| 7 Aug 2011  | GS-RU           | 550                      | 310                              | 12                     | 0.88                                 | 2.65                                 | 0.011              | 3.01            | 36               | HF                           |
|   | GS-RD           |                          |                                  |                        | 2.00                                 | 3.45                                 | 0.009              | 1.73            |                  |                              |
| 5 Sep 2011  | GS-RU           | 525                      | 210                              | 18                     | 0.52                                 | 1.96                                 | 0.013              | 3.77            | 86 <sup>c</sup>  | LF/MF                        |
|   | GS-RD           |                          |                                  |                        | 1.04                                 | 1.71                                 | 0.006              | 1.64            |                  |                              |
| 18 Sep 2011   | GS-RU           | 190                      | 150                              | 12                     | 0.46                                 | 1.2                                  | 0.009              | 2.61            | 105              | LF/MF                        |
|   | GS-RD           |                          |                                  |                        | 1.00                                 | 1.6                                  | 0.008              | 1.60            |                  |                              |
| 10 Oct 2011   | GS-RU           | 307                      | 120                              | 18                     | 0.45                                 | 3.16                                 | 0.043              | 7.02            | 34               | HF                           |
|   | GS-RD           |                          |                                  |                        | 0.9                                  | 2.87                                 | 0.031              | 3.19            |                  |                              |
| mean values of 2006 to 2011 (excluding extreme event in 2006) |                 |                          |                                  | GS-RU                  | 1.04                                 | 2.65                                 | 0.036              | 2.65            |                  |                              |
|   |                 |                          |                                  | GS-RD                  | 1.80                                 | 3.22                                 | 0.032              | 1.93            |                  |                              |

<sup>a</sup> Sum of precipitation until peak discharge at GS-RU;

<sup>b</sup> Note that maximum resolution of sum of precipitation is 6 h;

<sup>c</sup> Obtained by impulse-response-analysis;

<sup>d</sup> HF: high-flow conditions; LF/MF: low- to moderate flow conditions.

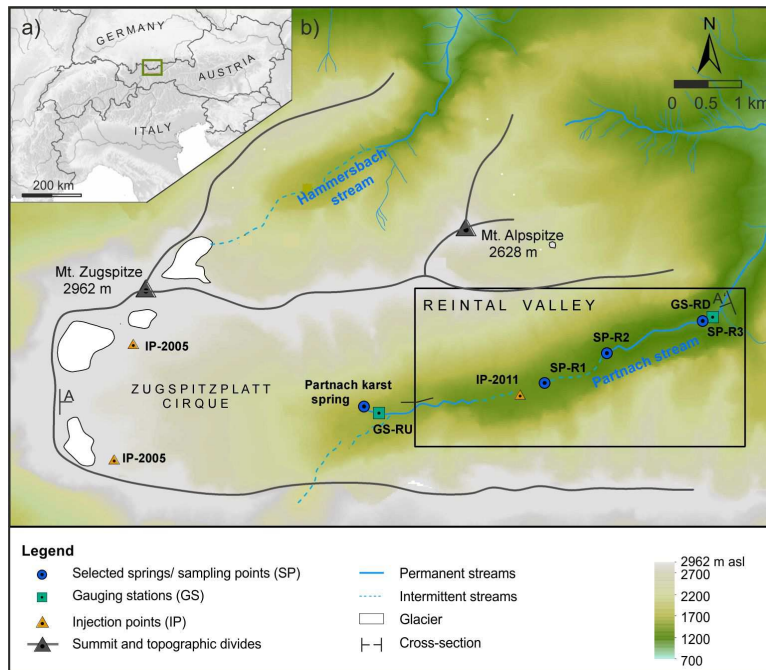
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**Table 3.** Results of the impulse-response analysis for three discharge events in 2006 ( $A_{\text{in}}$ : area under input signal at site GS-RU;  $A_{\text{out}}$ : area under output signal at site GS-RD;  $t_m$ : mean transit time;  $\omega$ : variance of time;  $R^2$ : coefficient of determination from impulse-response function).

| Date        | $A_{\text{in}}$ | $A_{\text{out}}$ | $t_m$ | $\omega$ | $R^2$ |
|-------------|-----------------|------------------|-------|----------|-------|
| 20 Sep 2006 | 10.7            | 30.5             | 100.7 | 0.379    | 0.915 |
| 28 Sep 2006 | 5.5             | 19.4             | 93.2  | 0.388    | 0.897 |
| 03 Oct 2006 | 24.9            | 131.1            | 105.9 | 0.542    | 0.972 |

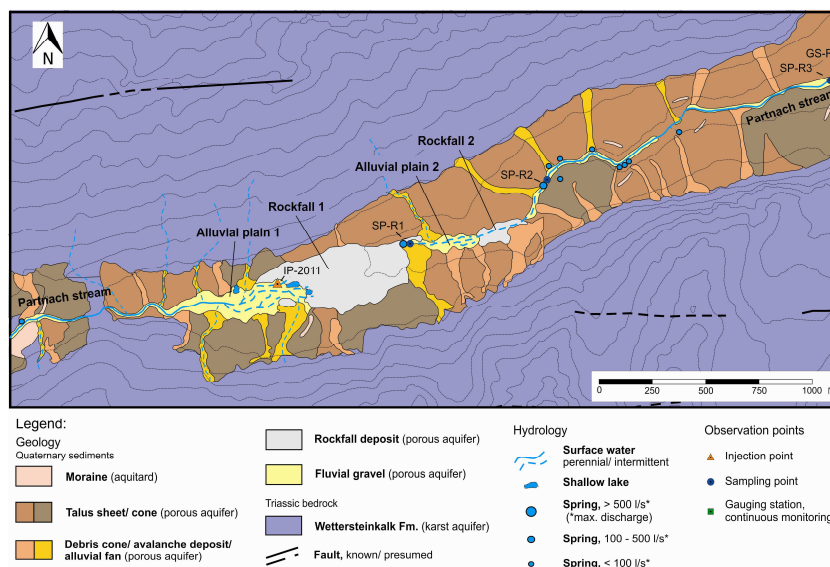
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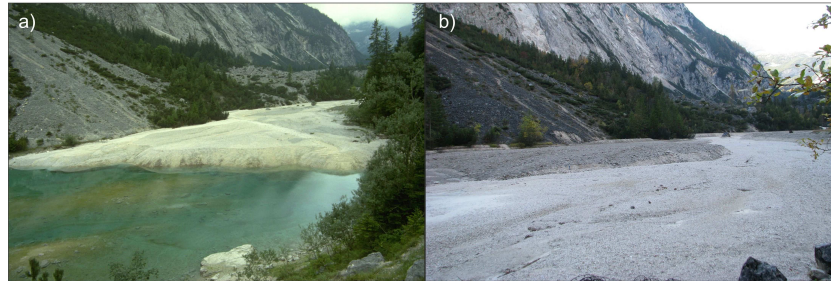
**Figure 1.** (a) Map of the study site (Wetterstein Mountains) in the German Alps; (b) Wetterstein Mountains, including Germany's highest summit (Mt. Zugspitze), the large Zugspitz cirque, and the high-alpine Reintal valley extending to the east. Tracer injections at the Zugspitz cirque (IP-2005) were conducted by Rappl et al. (2010); IP-2011 is part of this study. GS-RU and GS-RD are gauging stations in the Reintal valley, upstream (RU) and downstream (RD) from the alluvial/rockfall aquifers. The cross-section A–A' is provided in Fig. 4.

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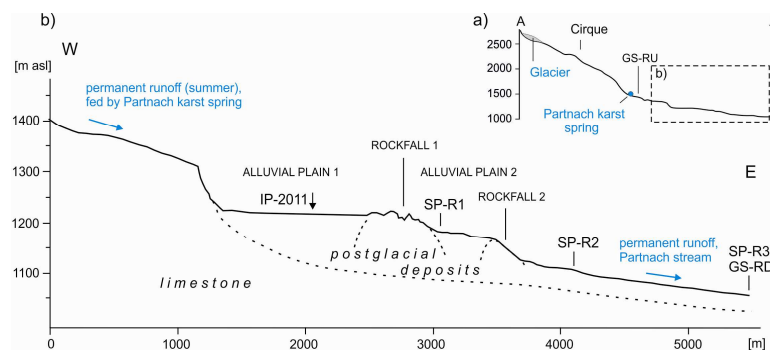
**Figure 2.** Hydrogeologic map of the Reintal valley covered with postglacial sediments, including alluvial plains and rockfall deposits (Schrott et al., 2006). The occurrence and location of surface streams and springs depends on hydrologic conditions. A longitudinal profile is provided in Fig. 4.

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**Figure 3.** View of the second alluvial plain: **(a)** an ephemeral mountain lake created by a natural rockfall dam; **(b)** the same area filled with sediment after a high precipitation event in 2005.

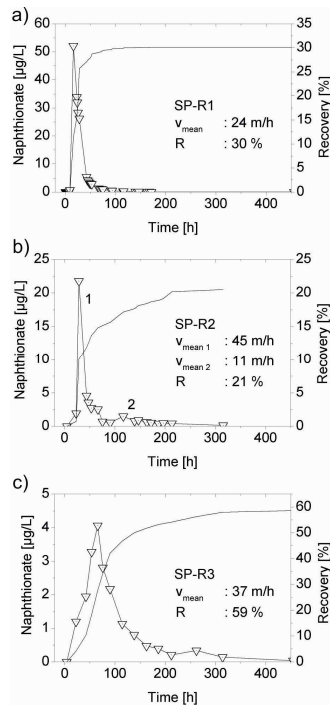
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**Figure 4.** **(a)** Overview over the Reintal valley indicating the major hydrologic inflow from the glacier and the karst spring. **(b)** Schematic diagram of the alluvial/rockfall aquifer system in the Reintal valley. Although perennial flow exists upstream and downstream, several sinks and springs between the alluvial/rockfall deposits result in intermittent discharge. Cross sections are vertically exaggerated.

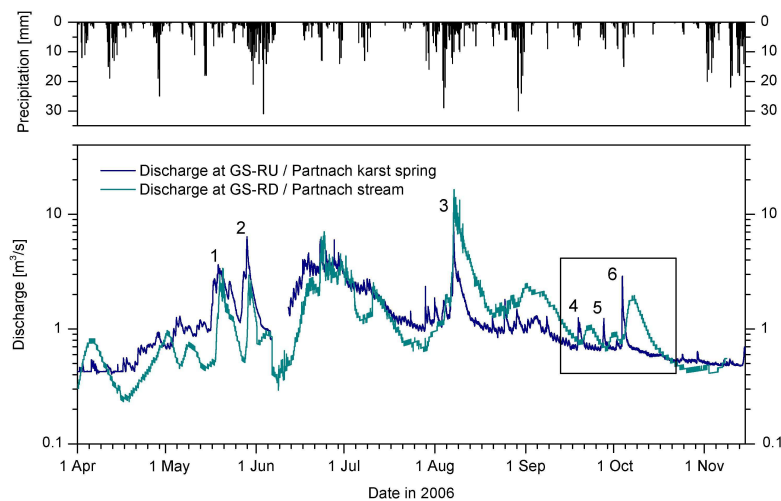
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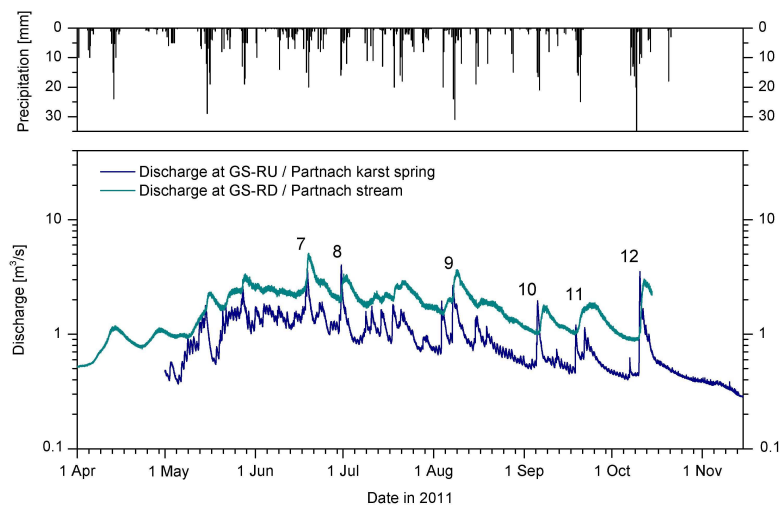
**Figure 7.** Naphthionate breakthrough curves at sampling points SP-R1 (a), SP-R2 (b) and SP-R3 (c) in the Reintal valley. Sampling points were located in the river bed and show dispersion of the tracer downstream the injection point. Total recovery was measured at the outlet of the system at SP-R3.

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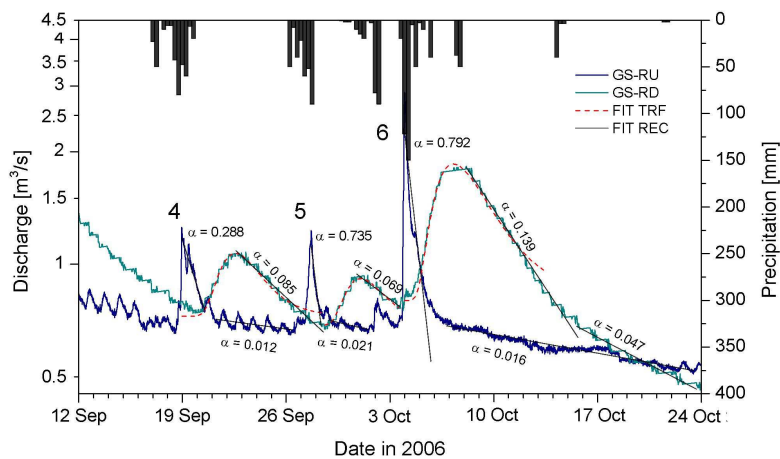
**Figure 8.** Hydrographs at the upstream (Partnach karst spring, site GS-RU) and downstream (Partnach stream, site GS-RD) gauging stations in the Reintal valley in 2006. Precipitation data (6 h time step) was obtained from the weather station at Mt. Zugspitze (DWD).

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**Figure 9.** Hydrographs at the upstream (Partnach karst spring, site GS-RU) and downstream (Partnach stream, site GS-RD) gauging stations in the Reintal valley in 2011. Precipitation data (6 h time step) was obtained from the weather station at Mt. Zugspitze (DWD).

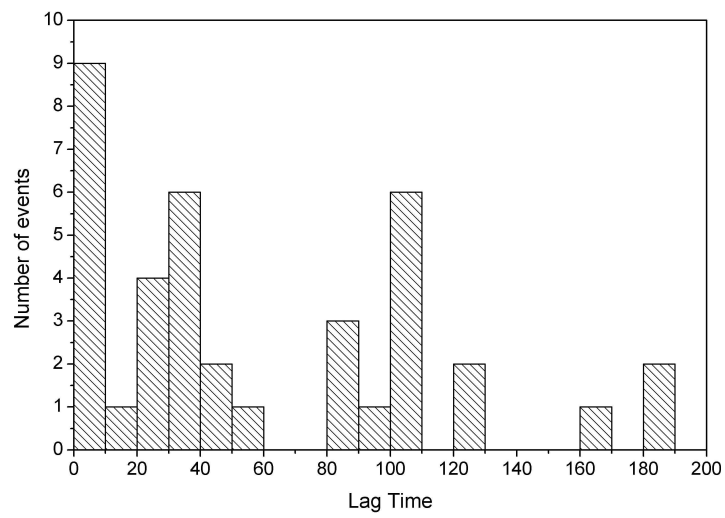
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**Figure 10.** Discharge characteristics in late summer and autumn of 2006 in the Reintal valley demonstrating dampening effects of the series of alpine alluvial/rockfall deposits (GS-RU: discharge from the karst spring upstream the alluvial/rockfall aquifer; GS-RD: discharge downstream at the outlet of the aquifer system; FIT-IRF: fit of impulse-response-function and FIT-REC: fit of recession analysis).

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**Figure 11.** Lag times between discharge peaks upstream (GS-RU) and downstream (GS-RD) from the alluvial/rockfall aquifer system, obtained from 38 discharge peaks during 2002–11.