1	Estimation of temporal and spatial variations in
2	groundwater recharge in unconfined sand aquifers using
3	Scots pine inventories
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#### 26 Abstract

27 Climate change and land use are rapidly changing the amount and temporal distribution of recharge in northern aquifers. This paper presents a novel method for distributing Monte Carlo 28 29 simulations of 1-D sandy sediment profile spatially to estimate transient recharge in an 30 unconfined esker aquifer. The modeling approach uses data-based estimates for the most 31 important parameters controlling the total amount (canopy cover) and timing (thickness of the 32 unsaturated zone) of groundwater recharge. Scots pine canopy was parameterized to leaf area 33 index (LAI) using forestry inventory data. Uncertainty in the parameters controlling sediment 34 hydraulic properties and evapotranspiration was carried over from the Monte Carlo runs to the final recharge estimates. Different mechanisms for lake, soil, and snow evaporation and 35 36 transpiration were used in the model set-up. Finally, the model output was validated with independent recharge estimates using the water table fluctuation method and baseflow 37 38 estimation. The results indicated that LAI is important in controlling total recharge amount. 39 Soil evaporation compensated for transpiration for areas with low LAI values, which may be 40 significant in optimal management of forestry and recharge. Different forest management 41 scenarios tested with the model showed differences in annual recharge of up to 100 mm. The 42 uncertainty in recharge estimates arising from the simulation parameters was lower than the interannual variation caused by climate conditions. It proved important to take unsaturated 43 44 thickness and vegetation cover into account when estimating spatially and temporally 45 distributed recharge in sandy unconfined aquifers.

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### 55 **1** Introduction

56 Eskers are permeable, unconfined sand and gravel aquifers (Banerjee, 1975). In addition to 57 water supply, they support groundwater-dependent ecosystems and provide recreational 58 services (Kløve et al., 2011). Esker hydrology is important as eskers and other glaciofluvial 59 aquifer types cover large areas of the North and are among the dominant aquifer types in the 60 boreal zone. Management of these complex aquifers has gained recent attention (Bolduc et al., 61 2005, Karjalainen et al., 2013, Koundouri et al., 2012, Kurki et al., 2013). The European 62 Groundwater Directive requires such systems to be characterized in order to determine their 63 quality status, so knowledge of how to estimate groundwater recharge in esker aquifers is becoming increasingly important (EC, 2006). Esker aquifers are commonly covered with 64 managed pine forests, where the forest canopy is likely to influence recharge amounts. The soil 65 surface profile of eskers is complex and highly variable, consisting of kettle holes and sand 66 dunes, resulting in variable thickness of the unsaturated zone (Aartolahti, 1973), a factor which 67 also needs to be accounted for in recharge estimation. 68

69 Computational methods to estimate groundwater recharge vary from simple water balance 70 models, where water stores and fluxes are represented conceptually and related with adjustable 71 parameters (Jyrkama et al., 2002), to physically-based models using the Richards equation 72 (Assefa and Woodbury, 2013, Okkonen and Kløve, 2011) to solve water fluxes through 73 unsaturated zone. Computational methods solving the Richards equation are often limited to 74 small-scale areal simulations (Scanlon et al., 2002a) and shallow unsaturated zones, and they commonly lack the soil freeze, thaw, and snow storage sub-routines relevant at higher northerly 75 76 latitudes (Okkonen, 2011). However, computational approaches can be employed to produce the values on spatial and temporal variability in recharge often needed in groundwater modeling 77 78 (Dripps and Bradbury, 2010). The methods commonly rely on a GIS platform for spatial representation and calculation approaches based on water balance to create the temporal 79 80 dimension of recharge (Croteau et al., 2010, Dripps and Bradbury, 2007, Jyrkama et al., 2002, Sophocleous, 2000, Westenbroeck et al., 2010). Neglecting variations in thickness of the 81 unsaturated zone is common practice in many water balance models used in recharge 82 estimations. However, the residence time in the unsaturated zone may play an important role, 83 especially in the timing of recharge in deep unsaturated zones (Hunt et al., 2008), as 84 85 acknowledged in recent work (Assefa and Woodbury, 2013, Jyrkama and Sykes, 2007, Scibek 86 and Allen, 2006, Smerdon et al., 2008).

87 In numerical recharge models, actual evapotranspiration (ET) is a difficult variable to estimate 88 accurately from climate, soil, and land use data. The vegetation is commonly parameterized 89 from land use or land cover maps (Assefa and Woodbury, 2013, Jyrkama et al., 2002, Jyrkama 90 and Sykes, 2007, Keese et al., 2005), where the vegetation characteristics and leaf area index 91 (LAI) are estimated based solely on vegetation type. In addition to tree canopy transpiration, 92 soil evaporation, i.e. evaporation from the pores of soil matrix, can constitute a large proportion 93 of total ET. Soil evaporation from the forest floor is generally reported to range from 3 to 40% 94 of total ET (Kelliher et al., 1993), although values as high as 92% have been recorded (Kelliher 95 et al., 1998). For conifer forest canopies, soil evaporation can largely compensate for low 96 transpiration in areas with lower LAI (Ohta et al., 2001, Vesala et al., 2005). Data on canopy-97 scale evaporation rates at latitudes above 60°N are rare (Kelliher et al., 1993). A few studies 98 have estimated ET from pine tree stands at patch scale (Kelliher et al., 1998, Lindroth, 1985), 99 but none has extended this analysis to spatially distributed groundwater recharge. Forest management practices have the potential to affect the transpiration characteristics of coniferous 100 101 forests, which typically leads to increased groundwater recharge (Bent, 2001, Lagergren et al., 102 2008, Rothacher, 1970).

The overall aim of the study was to provide novel information on groundwater recharge rates and factors contributing to the amount, timing, and uncertainty of groundwater recharge in unconfined sandy eskers aquifers. Study expands the application of physically-based 1-D unsaturated water flow modeling for groundwater recharge, while taking into account detailed information on vegetation (pine, lichen), unsaturated layer thickness, cold climate, and simulation parameter uncertainty. Furthermore, this study considers the effect that forestry land use has on vegetation parameters and how this is reflected in groundwater recharge.

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#### 111 **2** Materials and Methods

#### 112 **2.1** Study site

Groundwater recharge was estimated for the case of the Rokua esker aquifer in northern Finland (Fig. 1). Rokua is an unconfined aquifer consisting of unconsolidated sandy sediments underlain by chrystalline bedrock (Fig. 2). Aquifer was formed during previous deglaciation when rivers under the melting ice sheet deposited sandy sediments in the river bed (Aartolahti 1973). The Rokua esker has a rolling surface topography in the aquifer recharge area rising

- about 60 m above the flat peatland areas surrounding the esker. In the groundwater discharge
- areas, the aquifer is locally confined by peat soil with low hydraulic conductivity (Rossi et al.2012).
- The climate at the Rokua aquifer is characterized by precipitation exceeding evapotranspiration
  on an annual basis and statistics of the annual climate for the study period 1961 2010 in terms
  of precipitation, air temperature and FAO reference evapotranspiration according to Allen et al.
- 124 (1998) is presented in Table 1. Another important feature of the climate is annually recurring
- 125 winter periods when most precipitation is accumulated as snow.
- 126 2.1.1 Leaf area index from forestry inventories
- Forestry inventory data from the Finnish Forest Administration (Metsähallitus, MH) and Finnish Forest Centre (Metsäkeskus, MK) were used to estimate LAI for the Rokua esker groundwater recharge area. The available data consisted of 2786 individual plots covering an area of 52.4 km<sup>2</sup> (62.4% of the model domain). The forestry inventories, performed mainly during 2000-2011, showed that Scots pine (*Pinus sylvestris*) is the dominant tree in the model area (94.2% of plots). The forest inventory data include a number of data attributes and the following data fields, included in both the MH and MK datasets, were used in the analysis:
- 134 Plot area (p<sub>A</sub>); [ha]
- 135 Main canopy type
- 136 Average tree stand height (h); [m]
- 137 Average stand diameter at breast height (d<sub>bh</sub>); [cm]
- 138 Number of stems ( $n_{stm}$ ); [1 ha<sup>-1</sup>]
- 139 Stand base area ( $b_A$ );  $[m^2 ha^{-1}]$
- 140 Stand total volume (V); [m<sup>3</sup>]

Inventory plots were excluded from the analysis if: (1) main canopy type was not pine forest, (2) data were missing for  $d_{bh}$  and h or  $n_{stm}$ , or (3) the MH and MK datasets overlapped, in which case MH was retained. However, several plots in the MH dataset were lacking  $n_{stm}$  data, which would have created a large gap in data coverage. Therefore the  $n_{stm}$  variable was estimated with a log-transformed regression equation using data on  $d_{bh}$ ,  $p_A$ , and V as independent variables. This regression equation was built from 280 plots ( $R^2 = 0.88$ ) and used to estimate  $n_{stm}$  for 288 plots. LAI was estimated as described by Koivusalo et al. (2008). Needle mass for an average tree in stand/plot was estimated from h and d<sub>bh</sub> using empirical equations presented by Repola
et al. (2007). LAI for a stand was calculated as:

$$150 \quad LAI = N_t * n_{stm} * S_{LA} \tag{1}$$

where  $N_t$  = needle mass per average tree in stand [kg],  $n_{stm}$  = number of stems per hectare 152 [1 ha<sup>-1</sup>], and  $S_{LA}$  = specific leaf area = 4.43 m<sup>2</sup> kg<sup>-1</sup> = 4.43\*10<sup>-4</sup> ha kg<sup>-1</sup> (Xiao et al., 2006).

Detailed information on LAI was used to obtain an estimate of how different forest management
options, already actively in operation in the area, could potentially affect groundwater recharge.
Three scenarios were simulated testing the potential impact of forestry operations on
groundwater recharge:

157 158  The first "baseline" scenario simulated the current situation by using LAI pattern at the site (Fig. 3) estimated with Eq. (1).

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2) The second scenario simulated the impact of intensive forestry operations as clear160 cutting of the tree stand. Clear-cutting is an intensive land use form where almost the
161 entire tree stand is removed, and it is carried out in some parts of the study area. Low
162 LAI values of 0-0.2 for the whole study site were used in simulating this scenario.

3) The third scenario simulated the impact of no forestry operations, i.e. absence of
forestry cuttings. The hypothetical mature stand covering the study site was assumed
to have high LAI values of 3.2-3.5 found at the study site and reported in the literature
(Koivusalo et al., 2008, Rautiainen et al., 2012, Vincke and Thiry, 2008, Wang et al.,
2004).

### 168 2.1.2 Lichen water retention

169 An organic lichen layer covers much of the sandy soil at the Rokua study site (Kumpula et al., 170 2000), so this lichen layer was introduced in soil evaporation (SE) calculations. Although 171 lichens do not transpire water, their structural properties allow water storage in the lichen matrix 172 and capillary water uptake from the soil (Blum, 1973, Larson, 1979). In this study lichen layer 173 was explicitly included in the simulations to create an additional storage for water before the 174 mineral sandy sediments. Water interception storage by the lichen layer was estimated from lichen samples. In total, six samples (species Cladonia stellaris and C. rangiferina) were taken 175 176 in May 2011 from two locations 500 m apart, close to borehole MEA506 (see Fig. 1). These 177 samples were collected by pressing plastic cylinders (diameter 10.6 cm) through the lichen layer 178 and extracting intact cores, after which mineral soil was carefully removed from the base of the

179 sample. Thus the final sample consisted of a lichen layer on top and a layer of organic litter and 180 decomposed lichen at the bottom, and was sealed in a plastic bag for transportation. To obtain 181 estimates of water retention capacity, the samples were first wetted until saturation with a 182 sprinkler, left overnight at +4 °C to allow gravitational drainage and weighed to determine 'field 183 capacity'. The samples were then allowed to dry at room temperature and weighed daily until 184 stable final weight ('dry weight') was reached. The water retention capacity (w<sub>r</sub>) of the sample 185 was calculated as:

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$$W_r = \frac{m_{fc} - m_{dry}}{\rho_w} \cdot \frac{1}{\pi \cdot r^2}$$
(2)

187 where  $m_{fc}$  is the field capacity weight [M],  $m_{dry}$  is the final dry weight [M] at room temperature, 188  $\rho_w$  [M L<sup>-3</sup>] is the density of water, and r [L] is the radius of the sampling cylinder.

189 The mean water retention capacity of the lichen samples was found to be 9.85 mm (standard 190 deviation (SD) 2.71 mm) and approximations for these values were used in model 191 parameterization (Table 2). Measured lichen water retention capacity was introduced to the 192 simulations using parameters for soil porosity and layer thickness. Lichen porosity values were 193 varied between 7.5 - 12.5 % in simulation Monte Carlo runs (see section 2.2.1) while keeping 194 thickness of the lichen layer at 100 mm. In this manner the maximum amount of water retained 195 by the lichen layer after gravitational drainage was adjusted to vary between 7.5 mm - 12.5 mm, 196 as seen in the measurement data. To acknowledge the lack of information about B&C parameter 197 estimates for lichen, the parameters were included in the simulations Monte Carlo runs with 198 ranges which in our opinion produced reasonable shape of the pressure-saturation curve 199 allowing easy drainage of the lichen.

# 200 2.1.3 Sandy sediment hydraulic properties

201 Sediment texture was determined by sieving (ISO 3310-1 standard sieve, US sieve numbers 5, 202 10, 18, 35, 60, 120, and 230) 26 samples taken from five boreholes at various depths (Fig. 1). 203 14 of the samples were analyzed also for pressure saturation curves. Samples were characterized 204 as fine or medium sand, while sediment texture in the other boreholes (Fig. 1) had previously 205 been characterized as medium, fine or silty sand throughout the model domain by the Finnish 206 Environmental Administration as expert *in-situ* analysis during borehole drilling. Therefore the 207 sediment samples from the five boreholes were considered to be representative of the sediment 208 type in the area. Pressure saturation data from the samples was then used to define parameter 209 ranges for the Brooks and Corey equation used in the simulations (Table 2). Furthermore, texture values were employed to calculate the range of saturated vertical hydraulic conductivity for the samples, using empirical equations by Hazen, Kozeny-Carman, Breyer, Slitcher, and Terzaghi (Odong, 2007). The hydraulic conductivity for a given sample ranged approximately one order of magnitude between the equations. When using the five equations for the 26 samples in total, the calculated values were within  $1.99*10^{-5} - 1.47*10^{-3}$  [m s<sup>-1</sup>] for all but one sample. The obtained range was considered to reasonably represent the hydraulic conductivity variability in the study area and simulations.

#### 217 2.1.4 Climate data

Driving climate data for the model were taken from Finnish Meteorological Institute databases 218 219 for the modeling period 1 Jan 1961-31 Oct 2010. Daily mean temperature [°C] and sum of 220 precipitation [mm] were recorded at Pelso climate station, 6 km south of the study area (Fig. 1). The most representative long-term global radiation data  $[kJ m^{-2} d^{-1}]$  for the area were 221 available as interpolated values in a 10 x 10 km grid covering the whole of Finland. The 222 223 interpolation data point was found to be at approximately the same location as borehole MEA2110 (Fig. 1). Long-term data on wind speed  $[m s^{-1}]$  and relative humidity [%] were taken 224 from Oulunsalo and Kajaani airports, located 60 and 40 km from the study site, respectively. 225 The data from the airports were instantaneous observations at three-hour intervals, from which 226 227 daily mean values were calculated. All the climate variables were recorded at reference height 228 2 m except for wind speed, which was measured at 10 m height. The wind speed data were 229 therefore recalculated to correspond to 2 m measurement height according Allen et al. (1998) 230 by multiplying daily average wind speed by 0.748. The suitability of long-term climate data for 231 the study site conditions was verified with observations made at a climate station established at the study site in an overlapping time period (Dec 2009-Oct 2010) and the agreement between 232 233 the measurements was found to be satisfactory.

234 Data on long-term lake surface water temperature were needed to calculate lake evaporation 235 (see section 2.2.3), but were not available directly at the study site. However, surface water 236 temperature was recorded at Lake Oulujärvi by the Finnish environmental administration 237 (2013) 22 km from the study site in the direction of the Kajaani climate station (Fig. 1). The 238 Oulujärvi water temperature was found to be closely correlated (linear correlation coefficient 239 0.97) with daily lake water temperature recorded at Rokua during summer 2012. Daily lake 240 surface temperature data for Lake Oulujärvi starting from 21 July 1970 were used in lake 241 evaporation modeling. However, the data series had missing values for early spring and some gaps during five years in the observation period. These missing values were estimated with a sine function, corresponding to the average annual lake temperature cycle, and a daily time series was established for subsequent calculations.

Snowmelt was calculated with a degree-day approach model in Jansson and Karlberg (2004).
Snow routines were calibrated separately using bi-weekly snow water equivalent (SWE) data
from Vaala snowline measurements (Finnish environment administration, 2011) for the period
1960-2010 (Fig. 1). This separately calibrated snow model was used for all subsequent
simulations.

250 **2.2 Recharge modeling framework** 

#### 251 2.2.1 Water flow simulation in 1-D unsaturated sediment profile

252 Water flow through an unsaturated one-dimensional (1-D) sandy sediment profile (Fig. 2) was 253 estimated with the Richards equation using CoupModel (Jansson and Karlberg, 2004). 254 CoupModel was selected as the simulation code because of its ability to represent the full soil-255 plant-atmosphere continuum adequately and to include snow processes in the simulations (Okkonen and Kløve, 2011). The simulated sediment profile was vertically discretized into 61 256 257 layers with increasing layer thickness deeper in the profile. Layer thickness was 0.1 m for the 258 first 16 layers (until 1.6 m), where the topmost 0.1 m was represented as a lichen layer. Layer 259 thickness was progressively increased by defining 0.2 m thickness for the next 7 layers 260 (between 1.6 and 3 m), 0.5 m for the next 14 layers (between 3 and 10 m), 1 m for the next 7 261 layers (between 10 and 17 m) and 2 m for last 17 layers ranging from 17 m to the bottom of the 262 profile (51 m).

263 The time variable boundary condition for water flow at the top of the column was defined by 264 driving climate variables and affected by sub-routines accounting for snow processes with daily 265 time step. The short time step was chosen to fully capture the main recharge input from snowmelt. All water at the top of the domain was assumed to be subjected to infiltration. Deep 266 267 percolation as gravitational drainage was allowed from sediment column base using the unitgradient boundary condition (see e.g. Scanlon et al., 2002b). Simulations for the unsaturated 1-268 269 D sediment profile were made for the period 1970-2010, and before each run 10 years of data 270 (1960-1970) were used to spin up the model.

271 The simulation of the 1-D sediment profile was performed 400 times as Monte Carlo runs to 272 facilitate the propagation of model parameter uncertainty in the final model output. Model was 273 ran each time with different parameter values as specified in Table 2. For each individual 274 simulation homogeneity in the vertical direction in terms of sediment hydraulic properties was 275 assumed. The parameters for which values were randomly varied were chosen beforehand by 276 trial and error model runs exploring the sensitivity of parameters with respect to cumulative 277 recharge or evapotranspiration. The parameter ranges were specified from field data when 278 possible; otherwise we resorted to literature estimates or in some cases used  $\pm$  50% of the 279 CoupModel default providing a typical parameter for the used equation.

280 The sensitivity of the parameters varied in the simulations was tested with Kendall correlation 281 analysis, by testing the correlation between each model parameter and cumulative sums of 282 different evapotranspiration components and infiltration for the 400 model runs. Individual 283 simulation with unique parameter values did not produce a groundwater recharge value due to 284 the assembling strategy for recharge; therefore the ET components and infiltration were selected 285 as variables for comparison. In addition, correlations were examined as scatter plots to ensure that possible sensitivity not captured by the monotonic correlation coefficient was not 286 287 overlooked.

# 288 2.2.2 Method to distribute 1-D simulations spatially

289 Groundwater recharge was estimated for a model domain of 82.3 km<sup>2</sup> (Fig. 1). To distribute the 290 simulations in 1-D sediment column spatially, the simulation domain was subdivided into 291 different recharge zones, similarly to e.g. Jyrkämä et al. (2002). Zonation in the model was 292 based on two variables: LAI and unsaturated zone thickness (UZT). The calculation of spatially 293 distributed values for LAI and UZT is presented in detail in sections 2.1.1 and 2.1.4. Both 294 variables were presented as a grid maps with 20m x 20m cell size with a floating point number 295 assigned to each cell, resulting in a total of 205 708 cells for the model domain. The small 296 model cell size was selected to ensure full exploitation of the forest inventory plots in LAI 297 determination. The spatially distributed data were then divided into 15 classes for LAI and 30 298 classes for UZT. The classes are primarily equal intervals, which was convenient in the 299 subsequent data processing, but in addition the frequency distributions of LAI and UZT cell 300 values were used to assign narrower classes for parameter ranges with many values (see 301 histograms in Figs. 3 and 4). Class interval for LAI was 0.2 units up to a value of 2 (class 1: 302 LAI = 0-0.2, etc.) and 0.3 to the maximum LAI value of 3.5. Class interval for UZT was 1 m to 10 m depth and 2 m to the final depth of 51 m. Finally, the classified LAI and UZT data were
combined to a raster map with 20m x 20m cell size, producing 449 different zones with unique
combinations of LAI and UZT values. Spatial coupling was done with the ArcGIS software
(ESRI, 2011).

307 Variation in the LAI and UZD parameters were used to allocate the 1-D sediment profile 308 simulations spatially to the study site. LAI class in model cell specified a subset of the 400 1-309 D simulations that were applicable for a given cell. UZT class for each cell (Fig. 2) specified 310 the depth in the simulated 51 m sediment profile where the water flux output was extracted. 311 Using this approach each unique recharge zone (a combination of UZT and LAI class) had on average 27 water flow time series (number of total model runs [400] divided by number of LAI 312 313 cell classes [15]) produced by different random combinations of parameters (Table 2). Equation 314 (3) was used to propagate the variability in the 27 time series into the final areal recharge.

315 
$$R_{i,j} = \frac{\sum_{l=1}^{449} n(l) * R_{S_{i,rand(1:k)} * A_c}}{A_{tot}}$$
(3)

where  $R_{i,j}$  is the final sample of areal recharge [mm day<sup>-1</sup>], i is the index for simulation time step (= 1:14975), j is the index for sample for a given time step (1:150), l is the index for unique recharge zone, n(l) is the number of cells in a given recharge zone, Rs is the recharge sample [mm/day] for a given recharge zone at time step I, k is the number of time series for a given recharge zone, A<sub>c</sub> is the surface area of a model raster cell (=20 m \* 20 m = 400 m<sup>2</sup>), and A<sub>tot</sub> is the surface area of the total recharge area.

The resulting R matrix has 150 time series for areal recharge produced by simulations with different parameter realizations. The variability between the time series provides an indication of how much the simulated recharge varies due to different model parameter values. The method allows computationally efficient recharge simulations, because the different recharge zones do not all have to be simulated separately.

The simulation approach assumes that: (1) over the long-term, the water table remains at a constant level, i.e. the unsaturated thickness for each model cells stays the same. Monitoring data from 11 boreholes and seven lakes with more than 5 years of observation history shows level variability of 1 - 1.5 m, with depressions and recoveries of the water table. This variability is within the accuracy of water table estimation by interpolation. (2) the capillary fringe in the sandy sediment is thin enough not to affect the water flow before arriving at the 'imaginary' water table at the center of each UZT class. (3) only vertical flow takes place in the unsaturated 334 sediment matrix, a typical assumption in recharge estimation techniques (Dripps and Bradbury, 2010, Jyrkama et al., 2002, Scanlon et al., 2002a). (4) surface runoff is negligible primarily due 335 336 to the permeable sediment type (as noted by Keese et al., 2005), and also due to lichen cover 337 inhibiting runoff by increasing surface roughness (Rodríguez-Caballero et al., 2012). The 338 maximum observed daily rainfall for the area has been 57.4 mm. Further assuming that rain for the day fell only during one hour, it would equal to  $1.59*10^{-5} \text{ m s}^{-1}$  input rate of water, which 339 is close to the lower range of saturated hydraulic conductivity at the study site  $(1.99*10^{-5} \text{ m s}^{-1})$ 340 <sup>1</sup>). Therefore rainstorms at the site very rarely exceed the theoretical infiltration capacity. As a 341 342 field verification, surface runoff has not been observed during field visits and the area lacks 343 intermittent or ephemeral stream networks.

# 344 2.2.3 Estimation of evapotranspiration

Four different evaporation processes were considered in this study (Fig. 5); soil evaporation (evaporation from the topmost soil layer, i.e. the lichen matrix), snow evaporation (evaporation from snow surface), transpiration (evaporation through the vascular system of tree canopy) and lake evaporation (evaporation from free water surface). The first three components were estimated, along with water flow simulations, using CoupModel. However, as 3.6 % (2.9 km<sup>2</sup>) of the surface area of the study site consists of lakes (Fig. 1), lake evaporation from free water surfaces was calculated independently from the CoupModel simulations.

352 Transpiration from the Scots pine canopy  $(L_{\nu}E_{tn})$  was calculated using Penman-Monteith (P-353 M) combination (Appendix 1, Eq. 1). Whenever possible, all the parameters relating to the P-354 M equation were estimated based on data, namely LAI of the canopy. Surface resistance and 355 saturation vapor pressure difference are the main factors controlling conifer forest 356 evapotranspiration, while the aerodynamic resistance is of less importance (Lindroth, 1985, 357 Ohta et al., 2001). In the calculation of aerodynamic resistance with the P-M equation, roughness length is related to LAI and canopy height, according to Shaw and Pereira (1982). 358 359 Other parameters governing the aerodynamic resistance, except for LAI, were treated as 360 constant. The surface resistance of the pine canopy was estimated with the Lohammar equation 361 (see e.g. Lindroth, 1985), accounting for effects of solar radiation and air moisture deficit in 362 tree canopy gas exchange. Because LAI values have a strong influence in the surface resistance 363 Lohammar equation, the other parameters governing the surface resistance were excluded from 364 the Monte Carlo runs. Distribution of root biomass with respect to depth from the soil surface 365 was presented with an exponential function, because most Scots pine roots are concentrated in the shallow soil zone. A typical root depth value of 1 m was used for the entire canopy (Kalliokoski, 2011, Kelliher et al., 1998, Vincke and Thiry, 2008). Soil and snow evaporation were calculated using an empirical approach (Appendix 1, Eq. 4) based on the P-M equation, as described in detail in Jansson and Karlberg (2004). Soil evaporation is calculated for the snow-free fraction of the soil surface, and the snow evaporation is solved separately as a part of snow pack water balance.

372 In areas where the water table is close to the ground surface, the water table can provide an 373 additional source of water for evapotranspiration (Smerdon et al., 2008). To take into account 374 the decreased recharge for areas with near surface water tables, the recharge for cells with an unsaturated zone of <1 m (8.3% of the study site, 6.8 km<sup>2</sup>) was estimated with a water balance 375 376 approach. We assumed that for areas with a shallow water table, soil water content was not a 377 limiting factor for transpiration. Therefore an additional water source for transpiration was 378 considered by making the transpiration rate equal to simulated potential transpiration (T) during 379 times when the actual transpiration was simulated (T >0.05 mm). Increasing effect of the water 380 table located at 1 m depth on soil evaporation was tested with simulations and found to be 5-381 10% higher with than without a water table. Therefore a 7% addition was made to the simulated actual soil evaporation for cells with a shallow water table. Daily recharge  $(R_{1m}, LT^{-1})$  for cells 382 383 with unsaturated thickness below 1 m was estimated as:

$$384 \qquad \mathbf{R}_{1m} = \mathbf{I} - \mathbf{T}_{adj} - \mathbf{E}\mathbf{S}_{adj} \tag{4}$$

385 where I is infiltration water arriving to lake/soil surface, including both meltwater from the 386 snowpack and precipitation [L T<sup>-1</sup>], T<sub>adi</sub> [mm d<sup>-1</sup>] is adjusted transpiration, and ES<sub>adi</sub> [mm d<sup>-1</sup>] 387 is adjusted soil evaporation. Kettle hole lakes in esker aquifers often lack surface water inlets 388 and outlets and are therefore an integral part of the groundwater system (Ala-aho et al., 2013, 389 Winter et al., 1998), so we considered these lakes as contributors to total groundwater recharge. 390 In other words, rainfall per lake surface area is treated equally as addition to the aquifer water 391 storage as groundwater recharge. As a difference, lake water table is subjected to evaporation 392 unlike the groundwater table. Lake evaporation (E<sub>lake</sub>) was estimated with the mass transfer 393 approach (see e.g. Dingman, 2008) according to Eq. (7) in Appendix 1. The mass transfer 394 method was selected because of its simplicity, daily output resolution, low data requirement, 395 and physically-based approach. However various calculation methods could easily be used in 396 the modelling framework, depending on the data availability (see e.g. Rosenberry et al., 2007). 397 If lake percentage in the area of interest is high, more sophisticated methods may be required

to better represent the system. For the Rokua site the bias introduced by a simplistic approachwas considered minor.

#### 400 **2.3 Model validation**

401 Model performance was tested by comparing the simulated recharge values with two 402 independent recharge estimates in local and regional scale; the water table fluctuation (WTF) 403 method and base flow estimation, respectively. The WTF method is routinely used to estimate groundwater recharge because of its simplicity and ease of use. It assumes that any rise in water 404 405 level in an unconfined aquifer is caused by recharge arriving at the water table. For a detailed description of the method and its limitations, see e.g. Healy and Cook (2002). The recharge 406 amount (R, L T<sup>-1</sup>) is calculated based on the water level prior to and after the recharge event 407 and the specific yield of the sandy sediments: 408

$$409 \quad R = S_y \frac{\Delta h}{\Delta t} \tag{5}$$

where S<sub>y</sub> is the specific yield, h is the water table height [L], and t is the time of water table rise[T].

412 The WTF method requires groundwater level data with adequate resolution for both time and 413 water level, to identify periods of rising and falling water table. Water table was monitored 414 using pressure-based dataloggers (Solinst Levelogger Gold) recording with hourly interval 415 from six water table wells with average unsaturated zone thicknesses of 1.2, 1.6, 5.0, 8.0, 9.3, 416 and 14.7 m (Fig. 1). Wells where the water table was <2 m from the ground surface responded 417 to major precipitation events. In the deeper wells, only the recharge from snowmelt was seen 418 as water table rise. Estimates of the sandy sediment specific yield are required for the 419 calculations (Eq. 5), but no sediment samples were available from the wells used in water table 420 monitoring. Drilling records for these wells reported fine and medium sand, which was 421 consistent with the particle size distribution for other wells in the area. Therefore an estimated 422 value of 0.20-0.25 for the specific yield of all wells was used, according to typical values for 423 fine and medium sand (Johnson, 1967).

The recharge estimated with the WTF method was compared with the simulated recharge during the recorded water level rise in the well. For each well, the cumulative sum of simulated water flow was extracted from sediment profile depth corresponding to well water table depth. As an example, the simulated recharge in well ROK1 (unsaturated thickness on average 14.7 m) was extracted from UTZ class 12, corresponding to recharge for unsaturated thickness of
14-16 m. All 400 model runs were used, providing 400 estimates for recharge for each time
period of recorded water level rise.

431 A regional estimate of groundwater recharge was estimated as baseflow of streams originating 432 at the groundwater discharge area. Because the Rokua esker aquifer acts as a regional water 433 divide, stream flow was monitored around the esker, in total of 18 locations (Fig. 1). The flows 434 were measured total of 8 times between 6 July 2009 and 3 August 2010 (see Rossi et al., 2014). 435 The lowest total outflow during 9-10 February 2010 was recorded after three months of snow 436 cover period, when water contribution to streams from surface runoff was minimal. The 437 minimum outflow was considered as baseflow from the aquifer reflecting long term 438 groundwater recharge in the area.

439

#### 440 **3 Results**

#### 441 **3.1** Model validation with the WTF and baseflow methods

442 Model validation showed that the modeling approach could reasonably reproduce (1) the main 443 groundwater recharge events when compared to the WTF method (Fig. 6) and (2) the regional 444 level of recharge compared to stream baseflow. The WTF method agreed well with the 445 simulated values, with overlapping estimates between the methods for all but two recharge 446 events. Also the median value of simulations was close to WTF method, with some bias to 447 higher estimates from the simulations. The discrepancy can be due to very different assumptions 448 behind the methods and uncertainty in local parameterization; in the WTF method for the 449 specific yield  $(S_y)$  and for simulations mainly the hydraulic conductivity which dictates the 450 simulated timing of recharge. Uncertainty in the S<sub>y</sub> estimate is acknowledged by showing S<sub>y</sub> a 451 range rather than a single value (Fig. 6), but still S<sub>y</sub> is not truly known for the location of 452 observation boreholes. Simplifying assumptions and subjective interpretation of both timing 453 and height of water table rise create additional inaccuracies in the WTF estimate.

Independent regional estimate of recharge, stream baseflow, was 70 500 m<sup>3</sup> s<sup>-1</sup>, or 312.7 mm a<sup>-1</sup> when related to the recharge area. The order of magnitude agreed with long term simulated average of 362.8 mm a<sup>-1</sup>. Typical error in individual stream flow measurements is within 3-6 % of the measured value (Sauer and Meyer, 1992), which brings minor uncertainty in the baseflow value. The smaller value for stream baseflow compared to simulated long term average recharge can be explained with conceptual understanding of site hydrogeology (Ala-aho et al., 2015,
Ala-aho et al., 2013, Rossi et al., 2012, Rossi et al., 2014). Part of the recharged groundwater
does not discharge to the small streams whose baseflow was measured, but flows underneath
the stream catchments and seeps out to regional surface bodies (Lake Oulujärvi and River
Oulujoki) further away from the recharge area (Fig. 2). Fully integrated surface-subsurface
hydrological modeling study of the same site presented in Ala-aho et al. (2015) simulated an
outflow of 79 mm a<sup>-1</sup> to regional surface water bodies.

## 466 **3.2 Temporal variations in groundwater recharge**

467 When recharge simulation time series were summarized to annual values (1 Oct-30 Sept), 468 recharge rates co-varied with annual infiltration with linear correlation coefficient of 0.89 469 (Fig. 7) as expected based on previous work in humid climate and sandy aquifers (Keese et al., 470 2005, Lemmelä, 1990). Both annual recharge and infiltration displayed an increasing trend. The 471 plot also showed the level of uncertainty in annual recharge values introduced by differences 472 in model parameterization (black area). The difference between minimum and maximum value 473 for simulated annual recharge was on average 23.0 mm. Thus the variablity in recharge 474 estimates was 6.3 % of mean annual recharge 362.8 mm.

According to the simulations, the *effective rainfall*, i.e. the percentage of corrected rainfall resulting in groundwater recharge annually, was on average 59.3%. This is in agreement with previous studies on unconfined esker aquifers at northerly latitudes, in which the proportion of annual precipitation percolating to recharge is reported to be 50-70% (71% by Zaitsoff (1984), 54% by Lemmelä and Tattari (1986) and 56% by Lemmelä (1990)). The percentage of effective rainfall varied considerably, by almost 30 %-units, between different hydrological years, from 44.8% in some years up to 73.1% in others.

## 482 **3.3** Influence of LAI on spatial variation of groundwater recharge

The spatial distribution of groundwater recharge was mostly due to variations in LAI, but also influenced by distance to water table, and distribution of lakes (Fig. 8). Higher evaporation rates from lakes led to lower recharge in lakes (see red spots in Fig. 8). Similarly, high LAI led to high ET and resulted in low recharge in plots with high LAI. Other areas of low recharge, although not as obvious at the larger spatial scales shown in Fig. 8, were cells with a shallow water table (section 2.2.2). The effect of high ET at locations with a shallow water table canbest be seen in south-east parts of the aquifer.

490 Kendall correlation analysis of simulation parameters and annual average model outputs 491 identified LAI as the most important parameter controlling evapotranspiration and infiltration 492 (Table 3). Parameters related to sediment hydraulics and evaporation showed some sensitivity 493 to simulation results, while the parameters for lichen vegetation were only slightly sensitive or 494 insensitive to simulation output variables. The LAI parameter governed the level of evaporation 495 for different ET components (Fig. 9). Evaporation from soil (and snow) compensated for mean 496 annual ET for LAI values up to around 1.0, after which total ET increased as a function of LAI. 497 The scenarios for low  $(0 \dots 0.2)$  and high  $(3.2 \dots 3.5)$  LAI changed the groundwater recharge 498 rates compared to the current LAI distribution (in Fig. 7). In the high LAI scenario the annual

recharge was on average 101.7 mm lower than in the low LAI scenario. These results suggest
that management of the Scots pine canopy has a significant control on the total recharge rates
in unconfined esker aquifers.

502 Average land surface ET components remained relatively constant between years, but the 503 simulated ET displayed a wide spread between simulations (Fig. 10). Estimated annual 504 evapotranspiration (mean 237.6 mm) was somewhat lower than previous regional estimates of 505 total ET (300 mm; (Mustonen, 1986)). Lake evaporation rates were generally higher than 506 evapotranspiration from the land surface (420.0 mm). The variation in simulated lake 507 evaporation was considerably lower than that in ET, as a different approach was used to account 508 for uncertainty in the simulations. Transpiration showed greater variation between simulations 509 than soil evaporation and total land surface ET. On average, transpiration also comprised a 510 slightly larger share of total evaporation than soil evaporation. Simulated snow evaporation was 511 a small, yet not insignificant, component in the total ET.

#### 512 **4 Discussion**

The method used here to estimate LAI from forestry inventories introduces a new approach for incorporating large spatial coverage of detailed conifer canopy data into groundwater recharge estimations. LAI values reported for conifer forests in Nordic conditions similar to the study site are in the range 1-3, depending on canopy density and other attributes (Koivusalo et al., 2008, Rautiainen et al., 2012, Vincke and Thiry, 2008, Wang et al., 2004). The LAI values obtained for the study site (mean 1.25) were at the lower end of this range. Furthermore, the data showed a bimodal distribution, with many model cells with low LAI (< 0.4) lowering the 520 mean LAI. The low LAI values were expected because of active logging and clearcutting 521 activities in the study area. Although the equations to estimate LAI are empirical in nature and 522 based on simplified assumptions, the method can outline spatial differences in canopy structure. 523 Wider use of this method in Finland is practically possible, as active forestry operations in 524 Finland have yielded an extensive database on canopy coverage, which could be used in 525 groundwater management. However, the LAI estimation method could be further validated with 526 field measurements or Lidar techniques (Chasmer et al., 2012, Riaño et al., 2004).

527 Plant cover, represented as LAI, proved to be the most important model parameter important 528 parameter controlling total ET, and thereby the amount of groundwater recharge (Table 3, Fig. 529 9). The LAI parameter was included in the equations controlling both transpiration and soil 530 evaporation, and therefore the sensitivity of the parameter is not surprising. While soil 531 evaporation partly compensated for the lower transpiration with low LAI values, the total 532 annual ET values progressively increased as a function of LAI (Fig. 9). Interestingly, the 533 simulations suggested that ET remains constant at constant level in the LAI range 0-1, 534 potentially due to the sparse canopy changing the aerodynamic resistance and partitioning of 535 radiation limiting soil evaporation, while still not contributing much to transpiration in total ET. 536 This implies that the maximum groundwater recharge for boreal Scots pine remains rather 537 constant up to a threshold LAI value of around 1. This knowledge can be used when co-538 managing forest and groundwater resources in order to optimize both.

539 Importance of LAI has been reported in earlier studies estimating groundwater recharge 540 (Dripps, 2012, Keese et al., 2005, Sophocleous, 2000), but here the vegetation was represented 541 with more spatially detailed patterns and a field data-based approach for LAI. According to previous studies, average ET from boreal conifer forests is around 2 mm d<sup>-1</sup> during the growing 542 543 season (Kelliher et al., 1998), which is similar to our average value of 1.6 mm d<sup>-1</sup> for the period 544 1 May-31 Oct. Some earlier studies have claimed that the influence of LAI on total ET rates 545 from boreal conifer canopies is minor (Kelliher et al., 1993, Ohta et al., 2001, Vesala et al., 546 2005), but our simulation results indicate that higher LAI values lead to higher total ET values. 547 The simulations showed that variable intensity of forestry, from low canopy coverage (LAI = (0.0.2) to dense coverage (LAI = 3.2-3.5) resulted in a difference of over 100 mm in annual 548 549 recharge (Fig. 7). It can be argued that the scenarios are unrealistic, because high LAI values, 550 covering the whole study site, may not be achieved even with a complete absence of forestry 551 operations. Nevertheless, the result demonstrates a substantial impact of forestry operations on 552 esker aquifer groundwater resources. The lichen layer covering the soil surface was explicitly 553 accounted for in the simulation set-up, which to our knowledge is a novel modification. Kelliher 554 et al. (1998) concluded that precipitation intercepted by lichen was an important source of 555 understorey evaporation, especially directly after rain events. In addition, Bello and Arama 556 (1989) reported that lichen could intercept light rain showers completely and that only intense 557 rain events caused drainage from lichen canopy to mineral soil. While the lichen layer might 558 have an increasing effect on soil evaporation through 'interception storage', Fitzjarrald and 559 Moore (1992) suggest that a lichen cover may in fact have an insulating influence on heat and 560 vapor exchange between soil and atmosphere, therefore impeding evaporation from the mineral 561 soil. In the present study, the lichen layer appeared to have minor influence on total evaporation, 562 soil evaporation and infiltration, as these variables showed only little sensitivity to lichen B&C 563 parameters (Table 3). However, the approach to represent lichen with B&C model needs to 564 better examined, as water retention capacity of lichen layer was introduced to the simulations 565 using the concept of total porosity, which is not strictly coherent with the B&C model. Nevertheless, the used approach successfully produced an additional dynamic interception 566 567 storage of water in the correct range (generally 3-7 mm depending on random parameterization, 568 data not shown). The performed laboratory measurement of lichen water retention should be supplemented with detailed analysis of lichen pressure-saturation curve and hydraulic 569 570 conductivity to clarify the role of lichen in soil evaporation, and thereby groundwater recharge.

571 Stochastic variation of selected model parameters illustrated the uncertainties relating to 572 numerical recharge estimation using the Richards equation in one dimension. The capability 573 and robustness of the Richards equation to reproduce soil water content and water fluxes have 574 been demonstrated extensively in various studies (Assefa and Woodbury, 2013, Scanlon et al., 575 2002b, Stähli et al., 1999, Wierenga et al., 1991). Therefore we considered that model 576 calibration and validation with point observations of variables such as soil volumetric water 577 content or soil temperature would not provide novel insights into water flow in unsaturated 578 porous media. Instead, we incorporated the parameter uncertainty ranges, usually used in model calibration, to the final recharge simulation output. An important outcome was that the 579 580 uncertainty in the model output caused by different model parameterizations was small in 581 comparison with the interannual variation in recharge. The error caused by uncertainty in the 582 model assumptions or driving climate data was not addressed in this study.

583 The sensitivity analysis focused on total cumulative values of fluxes and did not address the 584 temporal variations in the variables. Sediment hydraulic parameters mainly influenced the 585 timing of recharge through residence time in the unsaturated zone, not so much the total amount. 586 Therefore the sediment hydraulic parameters showed only minor sensitivity, perhaps 587 misleadingly. It should be noted that vertical heterogeneity in the unsaturated sediment profile 588 hydraulic parameters can reduce the total recharge rates (Keese et al., 2005). However, vertical 589 heterogeneities were ignored in this study not only to simplify the model, but also because the 590 drilling logs showed only little variation in the area. Work of Wierenga et al. (1991) supports 591 the simplification by showing that excluding moderate vertical heterogeneities does not 592 significantly affect the performance of water flow simulations with the Richards equation.

593 Simulations acknowledged shallow water table contribution to evapotranspiration in an 594 indirect, conceptual approach. Including a water table fixed at different depths in the sediment 595 profile would have been possible in the CoupModel setup. Influence of water table fixed at 2 596 m depth was tested and found to increase ET 3.5% for LAI values of 3, but for LAI values of 597 0.5 and 1.5 the increase in ET was only trivial. We expect only minor increase in ET with deeper 598 water table configuration (with the given sediment texture), and therefore argue that excluding 599 water table results in only minimal overestimation of total recharge at the study site. It should 600 be noted that upward water fluxes were not excluded from the water flow time series and 601 negative fluxes were considered as "negative recharge" at any depth. The simplification is made 602 that water available for upward fluxes comes only form the soil moisture storage, not from the 603 water table.

604 According to the simulations, the percentage of precipitation forming groundwater recharge 605 varied considerably between years, as also reported in previous studies on transient recharge 606 (Assefa and Woodbury, 2013, Dripps and Bradbury, 2010). Even though annual recharge was 607 correlated with annual precipitation, and therefore years with high precipitation resulted in 608 higher absolute recharge (Fig. 7), the percentage of effective rainfall did not increase as a 609 function of annual sum of precipitation. This is somewhat surprising, because the rather 610 constant evaporation potential between years (Fig. 10) and high sediment hydraulic conductivity could be expected to result in a higher percentage of rainfall reaching the water 611 612 table in rainy years. Some studies (Dripps and Bradbury, 2010, Okkonen and Kløve, 2010) have 613 suggested that when the main annual water input arrives as snowmelt during the low 614 evaporation season, it is likely to result in higher percentage recharge than in a year with little snow storage and precipitation distributed evenly throughout summer and autumn, which may contribute to the variability in the effective rainfall coefficient. However, when the maximum annual SWE value was used as a proxy for annual snow storage, there was no evidence of snow amount explaining the interannual variability in the recharge coefficient. Other factors contributing to recharge coefficient variability may be related to soil moisture conditions prior to snowfall, or the intensity of summer precipitation events (Smerdon et al., 2008, Stähli et al., 1999).

The above-mentioned reasons make the concept of effective rainfall, which is currently routinely used to estimate groundwater recharge for groundwater management in e.g. Finland (Britschgi et al., 2009), susceptible to over- or under-estimation of actual annual recharge. This applies especially for aquifers with a thick unsaturated zone, where rainy years produce higher average recharge with some delay and for a longer duration (Zhou, 2009).

627

#### 628 **5 Conclusions**

629 A physically-based approach to simulate groundwater recharge for sandy unconfined aquifers in cold climates was developed. The method accounts for the influence of vegetation, 630 631 unsaturated zone thickness, presence of lakes, and uncertainty in simulation parameters in the 632 recharge estimate. It is capable of producing spatially and temporally distributed groundwater 633 recharge values with uncertainty margins, which are generally lacking in recharge estimates, 634 despite understanding of uncertainty related to recharge estimates being potentially crucial for 635 groundwater resource management. However, the parameter uncertainty defined for the study 636 area was of minor significance compared with interannual variations in the recharge rates 637 introduced by climate variations.

638 The simulations showed that Scots pine canopy, parameterized as leaf area index (LAI), was 639 important in controlling the total amount of groundwater recharge. Forestry inventory databases 640 were used to estimate and spatially allocate the LAI and the results showed that such inventories 641 could be better utilized in groundwater resource management. Forest cuttings were 642 demonstrated to increase groundwater recharge significantly. A sensitivity analysis on the parameters used showed that soil evaporation could compensate for low LAI-related 643 644 transpiration up to a LAI value of approximately 1, which may be important in finding the optimal level for forest management in groundwater resource areas. The concept of effective 645 rainfall gave inconsistent estimates of recharge in annual timescales, showing the importance 646

647 of using physically-based recharge estimation methods for sustainable groundwater recharge648 management.

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## 653 Author contribution

P. Ala-aho and P.M Rossi collected and analyzed the field data. P. Ala-aho designed the
simulation set-up, performed the simulations and interpreted the results. P. Ala-aho prepared
the manuscript with contributions from all co-authors.

657

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# 885 Tables

**Table 1.** Characteristics of the study site annual climate.

VARIABLE	MEAN	STD
Precipitation [mm]	591	91
Air Temperature [°C]	-0.7	1.1
Reference ET [mm]	426	26

**Table 2.** Randomly varied parameters, related equations and parameter ranges included in the

9 model runs. For full description of parameters and equations, see Jansson and Karlberg (2004).

Parameter	Part of the model affected	Range	Uni ts	Source
LAI (leaf area index)	Transpiratio n	0 3.5	-	Data, see section 2.1.1
h (canopy height)	Transpiratio n	5 15	m	Data
r <sub>alai</sub> (increase in aerodynamic resistance with LAI)	Soil evaporation	25 75	-	$\pm 50\%$ , estimate
$r_{\Psi}$ (soil surface resistance control)	Soil evaporation	100300	-	$\pm 50\%$ approximately to cover the surface resistance reported 150-1000 (Kelliher et al., 1998)
$\lambda_L$ (pore size distribution index)	Soil evaporation, lichen	0.4 1	-	Estimate, to cover an easily drainable range of pressure-saturation curves
$\Psi_L$ (air entry)	Soil evaporation, lichen	1.5 20	-	Estimate, to cover a easily drainable range of pressure- saturation curves
$\theta_L$ (porosity)	Soil evaporation, lichen	7.512.5	%	Data, lichen mean water retention ±SD from samples

two (coefficient in the soid temperature response function)Water uptake $10 \dots 20$ $\cdot$ $\pm 50\%$ , estimate $\Psi_c$ water uptake reduction)(critical pressure head for water uptakeWater uptake $200\dots 600$ $\cdot$ $\pm 50\%$ , estimate $k_{mat,S}$ saturated hydraulic conductivity)Sediment profile $1.707$ $10^3 \dots 127.2$ $10^3$ mm dr1Data from sediment sample particle size analysis $k_{minuc}$ (minimum unsaturated hydraulic conductivity)Sediment profile $1.10^{-4} \dots 1$ $10^{-1}$ mm dr1Data from sediment sample particle size analysis $\lambda_s$ (pore size distribution index)Sediment profile $0.4 \dots 1$ $0.4 \dots 1$ $-$ Range to cover measured pressure-saturation curves $\Psi_s$ (air entry)Sediment profile $20 \dots 40$ $-$ Range to cover measured pressure-saturation curves $\theta_s$ (porosity)Sediment profile $0.25 \dots 0.36$ %Range from soil samples $\theta_r$ (residual water content)Sediment profile $0.01 \dots 0.05$ %Range to cover measured pressure-saturation curves	k <sub>mat,L</sub> (matrix saturated hydraulic conductivity)	Soil evaporation, lichen	$5 10^4 \dots 5 10^7$	mm d <sup>-1</sup>	Estimate, high K values assumed
pressure head for water uptakeWater uptake $200600$ - $\pm 50\%$ , estimatekmat,s saturated hydraulic conductivity)Sediment profile $1.707$ $10^3127.2$ $10^3$ mm d <sup>-1</sup> Data from sediment sample particle size analysiskminuc (minimum unsaturated hydraulic conductivitySediment profile $1.10^{-4} \dots 1$ $10^{-1}$ mm d <sup>-1</sup> Data from sediment sample 	the soil temperature	Water uptake	10 20	-	±50%, estimate
Initial saturated hydraulic conductivity)Sediment profile $10^3 \dots 127.2$ $10^3$ mm d^{-1}Data from sediment sample particle size analysis $k_{minuc}$ (minimum unsaturated hydraulic conductivitySediment profile $1 \dots 10^{-4} \dots 1$ $10^{-1}$ mm d^{-1}Data from sediment sample particle size analysis $\lambda_s$ (pore size distribution index)Sediment profile $1 \dots 10^{-4} \dots 1$ $10^{-1}$ mm d^{-1}Estimate $k_{mat} * 1E-5$ $\lambda_s$ (pore size distribution index)Sediment profile $0.4 \dots 1$ $20 \dots 40$ -Range to cover measured pressure-saturation curves $\Psi_s$ (air entry)Sediment profile $20 \dots 40$ -Range to cover measured pressure-saturation curves $\theta_s$ (porosity)Sediment profile $0.25 \dots 0.36$ %Range from soil samples $\theta_r$ (residual waterSediment profile $0.01 \dots 0.05$ %%Range to cover measured pressure-saturation	pressure head for water uptake	Water uptake	200600	-	±50%, estimate
unsaturated hydraulic conductivitySediment profile $1 \ 10^{-4} \ 1$ 	saturated hydraulic		$10^3127.2$		-
distribution index)profile $0.4 \dots 1$ $-$ pressure-saturation curves $\Psi_s$ (air entry)Sediment profile $20 \dots 40$ $-$ Range to cover measured pressure-saturation curves $\theta_s$ (porosity)Sediment profile $0.25 \dots 0.36$ %Range from soil samples $\theta_r$ (residual waterSediment profile $0.01 \dots 0.05$ %%Range to cover measured	unsaturated hydraulic		$1 10^{-4} \dots 1$ $10^{-1}$	mm d <sup>-1</sup>	Estimate k <sub>mat</sub> * 1E-5
	-		0.4 1	-	6
$\theta_{\rm s}$ (porosity) profile 0.250.36 % Range from soil samples $\theta_{\rm r}$ (residual water Sediment 0.01 0.05 % Range to cover measured	$\Psi_{\rm s}$ (air entry)		20 40	-	6
	$\theta_s$ (porosity)		0.250.36	%	Range from soil samples
	<b>、</b>		0.010.05	%	6

Parameter	Total ET	Transpiratio n	Soil E	Snow E	Infiltration
LAI	0.59*	0.84*	-0.73*	-0.37*	0.18*
h	0.59*	0.84*	-0.73*	-0.37*	0.18*
<b>ľ</b> Ψ	-0.11*	-0.03	-0.03	-0.61*	0.58*
<b>r</b> <sub>alai</sub>	-0.13*	-0.02	-0.11*	0.03	-0.05
$\lambda_{L}$	-0.09*	-0.01	-0.11*	0.01	-0.03
$\Psi_{\rm L}$	0.01	-0.04	0.11*	-0.04	0.06
$\theta_L$	0.06	0.03	0.01	-0.00	0.09*
k <sub>mat,L</sub>	-0.01	0.02	-0.04	-0.00	-0.00
k <sub>mat,S</sub>	-0.10*	-0.04	-0.07*	0.02	0.01
k <sub>minuc</sub>	-0.10*	-0.04	-0.07*	0.02	0.01
t <sub>WD</sub>	-0.05	-0.02	-0.03	-0.05	0.03
$\Psi_{c}$	0.18*	0.12*	-0.02	-0.04	0.05
$\lambda_{s}$	0.13*	0.06	0.06	-0.00	-0.23*
$\Psi_{s}$	-0.11*	-0.05	-0.04	-0.05	0.04
$\theta_s$	0.02	-0.01	0.03	0.10*	-0.18*
$\theta_r$	0.07*	0.05	-0.01	0.01	0.16*

**Table 3.** Kendall correlation coefficient for simulation parameters and average annual sum of899simulation output variables. ET = evapotranspiration, E = evaporation, for other symbols see900Table 2.

901 \*Significant correlation, p<0.05

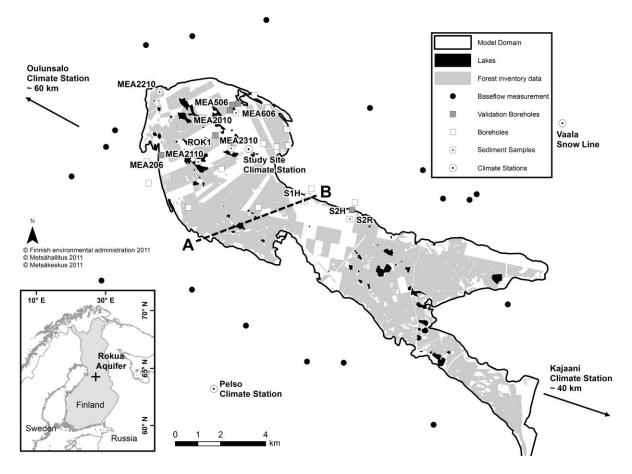
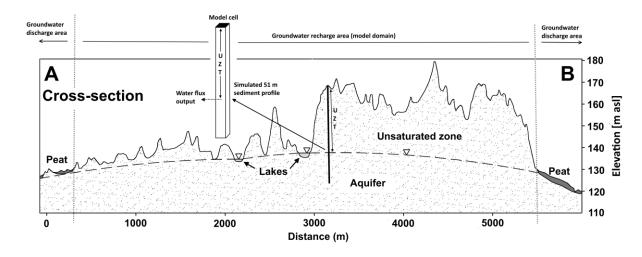
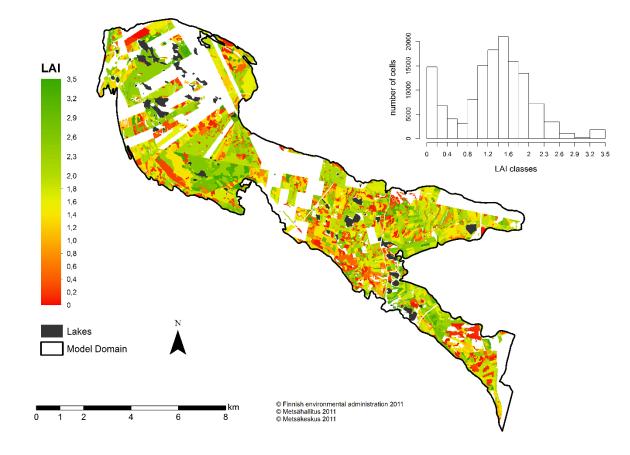


Figure 1. Recharge area of the Rokua esker aquifer. Boreholes in the area were used for model
validation and sediment type characterization. Baseflow was measured from streams
originating outside the groundwater recharge area. Profile of cross-section A-B is presented in
Fig. 2.

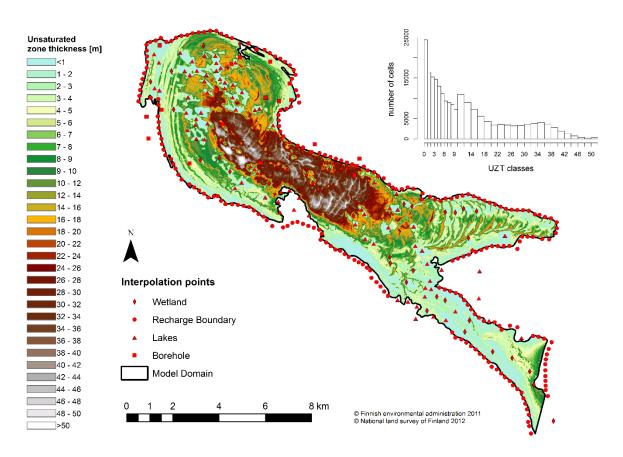


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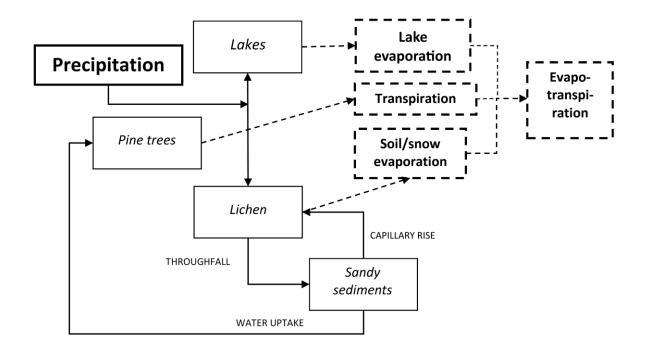
913 Figure 2. Cross-section A-B (Fig. 1) to demonstrate the geometry of the unsaturated zone and 914 the aquifer (vertical axes exaggerated). A simulated sediment profile is shown to give an 915 example on how 1-D simulations are represented in the model domain, UZT represents the 916 unsaturated zone thickness parameter.



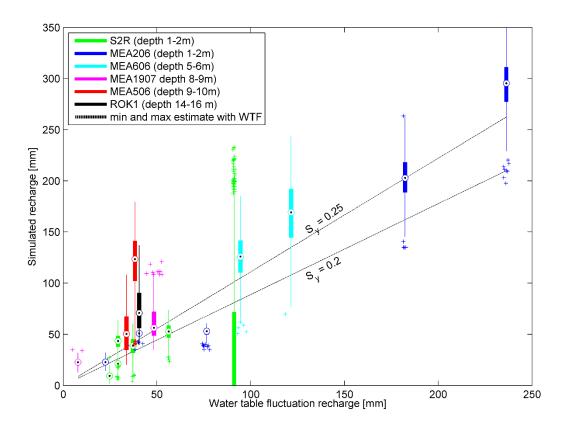
918 Figure 3. Spatial distribution of leaf area index (LAI) and a 20m x 20m cell-based histogram 919 of LAI values. In areas where forestry inventory data were lacking, a weighted average value 920 of 1.25 was used in simulations.



- 922 Figure 4. Estimated thickness of the unsaturated zone in the model area and interpolation points
- 923 for estimation of water table elevation.

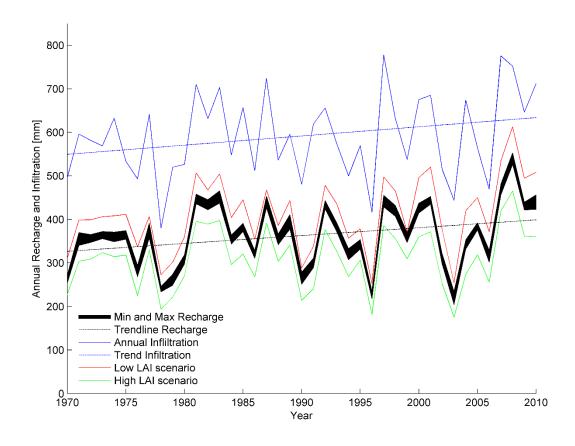


927 Figure 5. Flow chart of different evaporation processes considered in the study. Total 928 evapotranspiration comprises of soil evaporation from the topmost soil layer, i.e. the lichen 929 matrix, snow evaporation from snow surface, transpiration through the vascular system of tree 930 canopy and lake evaporation from free water surface.





**Figure 6.** Assemblage of simulated recharge for individual recharge events, shown as boxplots where circles represent the median, bold lines  $25-75^{\text{th}}$  percentiles of the simulations, thin lines the remaining upper and lower  $25^{\text{th}}$  percentiles and crosses are outliers. The location of the boxplots on the x-axis is the WTF estimate for a given recharge event using a specific yield value of 0.225. The dashed lines indicate the uncertainty in the WTF estimates caused by the selection of specific yield. The two estimates would agree perfectly (given the uncertainty in S<sub>y</sub>) if all simulations shown as boxplots fell between the dashed lines.



940 Figure 7. Annual recharge time series from simulations where the black area covers the 941 minimum and maximum values for different recharge samples. The annual recharge pattern 942 closely followed trends in infiltration. Effects of different land use management practices over

943 time on annual recharge rates are shown as high and low leaf area index (LAI) scenarios.

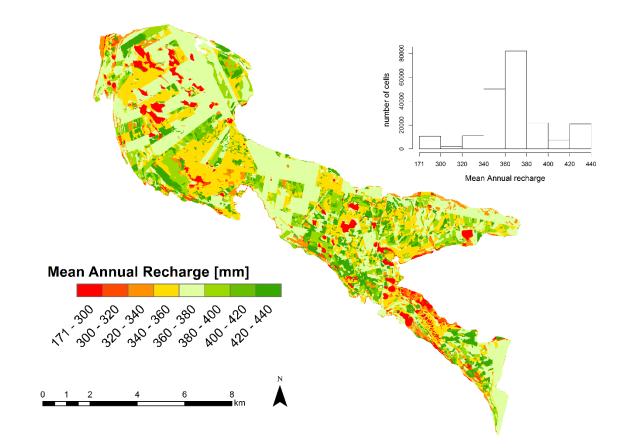


Figure 8. Spatial distribution of mean annual recharge, which was influenced mainly by the
Scots pine canopy (LAI), the presence of lakes and, to some extent, areas with a shallow water
table.

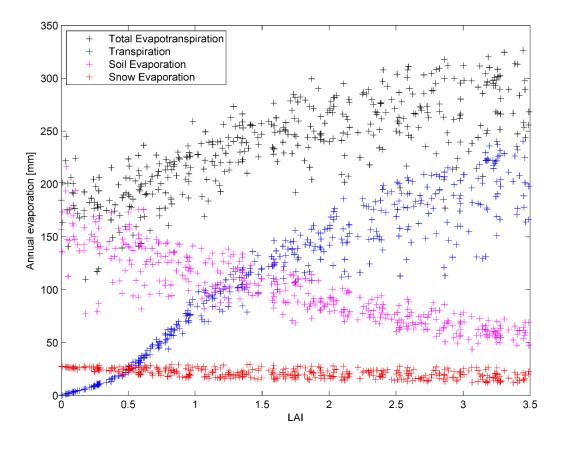
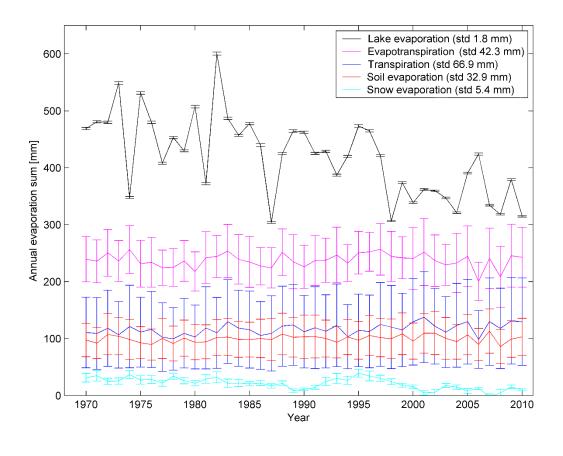


Figure 9. Example of scatter plots with the mean annual ET components are plotted as a
function of the variable leaf area index (LAI), showing clear dependence of all ET components
on LAI.



953 Figure 10. Values of different evapotranspiration (ET) components (mean and standard954 deviation) simulated for the study period.