- **Divergence of actual and reference evapotranspiration**
- 2 observations for irrigated sugarcane with windy tropical
- **3** conditions
- 4
- 5 R. G. Anderson<sup>1,\*</sup>, D. Wang<sup>1</sup>, R. Tirado-Corbalá<sup>1,\$</sup>, H. Zhang<sup>1,&</sup>, J. E. Ayars<sup>1</sup>
- 6 [1]{USDA, Agricultural Research Service, San Joaquin Valley Agricultural Sciences Center,
- 7 Water Management Research Unit, Parlier, California, USA $\}^1$
- 8 [\*]{now at: USDA, Agricultural Research Service, U.S. Salinity Laboratory, Contaminant
- 9 Fate and Transport Unit, Riverside, California, USA}
- 10 [\$]{now at: Crops and Agro-Environmental Science Department, University of Puerto Rico,
- 11 Mayagüez, Puerto Rico, USA}.
- 12 [&]{now at: USDA, Agricultural Research Service, Water Management Research Unit, Fort
- 13 Collins, Colorado, USA}
- 14 Correspondence to: R. G. Anderson (ray.anderson@ars.usda.gov)
- 15

## 16 Abstract

- 17 Standardized reference evapotranspiration (ET) and ecosystem-specific vegetation
- 18 coefficients are frequently used to estimate actual ET. However, equations for calculating
- 19 reference ET have not been well validated in tropical environments. We measured ET  $(ET_{EC})$
- 20 using Eddy Covariance (EC) towers at two irrigated sugarcane fields on the leeward (dry) side
- of Maui, Hawaii, USA in contrasting climates. We calculated reference ET at the fields using

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the short (ET<sub>0</sub>) and tall (ET<sub>r</sub>) vegetation versions of the American Society for Civil Engineers 1 (ASCE) equation. The ASCE equations were compared to the Priestley-Taylor ET (ET<sub>PT</sub>) and 2  $ET_{EC}$ . Reference ET from the ASCE approaches exceeded  $ET_{EC}$  during the mid-period (when 3 vegetation coefficients suggest ET<sub>EC</sub> should exceed reference ET). At the windier tower site, 4 5 cumulative  $ET_r$  exceeded  $ET_{EC}$  by 854 mm over the course of the mid-period (267 days). At the less windy site, mid-period  $ET_r$  still exceeded  $ET_{EC}$ , but the difference was smaller (443) 6 mm). At both sites, ET<sub>PT</sub> approximated mid-period ET<sub>EC</sub> more closely than the ASCE 7 equations ((ET<sub>PT</sub>-ET<sub>EC</sub>) <170 mm). Analysis of applied water and precipitation, soil moisture, 8 leaf stomatal resistance, and canopy cover suggest that the lower observed  $ET_{EC}$  was not the 9 result of water stress or reduced vegetation cover. Use of a custom calibrated bulk canopy 10 resistance improved the reference ET estimate and reduced seasonal ET discrepancy relative 11 to ET<sub>PT</sub> and ET<sub>EC</sub> for the less windy field and had mixed performance at the windier field. 12 These divergences suggest that modifications to reference ET equations may be warranted in 13 some tropical regions. 14

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### 16 **1** Introduction

Accurate estimates of evapotranspiration (ET) are needed for numerous purposes including 17 efficient irrigation scheduling (Davis and Dukes, 2010), parameterizing and running different 18 classes of biogeochemical and hydrologic models (Fisher et al., 2005; Zhao et al., 2013), 19 20 assessing changes in regional hydrology under different cultivation systems (Ferguson and Maxwell; 2011; Holwerda et al., 2013; Waterloo et al., 1999), and evaluating the impacts of 21 agricultural production on regional and global climate (Kueppers et al., 2007; Lo and 22 Famiglietti, 2013; Puma and Cook, 2010) and hydrology (Anderson et al., 2012; Vörösmarty 23 et al., 1998). In irrigated agriculture, underestimation of required ET can lead to sub-optimal 24 yield due to water stress (Kang et al., 2002), whereas overestimation of ET can lead to 25 excessive applied water, thus reducing water available for other uses or additional acreage 26 (Perry, 2005), degrading water quality (Smith, 2000), and decreasing economic 27 competitiveness (Hargreaves and Samani, 1984). 28 While accurate ET estimates are essential, ET can be challenging to measure. Numerous 29

30 approaches have been developed to measure or estimate ET, including lysimeters (Meissner et

- al., 2010), micrometeorological methods (Anderson and Goulden, 2009; Baldocchi, 2003;
- Hemakumara et al., 2003), satellite remote sensing (Bastiaanssen et al., 2005; Tang et al.

1 2009), and water balance methods. While these approaches vary in their spatial/temporal scale

2 and methodological assumptions and accuracy, most require significant observational costs,

3 technical expertise, or have operational difficulties that are too high for most farmers.

Because of the difficulties in actual ET measurement, the vegetation coefficient/reference ET
approach (Jensen, 1968) has gained widespread acceptance for estimating actual ET for varied
applications (e.g. Arnold et al., 1998; Cristea et al., 2012). This approach involves calculating
a reference ET for a standard land surface, usually grass or alfalfa, using meteorological data
and relating the reference surface to the ecosystem/land cover of interest with empirical
coefficient(s):

 $10 \quad \mathrm{ET}_{\mathrm{A}} = \mathrm{K}_{\mathrm{C}} * \mathrm{ET}_{\mathrm{0}}. \tag{1}$ 

where ET<sub>A</sub> is actual ET, ET<sub>0</sub> is reference ET, and K<sub>c</sub> is the coefficient for the specific land 11 cover type. Two of the most commonly used standard methods include the Food and 12 Agricultural Organization (FAO) approach presented in Irrigation and Drainage Paper 56, 13 hereafter referred to as FAO-56 (Allen et al., 1998), and the American Society of Civil 14 Engineers approach, hereafter referred to as ASCE (Allen et al., 2005). Both approaches are 15 16 based on the combination Penman-Monteith formula (Monteith, 1965) and account for ET from both solar irradiation and advectively-driven ET due to wind and vapor pressure deficit 17 (VPD). Both the FAO-56 and ASCE approaches assume standard measurement conditions 18 and surface parameters (e.g. canopy height, surface resistance, albedo, etc.), thus allowing 19 canopy and atmospheric resistance terms to be condensed into constants. Both methods also 20 provide scaling procedures to account for variation in meteorological measurements as well as 21 missing or erroneous data. 22

23 Validation work of standardized reference ET equations against large weighing lysimeters

24 with reference surfaces has been done primarily in the western continental U.S. with low

atmospheric humidity (Evett et al., 2000; Jensen et al., 1990). Internationally, most other

reference ET validation has been done in Mediterranean climates with similar, low, humidity

27 (Lecina et al., 2003; Ventura et al., 1999). Relatively little evaluation of these equations has

been done in areas with higher relative humidity, presumably because of the perceived lack of

- 29 use for reference ET equations in these areas. However, reference ET equations are used in
- 30 more humid regions for applications such as watershed modeling (Rao et al., 2011),
- 31 forecasting water demand (Tian and Martinez, 2012), and determining irrigation needs

1 (Suleiman and Hoogenboom, 2007). As such, it is necessary to test these reference ET equations in regions with high relative humidity to ensure accurate ET parameterization. 2 One major tropical and subtropical crop that has generally high ET is sugarcane. Sugarcane is 3 a good crop to test reference ET parameterizations because of its longer full canopy period, 4 when actual crop ET should be at its maximum relative to reference ET equations, and high 5 crop coefficient that generally exceeds 1. Previous research in irrigated sugarcane has found 6 full-canopy ET rates that equal or exceed evaporation rates from open-water pans (Campbell 7 et al., 1960; Thompson and Boyce, 1967). Since the development and implementation of 8 reference ET equations, researchers have generally found irrigated sugarcane to have a crop 9 10 coefficient (Kc) greater than 1 in Australia and Swaziland (Inman-Bamber and McGlinchey, 2003), Brazil (da Silva et al., 2012), and Texas (Salinas and Namken, 1977). However, all of 11 these studies found variable and differing Kc values, with Inman-Bamber and McGlinchey 12 noting a correspondence between meteorological events and outlying daily Kc values. 13 Sugarcane's high water use, the potential for expanded irrigation to reduce yield deficits and 14 increase production in tropical regions (Inman-Bamber et al., 1999), and the potential for 15 sugarcane irrigation to stress water resources during dry periods in tropical areas (Ramjeawon, 16 17 1994), make it a good case study for evaluating reference ET equations in tropical regions. To evaluate the performance of standardized reference ET equations, we established two Eddy 18 Covariance towers over irrigated sugarcane fields in Hawaii, USA to measure ET ( $ET_{EC}$ ). We 19 20 calculated reference ET using the ASCE approach for short  $(ET_0)$  and tall  $(ET_r)$  reference vegetation. The FAO-56  $ET_0$  was not used as it is identical to ASCE  $ET_0$  for calculations on a 21 daily time step (Irmak et al., 2006; Suleiman and Hoogenboom, 2009). We also compared 22  $ET_{FC}$  to the Priestley-Taylor (PT) ET equation ( $ET_{PT}$ ). Our objectives were (1) to determine if 23 standardized reference ET equations adequately parameterized actual ET across differing 24 microclimates, (2) determine the meteorological conditions that contribute to discrepancies in 25 the standardized equations and (3) examine corrections to improve estimates of reference ET 26 under relatively more humid conditions. 27

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29 2 Methods

30 2.1 Study region

1 We evaluated reference ET approaches in two sugarcane (Saccharum officinarum L.) fields with identical cultivars (Heinz et al., 1981) at a commercial farm on Maui, Hawaii, 2 USA (Fig. 1 and Table 1). Climatic conditions vary across the farm, with changes in 3 precipitation, wind, solar irradiation, and air temperature due to orographic effects. Normal 4 5 annual precipitation ranges from 275 mm/year to 1275 mm/year from the leeward (south) side to the windward (northeast) side of the plantation (Giambelluca et al., 2013). Elevations on 6 the plantation range from near sea level to ~340 m. The western side of the plantation is 7 generally windier (Table 1). Drip irrigation is used to maximize limited surface and ground 8 water resources (Moore and Fitschen, 1990); drip tape spacing is 2.70 m with sugarcane rows 9 planted 45 cm away from the tape on both sides; the tape irrigates at 1.58 L<sup>-1</sup> hour<sup>-1</sup> m<sup>-1</sup> and is 10 regulated to 83 kPa of pressure at the head of the row. Irrigation amounts were recorded by 11 12 the farm; rainfall was recorded at nearby weather stations (Supplemental S1). As is typical for Hawaii (Heinz and Osgood, 2009), sugarcane is grown on a 24 month rotation with planting 13 and harvesting throughout most of the year. Peak ET, as determined by the length of the mid-14 season period, lasts significantly longer (330 days) than for sugarcane in other regions (190-15 220 days) (Doorenbos and Pruitt, 1977; Inman-Bamber and McGlinchey, 2003). 16

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### 2.2 Eddy Covariance measurements and data analysis

We installed two micrometeorological towers in contrasting micro-climates (Fig. 1 and 18 Table 1). These towers are at the "Windy" site (lower elevation, higher wind velocity, more 19 constant wind direction, and sandy clay loam soil) and the "Lee" site (higher elevation, lower 20 wind velocity, and clay soil). Field fetch in the prevailing wind directions was over 200 m for 21 both towers. The slope in both fields, as determined using the 1/3 arcsec (~10 m) Digital 22 Elevation Model from the US Geological Survey's National Elevation Dataset 23 (http://ned.usgs/.gov/index.html), is less than 3% Beyond the edge of each field, Windy was 24 surrounded by sugarcane fields on all sides for over 1500 m; Lee was bordered by non-25 irrigated rangeland in the non-prevailing wind directions (east and south) and contiguous 26 27 sugarcane fields on the north and east.

Tower instrumentation included an integrated Eddy Covariance system (EC150 - Campbell 1 Scientific, Logan, Utah, USA<sup>2</sup>) with an open-path infrared gas analyzer, aspirated temperature 2 probe, attached 3-D sonic anemometer head (CSAT3A - Campbell Scientific), and enhanced 3 barometer (PTB110 - Vaisala, Vantaa, Finland). Relative humidity and air temperature were 4 5 measured by a combined temperature and relative humidity probe (HMP45C - Vaisala). Net radiation was measured with a single component net radiometer (NR-Lite2 – Kipp and Zonen, 6 Delft, Netherlands). We corrected the single component net radiometer for the effect of wind 7 following Cobos and Baker [2003). Ground heat flux was measured as the average of four 8 self-calibrating heat flux plates (HFP01SC - Huskeflux, Delft, Netherlands). The plates were 9 installed at 5 cm depth at four lateral locations perpendicular to the irrigation drip line 10 (Section 2.1): 0 cm (drip line), 45 cm (sugarcane row), 75 cm, and 135 cm (mid-point 11 between drip lines). All instruments were factory calibrated to ISO 9001:2008 standards prior 12 to deployment; data were recorded and processed on solid state dataloggers (CR3000, 13 Campbell Scientific). 14

Two Water Content Reflectometry probes (CS616 - Campbell Scientific) were installed at 20 15 cm depth at lateral two locations perpendicular to the drip line (45 and 135 cm) to measure 16 soil volumetric water content (VWC). These locations were chosen to correspond with the 17 sugarcane row (center of root zone) and halfway between sugarcane rows. VWC was 18 19 measured to independently assess potential water stress in both fields. VWC was calculated using a quadratic equation with empirically determined coefficients specific to each field 20 following the manufacturer's recommendation. For the calibration, three ~19 L (5 U.S. 21 gallon) water coolers (Internal height 46.6 cm, internal diameter 32.8 cm) were used to 22 23 calibrate each soil. We inserted the probe rod vertically in the center (middle) of the experimental coolers into the soil ensuring full contact with the soil. Then, the coolers were 24 closed with their respective lids to allow the system to equilibrate before taking account of the 25 period readings for each VWC. For the upper 40 cm of soil in each field, we determined bulk 26 density, porosity, and soil texture (Bouyoucus, 1962) and soil water retention characteristics 27 (Windy field only) with samples from 3 locations within the tower footprint. Soil water 28 retention characteristic (from saturation point to 1 bar) were determined for the Windy soil 29

<sup>&</sup>lt;sup>2</sup> Mention of trade names or commercial products in this publication is solely for the purpose of providing specific information and does not imply recommendation or endorsement by the U.S. Department of Agriculture.

using Tempe Cells (1400 Series, Soil Moisture Equipment Corp, Santa Barbara, California,
USA). Water retention characteristics could not be determined in Lee field because of the
logistical difficulty and equipment risk in obtaining intact Tempe Cell samples below the
surface due to rockiness at the Lee site. Permanent wilting point (PWP) was determined using
a dew point potentiometer (WP4C, Decagon Devices, Inc., Pullman, Washington, USA). Soil
water depth was determined for the upper 40 cm by converting soil VWC with porosity and
subtracting PWP.

The EC150 system measured CO<sub>2</sub>, H<sub>2</sub>O, wind velocity, and sonic temperature at 10 Hz. Other 8 variables were averaged to 30 minute fluxes. We processed raw covariances on the datalogger 9 10 and post-processed high frequency time series data with commercial software (Eddy Pro Advanced V 3.0 and 4.0 – LI-COR, Lincoln, Nebraska USA). Datalogger flux calculations 11 were downloaded daily via cellular modem. High frequency (10 Hz.) data and half hourly 12 fluxes were transferred monthly via data card. Raw time series data were checked following 13 Vickers and Mahrt's (1997) tests. Sonic anemometer tilt was corrected using double rotation 14 (Kaimal and Finnigan, 1994); lags between the infrared gas analyzer and sonic anemometer 15 were determined using maximum covariance. We corrected for density fluctuations (Webb et 16 al., 1980), low pass filtering (Moncrieff et al., 1997), and high pass filtering (Moncrieff et al., 17 2004). Flux footprint lengths were calculated following Kljun et al. (2004), and quality flags 18 19 were assigned following the CarboEurope standard (Mauder and Foken, 2004). We independently calculated stability (Obuhkov, 1971). After installation, tower heights were 20 21 periodically adjusted to keep meteorological instrumentation ~3.0-3.3 m above the zero plane displacement height, which was assumed to be 67% of canopy height (Arya, 2001). Canopy 22 23 height was measured biweekly, concurrent with the vegetation cover observations (Section 2.4). Additional, detailed, EC cross validation activities are described in Supplemental S1. 24

Half-hourly fluxes with instrumentation errors flagged by the EC150 system, rainfall, or lack 25 of turbulence (friction velocity < 0.1 m/s) were excluded. Excluded fluxes were gap-filled as a 26 function of fluxes measured from similar meteorological periods using the Max-Planck 27 Institute tool (http://www.bgc-jena.mpg.de/~MDIwork/eddyproc/index.php) (Reichstein et al., 28 2005). Gap filled fluxes were used to calculate daily and cumulative fluxes, but were excluded 29 from half hourly analyses. We corrected fluxes for energy budget closure by regressing daily 30 EC observed available energy against measured available energy (net radiation minus ground 31 heat flux) and forcing the regression through the origin, preserving the daily mean Bowen 32

ratio and adjusting each day's ET by the regression slope for the entire study period
 (Anderson and Wang, 2014; Leuning et al., 2012).

### 3 2.3 Reference ET equations

At each tower, daily and hourly reference ET was calculated using the ASCE short  $(ET_0)$  and tall  $(ET_r)$  reference equations, where short and tall refer to parameterized surfaces similar to well-watered fescue grass (short) and alfalfa (tall) with differences in the equations due to assumed leaf area index and bulk canopy resistance to ET

8 
$$ET_{sz} = \frac{0.408\Delta(R_n - G) + \gamma \frac{C_n}{T + 273} u_2(e_s - e_a)}{\Delta + \gamma (1 + C_d u_2)}$$
 (2)

As shown in equation 2, ET<sub>sz</sub> is the reference ET type (ET<sub>r</sub> or ET<sub>0</sub> in mm/day or mm/hour 9 depending on time step),  $R_n$  and G are net radiation and ground heat flux (MJ m<sup>-2</sup> day<sup>-1</sup> or MJ 10 m<sup>-2</sup> hour<sup>-1</sup>),  $\gamma$  is the psychrometric constant (kPa °C<sup>-1</sup>), T is mean daily or hourly air 11 temperature (°C), u<sub>2</sub> is mean daily or hourly wind speed measured at or scaled to 2 m height, 12 es and ea are mean saturation and actual vapor pressure (kPa), respectively, and Cn and Cd are 13 empirical numerator and denominator constants that change with reference surface and time 14 step (Table 1 in Allen et al., 2005). We scaled all meteorological variables from 3 m above the 15 zero plane displacement to 2 m height following the ASCE procedure for adjusting 16 meteorological measurements at non-standard height. Following ASCE, mean daily 17 meteorological values were calculated as an average of daily minimum and maximum values 18 as opposed to averaging all 24 hours of measurements. Differences between these averaging 19 approaches were small (mean T difference of 0.26 °C and 0.27 °C in Windy and Lee, 20 respectively). Measured net radiation and ground heat fluxes were used for all calculations. 21

We also calculated another reference using the Priestley-Taylor (PT) equation (Priestley and Taylor, 1972). PT was chosen as a comparison because of its different treatment of advection versus the Penman-Monteith (PM) type equations, its wide usage, and the relative simplicity of its meteorological inputs compared to PM. The PT equation is

26 
$$ET_{PT} = \frac{\alpha}{\lambda} * \frac{\Delta(R_n - G)}{\Delta + \gamma}$$
 (3)

ET<sub>PT</sub> is the PT ET (mm day<sup>-1</sup>);  $\Delta$ ,  $\gamma$ , R<sub>n</sub>, G are the same as in equation 2;  $\lambda$  is the latent heat of vaporization; and  $\alpha$  is an empirical constant. We assumed that  $\lambda$  is 2.45 MJ mm<sup>-1</sup>, which is the same as the ASCE/FAO-56 approach. We used an  $\alpha$  of 1.26, which is widely, but not universally, representative of a well-watered surface across a variety of climates (e.g.
 Eichinger et al., 1996; McAneney and Itier, 1996).

### 3 2.4 Canopy cover and determination of mid-period

We measured fractional canopy cover with an optical camera to obtain an independent, 4 conservative determination of the mid-season period (mid-period) for intercomparison of 5 measured and reference ET. The mid-period is one of the growth/ET stages in the FAO/ASCE 6 methodology and corresponds to maximum plant transpiration and the highest ecosystem 7 coefficient (K<sub>c-mid</sub>). In unstressed sugarcane, the mid-period coefficient should exceed 1 8 (Allen et al., 1998), thus measured ET should exceed reference ET. The camera (TetraCam 9 ADC multispectral camera, TetraCam Inc., Chatsworth, California, USA) contains a single 10 precision 3.2 megapixel image sensor optimized for capturing green, red, and near-infrared 11 wavebands of reflected light. A telescoping pole tripod system (GeoData Systems 12 Management Inc., Berea, Ohio, USA) was used to suspend the camera directly above the plant 13 at a height of 7 m and aim vertically downward at nadir view. Each field was photographed 14 every  $\sim 16\pm 2$  days. Ten images were taken in two lines perpendicular to the irrigation line at 15 16 pre-selected sampling locations in each field at solar noon  $\pm$  two hours; sampling locations were identical throughout the study. Each image was preprocessed in image processing 17 software (LView Pro 2006 - CoolMoom Corp., Hallandale, Florida, USA) to paint out the 18 pixels of soil, grass, shadow and other background. The preprocessed image was then 19 analyzed using proprietary software (PixelWrench, TetraCam Inc.) to classify fractional 20 vegetation cover based on threshold analysis, and the cover readings from the ten locations 21 were averaged to determine mean and standard error of field vegetation cover. We considered 22 the beginning of the mid-period to be the latter of the beginning date of mid-period from the 23 FAO-56 K<sub>C</sub> curve (Allen et al., 1998) or the date where canopy cover clearly exceeded 80%, 24 which has been shown to coincide with the start of mid-period (Carr and Knox, 2011). The 25 end of the K<sub>C-mid</sub> period was set to 27 August 2012, which was the last date of irrigation data 26 27 prior to the end of the FAO-56 mid-period. Finally we further restricted the end of the midperiod in the earlier planted field (Lee) to ensure that the length of the mid-period was 28 identical in both fields for intercomparison purposes. 29

### 30 2.5 Leaf Area Index and stomatal resistance measurements

We measured Leaf Area Index (LAI) and leaf stomatal resistance in a field campaign during 1 the mid-period for both EC fields (July 2012). LAI was measured using a non-destructive, 2 optical plant canopy analyzer (LAI 2200, LI-COR Inc.) on 13 July in the Lee field and 16 July 3 in the Windy field. At each of the 10 TetraCam sampling locations in each field (Section 2.4), 4 5 we made 10 below canopy and 5 above canopy measurements with the optical canopy analyzer; we then used the manufacturer's software (FV2200, LI-COR Inc.) to determine 6 mean and standard error of LAI for both fields. To observe leaf level stomatal resistance, we 7 used a steady-state diffusion porometer (SC-1, Decagon Devices Inc.), which has been used to 8 observe response to different irrigation regimes in multiple agronomic crops (e.g. Ballester et 9 al., 2013; Hirich et al., 2014; Mabhaudhi et al., 2013; Mendez-Costabel et al., 2014). At each 10 TetraCam point, 9 leaves were measured: 3 fully sunlit upper canopy leaves near (<20 vertical 11 cm away from) the top visible dewlap (TVD) point (Glaz et al., 2008), 3 mid-level leaves that 12 were attached to the cane stalk below the TVD height but which were still mostly sunlit, and 3 13 lower canopy leaves that were partially to mostly shaded. Porometry measurements were 14 made in a 30 s measurement window using the porometer's automatic mode. We also repeated 15 the stomatal resistance measurements at five of the TetraCam points in the Windy field to 16 evaluate the larger discrepancies in reference ET observed in that field. 17

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### 19 3 Results

### **3.1** Fractional vegetation cover, leaf area index, and leaf stomatal resistance

Fractional vegetation cover increased rapidly in both fields after the beginning of the EC 21 measurements (Fig. 2). Initial cover was <20% in Windy and <45% in Lee (112 and 142 days 22 23 after planting (DAP), respectively). Some early TetraCam sampling dates were missed due to initial equipment failures. Vegetation cover exceeded 80% in Lee on 3 November 2011 and 5 24 25 December 2011 in Windy (220 and 208 DAP, respectively); which we considered the onset of the mid-period. Both of these dates are later than the onset of mid-period according to the 26 FAO-56 curve (180 DAP). Variation in cover was largest at the beginning of the study period 27 (standard deviation of ~10%) (Fig. 2). Vegetation cover was least variable near the onset of 28 the mid-period (standard deviation <5%). 29

30 Mean (standard error) of measured Leaf Area Index (LAI) was 4.9 (0.2) in Windy on 13 July

31 2012 and 4.7 (0.3) in Lee on 16 July 2012. Midday leaf stomatal resistance  $(r_s)$  observations

of fully sunlit leaves in Windy (n=32) and Lee (n=21) showed substantial variation, ranging 1 from 45 to 259 s  $m^{-1}$  in Windy and 40 to 640 s  $m^{-1}$  in Lee. Median  $r_s$  in Windy and Lee were 2 112 and 114 s m<sup>-1</sup>, respectively. Mean (standard deviation) of r<sub>s</sub> in Windy and Lee were 125 3 (57) s m<sup>-1</sup> and 161 (157) s m<sup>-1</sup>, respectively. There were two observations in Lee of sunlit 4 stomatal resistance of >500 s m<sup>-1</sup>. Excluding these two observations resulted in a revised 5 mean and median  $r_s$  in Lee of 114 and 104 s m<sup>-1</sup>, respectively. Mean sunlit stomatal resistance 6 was not significantly different (p < 0.01) from 100 s m<sup>-1</sup> in either Windy (p=0.02) or Lee 7 (p=0.09). 8

### 9 3.2 Meteorological observations

Air temperature and net radiation were similar in both Windy and Lee (Figs. 3a and 3c; Table 10 1). In Windy, mean daily air temperature ranged from 19.0 to 25.0 °C over the Study Period 11 whereas in Lee mean daily air temperature ranged from 19.7 to 26.3 °C. Mean air temperature 12 was higher in Windy than Lee (23.5 and 22.3 °C, respectively) with a similar, low day to day 13 14 variability (standard deviation of 1.3 °C for both fields). Daily net radiation (Rn) was also similar between fields; Rn was slightly higher in Windy versus Lee (11.5 and 10.9 MJ m<sup>-2</sup> 15 day<sup>-1</sup>; Fig. 3c and Table 1). Both fields showed larger relative variations in Rn (~10 MJ m<sup>-2</sup> 16 day<sup>-1</sup>) than in other meteorological observations. Wind velocities were sharply divergent 17 between the two fields. Mean wind velocity was more than twice as high (4.6 m s<sup>-1</sup>versus 2.0 18 m s<sup>-1</sup>) in Windy compared to Lee (Fig. 3b; Table 1). Wind velocities were also more variable 19 in Windy than Lee (standard deviation of 1.4 and 0.7 m s<sup>-1</sup>, respectively). 20

Soil volumetric water content (VWC) observations in the Windy field underneath the sugar 21 22 cane row/line varied from 23-30% during the mid-period except after major rain events in December 2011 and March 2012 when they spiked to 36-37% (Fig. 3d). At all times, VWC 23 24 remained well above wilting point (12%) for both sensors (Table 1). Available plant water in the top 40 cm of the soil at minimum VWC was ~40 mm. Soil matric potentials in Windy near 25 typical maximum (30%) and minimum (24%) soil VWC were -0.01 and -0.033 MPa, 26 respectively (Table 1). Shallow VWC observations underneath the cane row are likely 27 28 indicative of plant water stress due to the majority of drip-irrigated Hawaiian sugarcane roots being at less than 50 cm depth (Evensen et al., 1997). VWC observations between drip lines 29 30 showed relatively little periodicity compared to underneath the cane row, indicating that neither irrigation events nor root depletion was impacting VWC at this location. Due to 31 difficulties with instrument installation and instrument failure, we were not able to obtain a 32

reliable time series of soil VWC observations in the Lee field. Precipitation at both fields was
less than 150 mm over the course of the study, with irrigation providing more than 90% of the
water input (Table 2)

From tower establishment to the end of the study period, daily EC measured 4 evapotranspiration (ET<sub>EC</sub>) ranged from 1.6 to 5.5 mm day<sup>-1</sup>, with a mean of 3.2 mm day<sup>-1</sup>, in 5 Lee and 1.6 to 5.5mm day<sup>-1</sup>, with a mean 3.8 mm day<sup>-1</sup>, in Windy (Fig. 4).  $ET_{EC}$  showed 6 relatively little seasonal variation (<3 mm day<sup>-1</sup> from summer maxima to winter minima) and 7 greater day to day variations of 1-2 mm day<sup>-1</sup>. Cumulatively, mid-period ET<sub>EC</sub> was 158 mm 8 higher in Windy than in Lee (Fig. 5; Table 2). Factors contributing to higher  $ET_{FC}$  in Windy 9 10 include higher wind speed, slightly higher Rn, a higher mean air temperature, and lower mean daily relative humidity. However, maximum daily air temperature is higher near Lee than 11 Windy. Ground heat flux was minimal (<3% of Rn during daytime periods) at both sites 12 during the mid-period. 13

14 Ouality control checks on the EC data indicated no significant issues with ET measurements. 15 Energy closure varied significantly between the sites, with daily energy closure of the turbulent fluxes of 75% at Lee and 97% at Windy. As data processing and instrumentation 16 were identical between sites, the difference in energy closure is very likely due to the 17 differences in topography and turbulence between the two fields, particularly nighttime 18 turbulence (Anderson and Wang, 2014). Friction velocity at Windy rarely dropped below the 19 critical threshold (0.1 m s<sup>-1</sup>) at night (2.5% of the half hourly fluxes). Mean 90% footprint 20 lengths during the Study Period determined following Kljun et al. (2004) were 158 m in 21 22 Windy and 124 m in Lee, which indicate that our EC towers were observing the field of interest even during the rare periods (~7% of record) where we were observing in the short 23 fetch direction (Table 1) such as during Kona winds (winds from the south and west). During 24 the predominant trade wind flows (prevailing winds from the northeast), our fetch in both 25 fields was >200 m. 26

### 27 **3.3 Reference ET at EC tower sites**

Daily short  $(ET_0)$  and tall  $(ET_r)$  ASCE reference ET were significantly different between the two sites (Fig. 4). In Windy,  $ET_0$  ranged from 1.6 to 8.1 mm day<sup>-1</sup> over the study period with a mean of 5.2 mm day<sup>-1</sup> (5.1 mm day<sup>-1</sup> over the mid-period).  $ET_r$  ranged from 2.0 to 12.3 mm

day with a mean of 7.14 mm day<sup>-1</sup> (7.0 mm day<sup>-1</sup> for mid-period). For Lee,  $ET_0$  varied from

1 0.6 to 6.5 mm day<sup>-1</sup> with a mean of 4.0 mm day<sup>-1</sup> (3.9 mm day<sup>-1</sup> for mid-period). For  $ET_r$ , the 2 range was 0.8 to 8.6 mm day<sup>-1</sup> with a mean of 5.0 mm day<sup>-1</sup> (4.8 mm day<sup>-1</sup> mid-period). The 3 Priestley-Taylor ET ( $ET_{PT}$ ) showed less difference between the two fields. Mean  $ET_{PT}$  was 4 slightly higher at Windy (4.3 mm day<sup>-1</sup> and 4.1 mm day<sup>-1</sup> mid-period) than at Lee (4.0 mm 5 day<sup>-1</sup> and 3.8 mm day<sup>-1</sup> mid-period).

6 Over the course of the study, Windy's cumulative  $ET_0$  was 612 mm higher than in Lee, and cumulative ETr was 1032 mm higher (Fig. 5; Table 2). Similar to the daily values, cumulative 7 ET<sub>PT</sub> values were considerably closer, with Windy exceeding Lee by 237 mm. As expected, 8 the cumulative difference between reference equations and ET<sub>EC</sub> grew in the early portion of 9 10 the study period, prior to the mid-period (Fig. 5). During the mid-period, the difference between ET<sub>r</sub> and ET<sub>EC</sub> grew significantly larger in both EC fields. Windy also saw increasing 11 differences between ET<sub>0</sub>, ET<sub>PT</sub>, and ET<sub>EC</sub>, whereas in Lee cumulative ET<sub>0</sub> and ET<sub>PT</sub> tracked 12 quite closely with each other. 13

14 To further evaluate these discrepancies between reference and  $ET_{EC}$ , we calculated the 15 cumulative difference between the 3 reference ET equations and ET<sub>EC</sub> during the mid-period (Fig. 6). ET<sub>PT</sub> was the only equation with near zero cumulative difference for a substantial 16 amount of the mid-period for both fields; ET<sub>0</sub> was near 0 for the Lee field from October 2011 17 - February 2012 but not for the Windy field. Over the mid-period in Windy, the difference 18 between cumulative ET<sub>EC</sub> and ET<sub>PT</sub> ranged from -40 mm in March 2012 to 92 mm at the end 19 20 of the study period (August 2012) with cumulative differences of < 40 mm until July 2012. In Lee, the differences were greater, varying between -33 and 161 mm. The difference with  $ET_0$ 21 ranged from 0 (at beginning of mid-period) to 362 mm and 195 mm in Windy and Lee, 22 respectively. ET<sub>r</sub> showed the greatest cumulative differences of 854 and 443 mm in Windy 23 and Lee. 24

# 3.4 Bulk canopy resistances at EC towers, soil observations, and patterns in ET discrepancies

To examine the discrepancies between the ASCE equations  $(ET_0 \text{ and } ET_r)$ , the Priestley-Taylor equation  $(ET_{PT})$ , and measured  $ET_{EC}$ , we inverted the Penman-Monteith (PM) equation to calculate bulk canopy resistance  $(r_c)$  from  $ET_{EC}$  and  $ET_{PT}$  and compared the calculated  $r_c$  to the constant  $r_c$  used to calculate  $ET_0$  and  $ET_r$  during the mid-period. The ASCE parameterization to calculate atmospheric resistance  $(r_a)$  was used in the inverted PM

equation. Days with Available Energy (net radiation (Rn) - ground heat flux (G)) of < 5 MJ 1 day  $^{-1}$  were excluded because low radiation values would result in extreme  $r_c$  values and to 2 avoid including days with precipitation, which would bias the net radiation measurement of 3 the NR-Lite2. r<sub>c</sub> varied considerably between Windy and Lee for ET<sub>EC</sub>. For the mid-period, 4 mean (standard deviation) of daily  $r_c$  at Lee and Windy were 201 (47) s m<sup>-1</sup> and 145 (36) s m<sup>-1</sup> 5 <sup>1</sup>, respectively (Fig. 7). With respect to  $ET_{PT}$ , mean (standard deviation (STD)) of daily rc at 6 Lee and Windy during the mid-period were 146 (28) s m<sup>-1</sup> and 175 (42) s m<sup>-1</sup>, respectively 7 (Fig. 8). In all cases, mean  $r_c$  values were significantly higher (>75 s m<sup>-1</sup>) than the daily  $r_c$ 8 9 values used to parameterize the  $ET_0$  and  $ET_r$  equations.

10 We calculated daytime and nighttime r<sub>c</sub> to see if there was a systematic time of day difference between the fields and to examine if errors in daytime or nighttime parameterized r<sub>c</sub> were 11 disproportionally contributing to discrepancies in reference ET. Daily daytime and nighttime 12 r<sub>c</sub> were calculated for days that had at least 8 (daytime) and 4 (nighttime) non-gap filled half 13 hourly flux measurements. For these calculations, daytime was defined as  $Rn>50 \text{ Wm}^{-2}$  and 14 nighttime as  $Rn < -10 Wm^{-2}$ . We used this definition to avoid including periods with near zero 15 Rn that would blow up the inverted PM equation. Daily daytime and nighttime r<sub>c</sub> are shown in 16 Fig. 9. Nighttime r<sub>c</sub> shows greater difference between towers, with mean (standard deviation) 17 in Windy and Lee of 675 s m<sup>-1</sup> (289 s m<sup>-1</sup>) and 808 s m<sup>-1</sup> (445 s m<sup>-1</sup>) and substantially larger 18 absolute and relative standard deviation in r<sub>c</sub>. For both fields, daytime and nighttime r<sub>c</sub> was 19 larger than the ASCE r<sub>c</sub> parameterizations for almost all days. One other notable feature of the 20 21 resistance terms was the low atmospheric resistance (r<sub>a</sub>); in Windy and Lee, mean daily r<sub>a</sub> was 17.7 and 38.6 s  $m^{-1}$ , respectively, over the study period. 22

We evaluated the correlation between meteorological observations and discrepancies between 23 the ASCE tall reference ET equation  $(ET_r)$  and  $ET_{EC}$  to assess the importance of the advective 24 and radiation terms in the PM equation. The only parameter that was highly correlated to ET 25 discrepancy (ET<sub>r</sub>-ET<sub>EC</sub>) was Vapor Pressure Deficit (VPD) with a coefficient of determination 26  $(r^2)$  of 0.66 (Fig. 10a). VPD showed a much stronger correlation with ET discrepancy than 27  $ET_{EC}$  (r<sup>2</sup>=0.19) (Fig. 10b). Available Energy was moderately correlated with ET discrepancy 28  $(r^2=0.37)$  while all other tested parameters (daily minimum, mean and maximum wind speed 29 and temperature) had weak or no correlation with ET discrepancy ( $r^2 < 0.1$ ). 30

### 31 **3.5 Corrections to better parameterize sugarcane water use**

We attempted two corrections to the ASCE reference ET approach to better parameterize
 sugarcane water use. One was a climatological correction to the ET coefficient (K<sub>C-adj</sub>).
 Following the FAO-56 approach (Allen et al., 1998), an adjustment term (K<sub>adj</sub>) was calculated

4 
$$K_{adj} = 0.04 * (U_{2avg} - 2) - 0.004 * (RH_{avg} - 45) * h_{avg}^{0.3}$$
, (4)  
5  $K_{C-adj} = K_{C-FAO} + K_{adj}$ , (5)

In equations 4 and 5, K<sub>C-FAO</sub> is the literature mid canopy K<sub>C</sub> value, U<sub>2avg</sub> is mean location wind 6 speed (m s<sup>-1</sup>) at 2 m height,  $RH_{avg}$  is mean location relative humidity, and  $h_{avg}$  is average 7 8 vegetation height. For our study we used average wind speed, relative humidity, and vegetation height over the mid-period to calculate these parameters in the absence of longer 9 term climate data. The FAO-56 provides a range of mid-period K<sub>C</sub> values for sugarcane (1.25-10 1.40) for short reference ET. For adjustment, we chose the lowest end of the range (1.25) for 11 12 K<sub>C-FAO</sub> to enable the most conservative estimate of parameterized ET. The climatological K<sub>C</sub> adjustment (Kadi) had relatively little impact on calculated water use. In the Windy field, Kadi 13 14 was -0.0126 and in Lee K<sub>adj</sub> was -0.0359. For both fields, the wind adjustment offset the relative humidity/vegetation height adjustment as all 3 parameters were greater than zero. The 15 16 magnitude of the K<sub>adj</sub> term was insufficient to account for the observed discrepancies between reference ET and  $ET_{EC}$ . 17

The second correction was to parameterize the ASCE-PM equation with a custom, constant, 18  $r_{\rm c}.$  To estimate a  $r_{\rm c}$  value, an intermediate bulk canopy resistance of 165 s  $m^{-1}$  was used, which 19 was chosen as the weighted average of the r<sub>c</sub> calculated by inverting the ET<sub>PT</sub> at Windy and 20 Lee. We then ran the full form PM equation to calculate a new reference ET  $(ET_{r-cane})$ . 21 Cumulative differences between ET<sub>r-cane</sub> and ET<sub>EC</sub> are shown in Fig. 11 along with the 22 differences between  $ET_{PT}$  and  $ET_{EC}$ .  $ET_{r-cane}$  showed some improvements over  $ET_{PT}$  in 23 predicting measured ET between Oct 2011 - March 2012; in particular ET<sub>r-cane</sub> had less 24 underestimation of ET (15 to 27 mm improvement) in winter and spring for both fields and 25 had consistently better performance in the Lee field. ET<sub>r-cane</sub> had worse performance than ET<sub>PT</sub> 26 27 during the summer in the Windy field (40 mm). The minimum cumulative difference between ET<sub>r-cane</sub> and ET<sub>EC</sub> was -12 mm and -18 mm in Windy and Lee, respectively. The maximum 28 cumulative difference between  $ET_{r-cane}$  and  $ET_{EC}$  was 132 and 164 mm at the end of the study 29 30 period in Windy and Lee, respectively.

### 1 4. Discussion

## 4.1 Is Hawaiian sugarcane representative of a fully-transpiring reference ET surface?

Well-irrigated, full canopy, sugarcane has generally been reported to have an ET rate 1.1 to 4 1.4 times the ASCE/FAO-56 reference ET<sub>0</sub> equation (da Silva et al., 2012; Inman-Bamber and 5 McGlinchey, 2003), and rain-fed sugarcane has been reported to have an ET rate approaching 6 ET<sub>0</sub> (Cabral et al., 2012). Furthermore, a reference PM ET equation designed specifically for 7 sugarcane created by McGlinchey and Inman-Bamber (1996) has a bulk canopy resistance 8 that is slightly lower than the daily ASCE  $ET_r$  equation (40 s m<sup>-1</sup> vs. 45 s m<sup>-1</sup> for ASCE  $ET_r$ ). 9 Therefore, the significant overestimation of measured ET (ET<sub>EC</sub>) by the ET<sub>0</sub> and ET<sub>r</sub> 10 equations found in this study was quite surprising. Although Windy and Lee fields had slight 11 differences in planting dates, available soil water capacity, and fetch (Table 1), we do not 12 believe these account for the observed ET/reference ET differences between the fields. 13 Seasonal variation in temperature in Hawaii is guite small, wind speeds appeared to be 14 uncorrelated to seasonality. Wind fields in Central Maui are generally very strong, and our 15 separate calculations of reference ET using independent farm weather station observations 16 (Supplemental S1) and publicly available airport weather data from Kahului airport 17 (http://mesonet.agron.iastate.edu/request/download.phtml?network=HI ASOS - station ID 18 PHOG) show higher than typical values of reference ET for a tropical region. 19

The quality of Eddy Covariance observations was good, especially at the Windy tower where 20 high turbulence, flux footprints that were well within field boundaries, low proportion of time 21 22 periods requiring gap-filling, and excellent energy budget closure (H+LE was >95% of daily Rn-G) indicated that the methodological requirements of the Eddy Covariance method were 23 24 well satisfied (Anderson and Wang, 2014). At the Lee tower, Eddy Covariance measurements showed a more typical pattern with a larger number of gaps during still nighttime periods 25 26 when ET is low. Furthermore, seasonal and annual totals of ET have been shown to be 27 relatively insensitive to gap-filling methodologies (Alavi et al., 2006). Finally, while the gap 28 filling method of Reichstein et al., (2005) may systematically underestimate wet canopy evaporation due to exclusion of all EC periods during and immediately after rain, this bias is 29 30 likely to be insignificant at our sites due to the low precipitation (Table 2) and drip irrigation 31 that would minimize wetting of the leaves.

One hypothesis is that portions of the fields measured by our Eddy Covariance towers were 1 under significant water stress or had less than optimal cover, and thus were not representative 2 of a reference ET type surface. Uniformity of irrigation is a major concern with drip irrigation, 3 particularly with sub and near surface drip lines where root development can plug or pinch 4 5 drip lines, leading to insufficient irrigation (e.g. Soopramanien et al., 1990). At our field with higher ET (Windy), visible dry lines arising from pinched drip tubes appeared in parts of the 6 field at and after the end of the study period. However, there are multiple independent lines of 7 evidence against this hypothesis. 8

9 With respect to canopy cover, the TetraCam observations of cover (Fig. 2) show that 10 fractional cover remained above 80%, a threshold for the mid-period  $K_C$  (Carr and Knox, 11 2011; Inman-Bamber and McGlinchey, 2003). More evidence for full canopy comes from the 12 leaf area index (LAI) measurements made in July 2012 toward the end of the mid-period. In 13 both Lee and Windy, mean LAI (4.7 and 4.9) were slightly higher than the LAI (4.5) 14 parameterized in the ET<sub>r</sub> equation (Allen et al., 2005). These two types of data indicate that 15 incomplete cover is not an issue with our study sites.

Another possibility is that the sugarcane leaves are under significant water stress and thus are 16 transpiring at a lower rate. Four factors show that the sugarcane is unlikely to be water 17 stressed. First, porometer measurements from the July 2012 campaign of midday, sunlit, leaf 18 stomatal resistance were not significantly >100 s m<sup>-1</sup>. The 100 s m<sup>-1</sup> comes from the mean leaf 19 level stomatal resistance of a sunlit leaf on a well-watered plant as measured by Szeicz and 20 Long (1969) and which is used as a basis for scaling bulk canopy resistance in the ASCE and 21 22 FAO-56 approaches (Allen et al., 1998; 2005). Second, we compared the daily observed ET coefficient (K<sub>C</sub>) from the day immediately preceding a substantial irrigation or rain event 23 (defined as  $>8 \text{ mm day}^{-1}$ ) during the mid-period with daily K<sub>C</sub> 2 and 3 days after the irrigation 24 event using a paired t-test (n=106 in Windy and n=98 in Lee). We reasoned that stressed full 25 canopy sugarcane would respond to irrigation within 3 days, but that 3 days were short 26 enough to avoid confounding changes due to variations in field water budgets. Neither field 27 showed significantly greater daily ET<sub>EC</sub> following an irrigation during the mid-period (p>0.40 28 for all tests). Third, the soil volumetric water content (VWC) data from the Windy field 29 indicate relatively high soil moisture content; available soil water underneath the cane row in 30 the middle of the root zone always remained at >50% of available capacity. Windy's soils 31 were also near field capacity (and far above permanent wilting point) based on matric 32

potential at typical maximum and minimum soil VWC (Table 1). The VWC content also 1 argues against severe water stress that might persist after irrigation relieves the soil moisture 2 deficit; thus if the ASCE reference ET equations and coefficients were applicable to this 3 situation, we should see at least some days with  $ET_{EC}$  in the range of  $ET_0$  and  $ET_r$  (6-10 mm 4 day <sup>-1</sup> in Windy) when soil moisture was near or above field capacity. Fourth, measured 5 irrigation plus precipitation as recorded by the plantation was compared to measured 6 cumulative  $ET_{EC}$ , with cumulative mid-period irrigation and precipitation exceeding  $ET_{EC}$  by 7 342 mm in Windy (Table 2). At all times in the Windy field, cumulative  $ET_{EC}$  was 8 significantly less than irrigation plus precipitation. In Lee, by early January 2012, cumulative 9 precipitation and irrigation exceeded ET<sub>EC</sub>; by the end of the mid-period (July 2012), 10 cumulative irrigation and precipitation exceeded cumulative  $ET_{EC}$  by >500 mm (Table 2). In 11 summary, the evidence of full canopy and the lack of evidence of water stress indicated that 12 the mid-period sugarcane at our study fields should be fully transpiring. 13

# 4.2 Why do the standardized ASCE reference ET equations differ between similar sites?

16 Without clear evidence of water stress or lack of canopy cover over the study sites, we examine some explanations for the overestimation of the ASCE ET<sub>0</sub> and ET<sub>r</sub> compared to 17 ET<sub>EC</sub> and ET<sub>PT</sub>. Four hypotheses include (1) scaling of leaf level stomatal resistance to whole 18 canopy bulk resistance, (2) incorrect parameterization of daytime leaf level resistance, (3) 19 underestimation of nighttime bulk canopy resistance, and (4) underestimation of atmospheric 20 resistance. Scaling up leaf level resistance measurements has long been recognized as a major 21 challenge (Bailey and Davies, 1981; Furon et al., 2007; Sprintsin et al., 2012) due to 22 heterogeneity of environmental variables. The ASCE/FAO reference ET methods take a 23 single layer "big leaf" approach to scaling to convert non-stressed leaf resistances  $(r_s)$  into 24 whole canopy bulk resistances  $(r_c)$  by using an "effective LAI" where  $r_c$  is calculated by 25 dividing r<sub>s</sub> by effective LAI. ASCE assumes that effective LAI is equivalent to 0.5 times 26 27 measured LAI, which is assumed to be 2.9 for  $ET_0$  and 4.5 for  $ET_r$  thus resulting in effective LAIs of 1.4 and 2.3, respectively. Studies of well watered crops have found effective LAIs 28 29 which vary quite significantly from those assumed for the reference surface. Tolk et al. (1996) found an effective LAI of 1.3 for irrigated maize in Texas that was only 30% of maximum 30 measured LAI. Other studies (Alfieri et al., 2008; Mehrez et al., 1992) have assumed effective 31 LAI as a linear function of LAI, with effective LAI equaling 50% of LAI when LAI is 6. 32

1 Ultimately, the effective LAI concept is only a presumed distribution of leaves with differing  $r_s$  (Bailey and Davies, 1981); there is a possibility that the relatively unique production system 2 in our study fields results in a different, distinctive leaf distribution with a lower effective 3 LAI. Along with effective LAI, another leaf parameter that could be different is leaf level 4 5 resistance  $(r_s)$ . Although we did not find a highly significant difference between measured  $r_s$ and the  $r_s$  assumed in the ASCE parameterizations (100 s m<sup>-1</sup>), we were able to measure  $r_s$  in 6 only one field campaign during the mid-period, where r<sub>s</sub> observations were limited by clouds 7 and other logistical limitations. A large number of r<sub>s</sub> observations are needed to accurately 8 characterize r<sub>c</sub> (Denmead, 1984); more than we could feasibly measure during our field 9 campaign. We also note that other researchers (e.g. Zhang et al., 2008) have found non-10 stressed r<sub>s</sub> values greater than 100 s m<sup>-1</sup>. 11

Two other non-biological factors could help explain the discrepancy between ASCE reference 12 and mid-period  $ET_{EC}$ . One is nighttime r<sub>c</sub>. Both ASCE approaches assume a nighttime r<sub>c</sub> of 13 200 s m<sup>-1</sup>, which is based on measurements of damp soil beneath a grass lysimeter (Allen et 14 al., 2006). Measured nighttime  $r_c$  at our fields was significantly higher. We suspect that the 15 taller sugarcane canopy and substantial layer of trash and lodged cane minimizes bare soil 16 water evaporation, thus increasing nighttime r<sub>c</sub>. Oliver and Singels (2012) found significant 17 decrease in soil evaporation in sugarcane with surfaces covered by crop residue. Furthermore, 18 19 the minimal daytime ground heat flux (<5%) further reduces nighttime ET. Another factor is canopy energy storage that is considerable in high biomass systems (Anderson and Wang, 20 2014). Finally, we note that nighttime  $r_c$  is likely to be a locally-specific value; 200 s m<sup>-1</sup> is 21 too low for our study region, but it is too high for other regions with significant advection 22 23 (Evett et al., 2012).

Along with nighttime  $r_c$ , we examined the role of atmospheric resistance ( $r_a$ ) in parameterizing 24 ET, given the low observed mean  $r_a$  at Windy (<20 s m<sup>-1</sup>) and the demonstrated importance of 25 atmospheric resistance/conductance parameterizations in coastal tropical regions for accurate 26 ET parameterization (e.g. Holwerda et al., 2012). Given the canopy architecture of mid-period 27 sugarcane in our study fields, we were not certain about the equations that are commonly used 28 to parameterize zero plane displacement height and roughness lengths, which are also used in 29 the ASCE reference ET equations. To test the effect of r<sub>a</sub> uncertainty, a sensitivity analysis 30 was conducted. We used  $r_a$  that was 200% and 50% of the original  $r_a$  and recalculated  $r_c$  for 31 both EC towers.. In all cases, the new  $r_a$  changed the  $r_c$  values by <10 s m<sup>-1</sup>, with most  $r_c$ 32

1 values changed by <5 s m<sup>-1</sup>. These values are too small to explain the discrepancy between 2 observed and parameterized r<sub>c</sub>. The presence of r<sub>a</sub> in both the numerator and denominator of 3 the PM equation limits the impact of variation in r<sub>a</sub> on r<sub>c</sub>.

Finally, we note that the ASCE and FAO reference ET equations show varying sensitivity to 4 meteorological variables depending upon climate. Multiple studies have shown spatial, 5 6 seasonal, and interannual variation in the sensitivity of reference ET to meteorological inputs, with the most sensitive input (air temperature, wind velocity, relative humidity, etc.) changing 7 depending upon season and location (e.g. Bandyopadhyay et al., 2009; Estevez et al., 2009; 8 Gong et al., 2006; Huo et al., 2013; Irmak et al., 2006; Liang et al., 2008; Liu et al., 2014). 9 10 Irmak et al. (2006) and Estevez et al. (2009) found increased sensitivity to reference ET parameterization at locations with higher wind velocities in the United States and Spain, 11 respectively. Bandyopadhyay et al. (2009) and Huo et al. (2013) reported that decreased wind 12 velocities accounted for the largest proportion of decreased reference ET in climatically 13 differing regions in India and China. Across a large river basin in China (Chiang Jiang), Gong 14 et al. (2006) showed that sensitivities of reference ET to other meteorological variables (air 15 temperature and relative humidity) depended significantly on the spatial pattern of wind 16 17 sensitivity.

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## 5 Summary and Conclusion

We investigated discrepancies between two standardized reference ET equations and Eddy 20 Covariance measured ET at two field sites over irrigated sugarcane in Maui, Hawaii, USA. At 21 both fields, measured daily ET during the mid-period should have approached the tall 22 reference ET equation and exceeded the short reference ET equation. At both fields, both 23 ASCE reference ET equations significantly overestimated mid-period ET compared to Eddy 24 Covariance observations of ET. The Priestley-Taylor (PT) equation performed substantially 25 better at the Windy field than the short reference ET, while the short reference ET equation 26 27 and PT were more closely matched at the Lee field. We used a custom bulk canopy resistance derived from inverting PT ET; the custom cane reference ET equation had less seasonal 28 29 variation in ET discrepancy. Multiple, independent, field observations did not indicate insufficient canopy cover or plant water stress reducing ET<sub>EC</sub> significantly. 30

This study indicated nighttime bulk canopy resistance, leaf stomatal resistance, and effective leaf area index as possible causes for the discrepancy in bulk canopy resistance (and reference

ET estimates) between the ASCE reference equations and mid-period  $ET_{EC}$ . The higher bulk 1 canopy resistances and relationship between ET discrepancies and vapor pressure deficit 2 indicated that the ASCE equations overestimated the advective component of ET. Ultimately, 3 validation with field methods, including micrometeorology and water balance methods, is 4 5 needed to establish the accuracy of the ASCE equations in a region where they have not been tested previously. Adjusting the bulk canopy resistance to local climate to reduce the 6 advective component of ET may make the full ASCE Penman-Monteith equation a more 7 appropriate equation in this region. 8

The Priestley-Taylor (PT) equation performs better than  $ET_r$  or  $ET_0$  in our study region. The 9 10 PT equation likely provides a more robust estimation of reference ET in regions with high humidity. The simplicity of the PT equation also makes it attractive for use in larger scale 11 project planning as it has been parameterized in satellite-based ET models (e.g. Choi et al., 12 2011; Jin et al., 2011) and can be used in regions with a relative paucity of surface 13 meteorological data, unlike the ASCE/FAO equations that require near surface wind speed 14 and humidity data that are currently supplied by surface meteorological stations and which are 15 interpolated in satellite-based approaches (Allen et al., 2007; Hart et al., 2009). 16

The results illustrate the importance of careful use of reference evapotranspiration equations 17 and coefficients for assessing actual evapotranspiration in hydrologic applications. 18 Our finding of high bulk canopy resistance and low atmospheric resistance supports Widmoser's 19 20 (2009) recommendation into research on the canopy resistance/atmospheric resistance ratio. Many areas with changing hydrology (Elison Timm et al., 2011) and areas that currently and 21 which may soon use irrigation in previously non-irrigated fields (Baker et al., 2012; Salazar et 22 al., 2012) are outside of the semi-arid areas where reference evapotranspiration methods have 23 been primarily developed and tested. As such, it will be important to ensure that the 24 appropriate reference equation is used to parameterize evaporative demand. 25

26

### 27 Acknowledgements

Don Schukraft discussed previous meteorological investigations and observations at the farm.
Jim Gartung, ARS-Parlier, assisted with the establishment of the EC tower and TetraCam measurements. David Grantz provided insight on historical evaluation of ET data for Hawaiian sugarcane. Adel Youkhana, Neil Abranyi, Jason Drogowski and the farm crew assisted with data collection and field logistical support. This research was supported by

- 1 USDA-Agricultural Research Service, National Program 211: Water Availability and
- 2 Watershed Management and by the U.S. Navy, Office of Naval Research.

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Micrometeorological site information			
Field	Lee	Windy	
Latitude (°N)	20 784664	20 824633	
Longitude (°W)	156 403869	156 / 91278	
Flevation (m)	203	130.471270	
Date field planted	March 28, 2011	May 11 2011	
Date tower established	Inly 21, 2011	July 23, 2011	
Begin of mid-period (cover >80%)	November 3 2011	December 5, 2011	
End of analysis	July 26, 2012	August 27, 2012	
Natural Resource Conservation Service	Wajakoa very stony	Pulehu cobbly silt	
(NRCS) Soil Series	silty clay loam	loam	
Bulk Density <sup>3</sup> $(g/cm^3)$	1.22	1.35	
Porosity (%)	54	49	
Soil texture classification <sup>4</sup>	Clav	Sandy clay loam	
Soil texture - Sand (%)	31	51	
Soil texture - Silt (%)	15	16	
Soil texture – Clay (%)	54	33	
Soil volumetric water content (VWC) at	216	196	
saturation (mm/40 cm depth)			
Soil Water storage (Water content at 30%	60	72	
VWC-wilting point) (mm)			
Wilting Point (% VWC)	15	12	
Matric potential at 30% VWC (MPa)	NA <sup>5</sup>	-0.01	
Matric potential at 24% VWC (MPa)	NA	-0.033	
Field Size (ha)	99.1	62.6	
Field length (m) (predominant wind)	>500	415	
Field length (m) (shortest direction)	220	150	
Mean meteorological observations (August 1,	2011 – July 31, 2012)		
Mean daily air temperature (°C)	22.3	23.4	
Mean minimum daily air temperature (°C)	17.8	20.4	
Mean maximum daily air temperature (°C)	27.3	26.9	
Mean daily wind speed (m s <sup>-1</sup> )	2.0	4.6	
Mean daily net radiation (MJ m <sup>-2</sup> day <sup>-1</sup> )	10.7	11.3	
Mean daily relative humidity (%)	65	62	

Table 1: Eddy Covariance field site information. 1

<sup>&</sup>lt;sup>3</sup> All reported soil properties averaged/summed over the first 40 cm of soil depth.
<sup>4</sup> Soil texture was determined in the lab using the Hydrometer method.
<sup>5</sup> Matric potential not available for Lee because of extreme logistical difficulty in obtaining intact Tempe Cell samples at depth for determination of water retention characteristics.

- 1 Table 2: A summary of cumulative irrigation, rain, actual measured evapotranspiration- $ET_{EC}$ ,
- 2 and reference evapotranspiration values (ASCE short- $ET_0$  and tall- $ET_r$ , Priestley-Taylor- $ET_{PT}$ ,
- and a custom cane reference  $\text{ET-ET}_{r-\text{cane}}$ ) for the entire study period and the mid-period. All
- 4 values are in mm.

	Lee		Windy	
	Whole Study	Mid-Period	Whole Study	Mid-Period
Irrigation	1599	1348	1928	1221
Rain	58	58	140	122
ET <sub>EC</sub>	1191	843	1389	1001
$ET_0$	1487	1042	2099	1367
ET <sub>r</sub>	1828	1292	2861	1861
ET <sub>PT</sub>	1470	1008	1707	1096
ET <sub>r-cane</sub>	1317	947	1662	1128

## 1 Figure captions



- 2
- 3 Figure 1: a) True color image of the main Hawaiian Islands from the MODerate resolution
- 4 Imaging Spectroradiometer (250 m resolution image date: May 27, 2003). Study region is
- 5 outlined in red box. b) The Study Region on Central Maui showing the location of the Eddy
- 6 Covariance (EC) towers (Windy and Lee) used in this study. Image is false color Landsat 7
- 7 (30 m resolution image date: February 5, 2000).
- 8



2 Figure 2: Measured mean and standard deviation of fractional vegetation cover from

3 TetraCam for Windy and Lee fields.





Figure 3: Meteorological and soil observations during the study period: a) Mean daily air
temperature; b) mean 24 hour wind velocity; c) Cumulative daily net radiation; and d) soil
volumetric water content (VWC) data from Windy field at 20- cm depth underneath cane row
(45 cm away from drip line) and inter row or midway between drip lines (137 cm away from
drip line). Wilting point noted as solid red line (12% VWC).



1

2 Figure 4: Daily measured and reference ETs for EC tower fields from tower establishment

3 until the end of the study period for each field.



Figure 5: Cumulative measured and reference ET for Windy and Lee plotted against Days
after Planting (DAP). Shaded background indicates mid-period when ground canopy cover >
80%.



Figure 6: Cumulative difference between reference and measured ET since the beginning of
the mid-period in each EC tower field.





Figure 7: Calculated daily bulk canopy resistance at Windy and Lee from the EC towers for the mid-period. Dotted lines show daily time step resistances from short canopy  $(ET_0 - 70 \text{ s} \text{ m}^{-1})$  and tall canopy  $(ET_r - 50 \text{ s} \text{ m}^{-1})$  reference surfaces.





2 Figure 8: Calculated daily bulk canopy resistances at Windy and Lee from inverting the

- 3 Priestley-Taylor (PT) ET for the mid-period. Dotted lines again show daily time step
- 4 resistances from short and tall canopy for comparison.

5



Figure 9: Calculated mean nighttime and daytime bulk canopy resistances (following Fig. 6)
compared to assumed resistances.





2 Figure 10: a) Relationship between daily ET discrepancy  $(ET_r - ET_{EC})$  and daily Vapor

3 Pressure Deficit (VPD) from the beginning of the mid-period to the end of the study period.

4 Regression equation is fitted to entire pool of data from Lee and Windy. b) Relationship

5 between measured ET and daily VPD. Time period and regression approach are the same as in

6 a).





Figure 11: Cumulative difference between new reference ET (custom bulk canopy resistance
of 165 s m<sup>-1</sup>) and measured ET for both EC tower fields during the mid-period.