Response to review

General response:

We agree with the critical comments of both Reviewers and we provide response to the issues in this letter. Some of the Reviewers' comments required major changes which for clarity were not included in this letter, but are presented in the revised version of the manuscript; if such a situation was the case an appropriate comment was made in the response. There was one comment out of twenty to which we agreed only partially: the Reviewer #2 comment according an additional plot (comment 3b). However, the comment concerns a minor issue which is outside the major criticism. Nonetheless, we provide a clear motivation for that and we hope that Editor and Reviewers will agree with us. Remaining Reviewers comments are fully employed in the revision. In our opinion the Reviewers comments led to improvement of the manuscript, especially the major revisions suggested by the Reviewer #2.

The version of the manuscript with indicated changes is provided at the end of this letter.

Anonymous Referee #1

General comment:

The paper contains numerous abbreviations and is therefore more difficult to read.

Response:

The abbreviations are now replaced with full names except SCF – snow cover fraction – which is used unabbreviated in many papers.

Comment 1:

Figure 3 shows as well numerous lakes, which are present in the basin. In the paper there is no information how these lakes influence the hydrology in the basin. Are the lake levels and discharges regulated in reality and how is this modelled using WetSpa.

Response to 1:

The lakes in WetSpa are modelled by incorporating appropriate values of hydraulic parameters. We now detail that in the section "2.2 Study area":

Several lakes in the northern part of the catchment are controlled by management schemes, which usually discharge into Biebrza tributaries after accumulation period. Lakes in WetSpa are modelled by setting appropriate values of the hydraulic parameters in the model e.g. by a high runoff coefficient and a low friction. The simulation of water management schemes in the controlled lakes is, however, not implemented.

Comment 2:

Snow accumulation was not calculated, but replaced with the input SCF. SCF is just a ratio of the area, but it's for me unclear what the magnitude is of ksnow and krain.

Response to 2:

The values of ksnow and krain are obtained during the calibration of the model. We now provide the values of ksnow and krain in the results section 3.1:

The snow related global WetSpa parameters were estimated during the calibration as: $k_{snow} = 5.03 \text{ mm C}^{-1} \text{day}^{-1}$, $k_{rain} = 0.02 \text{ mm mm}^{-1} * \text{C}^{-1} \text{ day}^{-1}$.

Comment 3:

In Fig. 6 the comparison of measured and calculated discharge is shown. It looks that the calculated discharge is underestimated. Perhaps discuss this and give reason: accuracy of Gauging station, too high actual evpotranspiration, or other ..

Response to 3:

The reason is most likely indeed the accuracy of the gauging stations during the highest peaks, as during these events water flows on a densely vegetated floodplain, where a correct measurement of water velocity is very difficult. We now discuss this issue in the paper:

The peak discharges underestimation are possibly determined by the uncertainty of the rating curve. During the yearly spring floods, the measurement profile near the gauging station widens outside the riverbed and extends into the densely vegetated floodplain, where proper hydraulic measurements are very difficult.

Comment 4:

Fig. 7 should be described in the text a bit more, what are the highlights and why do I see a pattern for the mean simulated snowmelt.

Response to 4:

In the introductory paragraph to the section 3.2 Figure 7 is only generally discussed, much broader discussion is provided in sections 3.2.2, 3.2.3 and 3.2.4. Reviewer #2 also commented on this issue, which lead us to separate section 3 into two sections. This results in a discussion on Figure 7 (Figure 8 in the new manuscript), which is much easier to follow for a reader.

Comment 5:

Figure 9 should be described in the section on the study area.

Response to 5:

Figure 9 is now moved into the "Study area" section with appropriate explanation:

The dominating landscape features, that certainly have influence on the functioning of the Biebrza hydrological system are the river valley and the large forest complex located in the north-eastern part of the catchment (Fig. 5).

Anonymous Referee #2

Comment 1:

The introduction refers to some interesting publications, however the content is not always logically structured which hampers the readability of the introduction.

Response to 1:

According to the comment, we have rewritten the majority of introduction, in order to apply all issues; see the detailed comments below.

Comment 1a:

A better differentiation should be made between previous methods applied to quantify the spatial sensitivity of parameters in hydrological models and the spatial data that could be applied for spatial sensitivity analysis (rainfall, Land surface temperature, impervious surfaces, et. . .).

Response to 1a:

As requested, we gave a better structure to the first four paragraphs of the introduction, so the evolution of the spatial sensitivity aspects from very general studies, into more complex approaches is now clearly visible. There is now a clear differentiation between aspects of various data used and spatial sensitivity in general. Due to a big portion of the text was changed we do not include it here but only in the revised manuscript.

Comment 1b:

Regarding the spatial sensitivity analysis methods the advantage of the presented LH-OAT compared to the methods used in the referenced studies should be addressed more clearly.

Response to 1b.

According to the comment, in the new version we put more emphasis on how the proposed method extends the former studies:

In this study, the various approaches of spatial sensitivity (or uncertainty) analysis presented above are compiled and extended in order to propose a method that would be generally applicable and thus would give a framework for inter-comparison of different models. Such a method would use a regular grid to quantify the spatial pattern of sensitivity as in Stisen et al. (2011), hence it differs from the irregular zonation in Younger et al. (2009). Furthermore, the perturbation of spatial input data in a general framework should be realized using a well-established algorithm, e.g. Latin-Hypercube One-factor-At-a-Time (LH-OAT) (van Griensven

et al., 2006). This change would give a straightforward interpretation of the sensitivity. Similarly, Hostache et al. (2010) used a well-established gradient method for spatial sensitivity analysis. However, unlike the gradient method, LH-OAT provides global insight into sensitivity. Such a method would also allow to quantify the sensitivity of spatial data with respect to the output and be able to explain the causes for the sensitivity patterns.

Comment 1c:

The authors should more clearly state for which purposes the spatial sensitivity analysis can/should be applied. Is the method for example suitable to locate areas which are, form a hydrological point of view, most or least suitable for deforestation, urbanization,..? This topic is now briefly addressed in section 3.3 but should also be addressed in the introduction.

Response to 1c:

We have modified section 4.4 (see the reviewed manuscript) and signalled the purpose also in the introduction as requested in the Reviewer's comment:

Main purpose of the application of spatial sensitivity analysis proposed in this study would be, after the Saltelli (2002) definition of sensitivity analysis, to quantify spatially the vulnerability of the model output to uncertainty of spatial input. Thus a result of this analysis would provide feedback e.g. where in a model domain a modeller should focus more on the quality of input data and parameters. However, the same method can be used for comprehensive spatial change (e.g. land-use change) analyses to show where the change (e.g. urbanization) would be least or most influencing the model output.

Comment 1d:

The sentence: ".. i.e.: is the uncertainty in different zones of the model dependent on the spatial patterns in the SCF" is unclear to me.

Response to 1d:

The sentence is now edited:

Purpose of this analysis is to show if the WetSpa model is spatially sensitive to SCF i.e.: identify zones where the model output is most vulnerable to input uncertainty.

Comment 2a:

The LH-OAT method is explained in section 2.4.1 while the spatial approach of the sensitivity is explained in section 2.4.3. I find this division somewhat confusing. It would be interesting to know what the ei, fi, j values used in this paper are while reading 2.4.1. The p number of parameters in

section 2.4.1 is for the spatial sensitivity analysis the number of snow zones? The authors might consider combining 2.4.1 and 2 .4.3.

Response to 2a:

According to the comment, the section 2.4.1 and 2.4.3 are now combined into "2.4.1 Spatial sensitivity analysis with Latin-Hypercube One-factor-At-a-Time algorithm". This combined section gives now a clear overview and presentation of the parameters in the spatial approach. For changes see the revised manuscript.

Comment 2b:

Do I understand correct that for each LH sampling the SCF is calculated by multiplying the SCF derived from the MODIS SCF by the ei? This would mean that for the sensitivity analysis the MODIS SCF is used only for the temporal dynamics? The SCF magnitude is sampled random between 0 and 1? If this is true this should be explained better in the data section about the MODIS SCF and/or around equation 1.

Response to 2b:

Yes, SCF is calculated by multiplying the SCF derived from the MODIS SCF by the ei. Indeed, the MODIS SCF is used only for the temporal dynamics. We now clarify this in the section "2.3 Data":

The in snow zones aggregated MOD10A1 SCF data was used to calibrate the WetSpa model. For the spatial sensitivity analysis, however, the daily time series of catchment averages of MOD10A1 SCF's were used, i.e.: the spatial pattern of SCF in snow zones was obtained by perturbing the catchment averages by random factors (Sect. 2.4.1).

In the section 2.4.1 we also address these issues:

Since e_i are randomly sampled the MOD10A1 data constrains only the temporal dynamic of SCF. Hence, results of the sensitivity analysis are interpretable in terms of SCF as input data in general, rather than in terms of MOD10A1 in particular.

The SCF magnitude is indeed sampled between 0 and 1, but as mentioned above, with respect to the temporal variability of MODIS data. It is explained in section 2.4.1:

The LH samples are taken from a uniform distribution ranging from 0 to 1.14, resulting in a range of 0 to 1 for the SCF in a snow zone (maximum mean SCF in the catchment was 88%, thus 1/0.88 = 1.14).

Note that, as explained at the beginning of the section 2.4.1, the LH samples (i.e. values of the e_i parameters) represent random multipliers for the daily averaged MOD10A1 SCF in the snow zones.

Comment 2c:

Figure 5 contains some interesting information regarding the methodology however some aspects remain unclear to me: 2c i. In the caption, check the references to left, right, left column, central column, right column? Is this correct?

Response to 2c i:

We have now corrected the referencing in the caption, so it can be interpreted correctly.

2c ii. Do the j snow zones refer to the 524 snow zones in the catchment? This is not clear

Response to 2c ii:

There was a typo in Figure 5, subscripts i and j were switched. The typo is now corrected. We also add clarification in the Figure 5 (now Figure 6) caption:

[...] e_i and e_{i+1} represent a fraction of the SCF in the snow zones i and i+1, [...].

2c iii. Do the 3 first rows refer to the simulations for the 524+1 for the first LH sample? Does the last row in the figure shows the first calculation of the second LH which also contains 525 calculations? This is not clear

Response to 2c iii:

As in the previous point the typo was corrected. Also we add information in the section 2.4.1. We change p.11997 l.4 from "[...] j is the current LH sample [...] to:

"[...] j is the current LH sample ranging between 1 and n [...]

2c iv. From section 2.4.3 I understood the perturbation factor fi was 1%, in the third row, the figure in the second row shows a perturbation factor of -1%? Why is this factor negative in this case?

Response to 2c iv:

According to the LH-OAT paper (van Griensven et al., 2006) f_i has a predefined magnitude (1% in our case) but its sign is random at each loop as the value can increase or decrease. We explain this in section 2.4.1 now:

[...] f_i is the fraction by which e_i was changed during the OAT perturbation, the sign of f_i is random at each loop as the value can increase or decrease. [...]

Comment 3a:

Separating this section in a results part and discussion part could improve the readability of this section. Consider this option.

Response to 3a:

The separation in two sections indeed makes the manuscript more clear, as the evaluation of the proposed method is now separated from the discussion about the functioning our study catchment.

Thus, according to the Reviewer's suggestion, we decided to split the results and discussion section. For changes see the revised version of the manuscript.

Comment 3b:

I understand you want to focus the sensitivity analysis on the spatial aspect but I would find it interesting to add a t-Q graph with the bounds from the SCF sensitivity analysis.

Response to 3b:

Such a hydrograph could be interesting for readers if one wants to see only the overall effect on discharge at the catchment outlet. This was one of the reasons we did not indicate the necessity of such a plot throughout the methods section. Another reason was that the main aspect of this work is the spatial look on the sensitivity. In our opinion, such a plot would distract a reader from the main idea of this research. Moreover, the multitude of response functions presented in Figure 8 (former Figure 7) describes in details and quantifies with numbers the discharge response, while a hydrograph with sensitivity analysis bounds would give just a general view and thus is less meaningful. As we understand this comment as a suggestion, we left the plot out of the manuscript.

Comment 3c:

Fig 6. the dates in the x-ax is not clear. Does the series start at the first of November, what is the time between the stripes?

Response to 3c:

Series starts at the first of November, this is an arbitrary beginning of the hydrological cycle in the study area (start of snow accumulation), see p.11998 l.25-27. Markers indicates beginning of a new month, however, the discharge is simulated daily. We changed the Figure 6 (now Figure 7) caption to make these issues clear:

Observed and simulated daily discharge from the calibrated WetSpa for the period in which the sensitivity analysis was conducted (upper panel). Also presented is WetSpa simulated groundwater and interflow discharge as well as only groundwater discharge. Catchment average daily temperature and SCF in the same period is presented in the lower panel. The ticks on the time axis indicate the 1st day of a month.

Comment 3d:

Discuss more in detail the maps representing the model output sensitivity to SCF presented in Figure 7. e.g. What does a high or low s_i^* value indicate? Why is the legend different for the figures in the last row?..

Response to 3d:

According to the request, the the detailed description of Figure 7 is provided in the sections 3.2.2, 3.2.3 and 3.2.4 (see the revised manuscript for changes). As well, we now address specifically the mentioned issues in section 2.4.1:

 s_i^* should be interpreted as a response measure of the changes in SCF in the snow zones to the value of F (.), a higher sensitivity stands for a stronger response and means that the model output is more vulnerable to uncertainty in a particular snow zone.

And in section 3.2:

The minimum, maximum and mean values are indicated on each map (Fig. 8). If the minimum is equal to 0, the model is completely insensitive in at least one snow zone for this response function. The values presented in the first four rows can be compared within a row, however, comparison between the rows is more difficult as in different rows the response functions concern discharge components of different magnitude. Note that the grey scale is different for all maps in the lowest row. This is because, unlike in the upper rows, the si* calculated from these response functions are not intended to be compared within this row as they concern different processes.

Comment 3e:

Section 3.3 would fit better in a separate discussion section. Additionally, a discussion about the number of simulations required for a spatial sensitivity would be interesting. The number of simulations applied in this study (52500) is difficult to achieve for some models. How could the number of simulation be reduced: e.g. less LH samples, less zones, which would be the better option?...

Response to 3e:

As requested, Section 3.3 is now in the discussion section. As well, we now provide our opinion about the number of simulations in new section "4.3 Computational constraints":

The total computation time, a product of simulation time and number of required runs, is a limitation of the applicability of this method and is similar as in all methods requiring a large number of model runs to achieve the desired output. This was also the case in this study, as WetSpa required about 1 minute for a single run, the total time for 52500 simulations was about 36.5 days. The advantage of any random sampling based sensitivity analysis method (including LH-OAT) is that it is easily parallelized, i.e. the LH-OAT samples are obtained before the simulations and the model runs are divided over a number of processors or computers.

One could, however, consider decreasing the number of zones (n) in which the input data is perturbed or the number LH samples (p) to receive the results faster. The latter implies that the LHOAT method may not converge (Nossent and Bauwens, 2012). Thus, it seems more reasonable to decrease the number of zones and be satisfied with results at lower spatial resolution.

Technical corrections:

All technical corrections were applied.

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Spatial sensitivity analysis of snow cover data in a distributed rainfall-runoff model

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Abstract. As the availability of spatially distributed data sets for distributed rainfall-runoff modelling is strongly growing, more attention should be paid to the influence of the quality of the data on the calibration. While a lot of progress has been made on using distributed data in simulations of hydrological models, sensitivity of spatial data with respect to model results is not well understood.

- In this paper we develop a spatial sensitivity analysis (SA) method for snow cover fraction method for spatial input data (snow cover fraction SCF) for a distributed rainfall-runoff model to investigate if the model is differently subjected to SCF uncertainty in different zones of the model. The analysis was focused on the relation between the SCF sensitivity and the physical, spatial parameters and processes of a distributed rainfall-runoff model. The methodology is tested for the Biebrza River catchment, Poland for which a distributed WetSpa model is setup to simulate two years of daily runoff. The SA sensitivity analysis uses the Latin-Hypercube One-factor-At-a-Time (LH-OAT) algorithm, which uses employs different response functions for each spatial parameter representing a 4 x 4 km snow zone. The results show that the spatial patterns of sensitivity can be easily interpreted by co-occurrence of different environmental factors such as: geomorphology, soil texture, land-use, precipitation and temperature. Moreover, the spatial pattern of sensitivity under different response
- precipitation and temperature. Moreover, the spatial pattern of sensitivity under different response functions is related to different spatial parameters and physical processes. The results clearly show that the LH-OAT algorithm is suitable for the our spatial sensitivity analysis approach and that the SCF is spatially sensitive in the WetSpa model. The developed method can be easily applied to other models and other spatial data.

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20 1 Introduction

Distributed hydrological models are developed to improve the simulation and analysis of physically based spatially distributed hydrological processes. While more spatially distributed parameters and input data are becoming available for modelling, most attention is paid to the influence of the data on the quality of the calibration and to the capacity of models to reproduce measured output time series. Several researchers focussed on the effect of using distributed precipitation data in hydrological models. Obled et al. (1994) showed with a semi-distributed TOPMODEL (Beven et al., 1995) application that although the number of stations used to generate a rainfall field appeared to have an important impact on discharge simulation, the response of the model to changes in the rainfall field was marginal. Schuurmans and Bierkens (2007) used the fully-distributed SIMGRO (Querner, 1997) model to analyse the effect of rainfall fields generated on basis of rain gauge and radar data on discharge, soil moisture and groundwater heads. In their study, the distributed data outperformed lumped data in the simulation results. A similar study was conducted by Fu et al. (2011) who used the MIKE SHE model (Abbott et al., 1986). However, in this case a clear effect of rainfall distribution was visible only on groundwater head and recharge. In summary, the advantage of spatially distributed precipitation over lumped data may vary, depending on the modeland, the study area used. These studies could be more easily compared if a universal approach to quantify the sensitivity of a model to spatially distributed input data or parameters would be available. Such a methodology should allow to quantify in which zones of a study area the sensitivity of spatially distributed data with respect to the output is higher or lower and point to the causes for these differences, and processes under consideration. Nonetheless, the spatial aspect of model parameters, input data and the way they are implemented in models clearly is an important research issue.

Several studies address classical sensitivity and uncertainty analysis methods to spatial data and parameters. An interesting stochastic uncertainty approach for spatial rainfall fields in the dynamic TOPMODEL (Beven and Freer, 2001) was presented by Younger et al. (2009). The results were obtained by dividing a catchment into homogeneous, irregular zones in which the precipitation was randomly perturbed by large factors. This Their study, however, focusses only on uncertainty and does not quantify rather on the model output uncertainty than on quantification of spatial sources of uncertainty., or spatial sensitivity.

Stisen et al. (2011) investigated if using Another study is presented by Stisen et al. (2011), who investigated if the use of spatially distributed surface temperature data in an objective function can provide robust calibration and evaluation of the MIKE SHE model compared to a lumped simulation. The study used a spatial perturbation of parameters by random factors between 0.75 to 1.25 in 2 km grid for the sensitivity analysis(SA), but the results were not analysed spatially. Thus no spatial pattern of sensitivity, showing which zones of the model are more vulnerable to uncertainty, was obtained.

Another spatial approach for SA-sensitivity analysis was presented by Hostache et al. (2010). In their work a local, gradient method was applied to conduct a SA-sensitivity analysis of the Manning coefficient in each mesh-computational node of a hydrodynamic model. The results shown This approach showed completely different sensitivity zonation than in the predefined land-use based Manning coefficient classes—used as a comparison scenario. This result stresses the importance of assessing the sensitivity in a spatially-distributed way.

While most of the research focusses on the rainfall fields, other In this study, the various approaches of spatial sensitivity (or uncertainty) analysis presented above are compiled and extended in order to propose a method that would be generally applicable and thus would give a framework for inter-comparison of different models. Such a method would use a regular grid to quantify the spatial pattern of sensitivity as in Stisen et al. (2011), hence it differs from the irregular zonation in Younger et al. (2009). Furthermore, the perturbation of spatial input data are also interesting, especially since remote sensing data is becoming more and more available. An important spatial parameter for hydrological modelling is imperviousness. The detailed remotely sensed distribution of impervious surfaces was tested against a standard, non-distributed, approach in the in a general framework should be realized using a well-established algorithm, e.g. Latin-Hypercube One-factor-At-a-Time (LH-OAT) (van Griensven et al., 2006). This change would give a straightforward interpretation of the sensitivity. Similarly, Hostache et al. (2010) used a well-established gradient method for spatial sensitivity analysis. However, unlike the gradient method, LH-OAT provides global insight into sensitivity. Such a method would also allow to quantify the sensitivity of spatial data with respect to the output and be able to explain the causes for the sensitivity patterns.

Main purpose of the application of spatial sensitivity analysis proposed in this study would be, after the Saltelli (2002) definition of sensitivity analysis, to quantify spatially the vulnerability of the model output to uncertainty of spatial input. Thus a result of this analysis would provide feedback e.g. where in a model domain a modeller should focus more on the quality of input data and parameters. However, the same method can be used for comprehensive spatial change (e.g. land-use change) analyses to show where the change (e.g. urbanization) would be least or most influencing the model output.

Important issue in this study is the selection of the hydrological model used to conduct the spatial sensitivity analysis. An option is the WetSpa model (De Smedt et al., 2000; Liu and De Smedt, 2004) . Remote sensing based estimation of impervious surfaces showed which shown to have a high sensitivity with respect to runoff prediction (Chormański et al., 2008; Verbeiren et al., 2013) and to give a considerably higher Nash-Sutcliffe efficiencies for discharge simulation as compared to the standard approach (Berezowski et al., 2012) when various scenarios of distributed impervious surfaces input data were tested (Chormański et al., 2008; Berezowski et al., 2012; Verbeiren et al., 2013) . Moreover, the WetSpa model was positively evaluated for possibility of utilizing distributed snow data from

a remote sensor (Berezowski and Chormański, 2011). Hence, the WetSpa model showed to be an interesting appropriate framework for analysis of spatially distributed phenomena.

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Another spatial issue is the selection of the input data used to conduct the spatial sensitivity analysis. A spatial data set, frequently tested and easier to obtain than rainfall fields, easy to obtain is snow cover. Snow cover fraction (SCF-SCF [-]) or snow water equivalent remote sensing products are widely available from a number of sensors. The different available products vary widely in spatial resolution (500 m to 25 km), temporal resolution (sub-daily to monthly) and temporal coverage (the oldest time series starts in 1966, while new products are regularly announced). One of the most frequently used remote sensing snow products comes from the MODIS instrument (Hall et al., 2006). Several studies show different strategies in respect to how hydrological models can benefit from snow cover data. A popular approach is to derive snow depletion curves from MODIS SCF SCF and use them in the Snowmelt Runoff Model - SRM (Martinec, 1975). This approach is still popular and used in recent studies (Lee et al., 2005; Tekeli et al., 2005; Li and Williams, 2008; Butt and Bilal, 2011; Tahir et al., 2011; Bavera et al., 2012). However, the SRM studies are focused mostly on the winter half-year and are limited to study sites where snowmelt processes are dominant. Another popular model which benefit from satellite derived SCF SCF is HBV (Sælthun, 1996); studies showing use of MODIS snow products are presented by Udnaes et al. (2007), Parajka and Blöschl (2008) and Sorman et al. (2009). Possibility of using MODIS SCF in In the WetSpa model was positively evaluated in Berezowski and Chormański (2011), while the MODIS snow products were used to evaluate spatial distribution of predicted snow cover in the WetSpa model (Zeinivand and De Smedt, 2010). The spatial sensitivity of model output to snow cover, despite its popularity as input data in distributed hydrological models, has not yet been evaluated.

The aim of this paper is to provide and test a methodology for a global spatial SA of SCF sensitivity analysis of SCF in a distributed rainfall-runoff model. Purpose of this analysis is to show if the WetSpa model is spatially sensitive to SCFSCF, i.e.: is the uncertainty in different zones of the model dependent on the spatial patterns in the SCF? identify zones where the model output is most vulnerable to input uncertainty. An important point of the analysis is to explain the existing patterns of spatial sensitivity in function of physical, spatial parameters used and hydrological processes in the study area. For the remainder of the paper, the section "Methods" presents the spatially distributed rainfall-runoff model WetSpa, the study area, data and spatial SAsensitivity analysis. In "Resultsand discussion" the output of the spatial SA of SCF sensitivity analysis of SCF for Biebrza River catchment is presented and described; the. The "Discussion" section presents the results in view of the hydrological processes occurring in the study area, but further applicability of the spatial SA method is also discussed in this sectionsensitivity analysis method and the limitation of the method (e.g. computation time) are also provided. The final section "Conclusions" presents recaps the main findings of the study.

2 Methods

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2.1 Hydrological model

Hydrological simulations The hydrological simulations in this study were conducted using the WetSpa model (Water and Energy Transfer between Soil, Plants and Atmosphere; De Smedt et al., 2000; Liu et al., 2003). The model divides a catchment into a regular grid with a specified dimension. In each grid cell, the water balance is simulated and the surface, interflow and groundwater discharge components are routed to the catchment outlet (Wang et al., 1996). Spatial parameters used to calculate the hydrological processes are obtained from land-use, soil and elevation input maps. Attribute tables based on literature data are linked to the maps and transformed to distributed physical values via a GIS preprocessing step (Chormański and Michałowski, 2011). Several studies have demonstrated that WetSpa and its steady state version WetSpass (Batelaan and De Smedt, 2007) are suited to integrate distributed remote sensing input data in the simulation of the hydrological processes (Poelmans et al., 2010; Dujardin et al., 2011; Ampe et al., 2012; Chormański, 2012; Demarchi et al., 2012; Dams et al., 2013).

The model consists of the following storages: interception, depression, root zone, interflow and groundwater. Water transport between the storages is based on physical and empirical equations. Rainfall, temperature and potential evapotranspiration based on data from meteorological stations are made spatially explicit by use of Thiessen polygons, but also a spatially distributed input form is possible.

In the standard WetSpa version, snow accumulation is calculated based on precipitation and a threshold temperature t_0 [°C]. If the temperature in a grid cell is t [°C] and falls below t_0 , precipitation is assumed to be snow. Snow melt is calculated based on t_0 , a degree-day coefficient k_{snow} [mm t°C $^{-1}$ day $^{-1}$] and coefficient t_{rain} [mm t(mm $^{-1}$ °C $^{-1}$ day $^{-1}$] reflecting the amount of snowmelt caused by rainfall t_{rain} [mm]. In this study t_0 SCF SCF was obtained from MODIS snow products and used as input data. Thus, snow accumulation was not calculated, but replaced with the input t_0 scF, SCF while the snowmelt amount t_0 [mm] per t_0 model time step (e.g. day) is calculated as:

$$55 \quad v_{sm} = SCF(k_{snow}(t - t_0) + k_{rain}v_{rain}(t - t_0))$$
(1)

This approach of calculating snowmelt based on SCF-SCF and snowmelt rate was proposed by Liston (1999). It allows to obtain a distributed v_{sm} values weighted by SCF-SCF from grid cells where SCF > 0. SCF>0. WetSpa is also capable to use an energy balance model for snowmelt calculation (Zeinivand and De Smedt, 2010), however, because of the higher demand on input data, this approach was not used.

Surface water routing is based on a geomorphological instantaneous unit hydrograph (IUH) (Liu et al., 2003). The IUH is calculated for a flow path starting in a grid cell and ending at the catchment

outlet, i.e. each grid cell has its own IUH. Groundwater flow and interflow are calculated on a sub-catchment level based on a linear reservoir method and routed to the catchment outlet with the IUH. Comparison of the WetSpa performance with other distributed hydrological models can be found in the results of the DMIP2 project (Safari et al., 2012).

The model was setup with a daily time step and 250 by 250 m grid cells. The calibration period was 1^{st} September 2008 till 31^{st} August 2009, while validation was from 1^{st} September 2007 till 31^{st} August 2008. The length of the calibration and validation was selected to optimize the model for snow conditions occurring in the period selected for SA (Section sensitivity analysis (Sect. 2.4.1). The global WetSpa parameters were calibrated using the Shuffled Complex Evolution algorithm (Duan et al., 1993). The calibration was conducted with the R software (R Development Core Team, 2013) and package "hydromad". The model was optimized to maximize the Nash and Sutcliffe (1970) efficiency (NS):

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$$NS = 1 - \frac{\sum_{x=1}^{\tau} (Q_x - \hat{Q}_x)^2}{\sum_{x=1}^{\tau} (Q_x - \bar{Q})^2}$$
 (2)

where: Q_x and \hat{Q}_x are observed and simulated discharges at time x, \bar{Q} is the mean observed discharge, τ is the total number of time steps. Sensitivity of the WetSpa model to the global parameters is presented in Yang et al. (2012).

2.2 Study area

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The study area is the Biebrza River catchment upstream from the discharge station at Burzyn. The total catchment area comprises 6845 km² (Fig. 1). Biebrza is a lowland catchment consisting of moraine plateaus and post-glacial valleys with low slopes (average 1.03 %, Fig. 2) and an elevation ranging from 102 m ASL at the catchment outlet to 298 m ASL at the northern water divide. Landuse is composed of agriculture (54%), forests (26%), wetlands and grasslands (17%), water (2%) and urban (1%) (Fig. 3). The area is considered as semi-natural, especially because of its large area of well preserved wetlands and forests and is therefore used as a reference area in wetlands research (Wassen et al., 2006). Several lakes in the northern part of the catchment are controlled by management schemes, which usually discharge into Biebrza tributaries after accumulation period. Lakes in WetSpa are modelled by setting appropriate values of the hydraulic parameters in the model e.g. by a high runoff coefficient and a low friction. The simulation of water management schemes in the controlled lakes is, however, not implemented. Dominant soil textures in the study area are sand (34%), loamy sand (26%) and sandy loam (18%), whereas minor parts are covered by sandy clay (4%) and silt (2%), other soils cover less than 1% of the area. In the river valley, organic soils are frequent and cover in total 16% of the study area (Fig. 4). The dominating landscape features, that certainly have influence on the functioning of the Biebrza hydrological system are the river valley and the large forest complex located in the north-eastern part of the catchment (Fig. 5).

The Biebrza River is characterized by a spring flood regime, the discharge of the spring flood is mostly related to the volume of snowmelt in the catchment (Stachý, 1987; Mioduszewski et al., 2004; Chormański and Batelaan, 2011). Based on the meteorological record from 25 stations and the flow record at the Burzyn profile (Fig. 1) managed by Polish Institute of Meteorology and Water Management - National Research Institute (IMGW) the study area can be characterized by the following figures. Mean yearly discharge (1951-2012) at Burzyn is 34.9 m³/s, while summer and winter average are respectively 26.0 and 43.9 m³/s. Recorded extreme low and high discharges (1951-2012) are 4.33 and 517 m³/s respectively. The climate in this area is transitional between continental and Atlantic, with relatively cold winters and warm summers, effectively making this area the coldest region in lowland Poland. The mean air temperature (1979-2009) is 7.0°C, in the winter half-year 0.3°C and in the summer half-year 13.7°C. The mean monthly temperature (1979-2009) has a maximum in July (17.6°C) and minimum in January (-3.3°C). The yearly precipitation (1979-2009) is 587 mm (375 mm in the summer half-year, 212 mm in the winter half-year). The yearly average number of days with temperature below 0°C (1979-2009) is 79 and with snow cover (1975-2012) is 93 (average snow depth is 12 cm). Based on the meteorological maps (Stachý, 1987; Rojek, 2000), the mean yearly evaporation from free water surface (1951-2000) is 550 mm, 465 mm in summer and 85 mm in winter (1951-1970).

2.3 Data

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Hydrometeorological data (precipitation, air temperature and discharge) was obtained from IMGW. Daily precipitation was obtained for 25 rain gauge stations, whereas air temperature was available for 5 stations (Fig. 1). Temperature was recorded as minimal and maximal minimum and maximum daily temperature, an average from these values was calculated to obtain the mean daily temperature for each station. Daily discharge was obtained for Burzyn. Potential evapotranspiration was estimated based on mean monthly evaporation from free water surface (Stachý, 1987) and uniformly disaggregated into daily values.

Daily SCF SCF was obtained from MODIS/TERRA snow product MOD10A1 (Hall et al., 2006, datasets used: IX 2007 to X 2009) with a 500 m resolution. The SCF SCF values in MOD10A1 are calculated based on the Normalized Difference Snow Index (NDSI):

$$NDSI = \frac{r_{vis} - r_{ir}}{r_{vis} + r_{ir}} \tag{3}$$

with r_{vis} and r_{ir} the reflectance in visible and in near-infrared bands, which for the MODIS sensor is respectively band 4 (545-565 nm) and band 6 (1628-1652 nm). In general, NDSI gives higher values if a larger part of a pixel is covered by snow. However, it may be affected by noise from many sources and has to be corrected for bias in forest areas (Klein et al., 1998). The MOD10A1 SCF—SCF input data was aggregated into 524 4 by 4 km snow zones, while zones close to the catchment boundary are fractions of a 4 km square. Purpose of the aggregation was to decrease

computation time of the SA sensitivity analysis and to reduce noise in the MOD10A1 data while keeping enough variability to obtain meaningful spatial results. In order to remove missing data related to cloud cover occurrence the SCF SCF in snow zones was linearly interpolated in over time. Finally, SCF SCF was set to 0 in months when there was no snow record recorded in lowland Poland, i.e. from May to September. The in snow zones aggregated MOD10A1 SCF data was used to calibrate the WetSpa model. For the spatial sensitivity analysis, however, the daily time series of catchment averages of MOD10A1 SCF's were used, i.e.: the spatial pattern of SCF in snow zones was obtained by perturbing the catchment averages by random factors (Sect. 2.4.1).

Spatial data (elevation, land-use and soil) used to calculate distributed model parameters were obtained from variable GIS sources. The elevation map (Fig. 1) was compiled from three sources: Digital Elevation Model of Poland in scale 1:26,000, digitized contours from the Topographical Map of Poland in scale 1:25,000 and from filed field surveys in the Biebrza valley. The land-use map (Fig. 3) was obtained from the Corine Land Cover 2006 project (Commission of the European Communities, 2013). In the catchment area outside the Polish border (56 km²), agricultural land-use was assigned. The soil map (Fig. 4) was obtained from the Soil Map of Poland in scale 1:50,000 for agricultural areas and 1:500,000 in forests and cities. Outside the Polish border the most frequent in the neighbourhood, sandy soil, was assigned. All the spatial data were interpolated to 250 m grid cells using the nearest-neighbourhood (soil, land-use) and the bilinear (elevation) algorithms.

250 2.4 Sensitivity analysis

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2.4.1 Spatial sensitivity analysis with Latin-Hypercube One-factor-At-a-Time algorithm

Latin-Hypercube One factor At a Time (LH-OAT)Usually a sensitivity analysis is performed for global parameters of a model (i.e. a set of parameters valid for the whole model area). The sensitivity analysis presented in this paper, however, follows a spatial approach, i.e. parameters are evaluated in different zones of the model area, as the parameter e_i represent a fraction of the daily averaged MOD10A1 SCF assigned into the zone i. In this study, each e_i is assigned to one of the 524 snow zones. Since e_i are randomly sampled the MOD10A1 data constrains only the temporal dynamics of SCF. Hence, results of the sensitivity analysis are interpretable in terms of SCF as input data in general, rather than in terms of MOD10A1 in particular.

LH-OAT (van Griensven et al., 2006) is an effective global sensitivity analysis method, similar to the Morris screening (Morris, 1991). The LH-OAT method is frequently used by SWAT users for ranking the the parameters according to their influence on the model output (Nossent and Bauwens, 2012). LH-OAT combines two different techniques. First, it selects n latin-hypercube (McKay et al., 1979) samples. Next, the LH points are used as starting points of p one-factor-at-a-time perturbations, where p is equal to the number of model parameters. A higher number of LH samples (n) will lead to a better convergence; a value of at least n = 100 is necessary to achieve convergence

(Nossent, 2012; Nossent et al., 2013). The method requires in total p(n+1) model evaluations to calculate the SA sensitivity analysis results. The sensitivity measure (final effect) for each i^{th} parameter is calculated by averaging partial effects for this parameter $(s_{i,j})$ from all LH samples (van Griensven et al., 2006):

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$$s_{i,j} = \frac{100 \left(\frac{F(e_1, \dots, e_i(1+f_i), \dots, e_P) - F(e_1, \dots, e_i, \dots, e_P)}{[F(e_1, \dots, e_i(1+f_i), \dots, e_P) + F(e_1, \dots, e_i, \dots, e_P)]/2} \right)}{f_i} \frac{100 \left(\frac{F(e_1, \dots, e_i(1+f_i), \dots, e_p) - F(e_1, \dots, e_i, \dots, e_p)}{[F(e_1, \dots, e_i(1+f_i), \dots, e_p) + F(e_1, \dots, e_i, \dots, e_p)]/2} \right)}{f_i} \frac{f_i}{f_i}$$

$$(4)$$

$$s_i = \frac{\sum\limits_{j=1}^n s_{ij}}{n} \tag{5}$$

where F(.) is a response or objective function of a model run with a set of e_1 to e_P e_p parameters, e_i is the current parameter, j is the current LH sample ranging between 1 and n; f_i is the fraction by which e_i was changed during the OAT perturbation. , the sign of f_i is random at each loop as the value can increase or decrease. Since the small snow zones at the catchment border would give relatively smaller sensitivity than similarly parametrized zones of bigger area, the s_i measure has to be normalized for non equal area (a_i) of snow zones. Thus, the normalised sensitivity (s_i^*) is defined as:

$$\dot{s}_i = \frac{s_i}{a_i} \tag{6}$$

 s_i should be interpreted as a response measure of the changes in SCF-SCF in the snow zones to the value of F(.), a higher sensitivity stands for a stronger response and means that a snow zone the model output is more vulnerable to uncertainty in a particular snow zone. This study design allows to obtain SCF sensitivity in each snow zone of the model. Insights into model sensitivity while simulating different processes can be achieved by using various response functions as F(.) (Sect. 2.4.2). The example of LH-OAT loops for spatial sensitivity analysis described above is presented in Fig. 6.

The experimental set-up for the spatial sensitivity was as follows. The values of the global parameters of the WetSpa model where the same as obtained from the model calibration. To be able to achieve convergence, a relatively large number of LH samples was selected (n=100). Together with the parameters representing the snow zones, p=524, this results in a total number of model evaluations of 52500. The LH samples are taken from a uniform distribution ranging from 0 to 1.14, resulting in a range of 0 to 1 for the SCF in a snow zone (maximum mean SCF in the catchment was 88%, thus $\frac{1}{0.88} = 1.14$). The perturbation f_i was set to 1%, in order to avoid that the OAT samples exceed the average distance between the LH samples. The sensitivity analysis was run for two full hydrological years from 1^{st} November 2007 till 31^{st} October 2009, preceded by a warm-up period of 2 months.

2.4.2 **Response functions**

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In order to investigate the relationship between parameters and different model processes, the SA sensitivity analysis was performed for a set of response functions (RF)F(.). A RF-response function quantifies a model behaviour, but unlike an objective function a RF-response function does not use observation (e.g. observed discharge). Table 1 lists the 15 RF's response functions which were used in the SAsensitivity analysis. This selection of RF's response functions allows to interpret the results in view of different components of the discharge as simulated by a number of model processes related to them. Moreover, the division into winter and summer half-years gives more insight into seasonal variability of the simulated results. The winter half-year response functions reflect processes occurring during snow accumulation and spring snowmelt, when the highest flows occur. On the other hand, the summer half-year response functions reflect processes occurring during the summer low flow period. Winter half-year RF response function were calculated for November until April, summer half-year RF-response function for May until October. The \bar{q}_{high} and \bar{q}_{low} reflect processes related to the highest and lowest flows. The \bar{v}_{sm} is calculated as the mean daily value of snowmelt [mm] and reflects processes related to snowmelt generation without routing.

2.4.3 Spatial approach

Usually a SA is performed for global parameters of a model (i.e. a set of parameters valid for 315 the whole model area). The SA presented in this paper however follows a spatial approach, i.e. parameters are evaluated in different zones of the model area, as the parameter e_i represent a fraction of the mean daily MOD10A1 SCF in the model catchment. Each e_i is assigned to one of the 524 snow zones. The resulting spatial distribution is random, but the dynamics of snowmelt and accumulation in time are preserved as in the observed MOD10A1 data. The example of LH-OAT loops for spatial SA is presented in Fig. 6. This study design allows to obtain SCF sensitivity in each snow zone of the model. The set of RF (Tab. 1) gives further insights into model sensitivity while simulating different processes.

Since the small snow zones at the catchment border would give relatively smaller sensitivity than similarly parametrized zones of bigger area, the s_i measure has to be normalized for non equal area (a_i) of snow zones:

$$\overset{\star}{s_i} = \frac{s_i}{a_i}$$

with $\frac{x}{i_i}$ the normalised sensitivity. The experimental set-up for the spatial sensitivity was as follows. The values of the global parameters of the WetSpa model where the same as obtained from the model calibration. To be able to achieve convergence, a relatively large number of LH samples was selected (n=100). Together with the parameters representing the snow zones, p=524, this results in a total number of model evaluations of 52500. The LH samples are taken from a

uniform distribution ranging from 0 to 1.14, resulting in a range of 0 to 1 for the SCF in a snow zone (maximum mean SCF in the catchment was 88%, thus $\frac{1}{0.88} = 1.14$). The perturbation f_i was set to 1%, in order to avoid that the OAT samples exceed the average distance between the LH samples. The SA was run for two full hydrological years from 1^{st} November 2007 till 31^{st} October 2009, preceded by a warm-up period of 2 months.

2.4.3 Output data analysis

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The spatial approach followed in this study gives a large output data set i.e. sensitivity maps based on different RFresponse functions. Each sensitivity map was analysed in view of 15 WetSpa parameter maps presented in Table 2. The Thiessen polygons for potential evapotranspiration were omitted, as there was only one polygon for the whole catchment.

In order to prepare the dataset for statistical analysis, each of the 15 parameter maps was spatially aggregated to fit the spatial extent of the SA sensitivity analysis results (s_i^*) —of the snow zones by calculating the mean (for continuous data) or the majority (for discrete data) of a parameter value in a snow zone. Based on this data set the coefficient of determination (ρ^2) was calculated for each pair of s_i^* and the aggregated parameter values. The ρ^2 describes the strength of the linear association between the variables by indicating the fraction of one variable's variance explained by the second variable. Since in literature the thresholds of ρ^2 for quantifying the strength of the linear association are vague, in this paper a $\rho^2 \geqslant 0.40$ is used as representing a moderate association. The selected threshold is justified by the fact that the $\rho^2 = 0.40$ is equivalent to the Pearson's correlation coefficient of 0.63, which is generally considered as representing a strong relationship between variables.

3 Resultsand discussion

3.1 Model calibration and performance

The calibrated model shows a good performance with high efficiencies: NS=0.86 for the calibration period, NS=0.73 for the validation period and NS=0.79 for the whole period. The snow related global WetSpa parameters were estimated during the calibration as: k_{snow} = 5.03 mm °C⁻¹day⁻¹, k_{rain} = 0.02 mm mm⁻¹ °C⁻¹day⁻¹. The comparison of observed and simulated discharge is presented in Fig. Figure 7. 90% of the simulated discharge at the catchment outlet has a groundwater origin, while surface runoff (5.3%) and interflow (4.7%) contribute mostly to the highest peaks (Fig. 7), which is in qualitative agreement with Pajnowska et al. (1984). The model performed very well during snowmelt-supplied spring floods. The peaks were underestimated by 8% of the observed value on average, but the shape of the events resembled very well the observed values, which can be an advantage of using observed SCF data instead of predicting snow cover in the model. This is supported by the comparison of the hydrograph (upper part of Fig. 7) with the timing of snowmelt

and temperature rise above 0 °C (lower part of Fig. 7), which shows a rapid discharge rise at the beginning of spring floods. Good results of using MODIS snow products in other hydrological models have also been shown by Lee et al. (2005); Udnaes et al. (2007); Şorman et al. (2009); Tahir et al. (2011). The model performed worse during periods of intensive summer storms. For these storms, a rapid discharge rise was simulated, which was not observed in reality. A possible reason for this low performance is the positively biased soil moisture prediction of the model during these periods.

3.2 Spatial sensitivity analysis

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The maps presenting model output sensitivity $\frac{1}{5}$ (with different RF) global model output sensitivities $\frac{1}{5}$ to variations of $\frac{1}{5}$ Spatial SCF are presented in Fig. Figure 8. The use of different RF response function results in different patterns of spatial sensitivity, although some similarities can be distinguished as well. The minimum, maximum and mean values are indicated on each map (Fig. 8). These values are however obtained for different RF and can therefore not be compared with each other. Nevertheless, if If the minimum is equal to 0, the model is completely insensitive in at least one snow zone for this RF. The response function. The values presented in the first four rows can be compared within a row, however, comparison between the rows is more difficult as in different rows the response functions concern discharge components of different magnitude. Note that the grey scale is different for all maps in the lowest row. This is because, unlike in the upper rows, the $\frac{1}{5}$ calculated from these response functions are not intended to be compared within this row as they concern different processes.

The analysis of ρ^2 values (Tab. 3) explains the spatial relations between SCF—SCF sensitivity with different RF response function and the spatial parameters. Most of the pairs in Tab. Table 3 have low ρ^2 indicating suggesting that a parameter was not relevant for sensitivity with this RF response function. However, for most of the RF response functions at least one $\rho^2 \geqslant 0.40$ was found, indicating that the SCF sensitivity with these RFs response functions can be partially explained by the values of the parameter maps. The values of ρ^2 show influential and unimportant spatial parameters for the SCF—SCF sensitivity i.e. for the snow related processes. Another aspect of the results, when looking at the spatial sensitivity patterns, is that higher sensitivity areas are more vulnerable to uncertainty in the input data. This feature can be used to highlight the areas which require more attention during the parametrization. Detailed analysis of Fig. 8 and Tab. 3 is provided in the subsequent subsections.

3.2.1 General relations of the spatial SA sensitivity analysis results with parameters maps

The last column of Table 3 shows the frequency of the parameters with moderately strong coefficient of determination under different RFsresponse functions. The most frequent occurring parameter with a coefficient of determination above the threshold (0.40) is slope(*slp*). *slp* is very important for calculating hydraulic parameters(e. g. manning coefficient), but also tunes values of depression

storage and potential runoffcoefficient. The second most frequent is the group of soil texture related parameters: wilting point, hydraulic conductivity, porosity, residual soil moisture and field capacity. The lowest frequency is observed for maximal and minimal interception, initial soil moisture and root depth, as well as for parameters responsible for generating surface runoff: runoff coefficient and depression storage.

The scatter plots of slp against different RFs (Figure 9) shows the slope versus different response functions (Fig. 9) show that this parameter explains nearly linear strongly correlates with the spatial sensitivity quantified with \bar{q} , $\bar{q}i$ and $q\bar{q}g$ and their winter/summer half-years equivalents. However, when looking closer at the plots for these RFs-response functions the lower values of slp-the slope (0.0% - 0.5%) give steeper relation with less scatter than higher slp-values. This means that even when slope values.

3.2.2 Discharge source response functions

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Using \bar{q} and \bar{q}_w as response function resulted in a clear pattern differentiating the upland from the valley (cfr. Fig 8 and Fig. 5), showing that SCF zones occurring in the flat, organic-soil dominated valley is much less sensitive than in the mineral upland. High sensitivity is obtained in snow zones with steeper slopes (cfr. Fig 8 and Fig. 2), what is confirmed by high ρ^2 values are high (Table 3) with the slope (Tab. 3). Several WetSpa parameters (mostly soil texture dependent: depression storage, wilting point, field capacity, porosity, residual soil moisture content) have high ρ^2 with \bar{q} and \bar{q}_w response functions (Tab. 3).

Some differences between \bar{q} and \bar{q}_8 are visible when analysing the ρ^2 (Tab. 3). The SCF sensitivity for \bar{q}_8 has higher ρ^2 for parameters that are related to groundwater flow, like: porosity, residual soil moisture content, field capacity and pore size distribution index.

When comparing \bar{q} , the spatial sensitivity can be explained by a given parameter only in a certain range of its values \bar{q}_w and \bar{q}_s with $q\bar{q}_s$, while for the remaining values the correlation is not that strong. $q\bar{q}_w$ and $q\bar{q}_s$ with respect to spatial patterns (Fig. 8) and ρ^2 (Tab. 3), the figures are very similar. The group of parameters responsible for groundwater processes (porosity, residual soil moisture content, field capacity and pore size distribution index) have higher ρ^2 with the groundwater response functions $q\bar{q}_s$ and $q\bar{q}_w$ than with $q\bar{q}_s$ and $q\bar{q}_w$.

The second most frequent is the group of soil texture related parameters: wilting point (w_p) , 430 hydraulic conductivity (h_eon) , porosity (por), residual soil moisture (res) The SCF sensitivity for $q\bar{s}$ and field capacity (f_e) $q\bar{s}_w$ differentiates the river valley and the north-western upland catchment from the south-eastern upland (cfr. Fig 8 and Fig. 5). The maps of SCF sensitivity for $q\bar{s}$ and $q\bar{s}_w$ are the only one that show clearly a relatively higher sensitivity in the river valley than in most of the upland.

The SCF sensitivity for the interflow response function differs from the groundwater and surface water response function results. The spatial pattern of SCF sensitivity for $q\bar{i}$ and $q\bar{i}_w$ seems opposite to the pattern of $q\bar{s}$ and $q\bar{s}_w$.

3.2.3 Extreme discharges response functions

The SCF sensitivity for \bar{q}_{high} and \bar{q}_{low} presents a spatial pattern that can not be visually related to land-use, soil, or slope maps (Fig. 8). These response functions do not correlate with any of the WetSpa spatial parameters (Tab. 3). The spatial pattern of \bar{q}_{high} shows high values both in the upland and in the valley, however it has also some zones of low sensitivity in the central part of valley. Low but noticeable ρ^2 is found only with the slope. The spatial pattern of \bar{q}_{low} is quite uniform, with some higher values in the western uplands, lower values in the central part of the valley and in flat regions in the northern upland (cfr. Fig 5 and Fig. 8).

3.2.4 Mean snowmelt response function

The pattern of \bar{v}_{sm} shows random values with different means in different Thiessen polygons for temperature stations used in the model (Fig. 8). This pattern is confirmed by high ρ^2 between v_{sm} and temperature, with no other parameters having noticeable ρ^2 (Tab. 3).

The groundwater dominated discharge composition obtained with the calibrated model is in conceptual

450 4 Discussion

4.1 Model calibration and performance

agreement with Pajnowska et al. (1984). The model performed well during snowmelt-supplied spring floods. Although, the peaks were underestimated by 8% of the observed value on average. The 455 peak discharges underestimation are possibly determined by the uncertainty of the rating curve. During the yearly spring floods, the measurement profile near the gauging station widens outside the riverbed and extends into the densely vegetated floodplain, where proper hydraulic measurements are very difficult. Nonetheless, the shape of the events resembled well the observed values, which can be an advantage of using observed SCF data instead of predicting snow cover in the model. 460 This is supported by the comparison of the hydrograph (upper part of Fig. 7) with the timing of snowmelt and temperature rise above 0 °C (lower part of Fig. 7), which shows a rapid discharge rise at the beginning of spring floods. Good results of using MODIS snow products in other hydrological models have also been shown by Lee et al. (2005); Udnaes et al. (2007); Parajka and Blöschl (2008); Sorman et al. (2009); Tahir et a The model performed worse during periods of intensive summer storms. For these storms, a rapid discharge rise was simulated, which was not observed in reality. A possible reason for this low 465 performance is the positively biased soil moisture prediction of the model during these periods.

4.2 Spatial sensitivity analysis

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The global model output sensitivities (\dot{s}_i) are calculated for a regular-structured grid (Fig. 8). This approach may be considered not perfect, as irregular, homogenous zonation (Younger et al., 2009) could more directly reference the sensitivity to spatial features of the model. Regular zonation used in this study was similar as in Stisen et al. (2011). This approach implies that the borders of spatial features do not resemble the zonation and the results are somewhat aggregated. Advantage of structured grid lies, however, in broad comparability of different models, e.g. spatial sensitivity analysis in a study area modelled with different spatial discretization like hydrological response unit (SWAT) or grid cell (WetSpa) could be easily compared when using the structured grid. Moreover, irregular approach would require much more zones if very fine spatial features were to be analysed. This would require additional computational time, as the number of zones determines the number of parameter for the sensitivity analysis (see Sect. 4.3 for further discussion on this topic).

Computational time could be decreased if other methods than LH-OAT would be used. Spatial sensitivity calculated based on a gradient method was presented by Hostache et al. (2010). Their results, although showing the importance of spatial sensitivity analysis, were calculated using a local method. Local methods are not handling properly the non-linear models (Turanyi and Rabitz, 2000). On the contrary, the method presented in this study results in a global sensitivity, i.e.: covering the whole parameter space and thus giving more insight into the model behaviour than a local method. There is still room for selecting other method for spatial sensitivity. Interesting results could be obtained when a variance-based method, like Sobol' (Sobol', 1993) would be used. Such an analysis would give additionally to LH-OAT information on interactions between the model parameters.

4.2.1 General relations of the spatial sensitivity analysis results with parameters maps

The reason why most sensitivity maps calculated for different response functions (Fig. 8) were correlated with slope (Tab. 3) is because slope has a large impact on other hydraulic parameters (e.g. manning coefficient), but also tunes values of depression storage and potential runoff coefficient (Liu and De Smedt, 2004).

A number of sensitivity maps were correlated with soil texture related parameters. These parameters have an influence on directing water that is stored as soil moisture, thus have general impact on groundwater, interflow and infiltrability. The soil texture related parameters have higher frequencies than the land-use related parameters (cfr. Table 2 and Table Tab. 2 and Tab. 3). This means that soil texture is a clearly more important WetSpa input than land-use with regard to the SCF SCF sensitivity. The reason may be that the groundwater discharge accounts for 90% of the total simulated discharge and the parametrization of the groundwater processes is strongly dependent on soil properties in WetSpa.

The lowest frequency is observed for maximal and minimal interception $(i_max \text{ and } i_min)$, initial soil moisture (i_sm) and root depth (r_d) . For the i_max and i_min . Some of the WetSpa parameter maps, have a ρ^2 not above the selected threshold for any of the sensitivity maps. In case of the interception related parameters the explanation is that the interception capacity is important in the summer half-year, when no SCF-SCF is present. A similar explanation holds for the r_d evapotranspiration parameter, root depth (an evapotranspiration-related parameter) which has a relatively negligible importance in the winter half-year. In case of i_sm , the low frequency may be related to the fact that initial soil moisture content affect the explanation could be that it affects mostly the beginning of the simulation, i.e. the warm-up period.

Low frequency is also observed for runoff coefficient (r_e) and depression storage (dep), which are, among others, the most important parameters Parameters responsible for generating surface runoff. The low frequencies of these parameters also did not have ρ^2 above the selected threshold for any of the sensitivity maps. This is explained by the fact that the catchment is not urbanized and areas of high r_e and low dep runoff coefficient and low depression storage are not frequent in this area. This situation is expected to be different for urbanized catchments, where the surface runoff would participate more in the total discharge than in this study area (Berezowski et al., 2012).

The frequency analysed in this subsection here is obviously dependent on the value of the ρ^2 threshold (in this case 0.40). The threshold is subjective, however, discriminates well allows discriminating between the high and low ρ^2 . The selected threshold is justified by the fact that the $\rho^2 = 0.40$ is equivalent to the Pearson's correlation coefficient of 0.63, which is generally considered as representing a strong correlation between variables. Nevertheless, the results should be viewed also in scope of the ρ^2 values themselves.

4.2.2 Discharge source response functions

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The analysis of correlation between slope and sensitivity maps provided in more details in Figure 9 shows that even when ρ^2 values are high (Tab. 3), the spatial sensitivity can be explained by a given parameter only in a certain range of its values, while for the remaining values the correlation is not that strong. This shows the complexity of the presented analysis. It has to be taken into account that the values presented in Table 3 shows only the general relation with the sensitivity maps (Fig. 8) while at different ranges of the analysed values different model behaviour is expected.

4.2.2 Spatial sensitivity in scope of the Biebrza River catchment functioning

All the sensitivity maps calculated for the winter half-year RF response functions resemble the full year RF response functions, both in the ρ^2 (Tab. 3) and in the spatial pattern (Fig. 8). This means that when looking at SCF SCF sensitivity, the winter processes dominate the whole year. The reason for this lies in the fact that snowmelt water is routed mostly in winter and spring, while in summer water routing is only affected by remaining snowmelt water in soil moisture and groundwater reservoirs.

Using \bar{q} and \bar{q}_w as RF resulted in a clear pattern differentiating the upland from the valley (cfr. Fig 8 and Fig. 5), showing that SCF zones occurring in the flat, organic-soil dominated valley is much less sensitive than in the mineral upland. High sensitivity is obtained in snow zones with steeper slopes (cfr. Fig 8 and Fig. 2), what is confirmed by high ρ^2 with slp (Tab. 3). Several WetSpa parameters (mostly soil texture dependent dep, w_p , f_peap , por, res) have high ρ^2 with these RFs (Tab. 3), which identifies a strong link between SCF sensitivity and general model behaviour. Moreover, this confirms the suitability of WetSpa for the selected study area and processes occurring within it. The parameters with lowest ρ^2 were: i_pmax , i_pmin and r_pmin , which are responsible for processes in summer half-year.

Some differences between \bar{q} and \bar{q}_s are visible when analysing the relationship strength (Tab. 3). The SCF sensitivity for \bar{q}_s has stronger relationship with parameters important for groundwater processes, like: por, res, f_eap and pore size distribution index (p_ind) . Thus, the SCF A confirmation that SCF appears to influence summer half-year discharges more by groundwater than by surface runoff.

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When comparing \bar{q} , \bar{q}_w and is its the sensitivity for \bar{q}_s with $q\bar{g}$, $q\bar{g}_w$ and $q\bar{g}_s$ with respect to spatial patterns (Fig. 8) and ρ^2 (Tab. 3), the figures are very similar. Obviously, the group of parameters responsible for groundwater processes (por, res, f_-eap and p_-ind) have higher ρ^2 with the groundwater RF's $q\bar{g}$ and $q\bar{g}_w$ than with $q\bar{g}$ and $q\bar{g}_w$. It is clear that the groundwater which has strong correlation with parameters related to groundwater flow. Nonetheless, the groundwater discharge dominates the total discharge in the model of Biebrza River catchment when looking at the similar results for the total discharge and groundwater discharge RF. This result response functions. This is also confirmed in functioning of the Biebrza River catchment as described in literature (Pajnowska et al., 1984; Batelaan and Kuntohadi, 2002; Wassen et al., 2006; Chormański et al., 2011a).

The SCF sensitivity for This surface runoff response functions (\bar{qs} and \bar{qs}_w differentiates the river valley and the north-western upland catchment from the south-eastern upland (cfr. Fig 8 and Fig. 5). This) sensitivity pattern may be related to the soil properties. As presented in Fig. Figure 4, the SE upland is dominated by loamy sand ($h_con = 1.7 \times 10^{-5} \text{ m/sms}^{-1}$), while much lower hydraulic conductivities are observed in the river valley (dominated by organic soils $h_con = 5.6 \times 10^{-6} \text{ m/sms}^{-1}$) and the NW upland (big share of sandy loam $h_con = 6.9 \times 10^{-6} \text{ m/sms}^{-1}$). The soil-sensitivity pattern is confirmed by the high ρ^2 with h_con the hydraulic conductivity and weak, but noticeable ρ^2 with r_e . The the runoff coefficient. Thus, the infiltration ability and surface water routing , plays an important role have a considerable effect in explaining the SCF SCF sensitivity for surface runoff. The maps of SCF sensitivity for $q\bar{s}$ and $q\bar{s}_w$ are the only one that show clearly a Another important role of surface runoff is revealed by relatively higher sensitivity of $q\bar{s}_w$ in the river valley than in most of the upland. This may be related to the fact that snowmelt in the Biebrza River valley is a considerable water source to spring floods and is transported as surface runoff (Chormański et al., 2011b).

The SCF sensitivity for $q\bar{s}_s$ shows a similar pattern as for opposite pattern to $q\bar{s}$, but faded (Fig. 8). As mentioned before, summer runoff is only influenced by SCF through antecedent soil moisture conditions, which in case of $q\bar{s}_s$ may be linked to the strong relationship with p_ind .

The SCF sensitivity for the interflow RF differs from the groundwater and surface water RF results. The spatial pattern of SCF sensitivity for is visible in $\bar{q}i$ and $\bar{q}i_w$ seems opposite to the pattern of $q\bar{s}$ and $q\bar{s}_w$. In the WetSpamodel the interflow, what may be explained by the way the interflow is modelled in WetSpa. Interflow depends not only on h_con the hydraulic conductivity (the key parameter for explaining sensitivity for $q\bar{s}_wq\bar{s}$), but also on slp the slope ($\rho^2=0$ for $q\bar{s}$), which is important for related to routing water in the subsoil and, thus shows high ρ^2 with SCF SCF sensitivity for $q\bar{i}$ and $q\bar{i}_w$. (Tab. 3).

No $\rho^2 \geqslant 0.40$ are found for the SCF-SCF sensitivity for qi_s (Tab. 3). In this case, the role of the parameters is limited. This is probably because most of the interflow water that could be related to SCF-SCF produced discharge during winter half-year. The highest ρ^2 , similarly like for qi and qi_w , is found with slpthe slope, which can also be easily linked by similarity of spatial patterns with the SCF-SCF sensitivity map (cfr. Fig. 2 and Fig. 8).

4.2.3 Extreme discharges response functions

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The SCF sensitivity for Similarly, no $\rho^2 \geqslant 0.40$ are found for the SCF sensitivity for \bar{q}_{low} and \bar{q}_{high} presents a spatial pattern that can not be visually related to land-use, soil, or slope maps (Fig. 8). The spatial pattern shows high values both in the upland and in the valley, however it has also some zones of low sensitivity in the central part of valley. Low but noticeable ρ^2 is found with slp indicating a link with runoff generation in WetSpa. Thus slp may directly influence the 10% highest discharges and the SCF sensitivity. Nevertheless (Tab. 3). Thus there are other sources of variance in the SCF sensitivity for \bar{q}_{high} SCF sensitivity for these response functions, which do not have an origin originate directly in the parameter maps. Detailed precipitation conditions and timing is e.g. not fully reflected by the aggregated P. Only a low but noticeable ρ^2 is found between \bar{q}_{high} and the slope indicating a link with runoff generation in WetSpa.

The spatial pattern of SCF sensitivity for \bar{q}_{low} is quite uniform, with some higher values in the western uplands, lower values in the central part of the valley and in flat regions in the northern upland (cfr. Fig 5 and Fig. 8). The pattern of \bar{q}_{low} may also be related to extreme groundwater deficits to which mineral soils in the uplands have a higher contribution than organic saturated soils in the valley (por porosity has low, but noticeable ρ^2). The spatial pattern of soil moisture in the Biebrza River valley presented by Dabrowska-Zielińska et al. (2009) partially confirms the spatial SA sensitivity analysis results presented in this paper.

4.2.3 Mean snowmelt response function

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A completely different pattern than for the other RF response functions is presented by SCF SCF sensitivity for \bar{v}_{sm} (Fig. 8). According to the eqEq. 1, v_{sm} in a model grid cell (and thus \bar{v}_{sm} in the entire catchment) is calculated based on temperature and precipitation, and then adjusted by SCFSCF. Hence, the sensitivity for \bar{v}_{sm} corresponds with the spatial pattern of the mean yearly temperature averaged in the Thiessen polygons(T), while yearly sum of precipitation in the Thiessen polygons (P) is less influential. The pattern of SCF SCF is not visible, because in this analysis the SCF values in eqsensitivity analysis the SCF values in Eq. 1 come from the random LH-OAT sampling. The reason that ρ^2 between v_{sm} and T and P \bar{v}_{sm} and temperature and precipitation is lower than 1.00 is because the values are aggregated in time and space and lose some of the variance important for the relation.

4.3 Applicability of the spatial SAComputational constraints

The total computation time, a product of simulation time and number of required runs, is a limitation of the applicability of this method and is similar as in all methods requiring a large number of model runs to achieve the desired output. This was also the case in this study, as WetSpa required about 1 minute for a single run, the total time for 52500 simulations was about 36.5 days. The advantage of any random sampling based sensitivity analysis method (including LH-OAT) is that it is easily parallelized, i.e. the LH-OAT samples are obtained before the simulations and the model runs are divided over a number of processors or computers.

One could, however, consider decreasing the number of zones (n) in which the input data is perturbed or the number LH samples (p) to receive the results faster. The latter implies that the LH-OAT method may not converge (Nossent and Bauwens, 2012). Thus, it seems more reasonable to decrease the number of zones and be satisfied with results at lower spatial resolution.

4.4 Applicability of the spatial sensitivity analysis

The analyses conducted in this case study are both a validation and an example application of spatial SA sensitivity analysis method. The further potential use of this method could be twofold: for generic sensitivity analysis and for a catchment change scenario analysis.

The generic sensitivity analysis would be similar to the presented approach in this paper. The sensitivity maps (e.g. Figure Fig. 8) would show zones of the catchment with high or low sensitivity. The correlation analysis as in Table 3 would show the parameters explaining the sensitivity pattern which thus require more attention during the parametrization. This would require possibly denser field sampling of the correlated parameters additionally to the data subjected to sensitivity analysis, or obtaining the parameters form data from a source with less uncertainty; as a result the prediction uncertainty would should be decreased. Additionally, the detailed scatter plots of parameters against

RFs response functions (e.g. Figure Fig. 9) would show which data ranges of the parameters are the most responsible for the spatial sensitivity pattern. In contrast the "standard" SA sensitivity analysis is performed for global parameters which usually are not spatially distributed, or are semi-distributed (i.e. grouped to few categories with the same values; e.g. Ayvaz, 2013).

The catchment change scenario analysis was not investigated in this paper but is a possible application of the presented spatial SA algorithmsensitivity analysis method. In such an analysis instead for SCF of SCF input time series the LH-OAT sampling would be done for e.g. different land covers proportions in the catchment zones. The output of such an analysis would be sensitivity of the zones to changes in land cover and could be used as e.g. a stochastic decision support for urban development.

650 5 Conclusions

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With increasing spatial data availability for distributed hydrological modelling a need appears for a methodology for sensitivity analysis of the spatial data. Such a methodology should point to zones of the study area where the sensitivity of a model spatial input to output is higher or lower and should relate these patterns to the processes simulated by the model. In order to answer these needs this paper presents an application of the LH-OAT sensitivity analysis to the WetSpa model of the Biebrza River catchment. Unlike a standard SA sensitivity analysis of global model parameters, a spatial approach is presented in this study. The catchment is divided into regular snow grid cells or zones in which sensitivity of SCF SCF as input data was evaluated. The aim of this study was to present an approach for using SA sensitivity analysis for spatial input data and to show that the WetSpa model is sensitive to spatial input data. Moreover, it was intended to show that the spatial sensitivity results are related to physical parameters used in the model.

The spatial approach of the LH-OAT SA sensitivity analysis results in spatial maps presenting areas of relatively higher and lower sensitivity. In order to extend the analysis, the SA sensitivity analysis was repeated with different response functions (RF). Most of the SA sensitivity analysis results were similar for the whole year and winter-half year RF response functions. Moreover, the sensitivity obtained for the mean discharge RF response function was very similar to the SA sensitivity analysis for the mean groundwater discharge RF response function. Hence, the snow-processes related model behaviour is dominated by winter half-year and groundwater processes, which is in agreement with the Biebrza River spring flood regime with a dominant share of groundwater discharge. Another important finding was that SCF SCF sensitivity was high in snow zones in the river valley under the winter half-year surface runoff RF response function. This is in agreement with the observation that the snowmelt in the river valley is a considerable surface runoff source to spring floods.

In this case study, the spatial patterns of SCF-SCF sensitivity could, for most of the RFresponse functions, easily be interpreted by co-occurrence of different landscape features like upland and river valley. However, for some of the RF-response functions a straightforward interpretation was impossible. A successful approach to interpret the patterns was performed by analysing the values of coefficients of determination between the physical model parameters and the SCF-SCF sensitivity. The spatial pattern of the sensitivity for different RFresponse functions, obtained from these results, is related to different spatial parameters and to different physical processes simulated by the model. The parameters which had a strong relationship with the SCF correlation with the SCF sensitivity for most of the RF-response functions were: slope, and the soil related parameters. The potential runoff coefficient and depression storage were important for only a few RP'sresponse functions, because the catchment is not urbanized. The temperature Temperature, which directly influences the snowmelt generation in the WetSpa model, shows a strong relationship correlation only with the mean snowmelt RFresponse function. It is important to mention that the spatial sensitivity quantified with several RP's response functions was correlated to more than one spatial parameter. This shows the importance of the links between the parameters and which were revealed by this spatially distributed analysis.

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In summary, a spatial approach of SA-sensitivity analysis can be performed with the LH-OAT algorithm, as presented in the results of this paper, and the SCF-SCF is spatially sensitive in the WetSpa model. The pattern of spatial sensitivity is related to spatially distributed physical parameters, the results are confirmed by a priori scientific understanding of the Biebrza River catchment functioning. The spatial sensitivity maps can by used to highlight areas which require better attention during the parametrization and to show which spatial parameters have influence on the analysed phenomena, in this case the snow related processes.

In future work, other input time series or input parameters should be evaluated in a spatial analysis. It would also be interesting to compare spatial sensitivity of the same input data with other models e.g. TOPMODEL or SWAT. Finally, since spatial <u>SCF_SCF</u> is sensitive in WetSpa, other sources of this input data should be tested in the model.

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Table 1. The descriptions Descriptions and abbreviations of the 15 response functions (RF's-) which were used in the SAsensitivity analysis.

Description	RF abbreviation					
Description	yearly	winter	summer			
mean simulated discharge	$ar{q}$	$ar{q}_w$	$ar{q}_{\overline{w}}ar{q}_{ar{s}}$			
mean simulated discharge from surface runoff	$q\bar{s}$	$q\bar{s}_w$	$q\bar{s}_s$			
mean simulated discharge from interflow	$ar{qi}$	\bar{qi}_w	$ar{qi}_s$			
mean simulated discharge from groundwater	$q\bar{g}$	$ar{qg}_w$	$q \bar{g}_s$			
mean of the highest 10% simulated discharges	\bar{q}_{high}	-	-			
mean of the lowest 10% simulated discharges	\bar{q}_{low}	-	-			
mean simulated snowmelt	\bar{v}_{sm}	-	-			

Table 2. The WetSpa parameter maps used to analyse the SA sensitivity analysis results. The generic input maps used to derive the parameters maps are marked with + if used and - if not used.

		Generic input map					
Parameter	Abbreviation	Soil	Land-use	Elevation			
slope	slp	-	-	+			
hydraulic conductivity	h_con	+	-	-			
soil field capacity	f_cap	+	-	-			
maximal interception	i_max	-	+	-			
minimal interception	i_min	-	+	-			
pore size distribution index	p_ind	+	-	-			
soil porosity	por	+	-	-			
residual soil moisture content	res	+	-	-			
root depth	r_d	-	+	-			
wilting point	w_p	+	-	-			
runoff coefficient	r_c	+	+	+			
depression storage	dep	+	+	+			
initial soil moisture content	i_sm	+	-	+			
Thiessen polygons for temperature	T		from the stations				
Thiessen polygons for precipitation	P		from the stations				

Table 3. The ρ^2 values calculated between for the WetSpa distributed parameters (rows) and the SCF SCF sensitivity maps under different RFs response functions (columns). The $\rho^2 \geqslant 0.40$ are bold; the frequency that this condition is true is summarized (\sum) in the last row and column. Explanation of the RFs response functions and parameters is presented in Tables 1 and 2.

	$ar{q}$	$ar{q}_w$	$ar{q}_s$	$q\bar{s}$	$q\bar{s}_w$	$q\bar{s}_s$	$ar{qi}$	$ar{q}i_w$	\bar{qi}_s	$q\bar{g}$	$q\bar{g}_w$	$q\bar{g}_s$	\bar{q}_{high}	\bar{q}_{low}	\bar{v}_{sm}	Σ
slp	0.58	0.58	0.48	0.00	0.00	0.02	0.45	0.44	0.23	0.56	0.56	0.45	0.36	0.12	0.09	8
h_con	0.00	0.00	0.00	0.40	0.40	0.28	0.16	0.15	0.11	0.00	0.00	0.00	0.01	0.00	0.00	2
f_cap	0.25	0.20	0.41	0.15	0.15	0.02	0.24	0.24	0.14	0.27	0.23	0.40	0.15	0.18	0.12	2
i_max	0.00	0.01	0.00	0.03	0.03	0.03	0.00	0.00	0.07	0.00	0.00	0.00	0.00	0.00	0.01	0
i_min	0.09	0.07	0.16	0.03	0.03	0.01	0.03	0.04	0.02	0.10	0.08	0.16	0.05	0.02	0.01	0
p_ind	0.09	0.07	0.20	0.21	0.20	0.42	0.00	0.00	0.01	0.08	0.06	0.18	0.06	0.18	0.20	1
por	0.25	0.20	0.44	0.03	0.04	0.00	0.16	0.16	0.10	0.26	0.22	0.42	0.15	0.22	0.17	2
res	0.25	0.20	0.42	0.10	0.11	0.01	0.20	0.20	0.12	0.27	0.23	0.41	0.15	0.19	0.13	2
r_d	0.00	0.01	0.00	0.12	0.12	0.08	0.00	0.00	0.04	0.00	0.00	0.01	0.00	0.00	0.01	0
w_p	0.25	0.21	0.42	0.14	0.14	0.02	0.23	0.23	0.13	0.27	0.23	0.41	0.15	0.18	0.12	2
r_c	0.03	0.02	0.11	0.30	0.30	0.12	0.11	0.10	0.04	0.05	0.03	0.12	0.02	0.08	0.06	0
dep	0.26	0.26	0.24	0.11	0.11	0.15	0.05	0.05	0.06	0.24	0.24	0.22	0.14	0.06	0.03	0
i_sm	0.07	0.06	0.10	0.00	0.00	0.00	0.07	0.07	0.00	0.07	0.06	0.10	0.05	0.04	0.00	0
T	0.05	0.05	0.02	0.03	0.03	0.16	0.08	0.09	0.00	0.04	0.05	0.02	0.01	0.00	0.42	1
P	0.02	0.03	0.00	0.00	0.00	0.02	0.01	0.01	0.06	0.02	0.03	0.00	0.04	0.08	0.19	0
\sum	1	1	5	1	1	1	1	1	0	1	1	5	0	0	1	

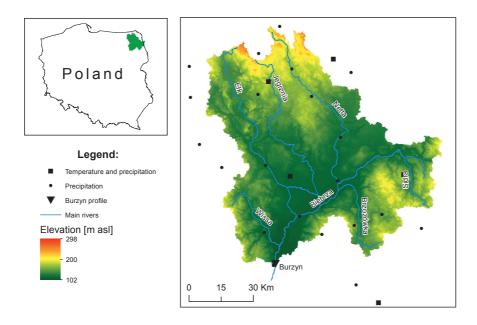


Figure 1. Topography of the study area and location of meteorological stations.

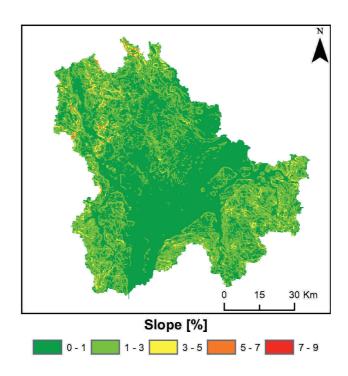


Figure 2. Slope map of the study area.

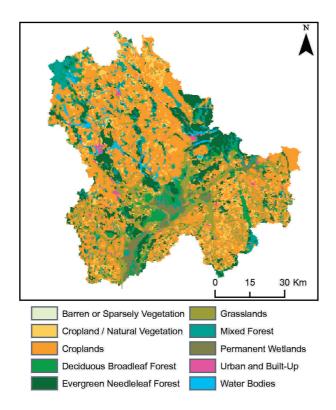


Figure 3. Land-use in the study area. Land-use classes are the same as used in the WetSpa model, defined by International Geosphere-Biosphere Program classification system.

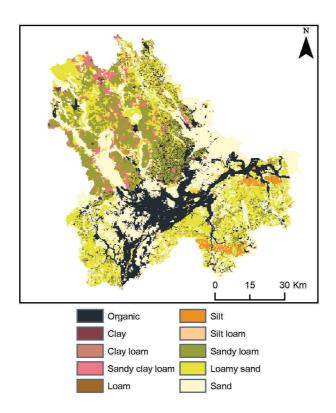


Figure 4. Soil texture map of the study area. Soil textures are the same as used in the WetSpa model, defined by U.S. Department of Agriculture.

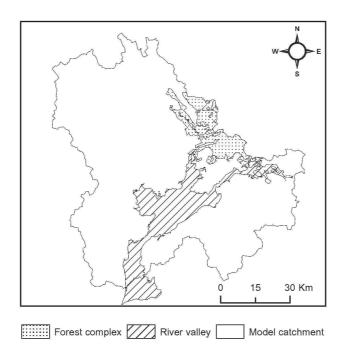


Figure 5. Major landscape features of the Biebrza River catchment. The Biebrza River valley runs NE-SW through the catchment with at the upstream part of the valley a large forest complex. Catchment area outside the river valley is upland/plateau with mineral soils.

Graph illustrating the spatial LH-OAT SCF sampling for calculating the SA. The top row presents a spatially averaged, observed SCF for an example catchment (left) and an example catchment with highlighted snow zones j and j+1 (right). The next rows presents SCF in the zones j (left column) and j+1 (central column) in the advancing LH-OAT loops starting from the loop j-1 and simulated discharge during these loops (right column). Symbols are the same as in eq. 4: e represent a fraction of the SCF, f is the fraction by which e was changed during the OAT perturbation, g is the discharge simulated at the catchment outlet.

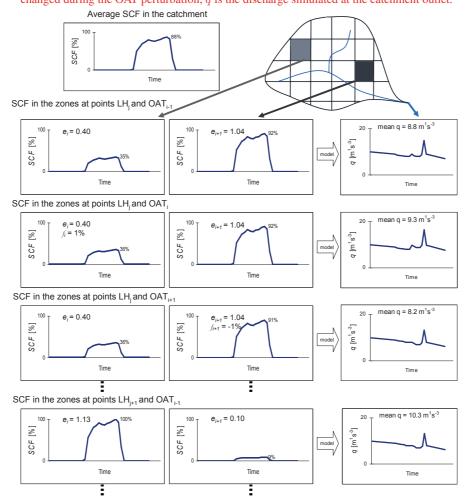


Figure 6. Graph illustrating the spatial LH-OAT SCF sampling for calculating the sensitivity analysis. The top row presents a spatially averaged, observed SCF for an example catchment (top left panel) and the example catchment with highlighted snow zones i and i+1 (top right panel). The next rows presents SCF in the zones i (panels in the left column) and i+1 (panels in the central column) in the advancing LH-OAT loops starting from the loop j-1 and the discharge simulated during these loops (panels in the right column). Symbols are the same as in Eq. 4: e_i and e_{i+1} represent a fraction of the SCF in the snow zones i and i+1, f is the fraction by which e was changed during the OAT perturbation, g is the discharge simulated at the catchment outlet.

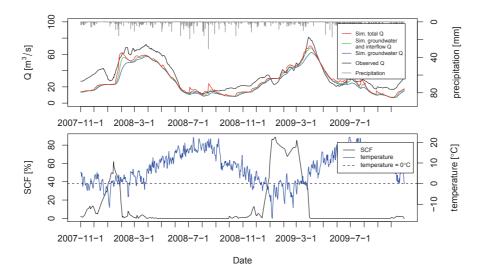


Figure 7. Observed and simulated daily discharge used from the calibrated WetSpa for SA the period in which the sensitivity analysis was conducted (upper figure panel). Also presented is WetSpa simulated groundwater and interflow discharge as well as only groundwater discharge. Catchment average daily temperature and SCF SCF in the same period is presented in the lower figure panel. The ticks on the time axis indicate the 1^{st} day of a month.

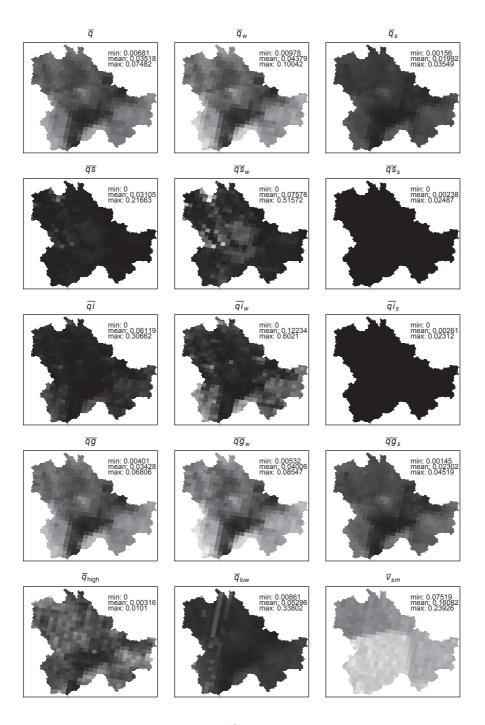


Figure 8. The SCF-SCF sensitivity maps showing s_i in snow zones of the WetSpa model for Biebrza River catchment for the WetSpa model for different RF response functions. The grey scale represents linearly stretched s_i values between minimum (black) and maximum (white) values; for the top four rows the minimum and maximum values are grey scale is selected to match the data range of all maps in each row; in the lowest row each map has individual grey scale between the minimum and maximum values indicated on the plots (see Sect. 3.2 for details). Explanation of the RF response functions is presented in Table 1.

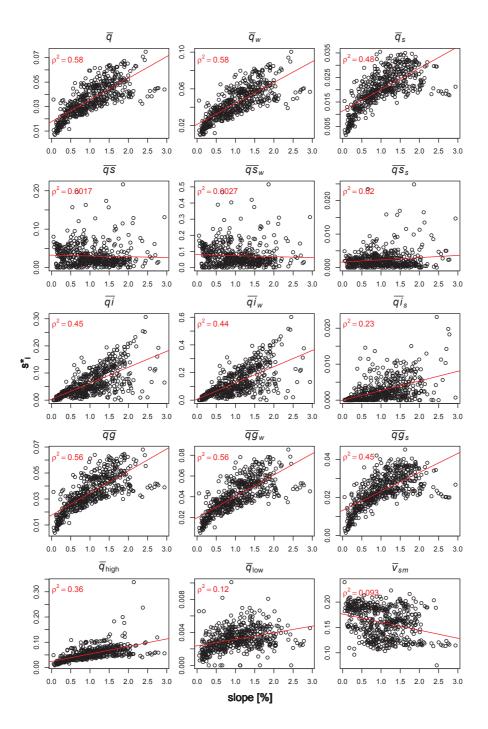


Figure 9. Relation between $\frac{slp}{t}$ the slope and spatial SA sensitivity analysis results (s_i) quantified with different RF's response functions. Explanation of the RF response functions is presented in Table 1.