

1 **Estimation of temporal and spatial variations in**  
2 **groundwater recharge in unconfined sand aquifers using**  
3 **Scots pine inventories**

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26 **Abstract**

27 Climate change and land use are rapidly changing the amount and temporal distribution of  
28 recharge in northern aquifers. This paper presents a novel method for distributing Monte Carlo  
29 simulations of 1-D sandy sediment profile spatially to estimate transient recharge in an  
30 unconfined esker aquifer. The modeling approach uses data-based estimates for the most  
31 important parameters controlling the total amount (canopy cover) and timing (thickness of the  
32 unsaturated zone) of groundwater recharge. Scots pine canopy was parameterized to leaf area  
33 index (LAI) using forestry inventory data. Uncertainty in the parameters controlling sediment  
34 hydraulic properties and evapotranspiration was carried over from the Monte Carlo runs to the  
35 final recharge estimates. Different mechanisms for lake, soil, and snow evaporation and  
36 transpiration were used in the model set-up. Finally, the model output was validated with  
37 independent recharge estimates using the water table fluctuation method and baseflow  
38 estimation. The results indicated that LAI is important in controlling total recharge amount.  
39 Soil evaporation compensated for transpiration for areas with low LAI values, which may be  
40 significant in optimal management of forestry and recharge. Different forest management  
41 scenarios tested with the model showed differences in annual recharge of up to 100 mm. The  
42 uncertainty in recharge estimates arising from the simulation parameters was lower than the  
43 interannual variation caused by climate conditions. It proved important to take unsaturated  
44 thickness and vegetation cover into account when estimating spatially and temporally  
45 distributed recharge in sandy unconfined aquifers.

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## 55 1 Introduction

56 Eskers are permeable, unconfined sand and gravel aquifers (Banerjee, 1975). In addition to  
57 water supply, they support groundwater-dependent ecosystems and provide recreational  
58 services (Kløve et al., 2011). Esker hydrology is important as eskers and other glaciofluvial  
59 aquifer types cover large areas of the North and are among the dominant aquifer types in the  
60 boreal zone. Management of these complex aquifers has gained recent attention (Bolduc et al.,  
61 2005, Karjalainen et al., 2013, Koundouri et al., 2012, Kurki et al., 2013). The European  
62 Groundwater Directive requires such systems to be characterized in order to determine their  
63 quality status, so knowledge of how to estimate groundwater recharge in esker aquifers is  
64 becoming increasingly important (EC, 2006). Esker aquifers are commonly covered with  
65 managed pine forests, where the forest canopy is likely to influence recharge amounts. The soil  
66 surface profile of eskers is complex and highly variable, consisting of kettle holes and sand  
67 dunes, resulting in variable thickness of the unsaturated zone (Aartolahti, 1973), a factor which  
68 also needs to be accounted for in recharge estimation.

69 Computational methods to estimate groundwater recharge vary from simple water balance  
70 models, where water stores and fluxes are represented conceptually and related with adjustable  
71 parameters (Jyrkama et al., 2002), to physically-based models using the Richards equation  
72 (Assefa and Woodbury, 2013, Okkonen and Kløve, 2011) to solve water fluxes through  
73 unsaturated zone. Computational methods solving the Richards equation are often limited to  
74 small-scale areal simulations (Scanlon et al., 2002a) and shallow unsaturated zones, and they  
75 commonly lack the soil freeze, thaw, and snow storage sub-routines relevant at higher northerly  
76 latitudes (Okkonen, 2011). However, computational approaches can be employed to produce  
77 the values on spatial and temporal variability in recharge often needed in groundwater modeling  
78 (Dripps and Bradbury, 2010). The methods commonly rely on a GIS platform for spatial  
79 representation and calculation approaches based on water balance to create the temporal  
80 dimension of recharge (Croteau et al., 2010, Dripps and Bradbury, 2007, Jyrkama et al., 2002,  
81 Sophocleous, 2000, Westenbroeck et al., 2010). Neglecting variations in thickness of the  
82 unsaturated zone is common practice in many water balance models used in recharge  
83 estimations. However, the residence time in the unsaturated zone may play an important role,  
84 especially in the timing of recharge in deep unsaturated zones (Hunt et al., 2008), as  
85 acknowledged in recent work (Assefa and Woodbury, 2013, Jyrkama and Sykes, 2007, Scibek  
86 and Allen, 2006, Smerdon et al., 2008).

87 In numerical recharge models, actual evapotranspiration (ET) is a difficult variable to estimate  
88 accurately from climate, soil, and land use data. The vegetation is commonly parameterized  
89 from land use or land cover maps (Assefa and Woodbury, 2013, Jyrkama et al., 2002, Jyrkama  
90 and Sykes, 2007, Keese et al., 2005), where the vegetation characteristics and leaf area index  
91 (LAI) are estimated based solely on vegetation type. In addition to tree canopy transpiration,  
92 soil evaporation, i.e. evaporation from the pores of soil matrix, can constitute a large proportion  
93 of total ET. Soil evaporation from the forest floor is generally reported to range from 3 to 40%  
94 of total ET (Kelliher et al., 1993), although values as high as 92% have been recorded (Kelliher  
95 et al., 1998). For conifer forest canopies, soil evaporation can largely compensate for low  
96 transpiration in areas with lower LAI (Ohta et al., 2001, Vesala et al., 2005). Data on canopy-  
97 scale evaporation rates at latitudes above 60°N are rare (Kelliher et al., 1993). A few studies  
98 have estimated ET from pine tree stands at patch scale (Kelliher et al., 1998, Lindroth, 1985),  
99 but none has extended this analysis to spatially distributed groundwater recharge. Forest  
100 management practices have the potential to affect the transpiration characteristics of coniferous  
101 forests, which typically leads to increased groundwater recharge (Bent, 2001, Lagergren et al.,  
102 2008, Rothacher, 1970).

103 The overall aim of the study was to provide novel information on groundwater recharge rates  
104 and factors contributing to the amount, timing, and uncertainty of groundwater recharge in  
105 unconfined sandy eskers aquifers. Study expands the application of physically-based 1-D  
106 unsaturated water flow modeling for groundwater recharge, while taking into account detailed  
107 information on vegetation (pine, lichen), unsaturated layer thickness, cold climate, and  
108 simulation parameter uncertainty. Furthermore, this study considers the effect that forestry land  
109 use has on vegetation parameters and how this is reflected in groundwater recharge.

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## 111 **2 Materials and Methods**

### 112 **2.1 Study site**

113 Groundwater recharge was estimated for the case of the Rokua esker aquifer in northern Finland  
114 (Fig. 1). Rokua is an unconfined aquifer consisting of unconsolidated sandy sediments  
115 underlain by crystalline bedrock (Fig. 2). Aquifer was formed during previous deglaciation  
116 when rivers under the melting ice sheet deposited sandy sediments in the river bed (Aartolahti  
117 1973). The Rokua esker has a rolling surface topography in the aquifer recharge area rising

118 about 60 m above the flat peatland areas surrounding the esker. In the groundwater discharge  
119 areas, the aquifer is locally confined by peat soil with low hydraulic conductivity (Rossi et al.  
120 2012).

121 The climate at the Rokua aquifer is characterized by precipitation exceeding evapotranspiration  
122 on an annual basis and statistics of the annual climate for the study period 1961 - 2010 in terms  
123 of precipitation, air temperature and FAO reference evapotranspiration according to Allen et al.  
124 (1998) is presented in Table 1. Another important feature of the climate is annually recurring  
125 winter periods when most precipitation is accumulated as snow.

### 126 2.1.1 Leaf area index from forestry inventories

127 Forestry inventory data from the Finnish Forest Administration (Metsähallitus, MH) and  
128 Finnish Forest Centre (Metsäkeskus, MK) were used to estimate LAI for the Rokua esker  
129 groundwater recharge area. The available data consisted of 2786 individual plots covering an  
130 area of 52.4 km<sup>2</sup> (62.4% of the model domain). The forestry inventories, performed mainly  
131 during 2000-2011, showed that Scots pine (*Pinus sylvestris*) is the dominant tree in the model  
132 area (94.2% of plots). The forest inventory data include a number of data attributes and the  
133 following data fields, included in both the MH and MK datasets, were used in the analysis:

- 134 - Plot area ( $p_A$ ); [ha]
- 135 - Main canopy type
- 136 - Average tree stand height ( $h$ ); [m]
- 137 - Average stand diameter at breast height ( $d_{bh}$ ); [cm]
- 138 - Number of stems ( $n_{stm}$ ); [ $1 \text{ ha}^{-1}$ ]
- 139 - Stand base area ( $b_A$ ); [ $\text{m}^2 \text{ ha}^{-1}$ ]
- 140 - Stand total volume ( $V$ ); [ $\text{m}^3$ ]

141 Inventory plots were excluded from the analysis if: (1) main canopy type was not pine forest,  
142 (2) data were missing for  $d_{bh}$  and  $h$  or  $n_{stm}$ , or (3) the MH and MK datasets overlapped, in which  
143 case MH was retained. However, several plots in the MH dataset were lacking  $n_{stm}$  data, which  
144 would have created a large gap in data coverage. Therefore the  $n_{stm}$  variable was estimated with  
145 a log-transformed regression equation using data on  $d_{bh}$ ,  $p_A$ , and  $V$  as independent variables.  
146 This regression equation was built from 280 plots ( $R^2 = 0.88$ ) and used to estimate  $n_{stm}$  for 288  
147 plots. LAI was estimated as described by Koivusalo et al. (2008). Needle mass for an average

148 tree in stand/plot was estimated from  $h$  and  $d_{bh}$  using empirical equations presented by Repola  
149 et al. (2007). LAI for a stand was calculated as:

$$150 \quad LAI = N_t * n_{stm} * S_{LA} \quad (1)$$

151 where  $N_t$  = needle mass per average tree in stand [kg],  $n_{stm}$  = number of stems per hectare  
152 [ $1 \text{ ha}^{-1}$ ], and  $S_{LA}$  = specific leaf area =  $4.43 \text{ m}^2 \text{ kg}^{-1} = 4.43 * 10^{-4} \text{ ha kg}^{-1}$  (Xiao et al., 2006).

153 Detailed information on LAI was used to obtain an estimate of how different forest management  
154 options, already actively in operation in the area, could potentially affect groundwater recharge.  
155 Three scenarios were simulated testing the potential impact of forestry operations on  
156 groundwater recharge:

- 157 1) The first “baseline” scenario simulated the current situation by using LAI pattern at  
158 the site (Fig. 3) estimated with Eq. (1).
- 159 2) The second scenario simulated the impact of intensive forestry operations as clear-  
160 cutting of the tree stand. Clear-cutting is an intensive land use form where almost the  
161 entire tree stand is removed, and it is carried out in some parts of the study area. Low  
162 LAI values of 0-0.2 for the whole study site were used in simulating this scenario.
- 163 3) The third scenario simulated the impact of no forestry operations, i.e. absence of  
164 forestry cuttings. The hypothetical mature stand covering the study site was assumed  
165 to have high LAI values of 3.2-3.5 found at the study site and reported in the literature  
166 (Koivusalo et al., 2008, Rautiainen et al., 2012, Vincke and Thiry, 2008, Wang et al.,  
167 2004).

### 168 2.1.2 Lichen water retention

169 An organic lichen layer covers much of the sandy soil at the Rokua study site (Kumpula et al.,  
170 2000), so this lichen layer was introduced in soil evaporation (SE) calculations. Although  
171 lichens do not transpire water, their structural properties allow water storage in the lichen matrix  
172 and capillary water uptake from the soil (Blum, 1973, Larson, 1979). In this study lichen layer  
173 was explicitly included in the simulations to create an additional storage for water before the  
174 mineral sandy sediments. Water interception storage by the lichen layer was estimated from  
175 lichen samples. In total, six samples (species *Cladonia stellaris* and *C. rangiferina*) were taken  
176 in May 2011 from two locations 500 m apart, close to borehole MEA506 (see Fig. 1). These  
177 samples were collected by pressing plastic cylinders (diameter 10.6 cm) through the lichen layer  
178 and extracting intact cores, after which mineral soil was carefully removed from the base of the

179 sample. Thus the final sample consisted of a lichen layer on top and a layer of organic litter and  
180 decomposed lichen at the bottom, and was sealed in a plastic bag for transportation. To obtain  
181 estimates of water retention capacity, the samples were first wetted until saturation with a  
182 sprinkler, left overnight at +4 °C to allow gravitational drainage and weighed to determine ‘field  
183 capacity’. The samples were then allowed to dry at room temperature and weighed daily until  
184 stable final weight (‘dry weight’) was reached. The water retention capacity ( $w_r$ ) of the sample  
185 was calculated as:

$$186 \quad w_r = \frac{m_{fc} - m_{dry}}{\rho_w} \cdot \frac{1}{\pi \cdot r^2} \quad (2)$$

187 where  $m_{fc}$  is the field capacity weight [M],  $m_{dry}$  is the final dry weight [M] at room temperature,  
188  $\rho_w$  [M L<sup>-3</sup>] is the density of water, and  $r$  [L] is the radius of the sampling cylinder.

189 The mean water retention capacity of the lichen samples was found to be 9.85 mm (standard  
190 deviation (SD) 2.71 mm) and approximations for these values were used in model  
191 parameterization (Table 2). Measured lichen water retention capacity was introduced to the  
192 simulations using parameters for soil porosity and layer thickness. Lichen porosity values were  
193 varied between 7.5 - 12.5 % in simulation Monte Carlo runs (see section 2.2.1) while keeping  
194 thickness of the lichen layer at 100 mm. In this manner the maximum amount of water retained  
195 by the lichen layer after gravitational drainage was adjusted to vary between 7.5 mm - 12.5 mm,  
196 as seen in the measurement data. To acknowledge the lack of information about B&C parameter  
197 estimates for lichen, the parameters were included in the simulations Monte Carlo runs with  
198 ranges which in our opinion produced reasonable shape of the pressure-saturation curve  
199 allowing easy drainage of the lichen.

### 200 2.1.3 Sandy sediment hydraulic properties

201 Sediment texture was determined by sieving (ISO 3310-1 standard sieve, US sieve numbers 5,  
202 10, 18, 35, 60, 120, and 230) 26 samples taken from five boreholes at various depths (Fig. 1).  
203 14 of the samples were analyzed also for pressure saturation curves. Samples were characterized  
204 as fine or medium sand, while sediment texture in the other boreholes (Fig. 1) had previously  
205 been characterized as medium, fine or silty sand throughout the model domain by the Finnish  
206 Environmental Administration as expert *in-situ* analysis during borehole drilling. Therefore the  
207 sediment samples from the five boreholes were considered to be representative of the sediment  
208 type in the area. Pressure saturation data from the samples was then used to define parameter  
209 ranges for the Brooks and Corey equation used in the simulations (Table 2). Furthermore,

210 texture values were employed to calculate the range of saturated vertical hydraulic conductivity  
211 for the samples, using empirical equations by Hazen, Kozeny-Carman, Breyer, Slitcher, and  
212 Terzaghi (Odong, 2007). The hydraulic conductivity for a given sample ranged approximately  
213 one order of magnitude between the equations. When using the five equations for the 26  
214 samples in total, the calculated values were within  $1.99 \cdot 10^{-5} - 1.47 \cdot 10^{-3} \text{ [m s}^{-1}\text{]}$  for all but one  
215 sample. The obtained range was considered to reasonably represent the hydraulic conductivity  
216 variability in the study area and simulations.

#### 217 2.1.4 Climate data

218 Driving climate data for the model were taken from Finnish Meteorological Institute databases  
219 for the modeling period 1 Jan 1961-31 Oct 2010. Daily mean temperature [ $^{\circ}\text{C}$ ] and sum of  
220 precipitation [mm] were recorded at Pelso climate station, 6 km south of the study area (Fig.  
221 1). The most representative long-term global radiation data [ $\text{kJ m}^{-2} \text{ d}^{-1}$ ] for the area were  
222 available as interpolated values in a 10 x 10 km grid covering the whole of Finland. The  
223 interpolation data point was found to be at approximately the same location as borehole  
224 MEA2110 (Fig. 1). Long-term data on wind speed [ $\text{m s}^{-1}$ ] and relative humidity [%] were taken  
225 from Oulunsalo and Kajaani airports, located 60 and 40 km from the study site, respectively.  
226 The data from the airports were instantaneous observations at three-hour intervals, from which  
227 daily mean values were calculated. All the climate variables were recorded at reference height  
228 2 m except for wind speed, which was measured at 10 m height. The wind speed data were  
229 therefore recalculated to correspond to 2 m measurement height according Allen et al. (1998)  
230 by multiplying daily average wind speed by 0.748. The suitability of long-term climate data for  
231 the study site conditions was verified with observations made at a climate station established at  
232 the study site in an overlapping time period (Dec 2009-Oct 2010) and the agreement between  
233 the measurements was found to be satisfactory.

234 Data on long-term lake surface water temperature were needed to calculate lake evaporation  
235 (see section 2.2.3), but were not available directly at the study site. However, surface water  
236 temperature was recorded at Lake Oulujärvi by the Finnish environmental administration  
237 (2013) 22 km from the study site in the direction of the Kajaani climate station (Fig. 1). The  
238 Oulujärvi water temperature was found to be closely correlated (linear correlation coefficient  
239 0.97) with daily lake water temperature recorded at Rokua during summer 2012. Daily lake  
240 surface temperature data for Lake Oulujärvi starting from 21 July 1970 were used in lake  
241 evaporation modeling. However, the data series had missing values for early spring and some



242 gaps during five years in the observation period. These missing values were estimated with a  
243 sine function, corresponding to the average annual lake temperature cycle, and a daily time  
244 series was established for subsequent calculations.

245 Snowmelt was calculated with a degree-day approach model in Jansson and Karlberg (2004).  
246 Snow routines were calibrated separately using bi-weekly snow water equivalent (SWE) data  
247 from Vaala snowline measurements (Finnish environment administration, 2011) for the period  
248 1960-2010 (Fig. 1). This separately calibrated snow model was used for all subsequent  
249 simulations.

## 250 **2.2 Recharge modeling framework**

### 251 **2.2.1 Water flow simulation in 1-D unsaturated sediment profile**

252 Water flow through an unsaturated one-dimensional (1-D) sandy sediment profile (Fig. 2) was  
253 estimated with the Richards equation using CoupModel (Jansson and Karlberg, 2004).  
254 CoupModel was selected as the simulation code because of its ability to represent the full soil-  
255 plant-atmosphere continuum adequately and to include snow processes in the simulations  
256 (Okkonen and Kløve, 2011). The simulated sediment profile was vertically discretized into 61  
257 layers with increasing layer thickness deeper in the profile. Layer thickness was 0.1 m for the  
258 first 16 layers (until 1.6 m), where the topmost 0.1 m was represented as a lichen layer. Layer  
259 thickness was progressively increased by defining 0.2 m thickness for the next 7 layers  
260 (between 1.6 and 3 m), 0.5 m for the next 14 layers (between 3 and 10 m), 1 m for the next 7  
261 layers (between 10 and 17 m) and 2 m for last 17 layers ranging from 17 m to the bottom of the  
262 profile (51 m).

263 The time variable boundary condition for water flow at the top of the column was defined by  
264 driving climate variables and affected by sub-routines accounting for snow processes with daily  
265 time step. The short time step was chosen to fully capture the main recharge input from  
266 snowmelt. All water at the top of the domain was assumed to be subjected to infiltration. Deep  
267 percolation as gravitational drainage was allowed from sediment column base using the unit-  
268 gradient boundary condition (see e.g. Scanlon et al., 2002b). Simulations for the unsaturated 1-  
269 D sediment profile were made for the period 1970-2010, and before each run 10 years of data  
270 (1960-1970) were used to spin up the model.

271 The simulation of the 1-D sediment profile was performed 400 times as Monte Carlo runs to  
272 facilitate the propagation of model parameter uncertainty in the final model output. Model was  
273 ran each time with different parameter values as specified in Table 2. For each individual  
274 simulation homogeneity in the vertical direction in terms of sediment hydraulic properties was  
275 assumed. The parameters for which values were randomly varied were chosen beforehand by  
276 trial and error model runs exploring the sensitivity of parameters with respect to cumulative  
277 recharge or evapotranspiration. The parameter ranges were specified from field data when  
278 possible; otherwise we resorted to literature estimates or in some cases used  $\pm 50\%$  of the  
279 CoupModel default providing a typical parameter for the used equation.

280 The sensitivity of the parameters varied in the simulations was tested with Kendall correlation  
281 analysis, by testing the correlation between each model parameter and cumulative sums of  
282 different evapotranspiration components and infiltration for the 400 model runs. Individual  
283 simulation with unique parameter values did not produce a groundwater recharge value due to  
284 the assembling strategy for recharge; therefore the ET components and infiltration were selected  
285 as variables for comparison. In addition, correlations were examined as scatter plots to ensure  
286 that possible sensitivity not captured by the monotonic correlation coefficient was not  
287 overlooked.

### 288 2.2.2 Method to distribute 1-D simulations spatially

289 Groundwater recharge was estimated for a model domain of 82.3 km<sup>2</sup> (Fig. 1). To distribute the  
290 simulations in 1-D sediment column spatially, the simulation domain was subdivided into  
291 different recharge zones, similarly to e.g. Jyrkämä et al. (2002). Zonation in the model was  
292 based on two variables: LAI and unsaturated zone thickness (UZT). The calculation of spatially  
293 distributed values for LAI and UZT is presented in detail in sections 2.1.1 and 2.1.4. Both  
294 variables were presented as a grid maps with 20m x 20m cell size with a floating point number  
295 assigned to each cell, resulting in a total of 205 708 cells for the model domain. The small  
296 model cell size was selected to ensure full exploitation of the forest inventory plots in LAI  
297 determination. The spatially distributed data were then divided into 15 classes for LAI and 30  
298 classes for UZT. The classes are primarily equal intervals, which was convenient in the  
299 subsequent data processing, but in addition the frequency distributions of LAI and UZT cell  
300 values were used to assign narrower classes for parameter ranges with many values (see  
301 histograms in Figs. 3 and 4). Class interval for LAI was 0.2 units up to a value of 2 (class 1:  
302 LAI = 0-0.2, etc.) and 0.3 to the maximum LAI value of 3.5. Class interval for UZT was 1 m

303 to 10 m depth and 2 m to the final depth of 51 m. Finally, the classified LAI and UZT data were  
 304 combined to a raster map with 20m x 20m cell size, producing 449 different zones with unique  
 305 combinations of LAI and UZT values. Spatial coupling was done with the ArcGIS software  
 306 (ESRI, 2011).

307 Variation in the LAI and UZD parameters were used to allocate the 1-D sediment profile  
 308 simulations spatially to the study site. LAI class in model cell specified a subset of the 400 1-  
 309 D simulations that were applicable for a given cell. UZT class for each cell (Fig. 2) specified  
 310 the depth in the simulated 51 m sediment profile where the water flux output was extracted.  
 311 Using this approach each unique recharge zone (a combination of UZT and LAI class) had on  
 312 average 27 water flow time series (number of total model runs [400] divided by number of LAI  
 313 cell classes [15]) produced by different random combinations of parameters (Table 2). Equation  
 314 (3) was used to propagate the variability in the 27 time series into the final areal recharge.

$$315 \quad R_{i,j} = \frac{\sum_{l=1}^{449} n(l) * R_{S_{i,rand(1:k)}} * A_c}{A_{tot}} \quad (3)$$

316 where  $R_{i,j}$  is the final sample of areal recharge [ $\text{mm day}^{-1}$ ],  $i$  is the index for simulation time  
 317 step ( $= 1:14975$ ),  $j$  is the index for sample for a given time step ( $1:150$ ),  $l$  is the index for unique  
 318 recharge zone,  $n(l)$  is the number of cells in a given recharge zone,  $R_s$  is the recharge sample  
 319 [ $\text{mm/day}$ ] for a given recharge zone at time step  $I$ ,  $k$  is the number of time series for a given  
 320 recharge zone,  $A_c$  is the surface area of a model raster cell ( $=20 \text{ m} * 20 \text{ m} = 400 \text{ m}^2$ ), and  $A_{tot}$   
 321 is the surface area of the total recharge area.

322 The resulting R matrix has 150 time series for areal recharge produced by simulations with  
 323 different parameter realizations. The variability between the time series provides an indication  
 324 of how much the simulated recharge varies due to different model parameter values. The  
 325 method allows computationally efficient recharge simulations, because the different recharge  
 326 zones do not all have to be simulated separately.

327 The simulation approach assumes that: (1) over the long-term, the water table remains at a  
 328 constant level, i.e. the unsaturated thickness for each model cells stays the same. Monitoring  
 329 data from 11 boreholes and seven lakes with more than 5 years of observation history shows  
 330 level variability of 1 – 1.5 m, with depressions and recoveries of the water table. This variability  
 331 is within the accuracy of water table estimation by interpolation. (2) the capillary fringe in the  
 332 sandy sediment is thin enough not to affect the water flow before arriving at the ‘imaginary’  
 333 water table at the center of each UZT class. (3) only vertical flow takes place in the unsaturated

334 sediment matrix, a typical assumption in recharge estimation techniques (Dripps and Bradbury,  
335 2010, Jyrkama et al., 2002, Scanlon et al., 2002a). (4) surface runoff is negligible primarily due  
336 to the permeable sediment type (as noted by Keese et al., 2005), and also due to lichen cover  
337 inhibiting runoff by increasing surface roughness (Rodríguez-Caballero et al., 2012). The  
338 maximum observed daily rainfall for the area has been 57.4 mm. Further assuming that rain for  
339 the day fell only during one hour, it would equal to  $1.59 \cdot 10^{-5} \text{ m s}^{-1}$  input rate of water, which  
340 is close to the lower range of saturated hydraulic conductivity at the study site ( $1.99 \cdot 10^{-5} \text{ m s}^{-1}$ ).  
341 Therefore rainstorms at the site very rarely exceed the theoretical infiltration capacity. As a  
342 field verification, surface runoff has not been observed during field visits and the area lacks  
343 intermittent or ephemeral stream networks.

### 344 2.2.3 Estimation of evapotranspiration

345 Four different evaporation processes were considered in this study (Fig. 5); soil evaporation  
346 (evaporation from the topmost soil layer, i.e. the lichen matrix), snow evaporation (evaporation  
347 from snow surface), transpiration (evaporation through the vascular system of tree canopy) and  
348 lake evaporation (evaporation from free water surface). The first three components were  
349 estimated, along with water flow simulations, using CoupModel. However, as 3.6 % ( $2.9 \text{ km}^2$ )  
350 of the surface area of the study site consists of lakes (Fig. 1), lake evaporation from free water  
351 surfaces was calculated independently from the CoupModel simulations.

352 Transpiration from the Scots pine canopy ( $L_v E_{tp}$ ) was calculated using Penman-Monteith (P-  
353 M) combination (Eq. A1). Whenever possible, all the parameters relating to the P-M equation  
354 were estimated based on data, namely LAI of the canopy. Surface resistance and saturation  
355 vapor pressure difference are the main factors controlling conifer forest evapotranspiration,  
356 while the aerodynamic resistance is of less importance (Lindroth, 1985, Ohta et al., 2001). In  
357 the calculation of aerodynamic resistance with the P-M equation, roughness length is related to  
358 LAI and canopy height, according to Shaw and Pereira (1982). Other parameters governing the  
359 aerodynamic resistance, except for LAI, were treated as constant. The surface resistance of the  
360 pine canopy was estimated with the Lohammar equation (see e.g. Lindroth, 1985), accounting  
361 for effects of solar radiation and air moisture deficit in tree canopy gas exchange. Because LAI  
362 values have a strong influence in the surface resistance Lohammar equation, the other  
363 parameters governing the surface resistance were excluded from the Monte Carlo runs.  
364 Distribution of root biomass with respect to depth from the soil surface was presented with an  
365 exponential function, because most Scots pine roots are concentrated in the shallow soil zone.

366 A typical root depth value of 1 m was used for the entire canopy (Kalliokoski, 2011, Kelliher  
367 et al., 1998, Vincke and Thiry, 2008). Soil and snow evaporation were calculated using an  
368 empirical approach (Eq. A4) based on the P-M equation, as described in detail in Jansson and  
369 Karlberg (2004). Soil evaporation is calculated for the snow-free fraction of the soil surface,  
370 and the snow evaporation is solved separately as a part of snow pack water balance.

371 In areas where the water table is close to the ground surface, the water table can provide an  
372 additional source of water for evapotranspiration (Smerdon et al., 2008). To take into account  
373 the decreased recharge for areas with near surface water tables, the recharge for cells with an  
374 unsaturated zone of <1 m (8.3% of the study site, 6.8 km<sup>2</sup>) was estimated with a water balance  
375 approach. We assumed that for areas with a shallow water table, soil water content was not a  
376 limiting factor for transpiration. Therefore an additional water source for transpiration was  
377 considered by making the transpiration rate equal to simulated potential transpiration (T) during  
378 times when the actual transpiration was simulated (T > 0.05 mm). Increasing effect of the water  
379 table located at 1 m depth on soil evaporation was tested with simulations and found to be 5-  
380 10% higher with than without a water table. Therefore a 7% addition was made to the simulated  
381 actual soil evaporation for cells with a shallow water table. Daily recharge ( $R_{1m}$ , L T<sup>-1</sup>) for cells  
382 with unsaturated thickness below 1 m was estimated as:

$$383 \quad R_{1m} = I - T_{adj} - ES_{adj} \quad (4)$$

384 where I is infiltration water arriving to lake/soil surface, including both meltwater from the  
385 snowpack and precipitation [L T<sup>-1</sup>],  $T_{adj}$  [mm d<sup>-1</sup>] is adjusted transpiration, and  $ES_{adj}$  [mm d<sup>-1</sup>]  
386 is adjusted soil evaporation. Kettle hole lakes in esker aquifers often lack surface water inlets  
387 and outlets and are therefore an integral part of the groundwater system (Ala-aho et al., 2013,  
388 Winter et al., 1998), so we considered these lakes as contributors to total groundwater recharge.  
389 In other words, rainfall per lake surface area is treated equally as addition to the aquifer water  
390 storage as groundwater recharge. As a difference, lake water table is subjected to evaporation  
391 unlike the groundwater table. Lake evaporation ( $E_{lake}$ ) was estimated with the mass transfer  
392 approach (see e.g. Dingman, 2008) according to Eq. (A7). The mass transfer method was  
393 selected because of its simplicity, daily output resolution, low data requirement, and physically-  
394 based approach. However various calculation methods could easily be used in the modelling  
395 framework, depending on the data availability (see e.g. Rosenberry et al., 2007). If lake  
396 percentage in the area of interest is high, more sophisticated methods may be required to better

397 represent the system. For the Rokua site the bias introduced by a simplistic approach was  
398 considered minor.

### 399 **2.3 Model validation**

400 Model performance was tested by comparing the simulated recharge values with two  
401 independent recharge estimates in local and regional scale; the water table fluctuation (WTF)  
402 method and base flow estimation, respectively. The WTF method is routinely used to estimate  
403 groundwater recharge because of its simplicity and ease of use. It assumes that any rise in water  
404 level in an unconfined aquifer is caused by recharge arriving at the water table. For a detailed  
405 description of the method and its limitations, see e.g. Healy and Cook (2002). The recharge  
406 amount ( $R$ ,  $L T^{-1}$ ) is calculated based on the water level prior to and after the recharge event  
407 and the specific yield of the sandy sediments:

$$408 \quad R = S_y \frac{\Delta h}{\Delta t} \quad (5)$$

409 where  $S_y$  is the specific yield,  $h$  is the water table height [L], and  $t$  is the time of water table rise  
410 [T].

411 The WTF method requires groundwater level data with adequate resolution for both time and  
412 water level, to identify periods of rising and falling water table. Water table was monitored  
413 using pressure-based dataloggers (Solinst Levellogger Gold) recording with hourly interval  
414 from six water table wells with average unsaturated zone thicknesses of 1.2, 1.6, 5.0, 8.0, 9.3,  
415 and 14.7 m (Fig. 1). Wells where the water table was  $<2$  m from the ground surface responded  
416 to major precipitation events. In the deeper wells, only the recharge from snowmelt was seen  
417 as water table rise. Estimates of the sandy sediment specific yield are required for the  
418 calculations (Eq. 5), but no sediment samples were available from the wells used in water table  
419 monitoring. Drilling records for these wells reported fine and medium sand, which was  
420 consistent with the particle size distribution for other wells in the area. Therefore an estimated  
421 value of 0.20-0.25 for the specific yield of all wells was used, according to typical values for  
422 fine and medium sand (Johnson, 1967).

423 The recharge estimated with the WTF method was compared with the simulated recharge  
424 during the recorded water level rise in the well. For each well, the cumulative sum of simulated  
425 water flow was extracted from sediment profile depth corresponding to well water table depth.  
426 As an example, the simulated recharge in well ROK1 (unsaturated thickness on average 14.7

427 m) was extracted from UTZ class 12, corresponding to recharge for unsaturated thickness of  
428 14-16 m. All 400 model runs were used, providing 400 estimates for recharge for each time  
429 period of recorded water level rise.

430 A regional estimate of groundwater recharge was estimated as baseflow of streams originating  
431 at the groundwater discharge area. Because the Rokua esker aquifer acts as a regional water  
432 divide, stream flow was monitored around the esker, in total of 18 locations (Fig. 1). The flows  
433 were measured total of 8 times between 6 July 2009 and 3 August 2010 (see Rossi et al., 2014).  
434 The lowest total outflow during 9-10 February 2010 was recorded after three months of snow  
435 cover period, when water contribution to streams from surface runoff was minimal. The  
436 minimum outflow was considered as baseflow from the aquifer reflecting long term  
437 groundwater recharge in the area.

438

### 439 **3 Results**

#### 440 **3.1 Model validation with the WTF and baseflow methods**

441 Model validation showed that the modeling approach could reasonably reproduce (1) the main  
442 groundwater recharge events when compared to the WTF method (Fig. 6) and (2) the regional  
443 level of recharge compared to stream baseflow. The WTF method agreed well with the  
444 simulated values, with overlapping estimates between the methods for all but two recharge  
445 events. Also the median value of simulations was close to WTF method, with some bias to  
446 higher estimates from the simulations. The discrepancy can be due to very different assumptions  
447 behind the methods and uncertainty in local parameterization; in the WTF method for the  
448 specific yield ( $S_y$ ) and for simulations mainly the hydraulic conductivity which dictates the  
449 simulated timing of recharge. Uncertainty in the  $S_y$  estimate is acknowledged by showing  $S_y$  a  
450 range rather than a single value (Fig. 6), but still  $S_y$  is not truly known for the location of  
451 observation boreholes. Simplifying assumptions and subjective interpretation of both timing  
452 and height of water table rise create additional inaccuracies in the WTF estimate.

453 Independent regional estimate of recharge, stream baseflow, was  $70\ 500\ \text{m}^3\ \text{s}^{-1}$ , or  $312.7\ \text{mm}$   
454  $\text{a}^{-1}$  when related to the recharge area. The order of magnitude agreed with long term simulated  
455 average of  $362.8\ \text{mm}\ \text{a}^{-1}$ . Typical error in individual stream flow measurements is within 3-6 %  
456 of the measured value (Sauer and Meyer, 1992), which brings minor uncertainty in the baseflow  
457 value. The smaller value for stream baseflow compared to simulated long term average recharge

458 can be explained with conceptual understanding of site hydrogeology (Ala-aho et al., 2015,  
459 Ala-aho et al., 2013, Rossi et al., 2012, Rossi et al., 2014). Part of the recharged groundwater  
460 does not discharge to the small streams whose baseflow was measured, but flows underneath  
461 the stream catchments and seeps out to regional surface bodies (Lake Oulujärvi and River  
462 Oulujoki) further away from the recharge area (Fig. 2). Fully integrated surface-subsurface  
463 hydrological modeling study of the same site presented in Ala-aho et al. (2015) simulated an  
464 outflow of  $79 \text{ mm a}^{-1}$  to regional surface water bodies.

### 465 **3.2 Temporal variations in groundwater recharge**

466 When recharge simulation time series were summarized to annual values (1 Oct-30 Sept),  
467 recharge rates co-varied with annual infiltration with linear correlation coefficient of 0.89  
468 (Fig. 7) as expected based on previous work in humid climate and sandy aquifers (Keese et al.,  
469 2005, Lemmelä, 1990). Both annual recharge and infiltration displayed an increasing trend. The  
470 plot also showed the level of uncertainty in annual recharge values introduced by differences  
471 in model parameterization (black area). The difference between minimum and maximum value  
472 for simulated annual recharge was on average 23.0 mm. Thus the variability in recharge  
473 estimates was 6.3 % of mean annual recharge 362.8 mm.

474 According to the simulations, the *effective rainfall*, i.e. the percentage of corrected rainfall  
475 resulting in groundwater recharge annually, was on average 59.3%. This is in agreement with  
476 previous studies on unconfined esker aquifers at northerly latitudes, in which the proportion of  
477 annual precipitation percolating to recharge is reported to be 50-70% (71% by Zaitsoff (1984),  
478 54% by Lemmelä and Tattari (1986) and 56% by Lemmelä (1990)). The percentage of effective  
479 rainfall varied considerably, by almost 30 %-units, between different hydrological years, from  
480 44.8% in some years up to 73.1% in others.

### 481 **3.3 Influence of LAI on spatial variation of groundwater recharge**

482 The spatial distribution of groundwater recharge was mostly due to variations in LAI, but also  
483 influenced by distance to water table, and distribution of lakes (Fig. 8). Higher evaporation rates  
484 from lakes led to lower recharge in lakes (see red spots in Fig. 8). Similarly, high LAI led to  
485 high ET and resulted in low recharge in plots with high LAI. Other areas of low recharge,  
486 although not as obvious at the larger spatial scales shown in Fig. 8, were cells with a shallow



487 water table (section 2.2.2). The effect of high ET at locations with a shallow water table can  
488 best be seen in south-east parts of the aquifer.

489 Kendall correlation analysis of simulation parameters and annual average model outputs  
490 identified LAI as the most important parameter controlling evapotranspiration and infiltration  
491 (Table 3). Parameters related to sediment hydraulics and evaporation showed some sensitivity  
492 to simulation results, while the parameters for lichen vegetation were only slightly sensitive or  
493 insensitive to simulation output variables. The LAI parameter governed the level of evaporation  
494 for different ET components (Fig. 9). Evaporation from soil (and snow) compensated for mean  
495 annual ET for LAI values up to around 1.0, after which total ET increased as a function of LAI.  
496 The scenarios for low (0 ... 0.2) and high (3.2 ... 3.5) LAI changed the groundwater recharge  
497 rates compared to the current LAI distribution (in Fig. 7). In the high LAI scenario the annual  
498 recharge was on average 101.7 mm lower than in the low LAI scenario. These results suggest  
499 that management of the Scots pine canopy has a significant control on the total recharge rates  
500 in unconfined esker aquifers.

501 Average land surface ET components remained relatively constant between years, but the  
502 simulated ET displayed a wide spread between simulations (Fig. 10). Estimated annual  
503 evapotranspiration (mean 237.6 mm) was somewhat lower than previous regional estimates of  
504 total ET (300 mm; (Mustonen, 1986)). Lake evaporation rates were generally higher than  
505 evapotranspiration from the land surface (420.0 mm). The variation in simulated lake  
506 evaporation was considerably lower than that in ET, as a different approach was used to account  
507 for uncertainty in the simulations. Transpiration showed greater variation between simulations  
508 than soil evaporation and total land surface ET. On average, transpiration also comprised a  
509 slightly larger share of total evaporation than soil evaporation. Simulated snow evaporation was  
510 a small, yet not insignificant, component in the total ET.

#### 511 **4 Discussion**

512 The method used here to estimate LAI from forestry inventories introduces a new approach for  
513 incorporating large spatial coverage of detailed conifer canopy data into groundwater recharge  
514 estimations. LAI values reported for conifer forests in Nordic conditions similar to the study  
515 site are in the range 1-3, depending on canopy density and other attributes (Koivusalo et al.,  
516 2008, Rautiainen et al., 2012, Vincke and Thiry, 2008, Wang et al., 2004). The LAI values  
517 obtained for the study site (mean 1.25) were at the lower end of this range. Furthermore, the  
518 data showed a bimodal distribution, with many model cells with low LAI (< 0.4) lowering the

519 mean LAI. The low LAI values were expected because of active logging and clearcutting  
520 activities in the study area. Although the equations to estimate LAI are empirical in nature and  
521 based on simplified assumptions, the method can outline spatial differences in canopy structure.  
522 Wider use of this method in Finland is practically possible, as active forestry operations in  
523 Finland have yielded an extensive database on canopy coverage, which could be used in  
524 groundwater management. However, the LAI estimation method could be further validated with  
525 field measurements or Lidar techniques (Chasmer et al., 2012, Riaño et al., 2004).

526 Plant cover, represented as LAI, proved to be the most important model parameter important  
527 parameter controlling total ET, and thereby the amount of groundwater recharge (Table 3, Fig.  
528 9). The LAI parameter was included in the equations controlling both transpiration and soil  
529 evaporation, and therefore the sensitivity of the parameter is not surprising. While soil  
530 evaporation partly compensated for the lower transpiration with low LAI values, the total  
531 annual ET values progressively increased as a function of LAI (Fig. 9). Interestingly, the  
532 simulations suggested that ET remains constant at constant level in the LAI range 0-1,  
533 potentially due to the sparse canopy changing the aerodynamic resistance and partitioning of  
534 radiation limiting soil evaporation, while still not contributing much to transpiration in total ET.  
535 This implies that the maximum groundwater recharge for boreal Scots pine remains rather  
536 constant up to a threshold LAI value of around 1. This knowledge can be used when co-  
537 managing forest and groundwater resources in order to optimize both.

538 Importance of LAI has been reported in earlier studies estimating groundwater recharge  
539 (Dripps, 2012, Keese et al., 2005, Sophocleous, 2000), but here the vegetation was represented  
540 with more spatially detailed patterns and a field data-based approach for LAI. According to  
541 previous studies, average ET from boreal conifer forests is around  $2 \text{ mm d}^{-1}$  during the growing  
542 season (Kelliher et al., 1998), which is similar to our average value of  $1.6 \text{ mm d}^{-1}$  for the period  
543 1 May-31 Oct. Some earlier studies have claimed that the influence of LAI on total ET rates  
544 from boreal conifer canopies is minor (Kelliher et al., 1993, Ohta et al., 2001, Vesala et al.,  
545 2005), but our simulation results indicate that higher LAI values lead to higher total ET values.  
546 The simulations showed that variable intensity of forestry, from low canopy coverage (LAI =  
547 0-0.2) to dense coverage (LAI = 3.2-3.5) resulted in a difference of over 100 mm in annual  
548 recharge (Fig. 7). It can be argued that the scenarios are unrealistic, because high LAI values,  
549 covering the whole study site, may not be achieved even with a complete absence of forestry  
550 operations. Nevertheless, the result demonstrates a substantial impact of forestry operations on

551 esker aquifer groundwater resources. The lichen layer covering the soil surface was explicitly  
552 accounted for in the simulation set-up, which to our knowledge is a novel modification. Kelliher  
553 et al. (1998) concluded that precipitation intercepted by lichen was an important source of  
554 understorey evaporation, especially directly after rain events. In addition, Bello and Arama  
555 (1989) reported that lichen could intercept light rain showers completely and that only intense  
556 rain events caused drainage from lichen canopy to mineral soil. While the lichen layer might  
557 have an increasing effect on soil evaporation through ‘interception storage’, Fitzjarrald and  
558 Moore (1992) suggest that a lichen cover may in fact have an insulating influence on heat and  
559 vapor exchange between soil and atmosphere, therefore impeding evaporation from the mineral  
560 soil. In the present study, the lichen layer appeared to have minor influence on total evaporation,  
561 soil evaporation and infiltration, as these variables showed only little sensitivity to lichen B&C  
562 parameters (Table 3). However, the approach to represent lichen with B&C model needs to  
563 better examined, as water retention capacity of lichen layer was introduced to the simulations  
564 using the concept of total porosity, which is not strictly coherent with the B&C model.  
565 Nevertheless, the used approach successfully produced an additional dynamic interception  
566 storage of water in the correct range (generally 3-7 mm depending on random parameterization,  
567 data not shown). The performed laboratory measurement of lichen water retention should be  
568 supplemented with detailed analysis of lichen pressure-saturation curve and hydraulic  
569 conductivity to clarify the role of lichen in soil evaporation, and thereby groundwater recharge.

570 Stochastic variation of selected model parameters illustrated the uncertainties relating to  
571 numerical recharge estimation using the Richards equation in one dimension. The capability  
572 and robustness of the Richards equation to reproduce soil water content and water fluxes have  
573 been demonstrated extensively in various studies (Assefa and Woodbury, 2013, Scanlon et al.,  
574 2002b, Stähli et al., 1999, Wierenga et al., 1991). Therefore we considered that model  
575 calibration and validation with point observations of variables such as soil volumetric water  
576 content or soil temperature would not provide novel insights into water flow in unsaturated  
577 porous media. Instead, we incorporated the parameter uncertainty ranges, usually used in model  
578 calibration, to the final recharge simulation output. An important outcome was that the  
579 uncertainty in the model output caused by different model parameterizations was small in  
580 comparison with the interannual variation in recharge. The error caused by uncertainty in the  
581 model assumptions or driving climate data was not addressed in this study.

582 The sensitivity analysis focused on total cumulative values of fluxes and did not address the  
583 temporal variations in the variables. Sediment hydraulic parameters mainly influenced the  
584 timing of recharge through residence time in the unsaturated zone, not so much the total amount.  
585 Therefore the sediment hydraulic parameters showed only minor sensitivity, perhaps  
586 misleadingly. It should be noted that vertical heterogeneity in the unsaturated sediment profile  
587 hydraulic parameters can reduce the total recharge rates (Keese et al., 2005). However, vertical  
588 heterogeneities were ignored in this study not only to simplify the model, but also because the  
589 drilling logs showed only little variation in the area. Work of Wierenga et al. (1991) supports  
590 the simplification by showing that excluding moderate vertical heterogeneities does not  
591 significantly affect the performance of water flow simulations with the Richards equation.

592 Simulations acknowledged shallow water table contribution to evapotranspiration in an  
593 indirect, conceptual approach. Including a water table fixed at different depths in the sediment  
594 profile would have been possible in the CoupModel setup. Influence of water table fixed at 2  
595 m depth was tested and found to increase ET 3.5% for LAI values of 3, but for LAI values of  
596 0.5 and 1.5 the increase in ET was only trivial. We expect only minor increase in ET with deeper  
597 water table configuration (with the given sediment texture), and therefore argue that excluding  
598 water table results in only minimal overestimation of total recharge at the study site. It should  
599 be noted that upward water fluxes were not excluded from the water flow time series and  
600 negative fluxes were considered as “negative recharge” at any depth. The simplification is made  
601 that water available for upward fluxes comes only from the soil moisture storage, not from the  
602 water table.

603 According to the simulations, the percentage of precipitation forming groundwater recharge  
604 varied considerably between years, as also reported in previous studies on transient recharge  
605 (Assefa and Woodbury, 2013, Dripps and Bradbury, 2010). Even though annual recharge was  
606 correlated with annual precipitation, and therefore years with high precipitation resulted in  
607 higher absolute recharge (Fig. 7), the percentage of effective rainfall did not increase as a  
608 function of annual sum of precipitation. This is somewhat surprising, because the rather  
609 constant evaporation potential between years (Fig. 10) and high sediment hydraulic  
610 conductivity could be expected to result in a higher percentage of rainfall reaching the water  
611 table in rainy years. Some studies (Dripps and Bradbury, 2010, Okkonen and Kløve, 2010) have  
612 suggested that when the main annual water input arrives as snowmelt during the low  
613 evaporation season, it is likely to result in higher percentage recharge than in a year with little

614 snow storage and precipitation distributed evenly throughout summer and autumn, which may  
615 contribute to the variability in the effective rainfall coefficient. However, when the maximum  
616 annual SWE value was used as a proxy for annual snow storage, there was no evidence of snow  
617 amount explaining the interannual variability in the recharge coefficient. Other factors  
618 contributing to recharge coefficient variability may be related to soil moisture conditions prior  
619 to snowfall, or the intensity of summer precipitation events (Smerdon et al., 2008, Stähli et al.,  
620 1999).

621 The above-mentioned reasons make the concept of effective rainfall, which is currently  
622 routinely used to estimate groundwater recharge for groundwater management in e.g. Finland  
623 (Britschgi et al., 2009), susceptible to over- or under-estimation of actual annual recharge. This  
624 applies especially for aquifers with a thick unsaturated zone, where rainy years produce higher  
625 average recharge with some delay and for a longer duration (Zhou, 2009).

626

## 627 **5 Conclusions**

628 A physically-based approach to simulate groundwater recharge for sandy unconfined aquifers  
629 in cold climates was developed. The method accounts for the influence of vegetation,  
630 unsaturated zone thickness, presence of lakes, and uncertainty in simulation parameters in the  
631 recharge estimate. It is capable of producing spatially and temporally distributed groundwater  
632 recharge values with uncertainty margins, which are generally lacking in recharge estimates,  
633 despite understanding of uncertainty related to recharge estimates being potentially crucial for  
634 groundwater resource management. However, the parameter uncertainty defined for the study  
635 area was of minor significance compared with interannual variations in the recharge rates  
636 introduced by climate variations.

637 The simulations showed that Scots pine canopy, parameterized as leaf area index (LAI), was  
638 important in controlling the total amount of groundwater recharge. Forestry inventory databases  
639 were used to estimate and spatially allocate the LAI and the results showed that such inventories  
640 could be better utilized in groundwater resource management. Forest cuttings were  
641 demonstrated to increase groundwater recharge significantly. A sensitivity analysis on the  
642 parameters used showed that soil evaporation could compensate for low LAI-related  
643 transpiration up to a LAI value of approximately 1, which may be important in finding the  
644 optimal level for forest management in groundwater resource areas. The concept of effective  
645 rainfall gave inconsistent estimates of recharge in annual timescales, showing the importance

646 of using physically-based recharge estimation methods for sustainable groundwater recharge  
647 management.

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## 652 **Author contribution**

653 P. Ala-aho and P.M Rossi collected and analyzed the field data. P. Ala-aho designed the  
654 simulation set-up, performed the simulations and interpreted the results. P. Ala-aho prepared  
655 the manuscript with contributions from all co-authors.

656

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884 **Tables**885 **Table 1.** Characteristics of the study site annual climate.

VARIABLE	MEAN	STD
Precipitation [mm]	591	91
Air Temperature [°C]	-0.7	1.1
Reference ET [mm]	426	26

886

887 **Table 2.** Randomly varied parameters, related equations and parameter ranges included in the  
888 model runs. For full description of parameters and equations, see Jansson and Karlberg (2004).

Parameter	Part of the model affected	Range	Units	Source
LAI (leaf area index)	Transpiration	0 ... 3.5	-	Data, see section 2.1.1
h (canopy height)	Transpiration	5 ... 15	m	Data
$r_{lai}$ (increase in aerodynamic resistance with LAI)	Soil evaporation	25 ... 75	-	$\pm 50\%$ , estimate
$r_{\psi}$ (soil surface resistance control)	Soil evaporation	100...300	-	$\pm 50\%$ approximately to cover the surface resistance reported 150-1000 (Kelliher et al., 1998)
$\lambda_L$ (pore size distribution index)	Soil evaporation, lichen	0.4 ... 1	-	Estimate, to cover an easily drainable range of pressure-saturation curves
$\Psi_L$ (air entry)	Soil evaporation, lichen	1.5 ... 20	-	Estimate, to cover a easily drainable range of pressure-saturation curves
$\theta_L$ (porosity)	Soil evaporation, lichen	7.5...12.5	%	Data, lichen mean water retention $\pm SD$ from samples

$k_{mat,L}$ (matrix saturated hydraulic conductivity)	Soil evaporation, lichen	$5 \cdot 10^4 \dots 5 \cdot 10^7$	mm d <sup>-1</sup>	Estimate, high K values assumed
$t_{WD}$ (coefficient in the soil temperature response function)	Water uptake	10 ... 20	-	±50%, estimate
$\Psi_c$ (critical pressure head for water uptake reduction)	Water uptake	200...600	-	±50%, estimate
$k_{mat,S}$ (matrix saturated hydraulic conductivity)	Sediment profile	$1.707 \cdot 10^3 \dots 127.2 \cdot 10^3$	mm d <sup>-1</sup>	Data from sediment sample particle size analysis
$k_{minuc}$ (minimum unsaturated hydraulic conductivity)	Sediment profile	$1 \cdot 10^{-4} \dots 1 \cdot 10^{-1}$	mm d <sup>-1</sup>	Estimate $k_{mat} \cdot 1E-5$
$\lambda_s$ (pore size distribution index)	Sediment profile	0.4 ... 1	-	Range to cover measured pressure-saturation curves
$\Psi_s$ (air entry)	Sediment profile	20 ... 40	-	Range to cover measured pressure-saturation curves
$\theta_s$ (porosity)	Sediment profile	0.25...0.36	%	Range from soil samples
$\theta_r$ (residual water content)	Sediment profile	0.01...0.05	%	Range to cover measured pressure-saturation curves

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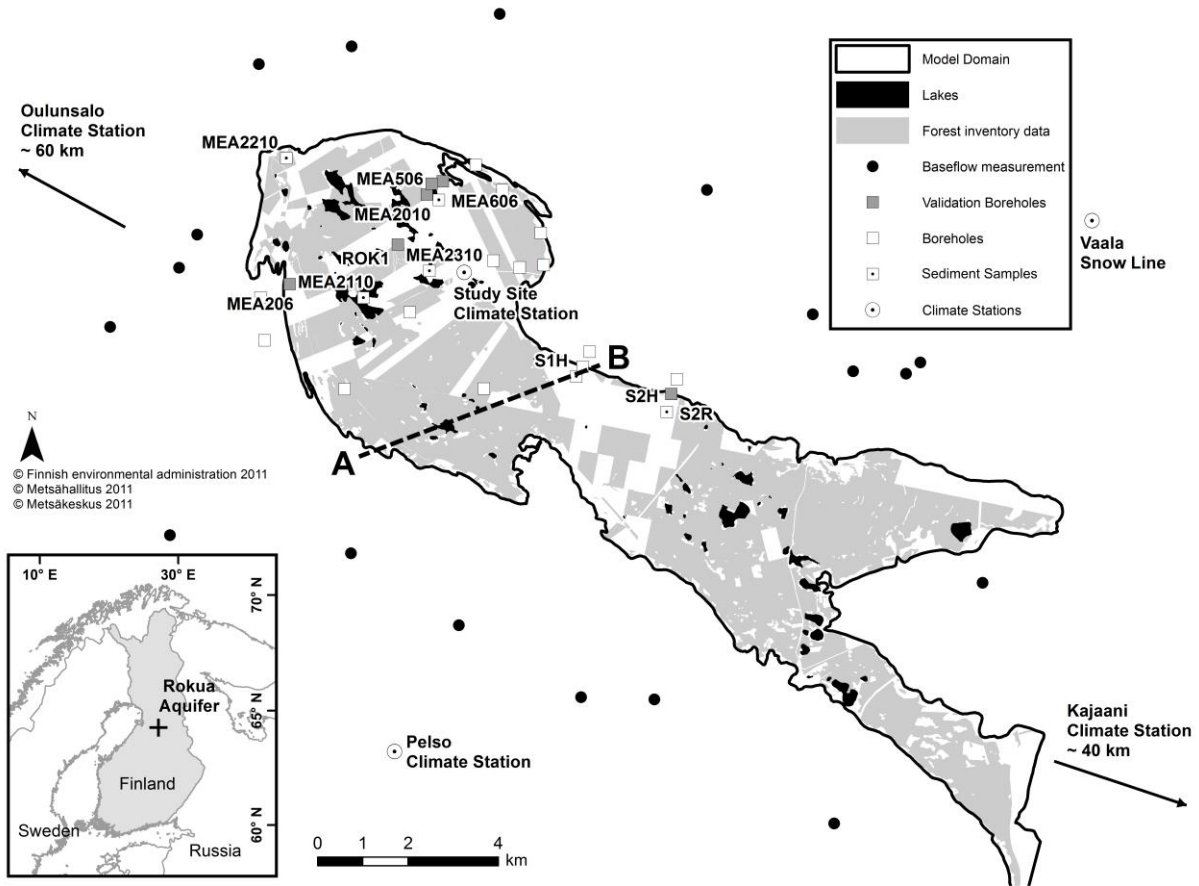
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897 **Table 3.** Kendall correlation coefficient for simulation parameters and average annual sum of  
 898 simulation output variables. ET = evapotranspiration, E = evaporation, for other symbols see  
 899 Table 2.

Parameter	Total ET	Transpiration	Soil E	Snow E	Infiltration
LAI	0.59*	0.84*	-0.73*	-0.37*	0.18*
h	0.59*	0.84*	-0.73*	-0.37*	0.18*
$r_{\Psi}$	-0.11*	-0.03	-0.03	-0.61*	0.58*
$r_{lai}$	-0.13*	-0.02	-0.11*	0.03	-0.05
$\lambda_L$	-0.09*	-0.01	-0.11*	0.01	-0.03
$\Psi_L$	0.01	-0.04	0.11*	-0.04	0.06
$\theta_L$	0.06	0.03	0.01	-0.00	0.09*
$k_{mat,L}$	-0.01	0.02	-0.04	-0.00	-0.00
$k_{mat,S}$	-0.10*	-0.04	-0.07*	0.02	0.01
$k_{minuc}$	-0.10*	-0.04	-0.07*	0.02	0.01
$t_{wD}$	-0.05	-0.02	-0.03	-0.05	0.03
$\Psi_c$	0.18*	0.12*	-0.02	-0.04	0.05
$\lambda_s$	0.13*	0.06	0.06	-0.00	-0.23*
$\Psi_s$	-0.11*	-0.05	-0.04	-0.05	0.04
$\theta_s$	0.02	-0.01	0.03	0.10*	-0.18*
$\theta_r$	0.07*	0.05	-0.01	0.01	0.16*

900 \*Significant correlation,  $p < 0.05$

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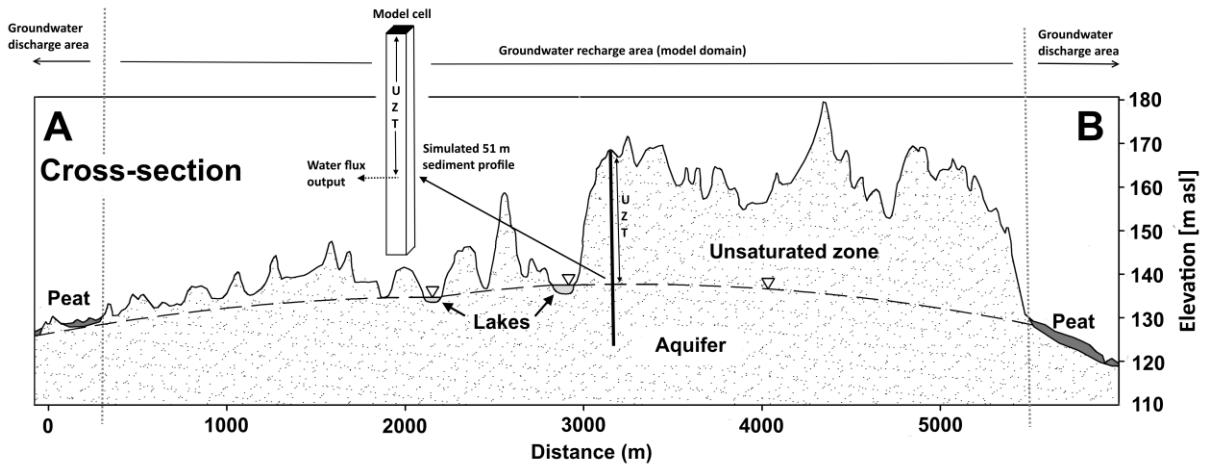
903  
904 **Figure 1.** Recharge area of the Rokua esker aquifer. Boreholes in the area were used for model  
905 validation and sediment type characterization. Baseflow was measured from streams  
906 originating outside the groundwater recharge area. Profile of cross-section A-B is presented in  
907 Fig. 2.

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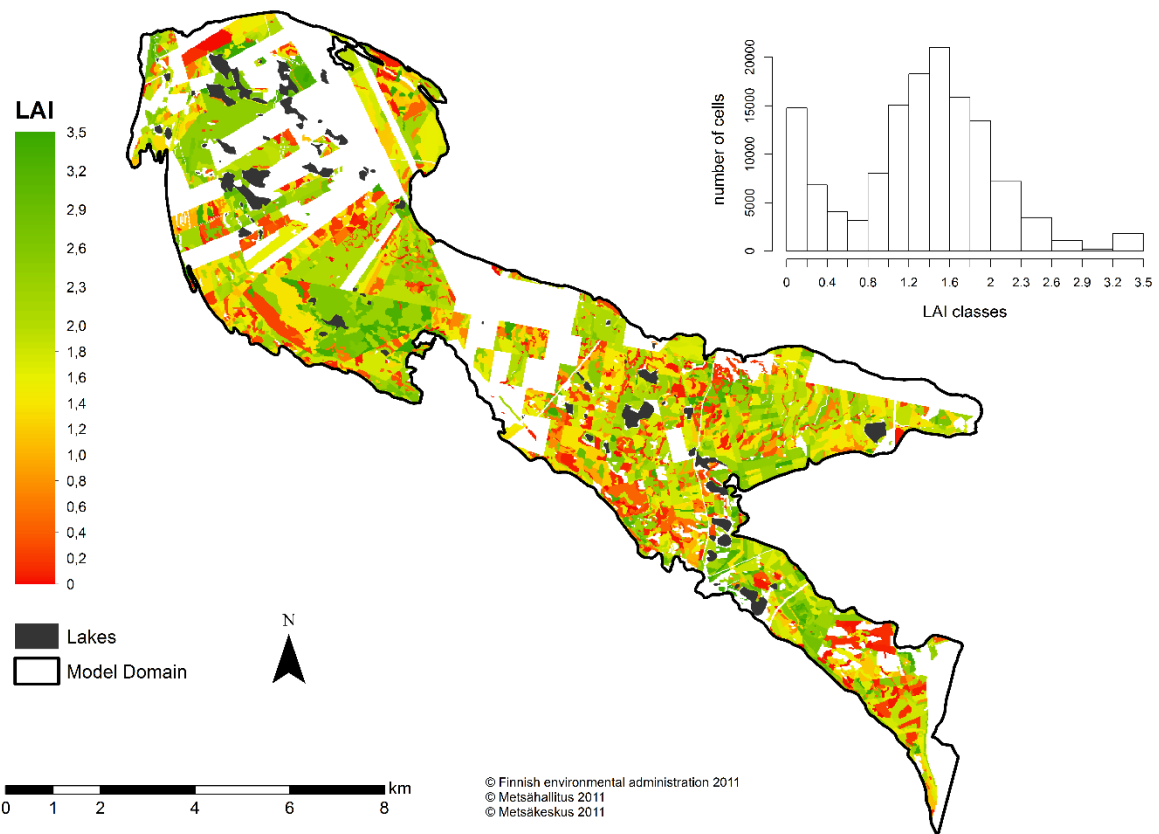
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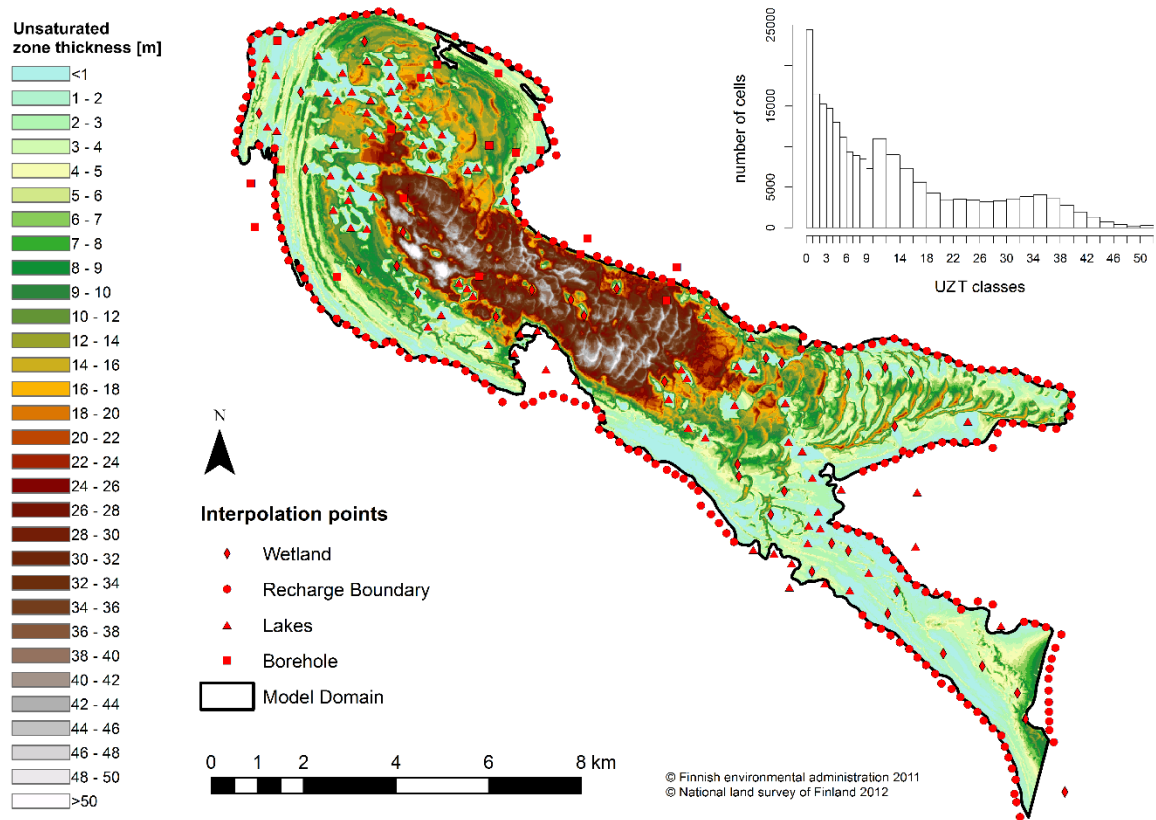
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912 **Figure 2.** Cross-section A-B (Fig. 1) to demonstrate the geometry of the unsaturated zone and  
 913 the aquifer (vertical axes exaggerated). A simulated sediment profile is shown to give an  
 914 example on how 1-D simulations are represented in the model domain, UZT represents the  
 915 unsaturated zone thickness parameter.



916

917 **Figure 3.** Spatial distribution of leaf area index (LAI) and a 20m x 20m cell-based histogram  
 918 of LAI values. In areas where forestry inventory data were lacking, a weighted average value  
 919 of 1.25 was used in simulations.

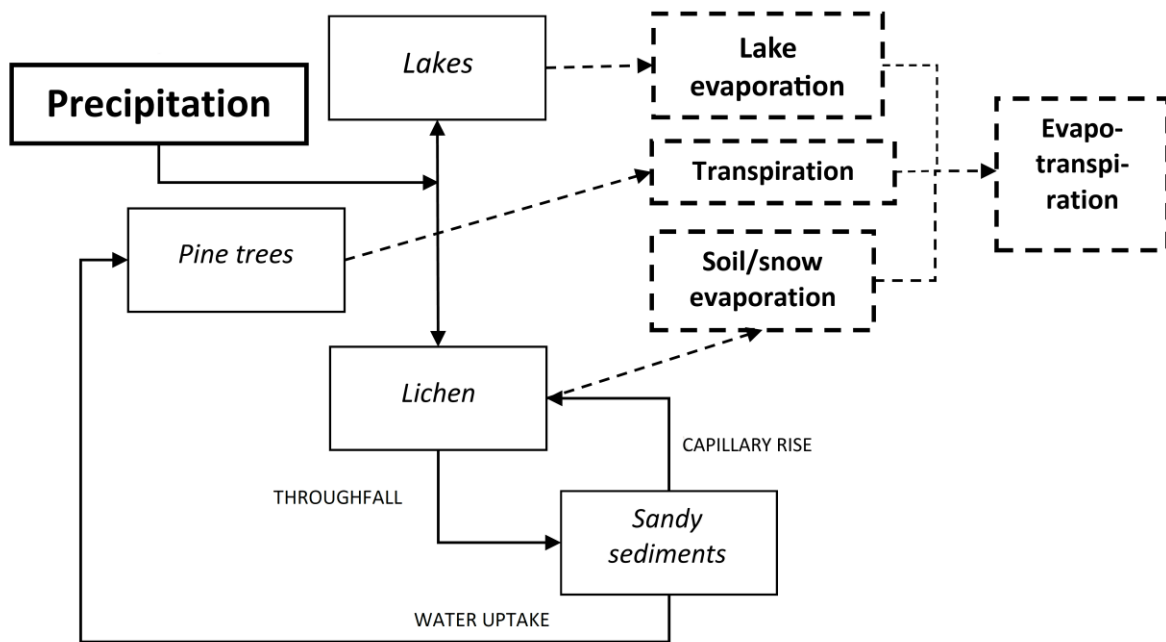


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921 **Figure 4.** Estimated thickness of the unsaturated zone in the model area and interpolation points  
 922 for estimation of water table elevation.

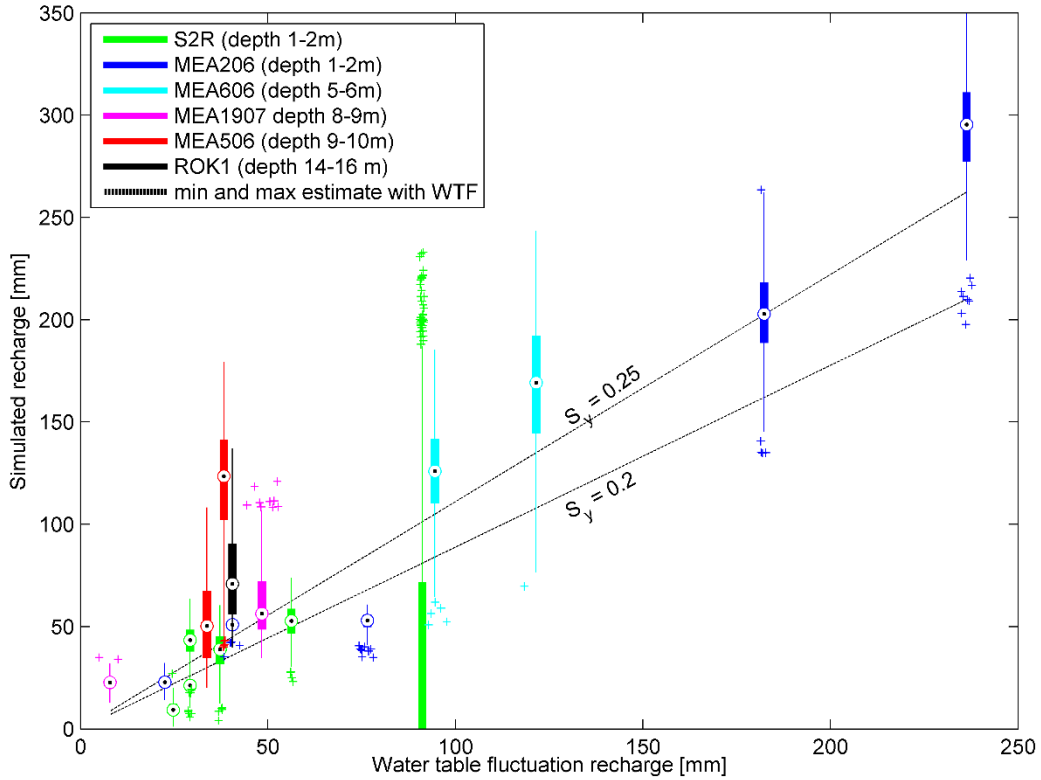
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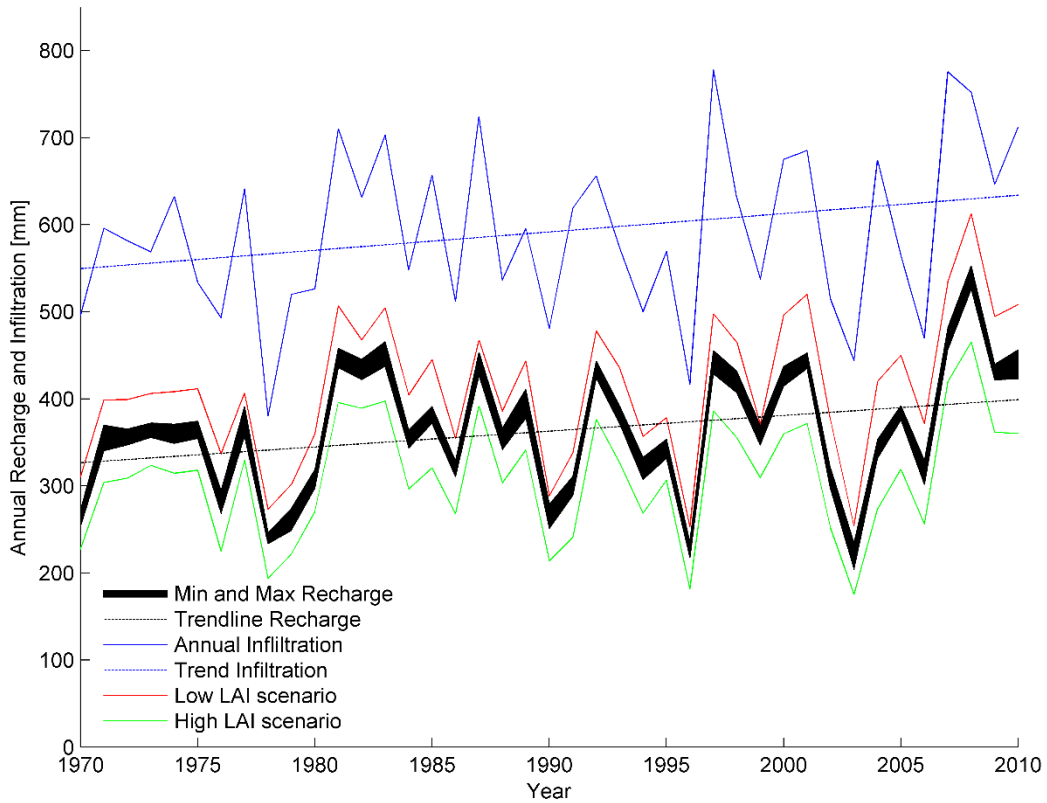
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926 **Figure 5.** Flow chart of different evaporation processes considered in the study. Total  
 927 evapotranspiration comprises of soil evaporation from the topmost soil layer, i.e. the lichen  
 928 matrix, snow evaporation from snow surface, transpiration through the vascular system of tree  
 929 canopy and lake evaporation from free water surface.



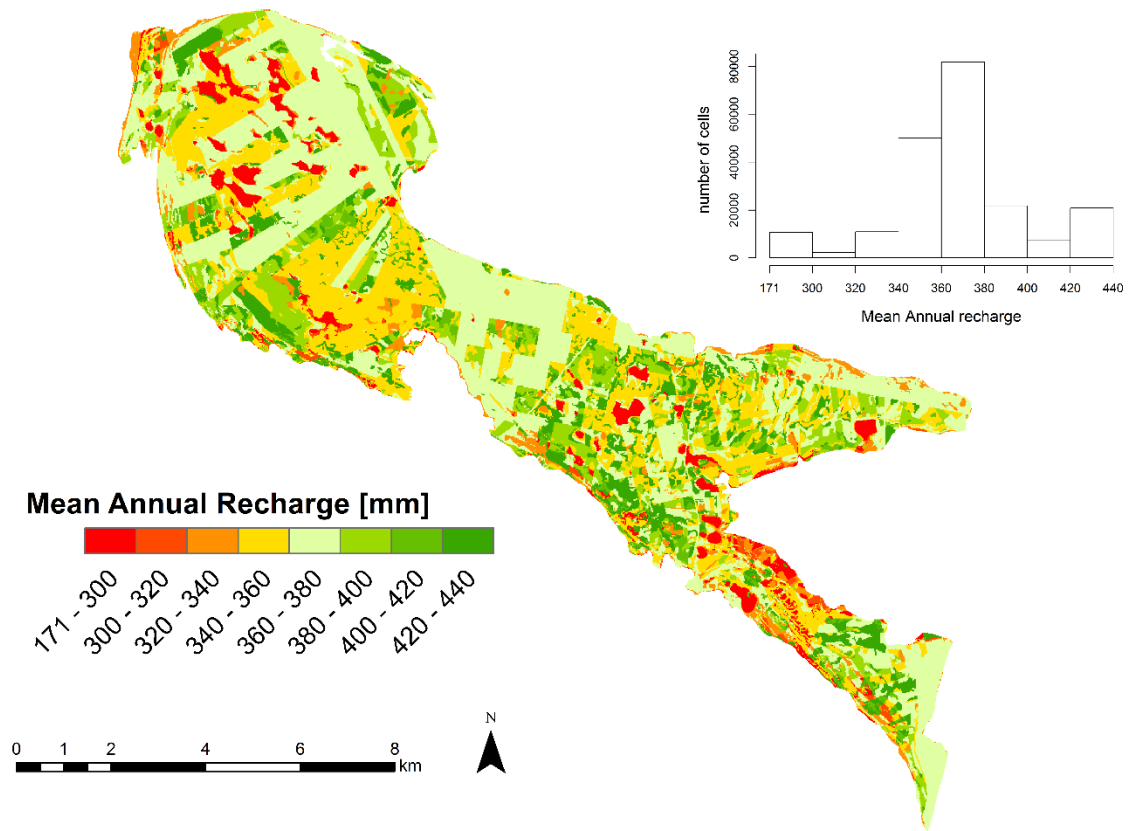
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931 **Figure 6.** Assemblage of simulated recharge for individual recharge events, shown as boxplots  
 932 where circles represent the median, bold lines 25-75<sup>th</sup> percentiles of the simulations, thin lines  
 933 the remaining upper and lower 25<sup>th</sup> percentiles and crosses are outliers. The location of the  
 934 boxplots on the x-axis is the WTF estimate for a given recharge event using a specific yield  
 935 value of 0.225. The dashed lines indicate the uncertainty in the WTF estimates caused by the  
 936 selection of specific yield. The two estimates would agree perfectly (given the uncertainty in  
 937  $S_y$ ) if all simulations shown as boxplots fell between the dashed lines.



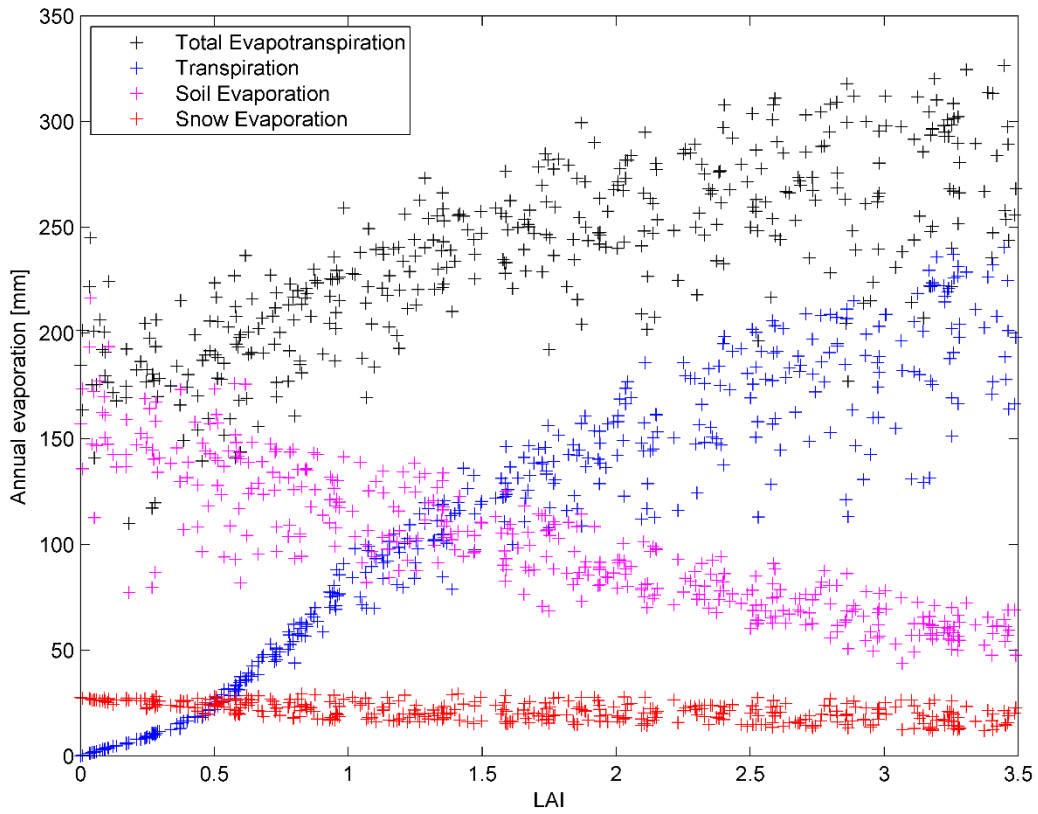
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939 **Figure 7.** Annual recharge time series from simulations where the black area covers the  
 940 minimum and maximum values for different recharge samples. The annual recharge pattern  
 941 closely followed trends in infiltration. Effects of different land use management practices over  
 942 time on annual recharge rates are shown as high and low leaf area index (LAI) scenarios.



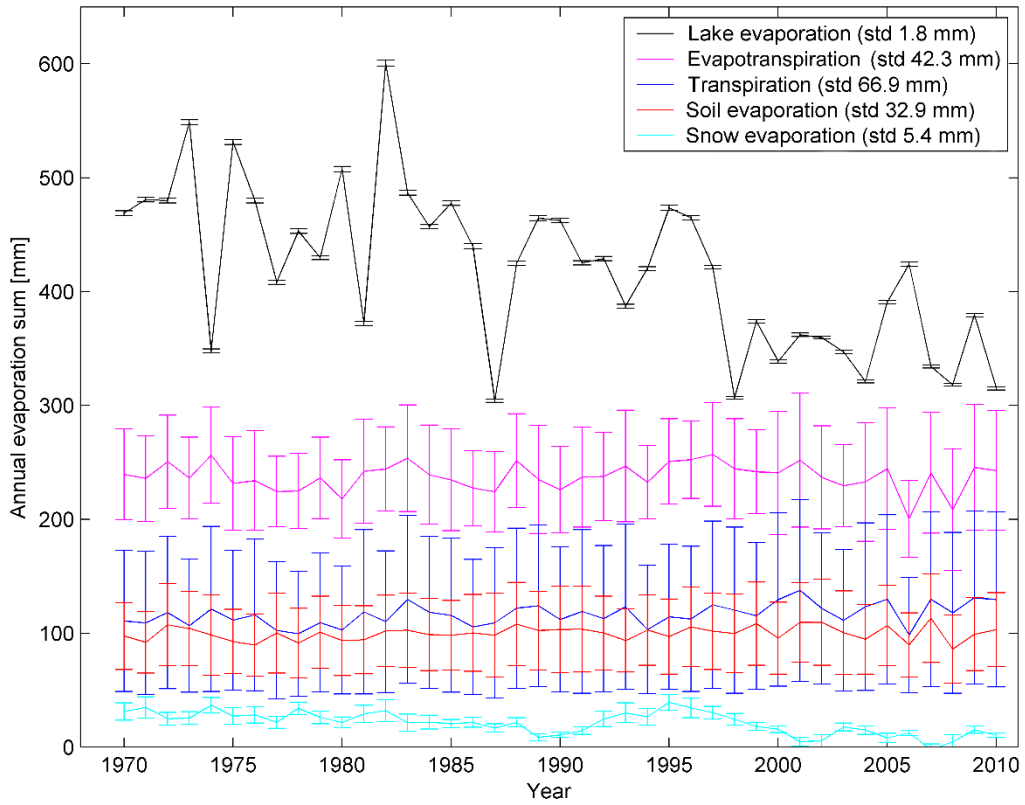
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944 **Figure 8.** Spatial distribution of mean annual recharge, which was influenced mainly by the  
 945 Scots pine canopy (LAI), the presence of lakes and, to some extent, areas with a shallow water  
 946 table.



947

948 **Figure 9.** Example of scatter plots with the mean annual ET components are plotted as a  
 949 function of the variable leaf area index (LAI), showing clear dependence of all ET components  
 950 on LAI.



951

952 **Figure 10.** Values of different evapotranspiration (ET) components (mean and standard  
 953 deviation) simulated for the study period.