

1 **Shallow groundwater thermal sensitivity to climate change and land cover**  
2 **disturbances: derivation of analytical expressions and implications for stream**  
3 **temperature modelling**

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5 Barret L. Kurylyk<sup>1\*</sup>, Kerry T. B. MacQuarrie<sup>1</sup>, Daniel Caissie<sup>2</sup>, and Jeffrey M. McKenzie<sup>3</sup>

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7 <sup>1</sup>University of New Brunswick, Department of Civil Engineering and Canadian Rivers Institute,  
8 Fredericton, New Brunswick, Canada.

9  
10 <sup>2</sup>Fisheries and Oceans Canada, Gulf Fisheries Centre, Moncton, New Brunswick, Canada.

11  
12 <sup>3</sup>McGill University, Department of Earth and Planetary Sciences, McGill University, Montreal,  
13 Quebec, Canada.

14  
15 \*Now at: University of Calgary, Department of Geoscience, Calgary, Alberta, Canada

16  
17 Correspondence to: B.L. Kurylyk (barret.kurylyk@unb.ca).

18  
19 **Abstract**

20 Climate change is expected to increase stream temperatures, and the projected warming may  
21 alter the spatial extent of habitat for coldwater fish and other aquatic taxa. Recent studies have  
22 proposed that stream thermal sensitivities, derived from short term air temperature variations,  
23 can be employed to infer future stream warming due to long term climate change. However, this  
24 approach does not consider the potential for streambed heat fluxes to increase due to gradual  
25 warming of shallow groundwater. The temperature of shallow groundwater is particularly  
26 important for the thermal regimes of groundwater-dominated streams and rivers. Also, other  
27 recent stream temperature studies have investigated how land surface perturbations, such as  
28 wildfires or timber harvesting, can influence stream temperatures by changing surface heat  
29 fluxes, but these studies have typically not considered how these surface disturbances can also  
30 alter shallow groundwater temperatures and consequent streambed heat fluxes.

31 In this study, several analytical solutions to the one-dimensional unsteady advection-diffusion  
32 equation for subsurface heat transport are employed to estimate the timing and magnitude of  
33 groundwater warming due to seasonal and long term variability in land surface temperatures.

1 Groundwater thermal sensitivity formulae are proposed that accommodate different surface  
2 warming scenarios. The thermal sensitivity formulae suggest that shallow groundwater will  
3 likely warm in response to climate change and other surface perturbations, but the timing and  
4 magnitude of the warming depends on the rate of surface warming, subsurface thermal  
5 properties, bulk aquifer depth, and groundwater velocity. The results also emphasize the  
6 difference between the thermal sensitivity of shallow groundwater to short term (e.g., seasonal)  
7 and long term (e.g., multi-decadal) land surface temperature variability, and thus demonstrate the  
8 limitations of using short term air and water temperature records to project future stream  
9 warming. Suggestions are provided for implementing these formulae in stream temperature  
10 models to accommodate groundwater warming.

11 **Keywords:** groundwater temperature, subsurface warming, analytical solutions, deforestation,  
12 urbanization, river thermal sensitivity, wildfires, groundwater dependent ecosystems

### 13 **1. Introduction**

14 The ambient water temperature of streams and rivers is an important determinant of aquatic  
15 ecosystem health due to its influence on physicochemical conditions and the fact that many  
16 freshwater fish species can only tolerate a certain temperature range (Caissie 2006; Elliott and  
17 Elliott 2010; Hannah and Garner, 2015; Webb et al., 2008). Also, river thermal diversity  
18 enhances ecosystem complexity by providing thermally suitable habitat in reaches that would  
19 otherwise be uninhabitable for certain species (Cunjak et al. 2013, Ebersole et al. 2003; Kurylyk  
20 et al., 2015; Sutton et al., 2007). The thermal regimes of streams and rivers are controlled by  
21 energy fluxes across the water surface and the streambed (Fig. 1) as well as the internal structure  
22 of the stream or river network (Guenther et al., 2014; Hannah et al., 2004; Leach and Moore  
23 2011; Poole and Berman, 2001). The total streambed heat flux is composed of conductive and  
24 advective heat fluxes, which both depend on subsurface temperatures (Caissie et al., 2014;  
25 Moore et al., 2005; St-Hilaire et al., 2000).

26 Large rivers tend to be dominated by surface heat fluxes, but streambed advective heat fluxes  
27 induced by groundwater-surface water interactions can influence the thermal regimes of certain  
28 streams or rivers (Caissie, 2006). The significance of streambed advective heat fluxes generally  
29 varies spatially and temporally within a channel and depends on, among other things, the

1 groundwater discharge rate and the degree of shading (e.g., Brown and Hannah, 2008; Leach and  
2 Moore, 2011; Story et al., 2003). Due to the thermal inertia of the subsurface soil-water matrix,  
3 groundwater-dominated streams and rivers typically exhibit attenuated thermal responses to diel  
4 and seasonal variations in air temperature compared to surface runoff-dominated streams and  
5 rivers (Caissie et al., 2014; Constantz, 1998; Garner et al., 2014; O'Driscoll and DeWalle, 2006;  
6 Tague et al., 2007). Kelleher et al. (2012) defined the *thermal sensitivity* of a stream as the slope  
7 of the linear regression between air and water temperatures. These regressions are typically  
8 performed on temperature data collected for a period of at least one year and averaged on a daily,  
9 weekly, or monthly basis. The stream thermal sensitivity is thus a measure of the short term (e.g.,  
10 seasonal) change in water temperature in response to a short term change in air temperature  
11 (Kelleher et al., 2012; Mayer 2012).

12 Many studies have addressed the response of river and stream thermal regimes to climate change  
13 (e.g., Isaak et al., 2012; Luce et al., 2014; MacDonald et al., 2014; van Vliet et al., 2011),  
14 deforestation for land development and/or timber harvesting (e.g., Janisch et al., 2012; Moore et  
15 al., 2005; Studinski et al., 2012), and wildfires (e.g., Hitt, 2003; Isaak et al., 2010; Wagner et al.,  
16 2014). Several very recent studies have proposed that the empirical relationship (e.g., linear  
17 regression) between seasonal records of air and stream temperatures can be applied to estimate  
18 long term stream warming due to future climate change (e.g., Caldwell et al., 2014a; Gu et al.,  
19 2014; Hilderbrand et al., 2014; Trumbo et al., 2014).

20 Because groundwater temperature exhibits less seasonal variability than surface water  
21 temperature, it is not surprising that extrapolated stream thermal sensitivities obtained from short  
22 term temperature data will typically indicate that the temperature of groundwater-dominated  
23 streams will be relatively insensitive to climate change. As noted by Johnson (2003), care should  
24 be taken when using air temperature correlations to explain stream temperature dynamics, as air  
25 temperature is not the dominant controlling factor in stream temperature dynamics. Rather, the  
26 high correlation between stream and air temperature arises because both variables are influenced  
27 by incoming solar radiation, the primary driver of stream temperatures (Allan and Castillo,  
28 2007). The approach of using short term stream thermal sensitivities to estimate multi-decadal  
29 stream warming essentially employs future air temperature as a surrogate for future stream  
30 surface heat fluxes (Gu et al., 2014; Johnson et al., 2014; Mohseni and Stefan 1999), but it

1 ignores changes to streambed heat fluxes due to groundwater warming. Thus, the short term  
2 relationship between air and water temperatures is not necessarily representative of the  
3 concomitant warming of the lower atmosphere and surface water bodies on inter-annual or multi-  
4 decadal time scales (Arismendi et al., 2014; Bal et al., 2014; Luce et al., 2014).

5 Furthermore, many studies have investigated the response of stream thermal regimes to land  
6 surface perturbations, such as wildfires and deforestations, for the first few years following the  
7 disturbance. However, very few studies have considered how these perturbations could increase  
8 the temperature of groundwater discharge to these streams and thereby produce enhanced or  
9 sustained stream warming. In general, the common approach of ignoring future increases in  
10 groundwater temperature and streambed heat fluxes in stream temperature models may  
11 underestimate future stream warming and associated environmental impacts (e.g., habitat loss for  
12 coldwater fish, Snyder et al., 2015).

13 There is increasing evidence that the thermal regimes of shallow aquifers are sensitive to climate  
14 change, permanent deforestation, and wildfires. Observed shallow groundwater temperature  
15 warming has already been related to recent trends in air temperature (an indicator of climate  
16 change) in Taiwan (Chen et al., 2011), Switzerland (Figura et al., 2011; 2014) and Germany  
17 (Menberg et al., 2014). Empirical and process-based models of energy transport in shallow  
18 aquifers have been used to suggest that future climate change will continue to warm shallow  
19 groundwater bodies (e.g., Gunawardhana and Kazama, 2011; Kurylyk et al., 2013, 2014a; Taylor  
20 and Stefan, 2009) as reviewed in detail by Kurylyk et al. (2014b). Previous studies have also  
21 noted groundwater warming in response to deforestation due to the removal of the forest canopy  
22 (e.g., Alexander, 2006; Guenther et al., 2014; Henriksen and Kirkhusmo, 2000; Steeves, 2004;  
23 Taniguchi et al., 1998). Others have observed subsurface warming following wildfires. Burn  
24 (1998) found that the mean annual surface temperature at a burned site in southern Yukon,  
25 Canada was 0.6°C warmer than the surrounding surface thermal regime, and this surface thermal  
26 perturbation rapidly warmed shallow subsurface temperatures.

27 In all cases (i.e., climate change, deforestation, and wildfires), the surface disturbance warms  
28 shallow aquifers by increasing the downward heat flux from the warming land surface. For  
29 example, climate change can influence surface thermal regimes and subsurface heat fluxes by  
30 altering convective energy fluxes from the lower atmosphere and causing increased net radiation

1 at the ground surface (Jungqvist et al., 2014; Kurylyk et al., 2013; Mellander et al., 2007). The  
2 influence of wildfires or forest harvesting on surface thermal regimes can be complex. The  
3 removal of the forest canopy can decrease transpiration and thus increase the energy available to  
4 warm the land surface (Rouse, 1976). Lewis and Wang (1998) demonstrated that the majority of  
5 surface and subsurface warming caused by wildfires at sites in British Columbia and Yukon,  
6 Canada could be attributed to decreased transpiration. Decreased surface albedo and consequent  
7 increased net radiation at the land surface can also arise due to wildfires (Yoshikawa et al.,  
8 2003). The increase in surface temperature as a result of a land cover disturbance will depend on  
9 the original vegetative state, climate, ground ice conditions, and potential for vegetative regrowth  
10 (Liljedahl et al., 2007). In the case of a wildfire or in post-harvest tree planting, the vegetation  
11 may eventually regenerate, and the surface energy balance and temperature return to the pre-fire  
12 conditions (Burn, 1998).

13 Kurylyk et al. (2013, 2014a) demonstrated that shallow groundwater warming may eventually  
14 exceed the magnitude of surface water warming and thus stream temperature models that do not  
15 consider this phenomenon may be overly conservative. The empirical method proposed by  
16 Kurylyk et al. (2013) for estimating the magnitude of groundwater warming requires measured  
17 land surface and depth-dependent groundwater temperature for model calibration, but there is  
18 often a paucity of such temperature data available at the catchment scale. Also, the numerical  
19 modeling described by Kurylyk et al. (2014a) is time intensive and requires considerable data for  
20 model parameterization. These previous approaches for quantifying groundwater warming are  
21 site specific, and thus the results are not generally transferable to existing models that are used to  
22 investigate stream thermal regimes.

23 The intent of this contribution is to provide alternative, parsimonious approaches for  
24 investigating factors that influence the timing and magnitude of groundwater temperature  
25 changes in response to climate change or land cover disturbances. The specific objectives of this  
26 paper are twofold:

- 27 1. Derive easy-to-use formulae to estimate the thermal sensitivity of groundwater to  
28 different surface temperature changes (e.g., seasonal cycle or multi-decadal increases).

1        2. Demonstrate how these formulae can be utilised to estimate how the groundwater thermal  
2            sensitivity in idealized environments is influenced by the depth, groundwater recharge  
3            rate, and subsurface thermal properties.

4        The illustrative examples (Objective 2) will also be used to demonstrate the difference in the  
5        subsurface thermal response to short term (seasonal) and long term (multi-decadal) surface  
6        temperature trends. Consequently, the results will be employed to highlight the limitations of  
7        employing empirical stream temperature models with constant coefficients obtained from short-  
8        term temperature records to project future stream warming. The results will also be used to  
9        describe how stream temperature models can be improved to accommodate groundwater  
10        warming using these simple approaches.

## 11    **2. Methods**

12        There are several approaches for estimating future groundwater temperature warming in  
13        response to changes in land cover or climate. It is well known that mean annual ground surface  
14        temperature and shallow groundwater temperature are approximately equal to mean annual air  
15        temperature plus some thermal offset (e.g., 1-4°C) due to the insulating effect of snow (Zhang,  
16        2005). Meisner (1988) employed this knowledge to estimate future groundwater temperatures by  
17        adding a thermal offset to projections of future mean annual air temperature. The approach  
18        employed by Meisner (1988) utilized mean annual surface temperature as a proxy for  
19        groundwater temperature and thus implicitly assumed that the aquifer and surface are always in  
20        thermal equilibrium. The equilibrium assumption was also invoked in the empirical function  
21        employed by Kurylyk et al. (2013). Such an approach does not consider the lag that occurs  
22        between an increase in surface temperature and its subsequent realization at some depth within  
23        the subsurface (Lesperance et al., 2010) and thus is only valid for very shallow groundwater  
24        (e.g., <5 m) or for long time scales.

25        Analytical solutions to subsurface heat transfer differential equations can also be applied to  
26        estimate the influence of future climate change on groundwater temperature (Gunawardhana and  
27        Kazama, 2011; Kurylyk and MacQuarrie, 2014; Menberg et al., 2014), although these  
28        approaches have most often been applied for deeper aquifers. Finally, numerical models of  
29        groundwater flow and coupled heat transport can be applied to investigate the thermal evolution

1 of aquifers due to warming surface temperatures (e.g., Gunawardhana and Kazama, 2012;  
2 Kurylyk et al., 2014a). These numerical models are more flexible and can accommodate multi-  
3 dimensional groundwater flow and heat transport and inhomogeneities in subsurface thermal  
4 properties, but they require extensive subsurface field data for model parameterization.

5 Herein, we employ analytical solutions to a one-dimensional, unsteady heat transport equation to  
6 estimate subsurface temperature evolution due to climate change, permanent land cover changes,  
7 and wildfires. These solutions are physically based and account for the lag in the thermal  
8 response of groundwater to surface temperature changes. Also, unlike the solution employed by  
9 Taylor and Stefan (2009), these solutions accommodate the subsurface thermal effects of  
10 vertically moving groundwater. The solutions provide an indication of expected groundwater  
11 warming due to climate or land cover changes, and the results can be incorporated into stream  
12 temperature models in the absence of site-specific hydrogeological modeling. These simple  
13 analytical solutions are particularly useful for performing parsimonious analyses when there is a  
14 paucity of subsurface data (e.g., hydraulic conductivity distribution) for parameterizing  
15 groundwater flow and energy transport models. Also, analytical solutions limit the degrees of  
16 freedom for a particular analysis and thus facilitate a comprehensive evaluation of possible  
17 interactions between model inputs and resultant solutions. As we demonstrate, the forms of these  
18 solutions can also be utilized to derive mathematical expressions for groundwater thermal  
19 sensitivity to surface temperature perturbations. The analytical solutions discussed in this paper  
20 invoke assumptions, and the limitations arising from these assumptions will be discussed later.

## 21 **2.1 Advection-diffusion heat transport equation**

22 Shallow subsurface heat transfer occurs primarily due to heat conduction and heat advection  
23 (Domenico and Schwartz, 1990), although the latent heat released or absorbed during pore water  
24 freeze-thaw can also be important in cold regions (Kurylyk et al., 2014b). The one-dimensional,  
25 transient conduction-advection equation for subsurface heat transport is (Stallman, 1963):

$$26 \quad \lambda \frac{\partial^2 T}{\partial z^2} - qc_w \rho_w \frac{\partial T}{\partial z} = c\rho \frac{\partial T}{\partial t} \quad (1)$$

27 where  $\lambda$  is the bulk thermal conductivity of the soil-water matrix ( $\text{W m}^{-1} \text{ }^\circ\text{C}^{-1}$ ),  $T$  is the  
28 temperature at any point in space or time ( $^\circ\text{C}$ ),  $z$  is the depth below the surface (m, down is

1 positive and the land surface occurs at  $z = 0$ ),  $q$  is the vertical Darcy flux ( $\text{m s}^{-1}$ , down is  
 2 positive),  $c_w \rho_w$  is the volumetric heat capacity of pure water ( $4.18 \times 10^6 \text{ J m}^{-3} \text{ }^\circ\text{C}^{-1}$ ; Bonan, 2008),  
 3  $t$  is time (s), and  $c\rho$  is the bulk volumetric heat capacity of the soil-water matrix ( $\text{J m}^{-3} \text{ }^\circ\text{C}^{-1}$ ). The  
 4 first term on the left of Eq. (1) represents the divergence of the conductive flux, the second term  
 5 on the left represents the divergence of the advective flux, and the term on the right represents  
 6 the rate of change of thermal storage. Subsurface heat transport phenomena and the physical  
 7 meaning of the terms in Eq. (1) are reviewed in more detail by Rau et al. (2014) and Kurylyk et  
 8 al. (2014b).

9 Equation (1) is often rewritten in the form (Carslaw and Jaeger, 1959):

$$10 \quad D \frac{\partial^2 T}{\partial z^2} - U \frac{\partial T}{\partial z} = \frac{\partial T}{\partial t} \quad (2)$$

11 where  $D$  is the bulk thermal diffusivity (thermal conductivity divided by heat capacity) of the  
 12 soil-water matrix ( $\text{m}^2 \text{ s}^{-1}$ ), and  $U$  is the velocity of a thermal plume due only to heat advection  
 13 ( $\text{m s}^{-1}$ ). Even in the absence of conduction, the thermal plume will not migrate at the same rate as  
 14 the Darcy velocity due to differences in the heat capacities of water and the medium (Markle and  
 15 Schincariol, 2007; Luce et al., 2013). An expression for  $U$  can be obtained via a comparison of  
 16 Eqs. (1) and (2):

$$17 \quad U = q \frac{c_w \rho_w}{c\rho} \quad (3)$$

18 Often an effective thermal diffusivity term, which accounts for the combined thermal  
 19 homogenizing effects of heat diffusion and heat dispersion, is utilized in place of the bulk  
 20 thermal diffusivity term  $D$  in Eq. (2). However, it is still common to ignore the subsurface  
 21 thermal effects of dispersion, which are often minimal in comparison to heat conduction  
 22 (Kurylyk et al., 2014b; Rau et al., 2014). Equation (2) represents vertical subsurface heat  
 23 transport processes and accounts for the thermal effects of heat conduction induced by a thermal  
 24 gradient and heat advection induced by groundwater flow. Analytical solutions to this equation  
 25 can be developed and applied to consider inter-relationships between groundwater flow, surface  
 26 temperature changes, and subsurface thermal regimes. We consider four analytical solutions to



1 Eq. (2) (Table 1) that vary based on the nature of the surface boundary condition. These are  
 2 discussed in subsequent sections.

### 3 **2.2 Analytical solution 1: Harmonic surface temperature changes**

4 The diel or seasonal land surface temperature cycle can be approximated with a harmonic  
 5 function. Suzuki (1960) derived an analytical solution to Eq. (2) subject to a sinusoidal surface  
 6 temperature boundary condition:

$$7 \quad \text{Boundary condition: } T(z = 0, t) = T_m + A \sin\left(\frac{2\pi t}{p} - \phi\right) \quad (4)$$

$$8 \quad \text{Solution: } T(z, t) = T_m + A \exp(-dz) \sin\left(\frac{2\pi t}{p} - \phi - Lz\right) \quad (5)$$

9 where  $A$  is the amplitude of the harmonic surface temperature cycle ( $^{\circ}\text{C}$ ),  $T_m$  is the mean surface  
 10 temperature ( $^{\circ}\text{C}$ ),  $p$  is the period of the surface temperature cycle (s),  $\phi$  is a phase shift to align  
 11 the timing of the surface temperature signal with the sinusoid (rad),  $d$  is a thermal damping term  
 12 ( $\text{m}^{-1}$ ), and  $L$  is a lag term ( $\text{m}^{-1}$ ). Eq. (5) thus states that the harmonic temperature signal at the  
 13 surface retains its period within the subsurface but is exponentially damped and linearly lagged  
 14 with depth. Stallman (1965) demonstrated that the exact expressions for  $d$  and  $L$  are:

$$15 \quad d = \left[ \left\{ \left( \frac{\pi}{Dp} \right)^2 + 0.25 \left( \frac{U}{2D} \right)^4 \right\}^{0.5} + 0.5 \left( \frac{U}{2D} \right)^2 \right] - \frac{U}{2D} \quad (6)$$

$$16 \quad L = \left[ \left\{ \left( \frac{\pi}{Dp} \right)^2 + 0.25 \left( \frac{U}{2D} \right)^4 \right\}^{0.5} - 0.5 \left( \frac{U}{2D} \right)^2 \right] \quad (7)$$

17 Equations (5) to (7) are generally collectively referred to as Stallman's equation. No initial  
 18 conditions are presented for Stallman's (1965) solution as it assumes that the boundary condition  
 19 has been repeating the harmonic cycle indefinitely. This solution also depends on a lower  
 20 boundary condition ( $T = T_m$ ) at infinite depth. Various forms of this solution have been  
 21 applied/inverted to infer rates of groundwater flow due to subsurface temperature-time series

1 arising from daily or seasonal harmonic variations in surface temperature (e.g., Anderson, 2005;  
 2 Hatch et al., 2006; Rau et al., 2014). Here, we employ Stallman’s (1965) solution in a forward  
 3 manner to demonstrate why seasonal changes in air and surface temperature are not manifested  
 4 in subsurface thermal regimes below certain depths, and thus why groundwater dominated  
 5 streams and rivers exhibit low thermal sensitivity to seasonal weather variability. In particular,  
 6 we consider the ratio of the amplitude of the seasonal groundwater temperature cycle at any  
 7 arbitrary depth to the amplitude of the surface temperature boundary condition. This  
 8 dimensionless parameter, herein referred to as the exponential damping factor  $\Omega$ , can be obtained  
 9 from Eqs. (4) and (5):

$$10 \quad \Omega = \frac{\text{Amplitude at depth} = z}{\text{Amplitude at depth} = 0} = \frac{A \exp(-dz)}{A} = \exp(-dz) \quad (8)$$

11 **2.3 Analytical solution 2: Step change(s) in surface temperature due to land cover**  
 12 **disturbances**

13 Taniguchi et al. (1999a) demonstrated how an analytical solution presented by Carslaw and  
 14 Jaeger (1959) could be modified to calculate the groundwater temperature warming arising from  
 15 a sudden and permanent increase in surface temperature. This increase in surface temperature  
 16 could arise due to rapid and large scale timber harvesting or changes in land use. Menberg et al.  
 17 (2014) proposed that superposition principles could be employed to modify the solution by  
 18 Taniguchi et al. (1999a) by considering a series of shifts in the surface temperature boundary  
 19 condition. Herein we employ the technique by Menberg et al. (2014) and consider up to two  
 20 sequential shifts in the boundary condition. The first shift, which warms the surface temperature,  
 21 occurs at  $t = 0$ , and after a period of time ( $t = t_1$ ), the surface temperature returns to its value prior  
 22 to the initial warming ( $T_0$ ). Such a boundary condition could approximate the sudden temporary  
 23 increase in mean annual surface temperature due to a wildfire and the subsequent return to pre-  
 24 fire surface temperatures due to vegetation regrowth (Burn, 1998). Alternatively, this boundary  
 25 condition could represent the effect of clearcutting followed by industrial tree planting. The  
 26 subsequent surface cooling due to gradual vegetative regrowth could also be represented with a  
 27 series of shorter less intense cooling phases, but for the illustrative examples in the present study  
 28 we assume one warming shift followed by one cooling shift of equal magnitude:

1 Initial conditions:  $T(z, t = 0) = T_0$  (9)

2 Boundary condition:  $T(z = 0, t) = \begin{cases} T_0 + \Delta T & \text{for } 0 < t < t_1 \\ T_0 & \text{for } t \geq t_1 \end{cases}$  (10)

3 Solution:  $T(z, t) = \begin{cases} T_0 + \frac{\Delta T}{2} \left\{ \operatorname{erfc}\left(\frac{z-Ut}{2\sqrt{Dt}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+Ut}{2\sqrt{Dt}}\right) \right\} & \text{for } 0 \leq t < t_1 \\ T_0 + \frac{\Delta T}{2} \left\{ \operatorname{erfc}\left(\frac{z-Ut}{2\sqrt{Dt}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+Ut}{2\sqrt{Dt}}\right) \right\} \\ - \frac{\Delta T}{2} \left\{ \operatorname{erfc}\left(\frac{z-U(t-t_1)}{2\sqrt{D(t-t_1)}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+U(t-t_1)}{2\sqrt{D(t-t_1)}}\right) \right\} & \text{for } t \geq t_1 \end{cases}$  (11)

4 where  $T_0$  is the uniform initial temperature ( $^{\circ}\text{C}$ ),  $\Delta T$  is the magnitude of the surface temperature  
 5 shift ( $^{\circ}\text{C}$ ),  $\operatorname{erfc}$  is the complementary error function, and  $t_1$  is the duration of the period  
 6 characterized by warmer surface temperatures (s).

7 This solution and the remaining three solutions presented below also require a lower boundary  
 8 condition at infinite depth ( $T=T_0$ ). Equation (11) can be employed to consider the subsurface  
 9 warming due to a permanent step change in surface temperature (i.e., no subsequent cooling due  
 10 to vegetative regrowth) by setting  $t_1$  to infinity. In this case, only the first line on the right hand  
 11 side of Eq. (11) is retained. Even when  $t_1$  is set to infinity, Eq. (11) differs slightly from the  
 12 solution presented by Taniguchi et al. (1999a) because uniform initial temperatures are assumed  
 13 in the present study (Eq. 9). These initial conditions ignore the influence of the geothermal  
 14 gradient and imply that the recent climate has been relatively stable. We employ these  
 15 simplifying assumptions given that we are primarily interested in shallower depths (e.g.,  $< 25$  m)  
 16 where the influence of the geothermal gradient is not significant. Also, the boundary conditions  
 17 for this solution and the solutions below do not accommodate seasonally varying surface  
 18 temperatures, thus these solutions are valid for predicting the evolution of mean annual  
 19 groundwater temperature.

20

1 **2.4 Analytical solution 3: Linear increase in surface temperature due to climate change**

2 Carslaw and Jaeger (1959) also presented an analytical solution to Eq. (2) subject to linearly  
3 increasing surface temperature. This solution was later adapted by Taniguchi et al. (1999b) and  
4 applied to study groundwater temperature evolution due to climate change. Herein, the analytical  
5 solution is presented in a slightly simpler form as thermally uniform initial conditions are  
6 assumed (i.e., initial conditions are given by Eq. 9):

7 
$$\text{Boundary condition: } T(z = 0, t) = T_0 + \beta t \quad (12)$$

8 
$$\text{Solution: } T(z, t) = T_0 + \frac{\beta}{2U} \left[ (Ut - z) \times \operatorname{erfc} \left( \frac{z - Ut}{2\sqrt{Dt}} \right) + (Ut + z) \exp \left( \frac{Uz}{D} \right) \operatorname{erfc} \left( \frac{z + Ut}{2\sqrt{Dt}} \right) \right] \quad (13)$$

9 where  $\beta$  is the rate of the increase in surface temperature ( $^{\circ}\text{C s}^{-1}$ ).

10 Equation (13) has been applied in an inverse manner to consider the complex relationships  
11 between past surface temperature changes, groundwater flow, and measured subsurface  
12 temperature-depth profiles (e.g., Miyakoshi et al., 2003; Taniguchi et al., 1999b; Uchida and  
13 Hayashi, 2005). It has also been applied to forward model future groundwater temperature  
14 evolution due to projected climate change (Gunawardhana and Kazama, 2011). Herein, the  
15 surface boundary condition (Eq. 12) is fitted to mean annual air temperature trends produced by  
16 climate models. Because it is surface temperature, rather than air temperature, that drives shallow  
17 subsurface thermal regimes, this approach tacitly assumes that mean annual surface and air  
18 temperature trends are coupled. Thus, air temperature is being used as a proxy for surface  
19 temperature in this approach. As previously indicated, snowpack evolution may invalidate this  
20 assumption (Mellander et al., 2007), and thus it is best employed where snowpack effects are  
21 minimal. Snowpack evolution would typically retard the rate of groundwater warming (Kurylyk  
22 et al., 2013).

23 **2.5 Analytical solution 4: Exponential increase in surface temperature due to climate**  
24 **change**

25 It may be inappropriate to assume a linear surface temperature rise as in Eq. (13), because many  
26 climate scenarios suggest that the rate of climate warming will increase over time. Figure 2  
27 presents the globally-averaged IPCC (2007) multi-model air temperature projections for two

1 different emission scenarios. The global air temperature series projected for the conservative  
 2 emission scenario B1 is much better represented by a linear function than the air temperature  
 3 series for the aggressive A2 emission scenario, which exhibits significant concavity.

4 In such cases the boundary condition would be better represented as an exponential function  
 5 (Kurylyk and MacQuarrie, 2014). The solution presented here is simpler than the original form  
 6 given that the initial conditions are assumed to be thermally uniform (initial conditions = Eq. 9):

7 
$$\text{Boundary condition: } T(z=0, t) = T_1 + b \exp(ct) \quad (14)$$

$$T(z, t) = T_0 + \frac{(T_1 - T_0)}{2} \left\{ \begin{array}{l} \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} - \frac{U}{2}\sqrt{\frac{t}{D}}\right) \\ + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} + \frac{U}{2}\sqrt{\frac{t}{D}}\right) \end{array} \right\} +$$

8 Solution:

$$\frac{b}{2} \exp\left(\frac{Uz}{2D} + ct\right) \left\{ \begin{array}{l} \exp\left(-z\sqrt{U^2/4D^2 + c/D}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} - \sqrt{\left(\frac{U^2}{4D} + c\right)t}\right) + \\ \exp\left(z\sqrt{U^2/4D^2 + c/D}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} + \sqrt{\left(\frac{U^2}{4D} + c\right)t}\right) \end{array} \right\} \quad (15)$$

9 where  $T_1$  (°C),  $b$  (°C), and  $c$  ( $s^{-1}$ ) are parameters for the surface temperature boundary condition  
 10 which can be fit to climate model projections. Note that  $T_1 + b$  must equal  $T_0$  for the boundary  
 11 and initial conditions to converge at  $t = 0$ ,  $z = 0$ . The original initial condition function proposed  
 12 by Kurylyk and MacQuarrie (2014) superimposed linear and exponential functions, and thus the  
 13 more complex form of the solution can also be applied to forward model future climate change  
 14 impacts on deeper subsurface temperature profiles. These temperature profiles can deviate from  
 15 the geothermal gradient due to groundwater flow or recent surface temperature changes  
 16 (Ferguson and Woodbury, 2005; Reiter, 2005). The alternate forms of the boundary conditions  
 17 presented in Eqs. (10), (12), and (14) are illustrated in Figure 3. Each of the listed analytical  
 18 solutions to the one-dimensional, transient diffusion-advection equation is provided in Table 1  
 19 with details to highlight their differences.

20

## 1   **2.6 Effective aquifer depth**

2   The one-dimensional analytical solutions discussed above can be utilized to estimate the  
3   influence of surface warming at any desired depth. However, groundwater discharge to streams  
4   is sourced from different depths within the aquifer depending on the recharge location and the  
5   subsurface flow paths (Fig. 4a). Because the water table slope in unconfined aquifers is typically  
6   subdued in comparison to the land surface slope (Domenico and Schwartz, 1990), soil water that  
7   recharges the aquifer further upslope typically has a longer residence time and reaches greater  
8   depths relative to the land surface than soil water recharging the aquifer close to the discharge  
9   point. Groundwater flow in aquifers is often conceptualized as occurring in different ‘flow  
10   channels’ or ‘flow tubes’ (Domenico and Schwartz, 1990), and groundwater discharge is a  
11   thermal and hydraulic mixture of different groundwater flow channels coming from different  
12   depths and converging at the discharge point (Hoehn and Cirpka, 2006 and Fig. 4). Thus, when  
13   employing one-dimensional solutions to investigate the thermal evolution of groundwater  
14   discharge to streams and rivers, an effective depth  $z_{eff}$  (m) must be considered that represents the  
15   bulk aquifer depth (i.e., accounting for all discharging groundwater flow channels) as a single  
16   point within the subsurface (Fig. 4). As a first estimate, this depth may be taken as the average  
17   unsaturated zone thickness. Figure 4b shows the conceptual model employed in this study.  
18   Above the effective depth, heat transport and water flow is assumed to be predominantly vertical  
19   as is often the case within the unsaturated zone, in overlying aquitards, or even in the upper  
20   portion of the aquifer (e.g., Kurylyk et al., 2014b). Within the aquifer (located at the effective  
21   depth), groundwater discharges horizontally towards a stream, and horizontal heat transport is  
22   assumed to be negligible due to the relatively low horizontal thermal gradients in this zone. Heat  
23   advection and associated thermal dispersion near the discharge point is assumed to dominate  
24   vertical heat transfer and thus create a thermally uniform zone. Thus, the aquifer is treated as a  
25   thin, horizontally well-mixed thermal reservoir discharging to a surface water body (Fig. 4b).  
26   This approach is somewhat analogous to how contaminant hydrogeology studies have considered  
27   aquifers to be well-mixed reservoirs with respect to solute concentrations (e.g., Gelhar and  
28   Wilson, 1974). Vertical heat transfer continues below the aquifer (Fig. 4b). Limitations of this  
29   approach are briefly discussed later.

30

## 1 **2.7 Groundwater thermal sensitivity to long term surface temperature perturbations**

2 Groundwater thermal sensitivity is herein defined as the change in groundwater temperature at  
3 some depth and time divided by the driving change in surface ( $z = 0$ ) temperature at the same  
4 time. For example, if the surface temperature increases by  $2^{\circ}\text{C}$  and the groundwater temperature  
5 has only increased by  $1.4^{\circ}\text{C}$  at that same time, then the groundwater thermal sensitivity is 0.7  
6 ( $1.4^{\circ}\text{C}/2^{\circ}\text{C}$ ). The temperature changes at the surface and in the aquifer are measured with respect  
7 to the initial temperatures at those locations. This definition for groundwater thermal sensitivity  $S$   
8 ( $^{\circ}\text{C } ^{\circ}\text{C}^{-1}$ ) can be expressed in the following manner:

$$9 \quad S(z, t) = \frac{\Delta \text{Subsurface Temp.}}{\Delta \text{Surface Temp.}} = \frac{T(z, t) - T(z, t = 0)}{T(z = 0, t) - T(z = 0, t = 0)} \quad (16)$$

10 This groundwater thermal sensitivity is the analogue to the stream thermal sensitivity defined by  
11 Kelleher et al. (2012), although the temperature changes are measured on a longer timescale for  
12 groundwater (e.g., multi-decadal vs. seasonal). Equation (16) represents the thermal sensitivity at  
13 any arbitrary depth within the aquifer. The bulk (i.e., the entire portion of the aquifer discharging  
14 to the stream or river) groundwater thermal sensitivity in Eq. (16) can be found by replacing  $z$   
15 with  $z_{eff}$ .

16

### 17 **2.7.1 Groundwater thermal sensitivity to a step increase in surface temperature (land cover** 18 **disturbance)**

19 The groundwater thermal sensitivity  $S_s$  (subscript denotes nature of boundary condition) to a step  
20 increase in surface temperature occurring at  $t = 0$  followed by subsequent surface cooling at  $t = t_I$   
21 can be found by inserting Eqs. (9), (10), and (11) into Eq. (16):

$$S_s(z,t) = \begin{cases} \frac{1}{2} \left\{ \operatorname{erfc}\left(\frac{z-Ut}{2\sqrt{Dt}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+Ut}{2\sqrt{Dt}}\right) \right\} & \text{for } 0 \leq t < t_1 \\ \frac{1}{2} \left\{ \operatorname{erfc}\left(\frac{z-Ut}{2\sqrt{Dt}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+Ut}{2\sqrt{Dt}}\right) \right\} \\ - \frac{1}{2} \left\{ \operatorname{erfc}\left(\frac{z-U(t-t_1)}{2\sqrt{D(t-t_1)}}\right) + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+U(t-t_1)}{2\sqrt{D(t-t_1)}}\right) \right\} & \text{for } t \geq t_1 \end{cases} \quad (17)$$

2 Sensitivities for all times greater than  $T_0$  were calculated with respect to the initial temperature  
3 perturbation  $\Delta T$ . Interestingly, the groundwater thermal sensitivity is not dependent on the  
4 magnitude of the step change in surface temperature  $\Delta T$  or the initial temperature  $T_0$ , provided  
5 that the initial temperature is uniform. Eq. (17) has the same form as the well-known solute  
6 transport analytical solution proposed by Ogata and Banks (1961) to calculate normalized solute  
7 concentrations.

8 As in the case of Eq. (11), Eq. (17) can be simplified to represent the influence of a permanent  
9 step increase (i.e., no subsequent cooling) in surface temperature by setting  $t_1$  to infinity and only  
10 considering the first line on the right hand side of the equation.

### 11 **2.7.2 Groundwater thermal sensitivity to gradual increases in surface temperature (climate** 12 **change)**

13 Equation (16) can also be applied to obtain an expression for the groundwater thermal sensitivity  
14  $S_L$  ( $^{\circ}\text{C } ^{\circ}\text{C}^{-1}$ ) due to a linear increase in the surface temperature boundary condition by inserting  
15 Eqs. (9), (12), and (13) into Eq. (16) and simplifying:

$$16 \quad S_L(z,t) = \frac{1}{2Ut} \left[ (Ut - z) \times \operatorname{erfc}\left(\frac{z-Ut}{2\sqrt{Dt}}\right) + (Ut + z) \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z+Ut}{2\sqrt{Dt}}\right) \right] \quad (18)$$

17 Thus,  $S_L$  is independent of the initial temperature  $T_0$  and the rate of surface warming  $\beta$ .

18 The groundwater thermal sensitivity  $S_E$  ( $^{\circ}\text{C } ^{\circ}\text{C}^{-1}$ ) to an exponentially increasing surface  
19 temperature can be obtained by inserting Eqs. (9), (14), and (15) into Eq. (16). The resultant



1 solution can be further simplified by canceling terms and by remembering that  $T_0$  is the sum of  
 2  $T_1$  and  $b$ :

$$\begin{aligned}
 S_E(z, t) = & \frac{(T_1 - T_0)}{2b\{\exp(ct) - 1\}} \left\{ \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} - \frac{U}{2}\sqrt{\frac{t}{D}}\right) \right. \\
 & \left. + \exp\left(\frac{Uz}{D}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} + \frac{U}{2}\sqrt{\frac{t}{D}}\right) \right\} + \\
 & \frac{1}{2\exp(ct) - 2} \exp\left(\frac{Uz}{2D} + ct\right) \left\{ \exp\left(-z\sqrt{\frac{U^2}{4D^2} + \frac{c}{D}}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} - \sqrt{\left(\frac{U^2}{4D} + c\right)t}\right) + \right. \\
 & \left. \exp\left(z\sqrt{\frac{U^2}{4D^2} + \frac{c}{D}}\right) \operatorname{erfc}\left(\frac{z}{2\sqrt{Dt}} + \sqrt{\left(\frac{U^2}{4D} + c\right)t}\right) \right\} \quad (19)
 \end{aligned}$$

4 A spreadsheet is included in the electronic supplement that facilitates the calculation of the  
 5 results for each of the analytical solutions and groundwater thermal sensitivity equations. The  
 6 user may vary input parameters such as depth, thermal properties, groundwater velocity, time,  
 7 initial temperature and the surface temperature boundary conditions.

## 8 **2.8 Subsurface thermal properties**

9 These analytical solutions assume that subsurface thermal properties are homogeneous, but in  
 10 reality the bulk thermal properties of unconsolidated soils depend on many factors, including the  
 11 mineral constituents, porosity, total moisture saturation, and the pore water phase (Farouki, 1981;  
 12 Kurylyk et al., 2014b). Water has a much higher thermal conductivity than air, thus the saturated  
 13 zone typically is characterized by a higher bulk thermal conductivity than the unsaturated zone  
 14 (Oke, 1988). Despite the existence of subsurface thermal property heterogeneities, natural  
 15 variability in soil thermal properties is orders of magnitude less than the natural variability in  
 16 hydraulic properties (Domenico and Schwartz, 1990), and thus homogeneous assumptions are  
 17 better justified for subsurface heat transport than for subsurface water flow. Table 2 lists the bulk  
 18 thermal properties for unfrozen sand, clay, and peat at three water saturations (volume of soil  
 19 water/pore volume). These values are used to represent the typical ranges of thermal  
 20 conductivities experienced in common unconsolidated soils. The bulk thermal diffusivities of  
 21 these soils do not vary significantly at pore water saturations above 0.5.

22

### 1 3. Results and Discussion

#### 2 3.1 Seasonal surface temperature influences on groundwater temperature

3 Stallman's (1965) equation (Eqs. 5-7) can be utilised to investigate how idealized subsurface  
4 environments respond to seasonal surface temperature changes. Figure 5 shows temperature-  
5 depth profiles for each month and temperature-time series for different depths in a soil column  
6 driven by a harmonic boundary condition at the surface (Eq. 4). The results were obtained from  
7 Eqs. (5) to (7) for sandy soil (thermal properties, Table 2) and for a downwards Darcy velocity  
8 (i.e., recharge) of  $0.2 \text{ m yr}^{-1}$ . This recharge value was chosen as a representative basin  
9 groundwater recharge (Döll and Fiedler, 2008; Healy, 2010). Stallman's equation generally  
10 matches seasonal groundwater temperature data reasonably well in shallow subsurface  
11 environments, except in locations where snowpack can make the surface temperature non-  
12 sinusoidal and the subsurface thermal envelope (Fig. 5a) asymmetrical (Lapham, 1989).  
13 Regardless, Eq. (5) and Fig. 5 both demonstrate that the seasonal subsurface temperature  
14 variability is exponentially attenuated with depth and is barely discernible beyond a certain depth  
15 (e.g., 10-14 m).

16 The exponential damping factor  $\Omega$  is the ratio of the amplitude of the seasonal temperature cycle  
17 at an arbitrary depth  $z$  to the amplitude of the seasonal surface temperature cycle (Eq. 8). It is  
18 thus a measure of how the subsurface thermal regime responds to seasonal temperature  
19 variations, and it can be considered the seasonal counterpart to the groundwater thermal  
20 sensitivities derived from the analytical solutions experiencing long term surface temperature  
21 variability (e.g., Eq. 17). Figure 6 illustrates that the exponential damping factor (or seasonal  
22 thermal sensitivity)  $\Omega$  for a given depth decreases for the discharge scenario (black series, Fig. 6)  
23 in comparison to the recharge scenario (dashed blue series). In a discharge scenario, the upward  
24 advective flux is impeding the downward propagation of the surface temperature signal, and thus  
25 the surface signal is more quickly attenuated.

26 Figures 6a, 6b, and 6c also indicate that the soil thermal properties greatly influence the  
27 subsurface thermal response to seasonal temperature variability. In particular, due to the  
28 significantly lower thermal diffusivity of partially saturated peat (Table 2), the surface  
29 temperature signal (Fig. 6c) is more quickly damped in the peat soil in comparison to the results

1 obtained for sand (Fig. 6a) and clay (Fig. 6b). However, in all of the nine scenarios presented in  
2 Fig. 6, the  $\Omega$  parameter is less than 0.2 (amplitude reduced by at least 80%) when the depth is  
3 greater than 5 m, which indicates that groundwater discharge does not have to be sourced from a  
4 very deep aquifer to decrease the stream thermal sensitivity to seasonal air temperature changes.

### 5 **3.2 Impacts of land cover disturbances on groundwater temperatures**

6 Beyond the depth of seasonal temperature fluctuations (Fig. 5), groundwater temperature will  
7 still be influenced by long term surface temperatures perturbations. For instance, Figure 7a  
8 (solid lines) shows the groundwater warming produced with Eq. (11) at different depths and for  
9 different soils due to a sudden and permanent ( $t_I = \infty$ , Eq. 10) mean annual surface temperature  
10 increase of 2°C. This is approximately the long term mean annual surface temperature increase  
11 observed by Lewis (1998) in response to deforestation. This is at the lower end of the range (1.6  
12 to 5.1°C) in the mean annual surface temperature increases noted by Taniguchi et al. (1998)  
13 following forest removal in Western Australia. The groundwater *warming*, rather than the  
14 *temperature*, is obtained by setting the initial temperature to zero ( $T_0$ , Eqs. 10 and 11).

15 Results are presented for sandy soil and peat soil as these two soils respectively exhibit the  
16 highest and lowest thermal diffusivities given in Table 2. Due to the nature of the surface thermal  
17 boundary condition, these groundwater warming series exhibit a convex upward curvature. The  
18 results for the two depths (5 and 20 m) indicate that the lag between the surface and subsurface  
19 warming increases with increasing depth. For the sandy soil, the temperature at a depth of 20 m  
20 increases by 1.77°C after 100 years, whereas at 5 m depth, this magnitude of warming was  
21 realized after only 14 years. Thus, for initially uniform conditions, deeper aquifers will generally  
22 remain colder longer than shallow aquifers, as it takes longer for the warming signal to be  
23 advected or conducted downwards. Furthermore, Fig. 7a also indicates that soils with a higher  
24 thermal diffusivity (i.e., sand) will initially transport the surficial warming signal through the  
25 subsurface more rapidly than soils with lower thermal diffusivity (i.e., peat). However, because  
26 the subsurface is slowly equilibrating with the new constant surface temperature, the solid series  
27 representing the results for the different depths and soils begin to converge as time increases.

28 In the case of vegetation regrowth, the surface temperature warming due to the land cover  
29 disturbance would be temporary. As an illustrative example, Fig. 7a (dashed lines) shows the

1 groundwater warming produced by Eq. (11) at two depths (5 and 20 m) and for two soils due to a  
2 sudden  $2^{\circ}\text{C}$  increase in surface temperature that persists for only 25 years ( $t_1$ , Eq. 10). If desired,  
3 the equation could be further enhanced to accommodate a gradual cooling phase, rather than the  
4 instant cooling employed in the present study, using the more general formula described by  
5 Menberg et al. (2014). In Fig. 7a, the dashed and solid lines overlap prior to the cooling phase  
6 occurring at 25 years. The dashed temperature curves after 25 years represent the thermal  
7 recovery period. The groundwater warming curve for a depth of 5 m and the more diffusive soil  
8 (sand) is sharp, whereas the groundwater warming curve for a depth of 20 m and the less  
9 diffusive soil (peat) is more diffused and lagged. For example, the maximum groundwater  
10 warming ( $0.88^{\circ}\text{C}$ ) for the peat soil at a depth of 20 m occurs at 33 years, which is 8 years after  
11 the surface warming has ceased. Thus, temporary deforestation thermal impacts to coldwater  
12 streams may persist several years after vegetation regrowth has occurred, particularly if  
13 groundwater discharge to the stream is sourced from a deeper aquifer. However, these effects  
14 would likely not be significant as the warming signal would be strongly damped.

15 Figure 7b shows the aquifer thermal sensitivities in response to a sudden permanent (solid lines)  
16 or temporary (dashed lines) step increase in surface temperature, which correspond to the same  
17 warming scenarios as shown in Fig. 7a. As indicated in Eq. (17), these thermal sensitivity curves  
18 are similar to the groundwater warming curves (Eq. 11 and Fig. 7a), but scaled by a factor of  $\Delta T$ .  
19 Hence, the thermal sensitivity curves due to a step increase in surface temperature are  
20 normalized with respect to the boundary temperature increase and are thus independent of the  $\Delta T$   
21 value. The results presented in Fig. 7 clearly demonstrate that shallow groundwater will initially  
22 warm rapidly in response to permanent deforestation and then the rate of temperature increase  
23 will decrease with time. This arises due to the initially high thermal gradient and heat conduction  
24 arising from the abrupt surface step change in temperature. The resultant impacts of groundwater  
25 warming on streambed conductive and advective heat fluxes should be considered in models that  
26 simulate stream temperature warming due to deforestation—at least for streams where  
27 groundwater discharge has been shown to influence stream temperature. Small headwater  
28 streams, which are often groundwater dominated, can warm more rapidly than larger streams in  
29 response to deforestation because, for natural vegetative conditions, smaller streams typically  
30 experience more shading than larger rivers (e.g., Caissie, 2006).

1 The results shown in Fig. 7 are presented for a recharge scenario ( $q = 0.2 \text{ m yr}^{-1}$ ). This approach  
2 is conservative because recharge environments will typically warm more rapidly in response to  
3 rising surface temperatures than discharge environments, as conduction and advection are acting  
4 in parallel in the former case. The analytical solutions provided in this study for simulating  
5 subsurface warming due to long term surface temperature trends (Eqs. 11, 13, and 15) are better  
6 suited for recharge environments than discharge environments as groundwater discharge can  
7 bring up warm groundwater from deeper within the aquifer in accordance with the geothermal  
8 gradient. This phenomenon is not accounted for in the uniform initial conditions (Eq. 9). These  
9 solutions can be modified to allow for linearly increasing temperature with depth to account for  
10 the geothermal gradient (Kurylyk and MacQuarrie, 2014; Taniguchi et al. 1999a, 1999b), but this  
11 adds complexity to the resultant sensitivity formulae. Also as previously noted, this study is  
12 primarily concerned with shallow aquifers where heat fluxes due to surface temperature changes  
13 can dominate the influence of the geothermal gradient.

### 14 **3.3 Impacts of climate change on groundwater temperatures**

15 Equations (13) and (15) can be employed to investigate the sensitivity of groundwater  
16 temperatures to long term gradual surface temperature changes such as those experienced during  
17 climate change. The IPCC (2007) multi-model results (Fig. 2) are globally averaged results, and  
18 these data will be used to form the surface boundary conditions for the illustrative examples.

#### 19 **3.3.1 Exponential and linear boundary conditions**

20 The IPCC air temperature anomalies (i.e., increases) for this century produced by the  
21 conservative emission scenario B1 were fit to a linear surface temperature function (Fig. 2). The  
22 best fit between the linear function and the projected B1 air temperature warming was obtained  
23 with a slope  $\beta$  of  $5.41 \times 10^{-10} \text{ }^\circ\text{C s}^{-1}$  ( $1.7 \text{ }^\circ\text{C per century}$ , see Eq. 12). Also, the exponential  
24 function was employed to represent the IPCC multi-model results obtained using the more  
25 aggressive, non-linear A2 emission scenario (Fig. 2). The optimal exponential fit was obtained  
26 with fitting parameters  $b$  and  $c$  of  $1.59^\circ\text{C}$  and  $3.67 \times 10^{-10} \text{ s}^{-1}$ , respectively (Eq. 14). The RMSE  
27 values for the exponential and linear fits are presented in Fig. 2. The fitting parameter  $T_1$  ( $T_0 - b$ )  
28 can be adjusted to obtain the desired initial temperature, and herein we consider the subsurface  
29 warming (rather than the temperature *per se*) by setting initial temperatures to  $0^\circ\text{C}$  (i.e.,  $T_1 = -b$ ).

### 1 **3.3.2 Groundwater warming due to climate change**

2 Eq. (13) was employed to illustrate how an idealised, shallow aquifer would respond to a slow  
3 linear surface temperature rise (Fig. 3c). Figure 8a shows the groundwater warming results at  
4 different depths and for different soils calculated with Eq. (13) by applying a  $0.017\text{ }^{\circ}\text{C yr}^{-1}$  linear  
5 surface warming as the boundary condition (B1, Fig. 2). The starting date is the year 2000.  
6 Similar to the results presented above for land cover disturbances, the surface warming is more  
7 rapidly propagated to shallower depths (i.e., 5 m vs. 20 m) and for more thermally diffusive soils  
8 (sand vs. peat). After 100 years, the  $1.7^{\circ}\text{C}$  surface warming produced a  $1.6^{\circ}\text{C}$  increase in  
9 groundwater temperature for the sandy soil at a depth of 5 m (solid red series), but only a  $0.94^{\circ}\text{C}$   
10 increase for the peat soil at a depth of 20 m (dashed black series, Fig. 8a).

11 Figure 8b shows the groundwater warming results produced with the analytical solution with an  
12 exponentially increasing surface temperature (Eq. 15 and Fig. 2). The soil thermal properties and  
13 recharge rates are identical for the results shown in Figs. 8a and 8b, and thus the only difference  
14 between the two figure panels is the surface temperature boundary condition. The results shown  
15 in Figs. 8a and 8b for a given soil type and depth (i.e., same colour and line type) begin to  
16 significantly diverge after approximately 30 years because the IPCC A2 multi-model projections  
17 exhibit more extreme warming than the B1 projections after 2030 (Fig. 2).

### 18 **3.3.3 Groundwater thermal sensitivity due to climate change**

19 Figures 8c and 8d show the groundwater thermal sensitivity (Eqs. 18 and 19) results due to the  
20 linear surface warming and the exponential surface warming shown in Figs. 8a and 8b,  
21 respectively. Although the surface warming scenario shown in Fig. 8b is much more pronounced  
22 than that shown in Fig. 8a, it is interesting to note that the groundwater thermal sensitivity results  
23 for these warming scenarios are very similar (Figs. 8c and 8d) because the thermal sensitivity is  
24 essentially the thermal effect divided by the driving cause.

25 Due to the lag between the surface warming and the subsurface thermal response, the subsurface  
26 thermal regime will never reach equilibrium with the surface thermal regime when the boundary  
27 condition represents continuous surface temperature increases. Hence, the groundwater thermal  
28 sensitivities will never attain unity unless a stable surface temperature regime is eventually  
29 established. However, Figs. 8c and 8d indicate that the groundwater thermal sensitivity increases

1 with time as the magnitudes of both the surface and subsurface temperature warming increase,  
2 and thus the relative impact of the lag decreases. For example, after 100 years, the thermal  
3 sensitivity of the sandy soil at a depth of 5 m is about 0.90 for both the B1 linear warming  
4 scenario (Fig. 8c) and the A2 exponential warming scenario (Fig. 8d). Thus, shallow  
5 groundwater at this depth and for these conditions would be expected to warm by approximately  
6 90% of the surface temperature increase within 100 years.

### 7 **3.4 Implications for groundwater-dominated streams and rivers**

8 The consideration of groundwater temperature in stream temperature modeling is especially  
9 relevant in small streams where surface heat fluxes do not dominate the total energy budget. In  
10 fact, small streams are generally very dependent on groundwater inputs and temperatures, and  
11 their low thermal capacity (shallow depth and volume) makes them very vulnerable to any  
12 surface or subsurface energy flux modifications (e.g., Matheswaran et al., 2014). This has been  
13 shown in many timber harvesting studies, where the smallest streams have experienced the  
14 greatest increase in stream temperature following forest removal (e.g., Brown and Krygier,  
15 1970). Thus, quantifying future changes in shallow groundwater flow and temperatures is  
16 essential for a better understanding of the future thermal regimes of groundwater-dominated  
17 rivers and associated impacts to aquatic organisms (Kanno et al., 2014).

18 The results presented in Fig. 8 demonstrate the limitations inherent in inferring future stream  
19 warming from stream thermal sensitivities obtained from seasonal stream and air temperature  
20 data. For instance, the seasonal groundwater thermal sensitivity ( $\Omega$ ) values presented in Fig. 6  
21 indicate that groundwater temperature beyond 10 m depth generally exhibits minimal sensitivity  
22 to seasonal variations in weather. Thus, groundwater-dominated stream thermal sensitivities  
23 obtained from seasonal air and stream temperature data are typically low (Kelleher et al., 2012).  
24 However, as Figs. 8c and 8d illustrate, groundwater warming at depths greater than 10 m may  
25 still be significant in response to long term surface temperature changes, such as would be  
26 experienced under climate change. Due to the interrelationships between the thermal regimes of  
27 stream and aquifers and the differences between the thermal sensitivities of shallow aquifers to  
28 short term (Fig. 6) and long term (e.g., Figs. 7b and 8) surface temperature changes, it is not  
29 generally valid to extrapolate thermal sensitivities for groundwater-dominated streams obtained  
30 from sub-annual data to project long term stream warming.

1 These results demonstrate the potential limitations of using relatively short (e.g., < 25 years)  
2 records of inter-annual air and water temperature data to obtain estimations of future stream  
3 warming (e.g., Luce et al., 2014). Results for the present study (Figs. 8c and 8d) indicate that  
4 even at a time scale of 25 years, the thermal sensitivities of relatively shallow (e.g., 10 m)  
5 groundwater reservoirs may be low compared to thermal sensitivities that could be attained after  
6 100 years of surface warming. These results suggest that what is interpreted as a damped  
7 groundwater-dominated stream thermal sensitivity to inter-annual air temperature variability may  
8 actually be a delayed thermal sensitivity due to the lag in the warming of groundwater and  
9 associated streambed heat fluxes. We acknowledge, however, that employing thermal  
10 sensitivities derived from inter-annual temperature data to project future stream warming is  
11 preferable to considering thermal sensitivities from seasonal temperature data (Luce et al., 2014).  
12 The appropriateness of these methods depends on the depth to the aquifer, the degree of  
13 groundwater contribution to the stream/river, the subsurface thermal properties, and the  
14 timescale of interest.

### 15 **3.5. Addressing groundwater warming in stream temperature models**

16 The present study demonstrates the importance of surface temperature forcing on groundwater  
17 temperature, particularly for shallow aquifers. The potential influence of shallow groundwater  
18 warming on stream temperatures is not generally considered in existing empirical stream  
19 temperature models. The equations proposed in this study can be used to develop an approach to  
20 approximate the timing and magnitude of groundwater temperature warming in response to long  
21 term surface temperature changes. As described below, this information may be integrated within  
22 existing stream temperature models that consider streambed heat fluxes.

23 The upper boundary condition for the equations presented in this study is the ground surface  
24 temperature. Thus, the projected trends in catchment land surface temperature due to future  
25 climate change or land cover disturbances must be obtained prior to utilising these equations. In  
26 the case of climate change without related snowpack changes, mean annual surface temperature  
27 trends are often assumed to follow mean annual air temperature trends (see Mann and Schmidt,  
28 2003). This simplification facilitates the boundary condition generation because air temperature  
29 trends can be readily obtained from the output of climate models. However, in the case of land  
30 cover changes (e.g. urbanisation) or snowpack evolution, mean annual air temperature trends



1 may be decoupled from mean annual surface temperature trends (Mann and Schmidt, 2003;  
2 Mellander et al., 2007). In this situation, a simple surface heat flux balance model can be applied  
3 to calculate the surface temperature changes due to changes in the climate and/or land cover. A  
4 detailed discussion on appropriate techniques for simulating these relationships can be found in  
5 Mellander et al. (2007), Kurylyk et al. (2013), and Jungqvist et al. (2014).

6 Once the surface temperature trends are obtained, they can then be fitted to the appropriate  
7 boundary condition function (Fig. 3). The associated analytical solution (Table 1) and  
8 groundwater thermal sensitivity formula can be utilized to perform simulations of future  
9 subsurface warming and/or groundwater thermal sensitivity due to the surface temperature  
10 change. It should be noted that these solutions only calculate increases in mean annual  
11 groundwater temperature and do not account for seasonality. It is generally reasonable to assume  
12 that the amplitude and timing of the seasonal groundwater cycle will not be greatly influenced by  
13 climate change (Taylor and Stefan, 2009), provided snowpack conditions or the seasonality of  
14 soil moisture will not change significantly (Kurylyk et al., 2013).

15 In addition to the surface temperature boundary condition terms, the analytical solutions must be  
16 parameterized with subsurface thermal properties, vertical groundwater flow information, and  
17 effective aquifer depth. Subsurface thermal properties can be obtained from information  
18 regarding the soil type and typical water saturation of the sediment overlying the aquifer (Table  
19 2). Vertical groundwater flow rates can be obtained from field measurements (e.g., using heat as  
20 a hydrologic tracer, Gordon et al., 2012; Lautz, 2010; Rau et al., 2014) or from regional or local  
21 groundwater recharge and discharge maps. Potential changes in groundwater recharge (Crosbie  
22 et al., 2011, Kurylyk and MacQuarrie, 2013; Hayashi and Farrow, 2014) and groundwater  
23 discharge (Kurylyk et al., 2014a; Levison et al., 2014) due to changes in climate or land cover  
24 could also be considered. The aquifer effective depth can be crudely estimated as the average  
25 unsaturated zone or aquitard thickness overlying the aquifer (e.g., Figure 4). Such information  
26 may be available from well data, geophysical surveys, or regional maps of the groundwater table  
27 depth (Fan et al., 2013; Snyder, 2008). Further research is required to assess approaches for more  
28 accurately determining the effective aquifer depth. A reasonable range of the input variables to  
29 these equations should be considered to generate an envelope of predicted groundwater warming  
30 (see Fig. 4 of Menberg et al., 2014). Such a range could incorporate uncertainties arising from,

1 for example, heterogeneities in soil thermal properties and inter-annual variability in  
2 groundwater recharge (Hayashi and Farrow, 2014). Table 3 lists alternative options for  
3 parameterizing the equations presented in this study. The parameter values used in the present  
4 study are representative of conditions often observed.

5 To determine the influence of warming groundwater on stream temperatures, the future  
6 groundwater thermal sensitivity can be applied to estimate the resultant changes to streambed  
7 heat fluxes. There are different approaches available for estimating streambed heat fluxes from  
8 subsurface temperatures depending on whether the total streambed energy flux or the apparent  
9 sensible flux is being considered (e.g., Caissie et al., 2014, Moore et al., 2005), but in either case,  
10 the streambed fluxes depend on subsurface temperature, particularly the temperature  
11 immediately below the stream. These changes in streambed heat fluxes can then be combined  
12 with simulated changes in stream surface heat fluxes, and the resultant change in stream  
13 temperature can be obtained in a deterministic stream temperature model. Such an approach to  
14 estimate long term evolution of stream temperatures would be more realistic than considering a  
15 stream temperature model driven by air temperature only, as both surface and streambed heat  
16 fluxes are important in stream temperature dynamics.

#### 17 **4. Limitations**

18 The unsteady heat diffusion-advection equation utilized in this study (Eq. 2) assumes one-  
19 dimensional groundwater flow and heat transport, spatiotemporally invariant groundwater flow,  
20 isothermal conditions between the soil grains and water at every point, and homogeneous  
21 thermal properties. Flashy groundwater flow regimes with very short residence times (e.g.,  
22 aquifers with large fractures) may invalidate the assumption of thermal equilibrium between the  
23 subsurface environment and the mobile water. In such settings, recharge seasonality may exert  
24 strong control on the temperature of groundwater discharge (Luhmann et al., 2011). Horizontal  
25 groundwater flow can perturb subsurface thermal regimes, at least in regions with significant  
26 horizontal thermal gradients (Ferguson and Bense, 2011; Reiter, 2001), and there may be a  
27 vertical discontinuity in vertical water flow across aquifers due to horizontal discharge to surface  
28 water bodies (e.g., Fig. 2). Aquifers that exhibit considerable lateral hydraulic heterogeneities  
29 may be characterized by flow regimes that are not well represented by the conceptual model  
30 (Fig. 2).

1 Herein, we propose that the average depth to the groundwater table may be a reasonable  
2 approximation for the effective depth ( $z_{eff}$ ). This approach assumes that the groundwater  
3 temperature at the bottom of the vertical flow tubes is fully mixed and that there is no  
4 modification of the temperature signal as the groundwater flows horizontally towards the  
5 discharge location (Fig. 4). This assumption may be violated in very shallow aquifers with slow  
6 groundwater flow (i.e., low horizontal advection and dispersion) due to vertical conductive heat  
7 fluxes from the surface in the vicinity of the discharge location.

8 In very shallow aquifers, groundwater velocity varies seasonally and is driven by the seasonality  
9 of precipitation, but subsurface hydraulic storage properties tend to damp the seasonality of  
10 groundwater flow in comparison to precipitation. Eq. (2) also assumes that no soil thawing  
11 occurs as a result of the surface temperature change, but latent heat absorbed during soil thaw  
12 can significantly retard subsurface warming (Kurylyk et al., 2014b). Ignoring soil thaw is  
13 reasonable, except in permafrost regions, because in ephemerally freezing regions the dynamic  
14 freeze-thaw process only influences the seasonality of groundwater temperature, and does not  
15 significantly influence the change in mean annual groundwater temperature in response to long  
16 term climate change (Kurylyk et al., 2014a).

17 At very shallow depths (e.g., < 3m), the subsurface thermal regime can be considered to be in  
18 equilibrium with the mean annual surface temperature. Because the lag between surface and  
19 subsurface warming is negligible in this case, the solutions presented in this study are not overly  
20 useful at very shallow depths. Also, at greater depths (e.g., 25 m), the influence of the  
21 geothermal gradient should be explicitly considered. In such cases, the equations proposed in this  
22 study can be modified to incorporate a geothermal gradient (Kurylyk and MacQuarrie, 2014;  
23 Taniguchi et al., 1999a; 1999b). Despite these limitations, the analytical solutions presented here  
24 can be employed to obtain reasonable estimates of the evolution of mean annual groundwater  
25 temperature due to climate change and land cover disturbances for a broad range of aquifer  
26 depths. For example, Menberg et al. (2014) applied a modified form of Eq. (11) to calculate  
27 groundwater warming trends that generally concurred with measured 1970-2010 groundwater  
28 warming trends recorded at forested and agricultural sites in Germany. We anticipate that other  
29 studies may also benefit from these approaches.

30

## 1 **5. Summary and conclusions**

2 Stream temperature models often ignore the potential for future groundwater warming. This  
3 simplifying assumption is employed because mean annual groundwater temperature is relatively  
4 constant (or thermally insensitive) on the intra-annual or short inter-annual time scales that it is  
5 typically measured. We have suggested in this study that although seasonal surface temperature  
6 changes are damped in the shallow subsurface, long term changes in surface temperatures can be  
7 propagated to much greater depths. This phenomenon has been known for some time in the field  
8 of thermal geophysics (e.g., Lesperance et al., 2010), but it is generally overlooked in stream  
9 temperature modeling. Due to the difference in the subsurface thermal response to seasonal and  
10 multi-decadal surface temperature changes, it may be inappropriate to infer multi-decadal  
11 warming of groundwater-dominated streams based on linear regressions of short term air and  
12 water temperature data.

13 Previous studies have identified the potential importance of considering shallow groundwater  
14 temperature warming when projecting future stream temperature (Kurylyk et al., 2013; 2014a).  
15 These studies have employed methods that either require extensive surface and subsurface  
16 temperature data collection or detailed numerical modeling. In many cases, these methods may  
17 be prohibitive. Several analytical solutions and associated groundwater thermal sensitivity  
18 equations are herein presented as alternative approaches for estimating a range for the potential  
19 timing and magnitude of future groundwater warming in response to climate change or land  
20 cover disturbances. These are most applicable to idealized environments, but the methods can be  
21 employed to obtain first-order approximations of future groundwater warming in natural  
22 environments (see Menberg et al., 2014). The subsurface warming scenarios can be considered  
23 within existing stream temperature models to investigate whether groundwater warming is an  
24 important consideration for the future thermal regime of a particular stream (Snyder et al., 2015).

25 The present study has highlighted the importance of shallow groundwater sensitivity to surface  
26 warming. Although groundwater warming has been inferred from subsurface temperature-depth  
27 profiles at many sites, few long term datasets of directly measured groundwater temperature exist  
28 to corroborate the methods proposed herein (Menberg et al, 2014). The initiation of long-term  
29 shallow groundwater temperature monitoring sites would provide a better understanding of the  
30 processes linking atmospheric and subsurface warming (e.g., Caldwell et al., 2014b).

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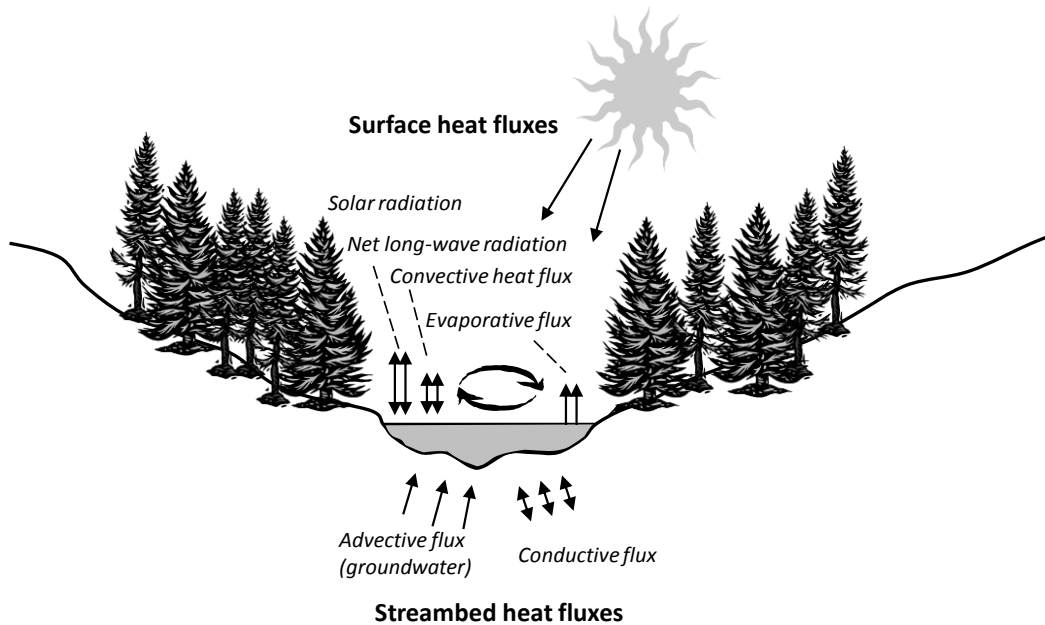
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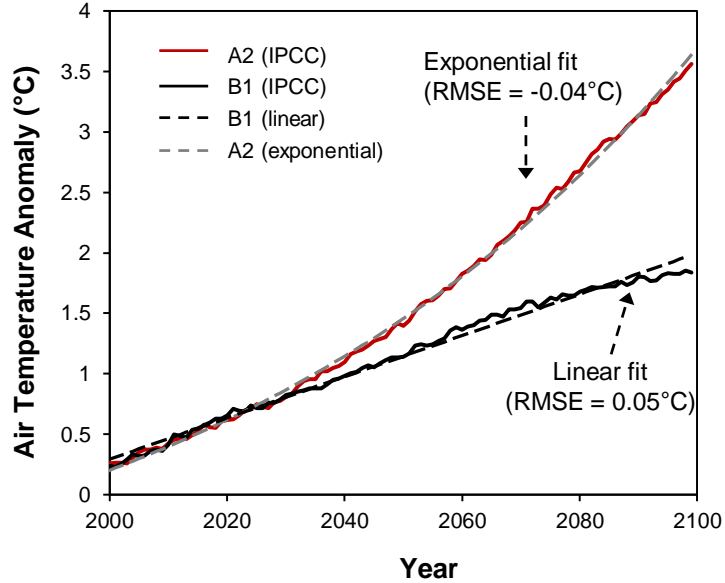
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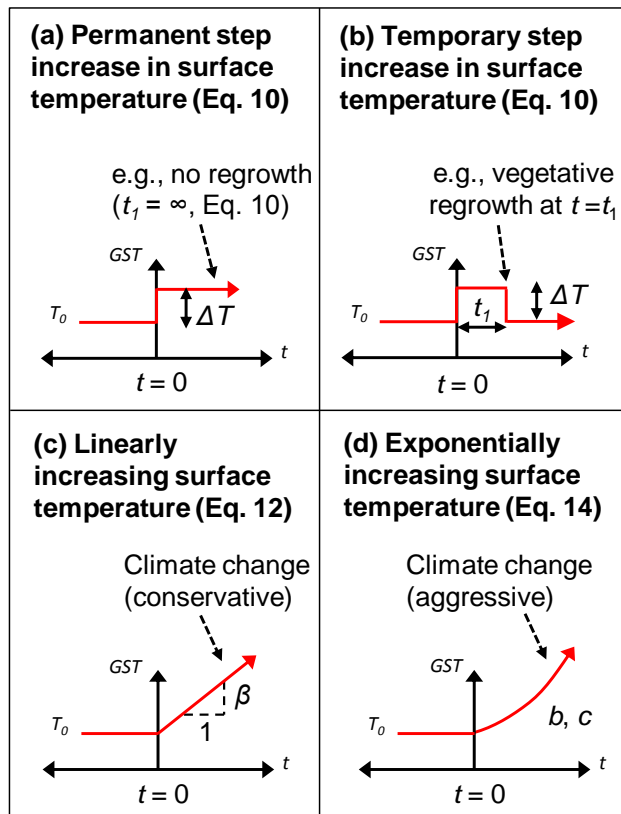


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 12 **Figure 1: Heat fluxes at the water surface and streambed for the cross-section of a gaining**  
 13 **stream or river** (modified from Caissie, 2006).

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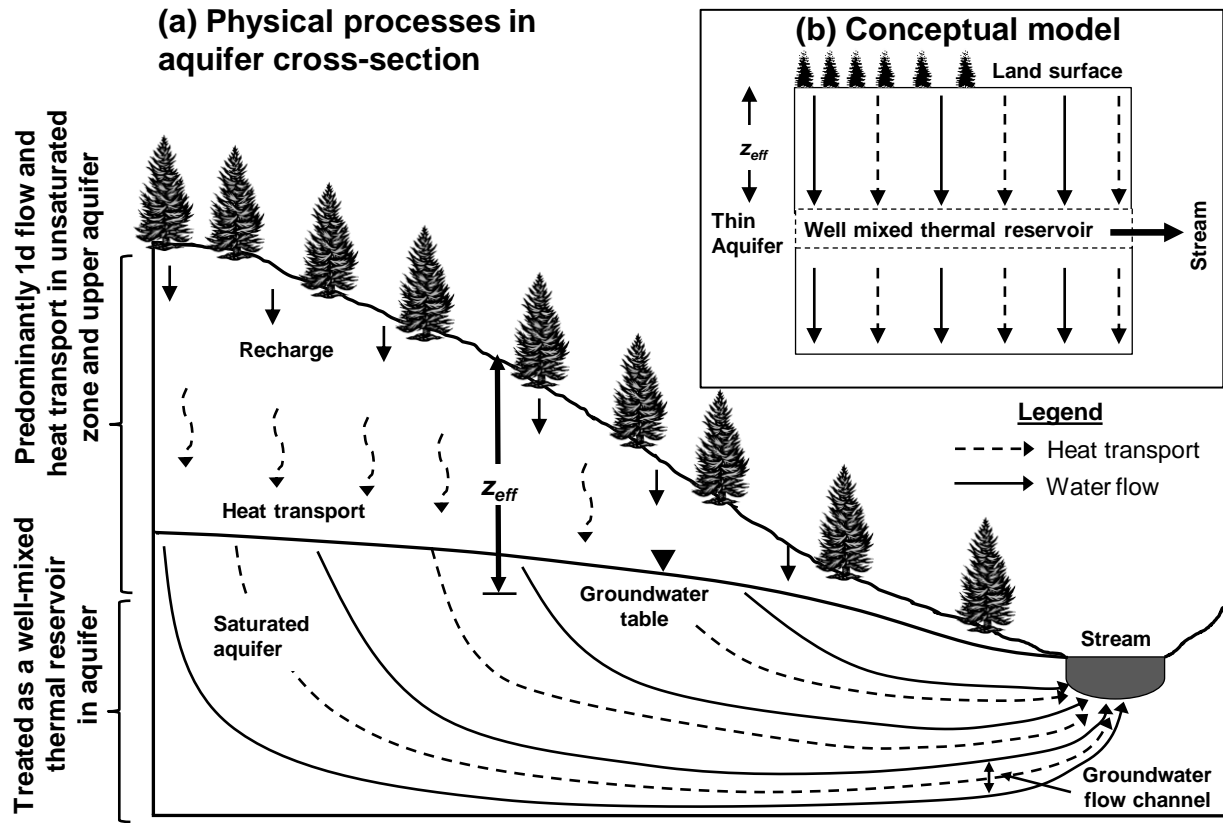
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 2 **Figure 2: IPCC Multi-model globally averaged air temperature anomaly projections for**  
 3 **the 21<sup>st</sup> century relative to the air temperature data for 1980-1999 for emission scenarios**  
 4 **B1 and A2** (data from, IPCC, 2007). Details concerning the exponential and linear fits to the  
 5 IPCC projections are given in Section 3.3.1. Modified from Kurylyk and MacQuarrie (2014).



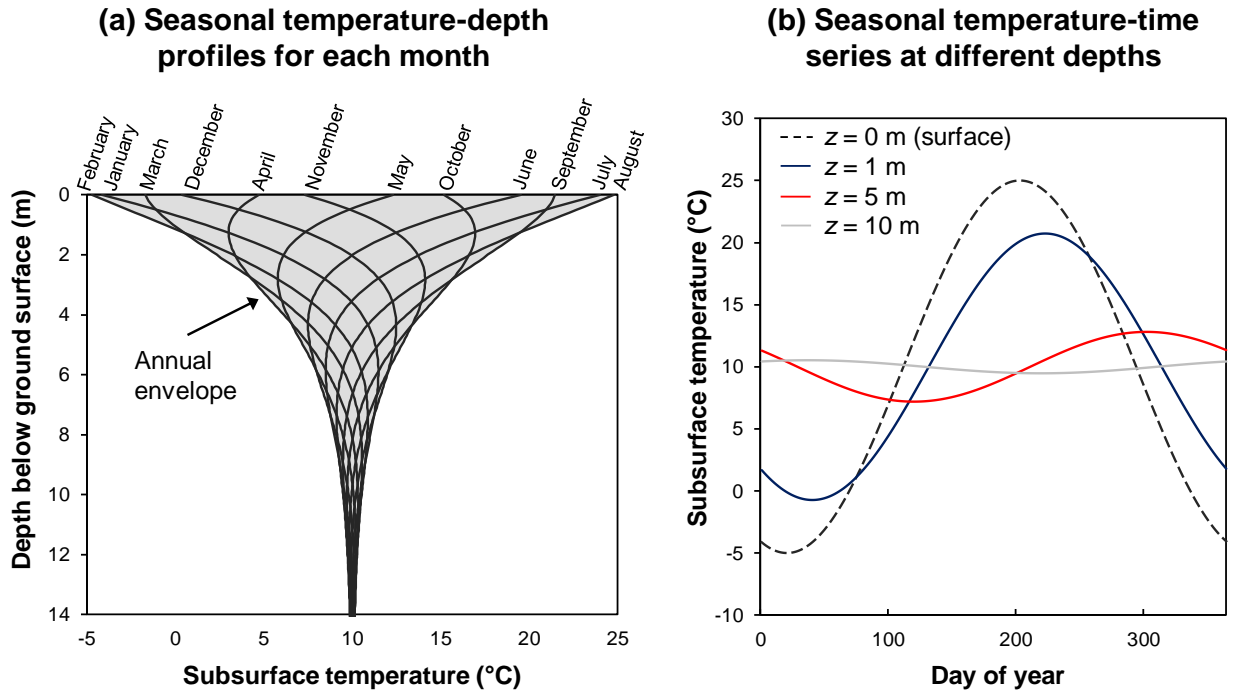
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1 **Figure 3: (a-b) The boundary conditions for ground surface temperature (GST)**  
 2 **disturbances due to land cover changes. Both (a) and (b) represent the boundary condition**  
 3 **given in Eq. (10). The difference between these is the duration of the period of warm**  
 4 **surface temperatures ( $t_I = \infty$  in (a)). (c-d) The boundary conditions for GST due to long**  
 5 **term climate change for conservative (linear, Eq. 12) and aggressive (exponential, Eq. 14)**  
 6 **climate scenarios.**

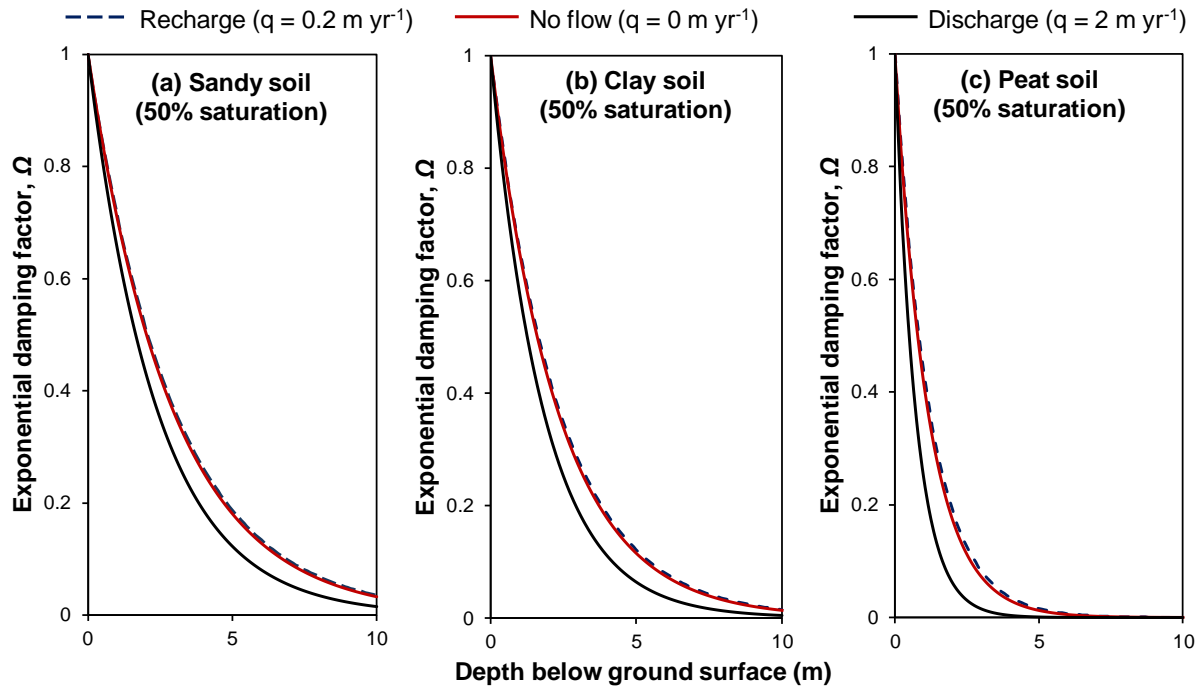


8 **Figure 4: (a) Groundwater flow and heat transport in a two-dimensional cross-section of an**  
 9 **aquifer-stream system. (b) Conceptual model of the physical processes shown in (a).**  
 10 **Dashed arrows indicate heat transport, and solid arrows indicate water flow.**



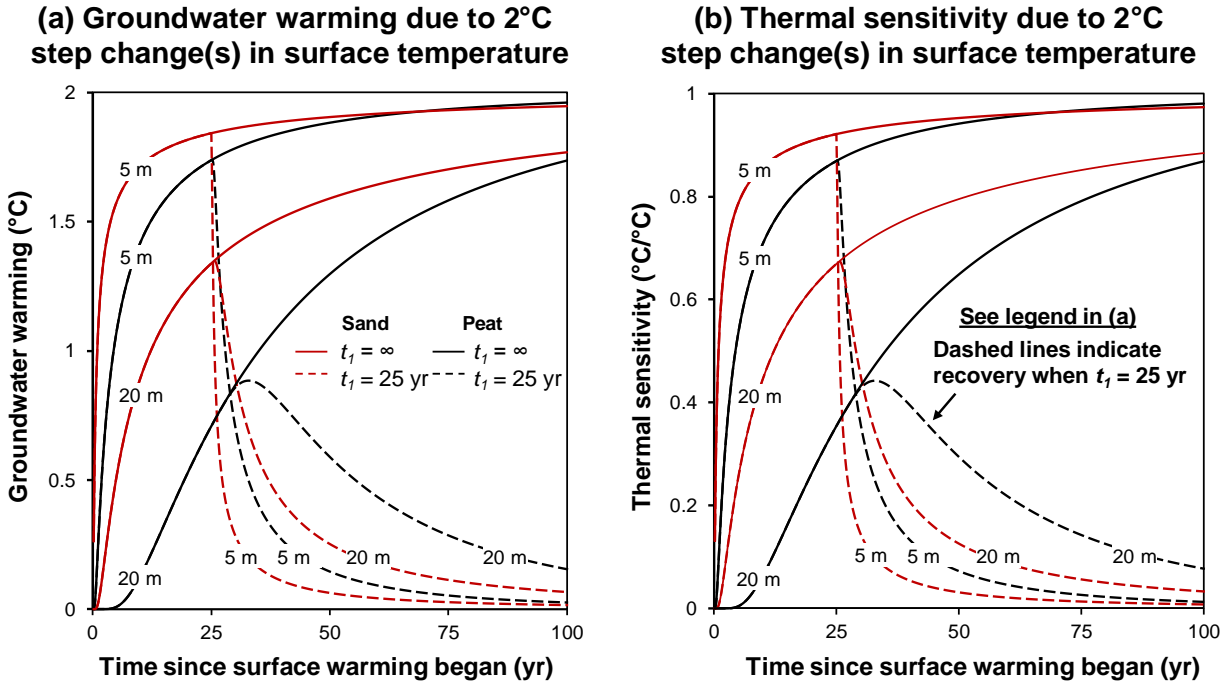
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3 **Figure 5: (a) Temperature-depth profiles for each month obtained from Stallman’s**  
 4 **equation (Eqs. 5-7) for homogeneous soil subject to harmonic seasonal surface temperature**  
 5 **variation. (b) Temperature-time series generated with Stallman’s equation for depths of 0,**  
 6 **1, 5, and 10 m.** In (a) and (b) the thermal properties for sand at 50% saturation (Table 2) were  
 7 employed, and a recharge Darcy velocity of  $0.2 \text{ m yr}^{-1}$  was assumed. The boundary condition  
 8 parameters  $T_m$ ,  $A$ ,  $\phi$ , and  $p$  were assigned values of  $10^\circ\text{C}$ ,  $15^\circ\text{C}$ ,  $-4.355$  radians, and  $31,536,000 \text{ s}$   
 9 (1 yr), respectively to represent typical surface temperature conditions for a forested site in New  
 10 Brunswick, Canada (e.g., Kurylyk et al., 2013).



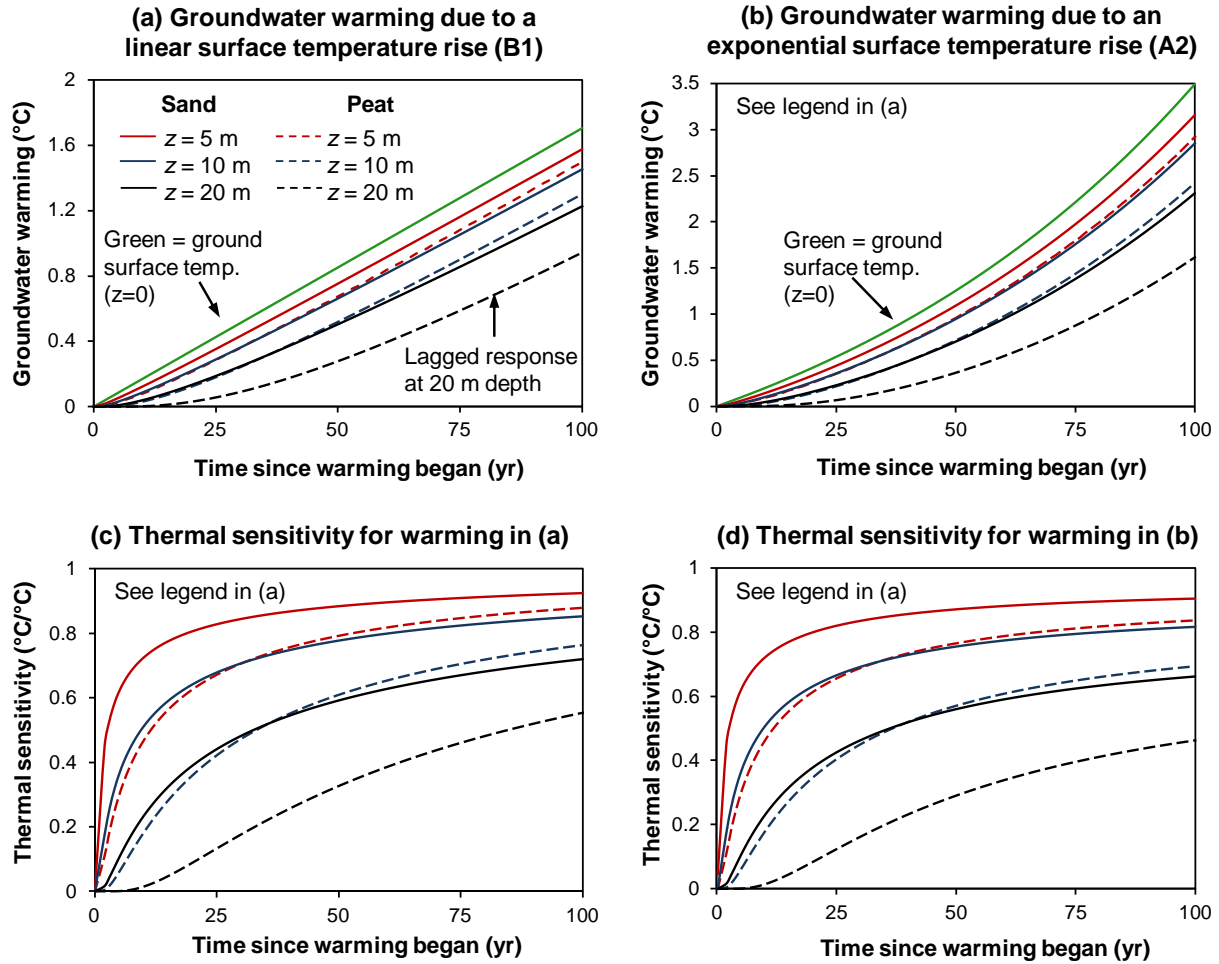
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2 **Figure 6: Exponential damping factor (seasonal temperature sensitivity)  $\Omega$  (Eq. 8) vs. depth**  
 3 **for (a) sandy soil, (b) clay soil, and (c) peat soil.** The thermal properties were taken from Table  
 4 2 assuming a volumetric water saturation of 50%. Results are presented for Darcy velocities of  
 5  $0.2 \text{ m yr}^{-1}$  (recharge, downwards flow), 0 (conduction-dominated thermal regime), and  $-2 \text{ m yr}^{-1}$   
 6 (discharge, upwards flow) and a period of 1 year. A higher discharge value was used in  
 7 comparison to the recharge value given that discharge is typically concentrated over a smaller  
 8 area than recharge.



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2 **Figure 7: (a) Groundwater temperature warming due to a permanent (solid lines) or**  
 3 **temporary (dashed lines) step increase in surface temperature vs. the time since the surface**  
 4 **warming began. (b) Groundwater thermal sensitivity vs. time for each of the eight**  
 5 **scenarios presented in (a). The results shown in (a) were obtained with Eq. (11) driven with the**  
 6 **step boundary condition (Eq. 10), with  $\Delta T = 2^\circ\text{C}$  and  $t_l = \text{infinity}$  (solid lines) or 25 years**  
 7 **(dashed lines). The subsurface thermal properties were taken from the 50% saturated sand and**  
 8 **peat values in Table 2, and the recharge rate was  $20 \text{ cm yr}^{-1}$ . The results shown in (b) were**  
 9 **calculated with Eq. (17) using the same parameters as (a).**



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**Figure 8: Groundwater temperature warming due to a linear trend (a) and an exponential trend (b) in surface temperature vs. the time since the surface warming began. (c) and (d) Groundwater thermal sensitivity vs. time for each of the six scenarios presented in (a) and (b), respectively.** The results shown in (a) were obtained with Eq. (13) with  $\beta = 5.41 \times 10^{-10} \text{ } ^\circ\text{C s}^{-1}$  based on the IPCC B1 projections and setting  $T_0 = 0^\circ\text{C}$ . The results shown in (b) were obtained with Eq. (15) with  $T_l$ ,  $b$ , and  $c = -1.59^\circ\text{C}$ ,  $1.59^\circ\text{C}$ , and  $3.68 \times 10^{-10} \text{ s}^{-1}$ , respectively (to match the IPCC A2 projections). The subsurface thermal properties were for 50% saturated soil (Table 2), and the recharge rate was  $20 \text{ cm yr}^{-1}$ . The aquifer thermal sensitivities shown in (c) and (d) were calculated with Eqs. (18) and (19) respectively.

1 **Table 1: Details regarding the four analytical solutions employed in this study<sup>1</sup>**

Solution ID	Equation number	Time scale	Surface temperature <sup>1</sup>	Solution reference
1	(5)	Seasonal or diel	Sinusoidal	(Stallman, 1965)
2	(11)	Multi-decadal	Step change(s)	(Menberg et al., 2014)
3	(13)	Multi-decadal	Linear increase	(Taniguchi et al., 1999a)
4	(15)	Multi-decadal	Exponential increase	(Kurylyk and MacQuarrie, 2014)

2 <sup>1</sup>For boundary conditions, see Eq. (4), (10), (12), and (14) respectively.

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4 **Table 2: Bulk thermal properties of some common soils and their dependence on saturation<sup>1</sup>**

Saturation (vol/vol)	Thermal conductivity $\lambda$ (W m <sup>-1</sup> °C <sup>-1</sup> )	Heat capacity $c\rho$ (10 <sup>6</sup> J m <sup>-3</sup> °C <sup>-1</sup> )	Thermal diffusivity $D$ (10 <sup>-6</sup> m <sup>2</sup> s <sup>-1</sup> )
<i>Sandy soil (porosity = 0.4)</i>			
0	0.30	1.28	0.24
0.5	1.80	2.12	0.85
1.0	2.20	2.96	0.74
<i>Clay soil (porosity = 0.4)</i>			
0	0.25	1.42	0.18
0.5	1.18	2.25	0.53
1.0	1.58	3.10	0.51
<i>Peat soil (porosity = 0.8)</i>			
0	0.06	0.60	0.10
0.5	0.29	2.23	0.13
1.0	0.50	4.17	0.12

5 <sup>1</sup>Data obtained from Monteith and Unsworth (2007).

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1 **Table 3: Parameters for equations considered in this study**

Symbol	Physical meaning	Units	Determination method	Example Sources
$D$	Thermal diffusivity	$\text{m}^2 \text{s}^{-1}$	Obtain from tabulated values (e.g. Table 2)	(Oke, 1978; Monteith and Unsworth, 2007)
$z, z_{eff}$	Depth, effective depth <sup>1</sup>	m	Geophysics, groundwater table maps, local wells	(Fan et al., 2013; Snyder, 2008)
$U, q$	Thermal plume velocity, groundwater recharge <sup>2</sup>	$\text{m s}^{-1}$	Thermal tracing, lysimeters, local recharge maps	(Healy, 2010; Scanlon et al., 2002)
$T_0$	Initial temperature	$^{\circ}\text{C}$	Mean annual surface temperature <sup>3</sup>	(USEPA, 2013)
$T_m, A, \Delta T, T_1, \beta, b,$ and $c,$	Surface temperature fitting parameters	Various	Climate model output, surface energy balance models <sup>4</sup>	(Kurylyk et al., 2013; Mellander et al., 2007; Taniguchi, 1993)

2 <sup>1</sup>The effective depth represents the bulk depth of the portion of the aquifer discharging to the stream (Fig. 4).

3 <sup>2</sup> $U$  represents the thermal plume velocity only due to advection. This can be easily obtained if the groundwater  
4 recharge rate is known (see Eq. 3).

5 <sup>3</sup>In the absence of persistent snowpack, the mean annual surface temperature can be approximated with the mean  
6 annual air temperature. Otherwise a thermal offset can be assumed from literature values (Zhang, 2005).

7 <sup>4</sup>See Section 3.5 for more information.

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