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Technical Note: On the Matt–Shuttleworth approach to estimate crop water requirements

J. P. Lhomme[1], **N. Boudhina**[2], **and M. M. Masmoudi**[2]

[1]IRD (UMR LISAH), 2 Place Viala, 34060 Montpellier, France
[2]INAT, 43 Avenue Charles Nicolle, 1082 Tunis, Tunisia

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Correspondence to: J. P. Lhomme (jean-paul.lhomme@ird.fr)

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Abstract

The Matt–Shuttleworth method provides a way to make a one-step estimate of crop water requirements with the Penman–Monteith equation by translating the crop coefficients, commonly available in FAO publications, into equivalent surface resistances. The methodology is based upon the theoretical relationship linking crop surface resistance to crop coefficient and involves the simplifying assumption that the reference crop evapotranspiration (ET_0) is equal to the Priestley–Taylor estimate with a fixed coefficient of 1.26. This assumption, used to eliminate the dependence of surface resistance on certain weather variables, is questionable: numerical simulations show that it can lead to substantial differences between the true value of surface resistance and its estimate. Consequently, the basic relationship between surface resistance and crop coefficient, without any assumption, appears to be more appropriate for inferring crop surface resistance, despite the interference of weather variables.

1 Introduction

The most common way of estimating crop water requirements, as recommended by the United Nations Food and Agriculture Organization (FAO) (Doorenbos and Pruitt, 1977; Allen et al., 1998), consists in the so-called "two-step" approach: first, a reference crop evapotranspiration (ET_0), defined under optimal conditions, is calculated from weather data measured at a reference height; second, evapotranspiration from any other well-watered crop (ET_c) is obtained by multiplying the reference evapotranspiration by an empirical crop coefficient K_c. The basic relationship writes

$$ET_c = K_c ET_0 \,. \tag{1}$$

The effect of weather conditions is supposed to be incorporated into ET_0 and the crop characteristics into K_c. The estimated values of crop coefficients exist in tabulated form and can be found in many FAO publications. Although the methods used to define and calculate ET_0 have changed along the years (Shuttleworth, 1993), FAO-56 (Allen et al., 1998) presently defines ET_0 as the daily evapotranspiration from "a hypothetical reference crop with an assumed crop height of 0.12 m, a fixed surface resistance $r_{s,0} = 70\,\mathrm{s\,m^{-1}}$ and an albedo of 0.23", calculated by means of the Penman–Monteith equation (Monteith, 1965)

$$ET_0 = \frac{\Delta A_0 + \rho c_p D_r / r_{a,0}}{\Delta + \gamma \left(1 + \frac{r_{s,0}}{r_{a,0}}\right)} . \quad (2)$$

$A_0 = R_{n,0} - G$ is the available energy of the reference crop ($R_{n,0}$: net radiation; G_0: soil heat flux); D_r is the water vapour pressure deficit at a reference height $z_r = 2$ m (screen height for weather data measurements); $r_{a,0}$ is the aerodynamic resistance calculated between the mean canopy source height and the reference height and the other parameters are defined in the nomenclature. It is specified that "the reference surface closely resembles an extensive surface of green grass of uniform height, actively growing, completely shading the ground and with adequate water". The "one-step" approach, as opposed to the "two-step" approach, consists in estimating crop evapotranspiration directly from a Penman–Monteith equation similar to Eq. (2), with the effective surface resistance of the crop used in replacement of the crop coefficient. Two main problems arise, however, in using the one-step method. First, several crops having a crop height close to (or greater than) the reference height of 2 m, a means should be designed to infer weather variables at a higher level than the reference height to be introduced in the Penman–Monteith equation. Second, the surface resistance is generally unknown for most of crops and should be determined, either experimentally or by calculation.

The Matt–Shuttleworth (M–S) approach (Shuttleworth, 2006) provides a response to both questions: it infers weather variables at a blending height higher than the screen height and it calculates crop surface resistance from FAO crop coefficient. These two steps are first summarized, stressing that the way the M–S approach infers crop surface resistance relies on a questionable assumption concerning the estimation of ET_0.

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Numerical simulations are carried out to prove that this assumption can be misleading. As a consequence, conclusions are drawn on the pertinence and reliability of the Matt–Shuttleworth one-step method.

2 Inferring weather variables at a higher level

In the Matt–Shuttleworth approach, the evapotranspiration from a given crop under standard conditions (i.e., unstressed vegetation, as defined in FAO-56), is expressed in the form of a Penman–Monteith equation, but with air characteristics taken at a blending height arbitrarily set at $z_b = 50\,\mathrm{m}$ (Shuttleworth, 2006, 2007)

$$\mathrm{ET_c} = \frac{\Delta A_c + \rho c_p D_b / r_{a,c}}{\Delta + \gamma \left(1 + \frac{r_{s,c}}{r_{a,c}}\right)} . \tag{3}$$

A_c is the available energy of the crop and $r_{s,c}$ is the crop surface resistance, which is unknown and should be determined. D_b is the water vapour pressure deficit at the blending height obtained by expressing $\mathrm{ET_0}$ in two different forms, with weather variables taken respectively at blending height z_b (= 50 m) and reference height z_r (= 2 m), and by assuming that there is no significant divergence of mass and energy fluxes between the reference height and the blending height (Shuttleworth, 2006)

$$\frac{\Delta A_0 + \rho c_p D_b / r_{a,0,b}}{\Delta + \gamma \left(1 + \frac{r_{s,0}}{r_{a,0,b}}\right)} = \frac{\Delta A_0 + \rho c_p D_r / r_{a,0}}{\Delta + \gamma \left(1 + \frac{r_{s,0}}{r_{a,0}}\right)} . \tag{4}$$

The resistance $r_{a,0,b}$ is the aerodynamic resistance between the reference crop and the blending height and Δ is calculated at the reference temperature T_r. Some mathematical manipulations of Eq. (4) lead to

$$D_b = \left(D_r + \frac{\Delta A_0 r_{a,0}}{\rho c_p}\right) \left[\frac{(\Delta + \gamma)\, r_{a,0,b} + \gamma r_{s,0}}{(\Delta + \gamma)\, r_{a,0} + \gamma r_{s,0}}\right] - \frac{\Delta A_0 r_{a,0,b}}{\rho c_p} . \tag{5}$$

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The crop aerodynamic resistance $r_{a,c}$ (see Eq. 16) is calculated from the wind speed at blending height (u_b), which is inferred from the one measured at reference height (u_r) assuming there is no divergence of momentum flux between these two heights

$$u_b = u_r \frac{\ln\left(\frac{z_b - d_0}{z_{0m,0}}\right)}{\ln\left(\frac{z_r - d_0}{z_{0m,0}}\right)}, \tag{6}$$

where d_0 is the zero plane displacement height of the reference crop and $z_{0m,0}$ its roughness length for momentum.

3 Inferring crop surface resistance from FAO crop coefficient

The evapotranspiration from any given crop $\mathrm{ET_c}$ (Eq. 3) can be expressed as a function of the reference evapotranspiration $\mathrm{ET_0}$ (Eq. 2) in the following way (Pereira et al., 1999, Eq. 25; Shuttleworth, 2006, Eq. 10)

$$\mathrm{ET_c} = \alpha_a \alpha_s ET_0, \tag{7}$$

where the coefficients α_a and α_s are given by

$$\alpha_a = \frac{\Delta f_c A_0 r_{a,c} + \rho c_p D_b}{\Delta A_0 r_{a,0} + \rho c_p D_r}, \tag{8}$$

$$\alpha_s = \frac{\left(1 + \Delta/\gamma\right) r_{a,0} + r_{s,0}}{\left(1 + \Delta/\gamma\right) r_{a,c} + r_{s,c}}. \tag{9}$$

The parameter $f_c = A_c/A_0$ allows for differences in available energy between the crop (A_c) and the reference crop (A_0). Comparing Eq. (7) with Eq. (1) leads to $K_c = \alpha_a \alpha_s$, from which the crop surface resistance can be inferred

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$$r_{s,c} = \frac{\alpha_a}{K_c}\left[\left(1+\frac{\Delta}{\gamma}\right) r_{a,0} + r_{s,0}\right] - \left(1+\frac{\Delta}{\gamma}\right) r_{a,c}\,. \tag{10}$$

The coefficient α_a can be rewritten in a different way by introducing the "equilibrium" resistance $r_{s,e}$ defined as (Pereira et al., 1999, Eq. 16)

$$r_{s,e} = \frac{\rho c_p}{\gamma}\frac{\Delta+\gamma}{\Delta}\frac{D_r}{A_0}\,, \tag{11}$$

which is slightly different from the "climatological" resistance (r_{clim}) used by Shuttleworth (2006) ($r_{s,e} = (1+\Delta/\gamma) r_{clim}$). Taking into account Eq. (5) and expressing α_a as a function of $r_{s,e}$ lead to

$$\alpha_a = (1+\Delta/\gamma)\,\frac{f_c r_{a,c} - r_{a,0,b}}{r_{s,e} + (1+\Delta/\gamma)\, r_{a,0}} + \frac{r_{s,0} + (1+\Delta/\gamma)\, r_{a,0,b}}{r_{s,0} + (1+\Delta/\gamma)\, r_{a,0}}\,. \tag{12}$$

The introduction of the equilibrium resistance $r_{s,e}$ into Eq. (12) allows the weather variables linked to radiation balance (A_0) and air moisture (D_r and D_b) to be encompassed into a unique parameter. Equation (10) constitutes the basic relationship linking crop surface resistance to crop coefficient. It shows that $r_{s,c}$ is not a unique function of K_c, but also depends on weather data: water vapour pressure deficit (D_r), net radiation (A_0), wind speed through the aerodynamic resistances ($r_{a,0}$, $r_{a,0,b}$ and $r_{a,c}$) and air temperature (T_r) through Δ. It is worthwhile noting that Eq. (10) is only valid under the standard climatic conditions used to derive the value of the crop coefficient. Consequently, the crop surface resistance $r_{s,c}$ should be first determined under the "fictitious" standard climatic conditions corresponding to the determination of crop coefficients and then introduced into Eq. (3) with the actual climatic conditions. The problem, however, is to define these "fictitious" or "preferred" weather conditions in order to estimate the most correct value of crop resistance through Eq. (10).

Shuttleworth (2006) eliminated the dependence of crop surface resistance on some weather variables by equating reference crop evapotranspiration ET_0 (Eq. 1) with the Priestley–Taylor estimate (Priestley and Taylor, 1972) expressed as

$$ET_{PT} = \alpha_{PT} \frac{\Delta A_0}{\Delta + \gamma} \text{ with } \alpha_{PT} = 1.26\,. \tag{13}$$

This assumption is supported by works on modeling experiments dealing with the daytime evolution of the atmospheric boundary-layer (de Bruin, 1983; McNaughton and Spriggs, 1989). It leads to

$$r_{s,e} = 1.26 r_{s,0} + 0.26 \left(1 + \frac{\Delta}{\gamma}\right) r_{a,0}\,. \tag{14}$$

By putting $ET_0 = ET_{PT}$ the Matt–Shuttleworth approach makes the equilibrium resistance a simple function of temperature (through Δ) and wind speed (through $r_{a,0}$). In this way, the relationship between crop surface resistance $r_{s,c}$ and crop coefficient K_c (Eq. 10) involves only wind speed through the three aerodynamic resistances ($r_{a,0}$, $r_{a,0,b}$ and $r_{a,c}$) and air temperature through Δ ($r_{s,0}$ being prescribed). The assumption ($ET_0 = ET_{PT}$) is questionable, however, because the effective value of the Priestley–Taylor coefficient depends upon the atmospheric conditions and can be fairly different from the preferred value of 1.26. For instance, Jensen et al. (1990) note that α_{PT} can be as high as 1.74 in arid conditions. This point is thoroughly discussed below using numerical simulations.

4 Basis of the numerical exploration

We examine hereafter whether the Matt–Shuttleworth assumption really holds and how the relationship between crop surface resistance and K_c depends on climatic conditions, assessing their impact on the determination of crop surface resistance. For this

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examination a different writing of the reference crop evapotranspiration is used. After some algebraic manipulations and introducing the equilibrium resistance $r_{s,e}$ defined by Eq. (11), the Penman–Monteith equation applied to the reference crop can be put in a form comparable to Eq. (13) (Pereira et al., 1999, Eq. 18):

$$\mathrm{ET}_0 = \alpha\left(\frac{\Delta A_0}{\Delta+\gamma}\right) \text{ with } \alpha = \frac{1+\frac{\gamma}{\Delta+\gamma}\frac{r_{s,e}}{r_{a,0}}}{1+\frac{\gamma}{\Delta+\gamma}\frac{r_{s,0}}{r_{a,0}}}. \tag{15}$$

This form of the Penman–Monteith equation allows exploring the effective value of the coefficient α compared to the preferred value of 1.26. It shows that the theoretical form of the Priestley–Taylor coefficient (α) is a complex function of the surface resistance ($r_{s,0}$) and of some weather variables involved in $r_{s,e}$ and $r_{a,0}$ (available energy, air humidity, temperature, wind speed). By setting its value at 1.26, the Matt–Shuttleworth assumption implicitly identifies specific atmosphere conditions, supposed to be the ones used to determine the crop coefficient.

In FAO-56 (Allen et al., 1998, p. 114), it is specified that the values of crop coefficients "represent those for a sub-humid climate with an average daytime minimum relative humidity ($\mathrm{RH}_{n,r}$) of about 45 % and with calm to moderate wind speeds (u_r) averaging $2\,\mathrm{m\,s^{-1}}$". When $\mathrm{RH}_{n,r}$ and u_r differ from 45 % and $2\,\mathrm{m\,s^{-1}}$ respectively, FAO-56 proposes an empirical equation (Allen et al., 1998, Eq. 62) to adjust the K_c value to the prevailing conditions. Nothing is said, however, about air temperature and incoming radiation. In the Matt–Shuttleworth approach, incoming radiation and air humidity are eliminated due to the assumption that $\mathrm{ET}_0 = \mathrm{ET}_{\mathrm{PT}}$ with $\alpha_{\mathrm{PT}} = 1.26$. In Shuttleworth (2006), a typical value of 15 °C was arbitrarily chosen for reference air temperature (T_r) with a wind speed of $2\,\mathrm{m\,s^{-1}}$, whereas in a study on irrigated crops in Australia, Shuttleworth and Wallace (2009) selected a value of 20 °C for air temperature.

Our simulation process makes use of the semi-empirical formulae given in FAO-56 (Allen et al., 1998) for the different parameters involved in the theoretical relationships described above. The three aerodynamic resistances ($r_{a,0}, r_{a,0,b}, r_{a,c}$) are calculated

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without stability corrections following the generic formula

$$r_a = \frac{\ln\left(\frac{z-d}{z_{0\,m}}\right)\ln\left(\frac{z-d}{z_{0\,h}}\right)}{k^2 u}, \tag{16}$$

where u is the wind speed a height z(z_r or z_b), d the zero plane displacement height, $z_{0\,m}$ the roughness length for momentum and $z_{0\,h}$ the roughness length for scalar (heat and water vapour). Aerodynamic parameters (for the reference crop and the given crop) are calculated as simple functions of crop height: $d = 0.67 z_h$, $z_{0\,m} = 0.123 z_h$ and $z_{0\,h} = z_{0\,m}/10$. The slope of the saturated vapour pressure curve (Δ) is a function of air temperature (Allen et al., 1998, Eq. 13). The psychrometric constant (γ) depends on atmospheric pressure and hence on elevation (Allen et al., 1998, Eqs. 8 and 7). Air density (ρ) is a function of atmospheric pressure and temperature (Allen et al., 1998, Eq. 3.5). Soil heat flux G_0 is generally neglected on a 24 h time step, which means that $A_0 \approx R_{n,0}$. The daily net radiation of the reference crop ($R_{n,0}$) is estimated following Allen et al. (1998, Eqs. 37, 38 and 39) from the measured or calculated solar radiation (R_s) and from the clear sky solar radiation ($R_{s,0}$), which is approximated by $R_{s,0} = (0.75 + 2 \times 10^{-5} z) R_a$ (Allen et al., 1998, Eq. 37), z (m) being the elevation a.s.l. and R_a the extraterrestrial solar radiation.

5 Results and discussion

Numerical explorations are carried out varying primarily air temperature and exploring different conditions of wind speed, air humidity and radiation. Following FAO-56 (Table 16 and Fig. 32), three types of climate shown in Table 1 are considered: they are defined as a function of their minimum ($RH_{n,r}$) and mean ($RH_{m,r}$) relative humidity at the reference height. Solar radiation is taken at sea level and assumed to be at its maximum value $R_{s,0}$ corresponding to a clear sky day: $R_s = R_{s,0} = 0.75 R_a$. In the lower latitudes of both hemispheres (below 40°), where irrigation is most needed,

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the range of value for the extraterrestrial radiation R_a is approximately between 30 and 40 $MJ\,m^{-2}\,day^{-1}$ during the growing season, which corresponds to R_s varying between 22.5 and 30 $MJ\,m^{-2}\,day^{-1}$. Additionally and for the sake of convenience, the ratio $f_c = A_c/A_0$ is set at 1 in all the simulations.

In Fig. 1 the coefficient α defined by Eq. (15) is plotted as a function of air temperature for different climatic conditions, extraterrestrial solar radiation (R_a) being set at a constant value of 35 $MJ\,m^{-2}\,day^{-1}$ (i.e., $R_s = R_{s,0} = 26.25\,MJ\,m^{-2}\,day^{-1}$). The value of α increases with the reference temperature, moderately for low wind speed and more significantly for higher wind speed. For the sub-humid climate (Fig. 1a) and a moderate wind speed (which correspond to the conditions under which the crop coefficients are supposedly derived), the value of α is much lower than the preferred value of 1.26 used in the Matt–Shuttleworth approach, whereas with the semi-arid climate α is closer to 1.26. Figure 1b shows that for a wide range of wind speed under a sub-humid climate the coefficient α is always below the 1.26 value. Therefore, the Matt–Shuttleworth assumption should be considered with much care: using a fixed value for α (1.26) is a way of hiding its complex dependence on weather conditions and can be truly misleading. As a consequence of this fixed value of α, the Matt–Shuttleworth estimate of the equilibrium resistance $r_{s,e}$ can be significantly greater than the true value for the current range of reference temperature (results not shown).

The influence of weather variables on the relationship between crop surface resistance $r_{s,c}$ and K_c, is investigated hereafter with and without the Matt–Shuttleworth assumption. A crop characterized by a crop coefficient $K_c = 1$ and a height $z_h = 1$ m is considered and the adjustment of crop coefficient to differing climate conditions is applied (Allen et al., 1998, Eq. 62). Figure 2 shows how the crop surface resistance varies as a function of reference temperature for different environmental conditions (semi-arid and sub-humid climates). For moderate wind speeds under sub-humid climate (Fig. 2a), the Matt–Shuttleworth assumption overestimates the crop resistance by around 30 $s\,m^{-1}$, whereas under semi-arid climate, the M–S estimate is much closer to the true value. For high wind speeds (Fig. 2b), the M–S assumption overestimates the true value of surface resistance in sub-humid climate, but underestimates it in semi-arid conditions. In Fig. 3 the same type of variation is presented for two different values of extraterrestrial solar radiation under sub-humid climate and moderate wind. The M–S approach systematically overestimates the true value of surface resistance and the higher the solar radiation, the greater the overestimation. These results show that there is a complex dependence of crop resistance on weather conditions, which is partially hidden with the Matt–Shuttleworth assumption. Consequently, it is certainly sounder to eliminate the assumption $\alpha = 1.26$ and to work directly with the basic relationship linking crop surface resistance and crop coefficient (i.e., Eqs. 10 and 12).

6 Conclusion

The relationship between crop surface resistance ($r_{s,c}$) and FAO crop coefficient (K_c) is not as straightforward as could be expected because of the interference of weather variables such as air temperature, solar radiation, wind speed and air humidity. It has been shown that the Matt–Shuttleworth assumption, which consists in the equality between reference crop evapotranspiration (ET_0) and the Priestley–Taylor estimate (ET_{PT} with $\alpha_{PT} = 1.26$), does not hold in most climatic conditions and can lead to substantial differences between the estimated and true value of surface resistance. Consequently, in order to infer the surface resistance of a given crop from its crop coefficient K_c, it seems preferable to use the theoretical relationship linking $r_{s,c}$ and K_c without any assumption (Eqs. 10 and 12) but with the most plausible weather conditions. Indeed, the weather conditions corresponding to a tropical crop (such as cassava, banana or millet) are certainly different from those corresponding to a temperate one (such as winter wheat or potato). We have to recognize, however, that the transformation of FAO crop coefficients into crop surface resistances is not an easy task, the interference of climatic conditions resulting in a large incertitude on the value of surface resistance.

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Table 1. Typical values of daily minimum relative humidity ($RH_{n,r}$) and its daily mean value ($RH_{m,r}$) for three types of climate (from FAO-56, Table 16).

Climatic classification	$RH_{n,r}$ (%)	$RH_{m,r}$ (%)
Semi-arid (SA)	30	55
Sub-humid (SH)	45	70
Humid (H)	70	85

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Table A1. Nomenclature

A_0	available energy of the reference crop ($\mathrm{W\,m^{-2}}$)
A_c	available energy of a given crop ($\mathrm{W\,m^{-2}}$)
c_p	specific heat of air at constant pressure ($\mathrm{J\,kg^{-1}\,K^{-1}}$)
D_r	water vapour pressure deficit at a reference height of 2 m (Pa)
D_b	water vapour pressure deficit at a blending height of 50 m (Pa)
d	zero plane displacement height of the crop (m)
ET_0	evapotranspiration from the reference crop ($\mathrm{W\,m^{-2}}$)
ET_c	evapotranspiration from a given crop under standard conditions ($\mathrm{W\,m^{-2}}$)
ET_{PT}	evaporation given by the Priestley–Taylor equation (Eq. 13) ($\mathrm{W\,m^{-2}}$)
f_c	ratio between crop available energy and that of the reference crop (dimensionless)
K_c	FAO crop coefficient defined by Eq. (1) (dimensionless)
k	von Karman's constant (dimensionless)
R_a	extraterrestrial solar radiation ($\mathrm{MJ\,m^{-2}\,day^{-1}}$)
$R_{s,0}$	clear sky solar radiation ($\mathrm{MJ\,m^{-2}\,day^{-1}}$)
R_s	incoming solar radiation ($\mathrm{MJ\,m^{-2}\,day^{-1}}$)
$\mathrm{RH}_{n,r}$	minimum relative humidity at reference height (%)
$\mathrm{RH}_{m,r}$	mean relative humidity at reference height (%)
$r_{a,0}$	aerodynamic resistance of the reference crop calculated up to the reference height z_r ($\mathrm{s\,m^{-1}}$)
$r_{a,0,b}$	aerodynamic resistance of the reference crop calculated up to the blending height z_b ($\mathrm{s\,m^{-1}}$)
$r_{a,c}$	aerodynamic resistance of a given crop calculated up to the blending height z_b ($\mathrm{s\,m^{-1}}$)
$r_{s,0}$	surface resistance of the reference crop $= 70\,\mathrm{s\,m^{-1}}$
$r_{s,c}$	surface resistance of a given crop under standard conditions ($\mathrm{s\,m^{-1}}$)
$r_{s,e}$	equilibrium resistance defined by Eq. (11) ($\mathrm{s\,m^{-1}}$)
T_r	air temperature at reference height (°C)
u_r	wind speed at reference height ($\mathrm{m\,s^{-1}}$)
u_b	wind speed at blending height ($\mathrm{m\,s^{-1}}$)
z_r	reference height = 2 m
z_b	blending height = 50 m
$z_{0\,m}$	roughness length for momentum of a given crop (m)
$z_{0\,h}$	roughness length for scalar of a given crop (m)
α	theoretical expression of the Priestley–Taylor coefficient (Eq. 15) (dimensionless)
α_{PT}	value of the Priestley–Taylor coefficient (= 1.26)
Δ	slope of the saturated vapour pressure curve ($\mathrm{Pa\,K^{-1}}$)
γ	psychrometric constant ($\mathrm{Pa\,K^{-1}}$)
ρ	air density ($\mathrm{kg\,m^{-3}}$)

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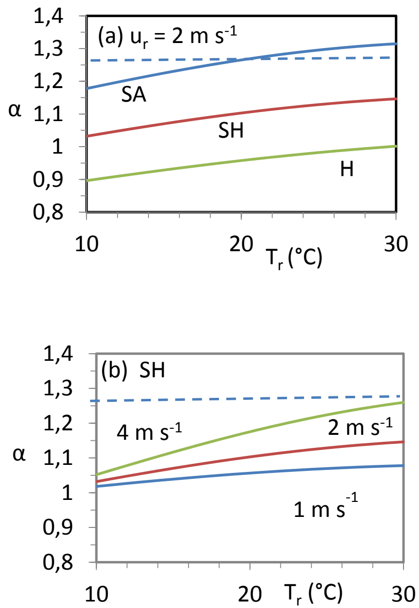

Fig. 1. Value of the coefficient α inferred from Eq. (15) as a function of air temperature at reference height, the straight dotted line representing the "preferred" value 1.26: **(a)** for different climatic conditions (see Table 1) with $u_r = 2\,\mathrm{m\,s^{-1}}$; **(b)** for different values of wind speed under sub-humid conditions (SH).

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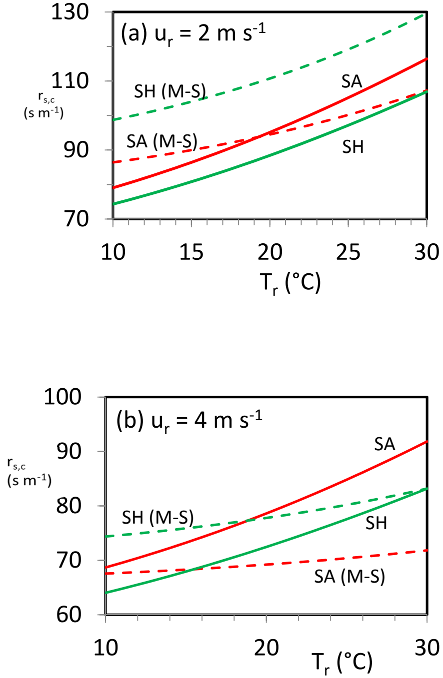

Fig. 2. For a crop with $K_c = 1$ and $z_h = 1$ m, variation of crop surface resistance as a function of air temperature for two climatic environments (SA: semi-arid, SH: sub-humid) and comparison with the Matt–Shuttleworth estimate (M–S) (dotted line): **(a)** wind speed $u_r = 2\,\mathrm{m\,s^{-1}}$; **(b)** $u_r = 4\,\mathrm{m\,s^{-1}}$.

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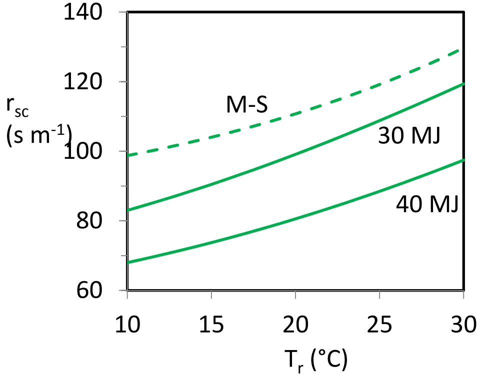

Fig. 3. For a crop with $K_c = 1$ and $z_h = 1$ m, under a sub-humid climate with $u_r = 2\,\mathrm{m\,s^{-1}}$, variation of crop surface resistance as a function of air temperature for two different values of extraterrestrial solar radiation (R_a) expressed in $\mathrm{MJ\,m^{-2}\,d^{-1}}$ (30 and 40) and comparison with the Matt–Shuttleworth estimate (M–S) (dotted line).

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