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# Technical note: Analytical drawdown solution for steady-state pumping tests in two-dimensional isotropic heterogeneous aquifers

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**Abstract.** A new method is presented which allows interpreting steady-state pumping tests in heterogeneous isotropic transmissivity fields. In contrast to mean uniform flow, pumping test drawdowns in heterogeneous media cannot be described by a single effective or equivalent value of hydraulic transmissivity. An effective description of transmissivity is required, being a function of the radial distance to the well and including the parameters of log-transmissivity: mean, variance, and correlation length. Such a model is provided by the upscaling procedure radial coarse graining, which describes the transition of near-well to far-field transmissivity effectively. Based on this approach, an analytical solution for a steady-state pumping test drawdown is deduced. The so-called effective well flow solution is derived for two cases: the ensemble mean of pumping tests and the drawdown within an individual heterogeneous transmissivity field. The analytical form of the solution allows inversely estimating the parameters of aquifer heterogeneity. For comparison with the effective well flow solution, virtual pumping tests are performed and analysed for both cases, the ensemble mean drawdown and pumping tests at individual transmissivity fields. Interpretation of ensemble mean drawdowns showed proof of the upscaling method. The effective well flow solution reproduces the drawdown for two-dimensional pumping tests in heterogeneous media in contrast to Thiem's solution for homogeneous media. Multiple pumping tests conducted at different locations within an individual transmissivity field are analysed, making use of the effective well flow solution to show that all statistical parameters of aquifer heterogeneity can be inferred under field conditions. Thus,

the presented method is a promising tool with which to estimate parameters of aquifer heterogeneity, in particular variance and horizontal correlation length of log-transmissivity fields from steady-state pumping test measurements.

## 1 Introduction

Pumping tests are a widely used tool to identify horizontal hydraulic conductivity, which is the parameter determining the groundwater flow velocity. Analytical solutions of the radial flow equation are used in practice to analyse measured drawdowns. In general, these solutions assume a constant homogeneous hydraulic conductivity like Thiem's solution for steady state (Thiem, 1906):

$$h_{\text{Thiem}}(r) = -\frac{Q_{\text{w}}}{2\pi D K_{\text{h}}} \ln \frac{r}{R} + h(R). \tag{1}$$

Thiem's solution (Eq. 1) gives the hydraulic head $h_{\text{Thiem}}(r)$ depending on the radial distance $r$ from the well for homogeneous horizontal hydraulic conductivity $K_{\text{h}}$. It is valid in a confined aquifer of thickness $D$ with a fully penetrating well, and a constant discharge $Q_{\text{w}}$, $h(R)$ is a known reference head at an arbitrary distance $R$ from the well.

In large-scale pumping tests the vertical extension of the aquifer is negligible compared to horizontal aquifer extent. Thus, flow is assumed to be horizontal and modelled as two-dimensional. Hydraulic conductivity is then replaced by transmissivity, which is defined as the product of conductivity and aquifer thickness $T = K_{\text{h}} D$. In the following,

transmissivity will be used instead of horizontal hydraulic conductivity, since the focus of the work will be on two-dimensional well flow.

Most natural aquifers exhibit geological heterogeneity in the sedimentary composition, which evolved from the complex geomorphological processes through which they were formed. In particular, transmissivity shows a strong spatial variability. Values measured in the field vary over orders of magnitude (Gelhar, 1993). Modelling transmissivity as a spatial random function is generally applied to capture the effects of aquifer heterogeneity. Transmissivity $T(x, y)$ is modelled as a log-normally distributed spatial random function: $\log T(x, y) = Y(x, y)$ is normally distributed with a Gaussian probability density function $\mathrm{pdf}_Y(x) = \frac{1}{2\pi\sigma^2}\exp\left(-\frac{(x-\mu)^2}{2\sigma^2}\right)$ in univariate form, with $\mu$ and $\sigma^2$ being the mean and the variance of $Y$, respectively. The correlation structure of transmissivity in space is captured by a covariance model $\mathrm{Cov}\left[T(x+s_1, y+s_2), T(x, y)\right] = \exp\left(2\mu + \sigma^2 + \mathrm{CV}_Y(s_1, s_2)\right)$.

In the stochastic framework, the solution of the groundwater flow equation with a log-normally distributed transmissivity is also a random spatial function. Since the solution of the stochastic differential equation is out of scope, the focus of investigation was on effective transmissivity values for describing well flow. As a first approach, Thiem's solution (Eq. 1) was applied to pumping tests in heterogeneous media. However, this requires a representative transmissivity value $T$ for the whole range of the depression cone (Matheron, 1967), which does not exist. Effective or equivalent descriptions of transmissivity in pumping tests have been investigated, e.g. by Desbarats (1992), Sánchez-Vila et al. (1999), Neuman et al. (2007), Dagan and Lessoff (2007), Schneider and Attinger (2008), and many more. For a detailed review see Sánchez-Vila et al. (2006).

In contrast to mean uniform flow, the pumping test drawdowns in heterogeneous media cannot be described by a single constant effective value of transmissivity (Matheron, 1967). Different transmissivities characterize the behaviour near and far from the well: the representative value close to the well is the harmonic mean of the log-normal transmissivity $T_H = \exp\left(\mu - \frac{1}{2}\sigma^2\right) = T_G \exp\left(-\frac{1}{2}\sigma^2\right)$. With increasing distance from the well, the drawdown behaviour is characterized by the effective transmissivity for uniform flow, which is the geometric mean $T_G = \exp(\mu)$ for flow in two-dimensional isotropic porous media.

It seems obvious that a representative description of transmissivity for well flow needs to be a radially dependent function, which interpolates between the harmonic and the geometric mean. The equivalent transmissivity $T_{eq}$ is a well-established approach of a radially dependent description, visualized in Fig. 1a. $T_{eq}(r) = -\frac{Q_w}{2\pi(h(r)-h(r_w))}\ln\frac{r}{r_w}$ was derived from Thiem's solution (Eq. 1) (Matheron, 1967; Indelman et al., 1996; Dagan and Lessoff, 2007). In this sense, the equivalent transmissivity $T_{eq}$ is defined as the value for
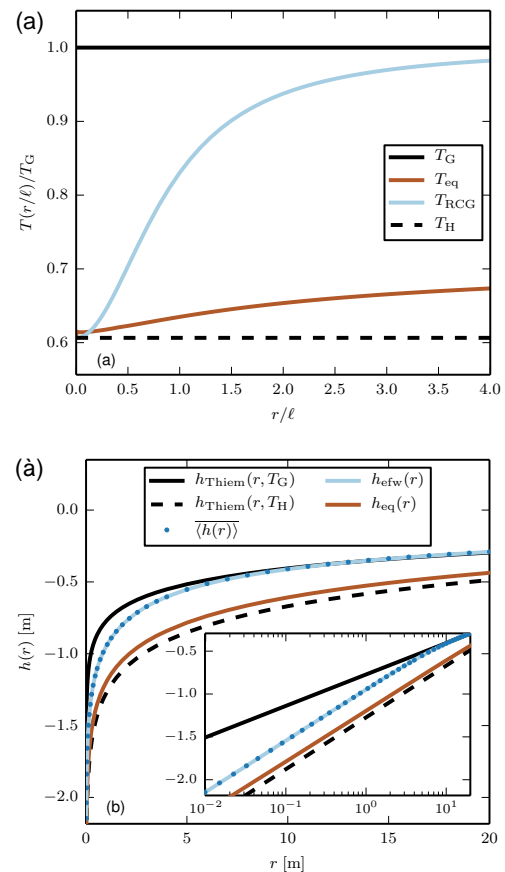


**Figure 1.** Comparison of equivalent and radial coarse graining approach: **(a)** radially dependent transmissivities interpolating between harmonic mean $T_H$ and geometric mean $T_G$: $T_{RCG}(r)$ from Eq. (4) and $T_{eq}(r)$ calculated based on Thiem's formula Eq. (1) with $h(r) = \overline{\langle h(r)\rangle}$, which is the ensemble mean for ensemble A (Table 1); **(b)** hydraulic head drawdowns after pumping with $h_{efw}(r)$ from Eq. (6) as a solution of the well flow equation using $T_{RCG}(r)$, $h_{eq}(r)$ as a solution of the well flow equation using $T_{eq}(r)$, Thiem's solution with constant values $T_G$ and $T_H$, and mean ensemble drawdown $\overline{\langle h(r)\rangle}$.

a homogeneous medium, which reproduces locally the same total outflow as observed in the heterogeneous domain of radius $r$. $T_{eq}$ is strongly impacted by the reference point $r_w$ and the corresponding head $h(r_w)$, which is generally chosen to be the drawdown at the well $h(r_w)$. Therefore, the equivalent conductivity stays close to the harmonic mean $T_H$, which is representative for the drawdown behaviour at the well (Fig. 1a). It takes more than 20 correlation lengths for $T_{eq}$ to reach the far-field representative value of $T_G$.

It is important to mention that $T_{eq}$ is not constructed to reproduce the drawdown which was used for calculating $T_{eq}$. Strictly speaking, replacing the heterogeneous transmissivity field with the equivalent transmissivity in a single forward model does not give the drawdown with which $T_{eq}$ was con-

structed as visualized in Fig. 1b. Instead $h_{eq}(r)$ stays close to Thiem's solution, with $T_H$ as a constant transmissivity value.

Schneider and Attinger (2008) introduced a novel approach to describe well flow effectively. They derived a radially adapted transmissivity $T_{RCG}(r)$ by applying the upscaling technique coarse graining to well flow. $T_{RCG}(r)$ depends not only on the radial distance $r$ but also on the statistical parameters of aquifer heterogeneity $T_G$, $\sigma^2$, and $\ell$. $T_{RCG}(r)$ captures the transition from near-well to far-field representative transmissivities, based on the radial distance to the well and the parameters of aquifer heterogeneity, as visualized in Fig. 1a.

In this study, an analytical solution for the hydraulic head $h_{efw}(r)$ is presented which is based on the radial coarse graining transmissivity $T_{RCG}(r)$ as an extension to the work of Schneider and Attinger (2008). Similar work has been done by Zech et al. (2012) for pumping tests in three-dimensional porous media. The "effective well flow solution" $h_{efw}(r)$ describes the mean depression cone of a pumping test in two-dimensional heterogeneous media effectively. It can be interpreted as an extension of Thiem's formula (Eq. 1) to log-normally distributed heterogeneous media. It accounts for the statistical parameters $T_G$, $\sigma^2$, and $\ell$ and thus allows inversely estimating them from measured drawdown data. In contrast to existing head solutions for well flow, $h_{efw}(r)$ is not limited to low variances but is applicable to highly heterogeneous media with variances $\sigma^2 \gg 1$. More explicitly, the effective well flow solution is not a solution derived from an effective equation but is the solution of the deterministic groundwater flow equation under well flow conditions in combination with an effective transmissivity. As an effective transmissivity description the radial coarse graining transmissivity is used because it mimics the filtering process taking place during pumping.

In a similar line Neuman et al. (2004) presented a graphical approach to estimate the statistical parameters of random transmissivity on the basis of steady-state head data. The authors constructed a mathematical description for the apparent transmissivity $T_a(r)$ as a function of the radial distance to the well $r$ from theoretical findings of near-well and far-field representative transmissivity and a cubic polynomial interpolation in between. The approach makes use of the ensemble average drawdown as well as of its variance, combining uncertainty within a unique methodology. From $T_a(r)$ the authors constructed type curves for the hydraulic head, depending on the variance $\sigma^2$ and the correlation length $\ell$. Neuman et al. (2004) further gave a multi-point strategy to analyse virtually measured drawdown data by type curve matching including parameter estimation. The solution was also applied in an actual field setting by Riva et al. (2009).

The radial coarse graining approach is similar to that of Neuman et al. (2004) in the idea of deriving a solution for the head drawdown for well flow depending on the statistics of the random transmissivity using an effective radially dependent transmissivity. Major differences are (i) the radial

coarse graining transmissivity $T_{RCG}(r)$ is derived from upscaling with physically motivated approximations, whereas the solution of Neuman et al. (2004) is based on the analytical solution of Riva et al. (2001) in combination with numerical Monte Carlo simulations; (ii) the functional form of $T_{RCG}(r)$ is different from the expression for $T_a$ of Neuman et al. (2004); (iii) the effective well flow solution $h_{efw}(r)$ is provided as a closed-form mathematical expression instead of type curves; and (iv) inverse parameter estimation can be done by minimizing the difference between the measured drawdown data and $h_{efw}(r)$ instead of type curve matching. The effective well flow method will be tested in a similar multi-point sampling strategy to analyse measured drawdown data of individual heterogeneous transmissivity fields as done by Neuman et al. (2004) as well as others (Copty and Findikakis, 2004; Firmani et al., 2006).

The work is organized as follows: Sect. 2 is dedicated to the method of radial coarse graining and the derivation of the effective well flow head solution. The concept of radial coarse graining is explained in detail. Furthermore distinction is made between the effective well flow solution for an ensemble mean and single realizations of heterogeneous transmissivity fields. Section 3 contains the application of the effective well flow solution to simulated pumping tests. It is shown that $h_{efw}(r)$ reproduces the drawdown in heterogeneous media and can be used to inversely estimate the statistical parameters of aquifer heterogeneity for both ensemble mean and single realizations. In Sect. 4, a sampling strategy is presented to infer the parameters of aquifer heterogeneity of an individual transmissivity field from multiple pumping tests at multiple locations, making use of $h_{efw}(r)$. Concluding remarks are given in Sect. 5.

## 2 Radial coarse graining transmissivity and effective well flow head

### 2.1 Steady-state well flow with radially dependent transmissivity

The drawdown of a steady-state pumping test with a radially dependent transmissivity $T(r)$ is given as the solution of the differential equation

$$
\begin{aligned}
0 &= \left( \frac{1}{r} \frac{dh}{dr} + \frac{d^2 h}{dr^2} \right) + \frac{dT(r)}{dr} \frac{dh}{dr} \\
&= T(r) \left[ \left( \frac{1}{r} + \frac{d \ln T(r)}{dr} \right) \frac{dh}{dr} + \frac{d^2 h}{dr^2} \right].
\end{aligned}
\tag{2}
$$

The equation can be solved in $\frac{dh}{dr}$ by separation of variables, resulting in $\frac{dh}{dr} = C_1 \frac{1}{rT(r)}$. The hydraulic head $h(r)$ is then given as the solution of the integral

$$
h(r_2) - h(r_1) = C_1 \int_{r_1}^{r_2} \frac{1}{r\,T(r)}\,dr.
\tag{3}
$$

The integration constant $C_1$ is determined by the boundary condition. Supposing a constant flux boundary condition at the well gives $Q_w = -2\pi r_w T(r_w) \frac{dh}{dr}(r_w) = -2\pi r_w T(r_w) \frac{C_1}{r_w T(r_w)}$ and, thus, $C_1 = -\frac{Q_w}{2\pi}$.

Equation (3) is the general solution of the radial flow Eq. (2) for radially dependent transmissivity, independent of the functional form of $T(r)$.

When comparing Eq. (3) with the definition of the equivalent transmissivity, it becomes obvious that $T_{eq}$ is not constructed to solve the equation. The combination of both formulas results in $\int_{r_1}^{r_2} \frac{1}{rT(r)} dr = \frac{1}{T_{eq}(r)} \ln \frac{r_1}{r_2}$, which is only fulfilled when $T(r)$ is constant in $r$.

In a heterogeneous transmissivity field, radially symmetric flow is not to be expected. However, angular fluctuations level out for ensemble average drawdowns. Thus, the assumption of a radially dependent effective transmissivity description $T(r)$ – independent of the angular coordinate – is well established and reasonable in the context of ensemble analysis. In this line, the radial coarse graining transmissivity and thus the effective well flow solution are considered to be purely radially dependent referring to ensemble averages.

## 2.2 Concept of radial coarse graining

A radially dependent transmissivity for log-normally distributed media with Gaussian correlation structure was derived by Schneider and Attinger (2008), denoted as $T_{RCG}(r)$. It is based on the upscaling approach radial coarse graining, which follows the basic idea of a spatial filtering of the flow equation appropriate to the non-uniform flow character of a pumping test. The method of radial coarse graining is an upscaling method based on mathematically solid filtering of the flow equation and physically reasonable assumptions and approximations. In its current state the procedure is limited to a multivariate Gaussian random field as a model for the heterogeneity of the transmissivity field.

The approach was further developed for three-dimensional well flow by Zech et al. (2012), introducing an effective well flow solution for the hydraulic head. Similarly, the concept of radial coarse graining for two-dimensional well flow will be expanded in the following. The process can be best explained within five major steps:

1. coarse graining for uniform flow,

2. transfer of coarse graining to radial flow conditions,

3. overcoming non-locality of head equation for non-uniform flow,

4. effective radial coarse graining transmissivity,

5. derivation of effective well flow head.

The first three steps will be discussed shortly in the following. Steps 4 and 5 will be explained in detail in Sects. 2.3 and 2.4.

The coarse graining approach for uniform flow (step 1) was introduced by Attinger (2003), including derivation, mathematical proof, and numerical simulations. The author started at a spatially variable transmissivity field $T(x)$ and derived a filtered version $T_\lambda^{CG}(x)$, where fluctuations smaller than a cut-off length $\lambda$ are filtered out. The resulting upscaled coarse graining transmissivity field $T_\lambda^{CG}(x)$ represents a log-normally distributed field with a smaller variance $\langle \sigma^2 \rangle_\lambda$ but larger correlation length $\langle \ell \rangle_\lambda$. Attinger (2003) showed that the statistical parameters relate to the parameter of the unfiltered field by $\langle \sigma^2 \rangle_\lambda \equiv \sigma^2 \frac{\ell^2}{\ell^2 + \lambda^2/4}$ and $\langle \ell \rangle_\lambda \equiv (\ell^2 + \lambda^2/4)^{1/2}$.

The concept of coarse graining can similarly be applied to non-uniform flow (step 2). The critical point when extrapolating the results of Attinger (2003) to radial flow is the Fourier back transformation of the filtered head equation after localization. For uniform flow, this can be done due to the reasonable assumption of constant head gradient. For non-uniform flow, this assumption is not valid, and thus localization is not possible straightforward.

A heuristic approach is taken to overcome the limitation of non-locality for well flow (step 3). Conditions of a quasi-constant head gradient are constructed by adapting the size of the volume elements over which flow takes place. The change in the volume size refers to the filtering procedure and is then realized by a radially dependent scaling parameter $\lambda(r)$. The step can be understood as a change from an equidistant Cartesian coordinate system to a polar coordinate system. Technically speaking, the head gradient in well flow is constant for volumes of size proportional to $r$, because it is proportional to the reciprocal of the distance to the well: $\nabla h(r) = \frac{h(r) - h(r+\Delta r)}{\Delta r} \propto \frac{1}{r}$. Therefore, the scaling parameter is chosen to be proportional to the radial distance $\lambda = 2\zeta r$. Then, the filter width increases with distance to the well, ensuring that head gradients can be assumed constant over volume elements of increasing size with distance to the well. Under this adaption, localization can be performed and thus also the following steps of the coarse graining procedure.

The result is an upscaled log-normally distributed field $T_r^{RCG}(x)$ with an arithmetic mean $T_A^{RCG}(r)$ and a filtered fluctuation term. The step was presented by Schneider and Attinger (2008). It is not performed in a mathematically straightforward way but problem-adapted to well flow conditions.

## 2.3 Radial coarse graining transmissivity

Spatial heterogeneity is still resolved in $T_r^{RCG}(x)$, albeit reduced to the amount relevant to the pumping test. A further step of averaging is necessary to derive an effective transmissivity which mimics the intrinsic filtering of the flow during pumping and thus reproduces the drawdown behaviour. Two different aspects are of interest: (i) an effective transmissivity for an ensemble and (ii) effective transmissivity for an individual field. This step includes the transfer from the stochastic picture of transmissivity to a deterministic description.

A result for an effective ensemble description is derived by averaging $T_r^{\text{RCG}}(\boldsymbol{x})$ appropriate to well flow conditions. The averaging rule is determined by the boundary condition at the well, which is the harmonic mean for two-dimensional well flow (Dagan, 1989). Thus, the effective mean transmissivity, denoted by $T_{\text{RCG}}(r)$, is calculated via the theoretical description of the harmonic mean for log-normally distributed fields, making use of the variance of the coarsened transmissivity $\langle \sigma^2 \rangle_r = \frac{\sigma^2}{1+\zeta^2 r^2/\ell^2}$:

$$
\begin{aligned}
T_{\text{RCG}}(r) &= T_{\text{G}} \exp\left(-\langle \sigma^2 \rangle_r / 2\right) \\
&= T_{\text{G}} \exp\left(-\frac{1}{2}\frac{\sigma^2}{(1+\zeta^2 r^2/\ell^2)}\right),
\end{aligned}
\tag{4}
$$

where $r$ is the distance to the well, $T_{\text{G}}$ is the geometric mean, $\sigma^2$ is the variance, and $\ell$ is the correlation length of the log-transmissivity $T(\boldsymbol{x})$. $\zeta$ is a factor of proportionality, which was determined to be $\zeta = 1.6$, as discussed in detail by Zech et al. (2012).

$T_{\text{RCG}}(r)$ can be interpreted as an interpolating function between the representative transmissivity at the well $T_{\text{H}} = T_{\text{G}} \exp\left(-\frac{1}{2}\sigma^2\right)$ to the far-field value $T_{\text{G}}$ depending on $r$, controlled by the correlation length $\ell$ (Fig. 1a).

An effective description of well flow transmissivity for an individual field is derived from Eq. (4). The behaviour of individual fields is different especially at the well due to a lack of ergodicity there. The local transmissivity at the well $T_{\text{well}}$ is not identical to the harmonic mean $T_{\text{H}}$ as expected for the ensemble but rather refers to the specific value of transmissivity at the well location. An adapted radial coarse graining transmissivity accounts for local effects by replacing the harmonic mean $T_{\text{H}} = T_{\text{G}} \exp\left(-\frac{1}{2}\sigma^2\right)$ by $T_{\text{well}}$. In Eq. (4) this refers to substituting the variance by $-\frac{1}{2}\sigma^2 = \ln T_{\text{well}} - \ln T_{\text{G}}$, and thus

$$
\begin{aligned}
T_{\text{RCG}}^{\text{local}}(r) &= T_{\text{G}} \exp\left(\frac{\ln T_{\text{well}} - \ln T_{\text{G}}}{1+\zeta^2 r^2/\ell^2}\right) \\
&= T_{\text{well}}^{\frac{1}{1+\zeta^2 r^2/\ell^2}} T_{\text{G}}^{\frac{\zeta^2 r^2/\ell^2}{1+\zeta^2 r^2/\ell^2}}.
\end{aligned}
\tag{5}
$$

$T_{\text{RCG}}^{\text{local}}(r)$ interpolates between the specific transmissivity at the well $T_{\text{well}}$ and the far-field value $T_{\text{G}}$ depending on the radial distance $r$ and the correlation length $\ell$.

## 2.4 Effective well flow head

An effective drawdown solution is derived by solving the deterministic groundwater flow equation in combination with an effective transmissivity description, namely the radial coarse graining transmissivity. This needs to be clearly distinguished from solving an effective well flow equation. In line with the deterministic nature of the radial coarse graining transmissivity $T_{\text{RCG}}(r)$, the associated effective well flow head is deterministic as well.

Explicit results for the hydraulic head drawdown in a steady-state pumping test are achieved by solving the integral in Eq. (3), making use of $T_{\text{RCG}}(r)$ (Eq. 4). The result is the effective well flow head $h_{\text{efw}}(r)$, given by

$$
\begin{aligned}
h_{\text{efw}}(r) = &-\frac{Q_{\text{w}}}{4\pi T_{\text{G}}} \exp\left(\frac{\sigma^2}{2}\right)\left(\Gamma\left(\frac{\sigma^2}{2}\frac{-\zeta^2 r^2/\ell^2}{1+\zeta^2 r^2/\ell^2}\right)\right. \\
&\left.-\Gamma\left(\frac{\sigma^2}{2}\frac{-\zeta^2 R^2/\ell^2}{1+\zeta^2 R^2/\ell^2}\right)\right) \\
&+\frac{Q_{\text{w}}}{4\pi T_{\text{G}}}\left(\Gamma\left(\frac{\sigma^2}{2}\frac{1}{1+\zeta^2 r^2/\ell^2}\right)\right. \\
&\left.-\Gamma\left(\frac{\sigma^2}{2}\frac{1}{1+\zeta^2 R^2/\ell^2}\right)\right) + h_R,
\end{aligned}
\tag{6}
$$

where $r$ is the radial distance from the well, $Q_{\text{w}}$ is the pumping rate, $T_{\text{G}}$ is the geometric mean, $\sigma^2$ is the log-transmissivity variance, and $\ell$ is the correlation length. Again, $\zeta$ is the factor of proportionality determined to be 1.6, and $R$ is an arbitrary distance from the well, where the hydraulic head $h(R) = h_R$ is known. $\Gamma(x) = \int_{-\infty}^x \frac{\exp(z)}{z} \mathrm{d}z$ is the exponential integral function. Details on the derivation of $h_{\text{efw}}(r)$ can be found in Appendix A.

An approximate solution $h_{\text{efw}}^{\text{approx}}(r)$ is derived from Eq. (6) by making use of an approximation of $\Gamma(x)$. Details are given in the Appendix.

$$
\begin{aligned}
h_{\text{efw}}^{\text{approx}}(r) = &-\frac{Q_{\text{w}}}{2\pi T_{\text{H}}} \ln\frac{r}{R} - \frac{Q_{\text{w}}}{4\pi T_{\text{G}}}\left(\mathrm{e}^{\frac{\sigma^2}{2}} - 1\right) \\
&\cdot\left(\ln\frac{1+\zeta^2 R^2/\ell^2}{1+\zeta^2 r^2/\ell^2} + \frac{\sigma^2}{2}\frac{1}{(1+\zeta^2 r^2/\ell^2)}\right. \\
&\left.-\frac{\sigma^2}{2}\frac{1}{(1+\zeta^2 R^2/\ell^2)}\right) + h_R.
\end{aligned}
\tag{7}
$$

$h_{\text{efw}}(r)$ is constructed to describe the mean drawdown of a pumping test in two-dimensional heterogeneous media effectively. The drawdown curve of $h_{\text{efw}}(r)$ for a specific choice of parameters (ensemble A of Table 1) is given in Fig. 1b in comparison to the equivalent drawdown $h_{\text{eq}}(r)$, as the solution of the radial flow equation using the equivalent transmissivity $T_{\text{eq}}$, based on the same statistical parameters.

The effective well flow solution can be adapted to analyse individual pumping tests by using $T_{\text{RCG}}^{\text{local}}(r)$ (Eq. 5) instead of $T_{\text{RCG}}(r)$ (Eq. 4). The local effective well flow solution $h_{\text{efw}}^{\text{local}}(r)$ is then given by Eq. (6) with $\frac{\sigma^2}{2}$ substituted by $-\ln\frac{T_{\text{well}}}{T_{\text{G}}}$ and $T_{\text{H}}$ substituted by $T_{\text{well}}$.

The local effective well flow solution $h_{\text{efw}}^{\text{local}}(r)$ can be used to analyse drawdowns of single pumping tests in heterogeneous media as encountered in practice. The solution is adapted to the lack of ergodicity at the well, by using transformed parameters $T_{\text{well}}$, $T_{\text{G}}$, and $\ell$. However, the randomness of hydraulic heads can affect the parameter estimation, in particular of the correlation length, which is related to drawdown fluctuations in the transition zone. There the impact of heterogeneity is neither fully determined by the local

**Table 1.** Ensemble input parameters $T_G$, $\sigma^2$, and $\ell$ and best-fitting inverse estimation results $\hat{T}_G$, $\hat{\sigma}^2$, and $\hat{\ell}$ with 95 % confidence intervals (in brackets) for ensemble mean $\overline{\langle h(r) \rangle}$ for all generated ensembles.

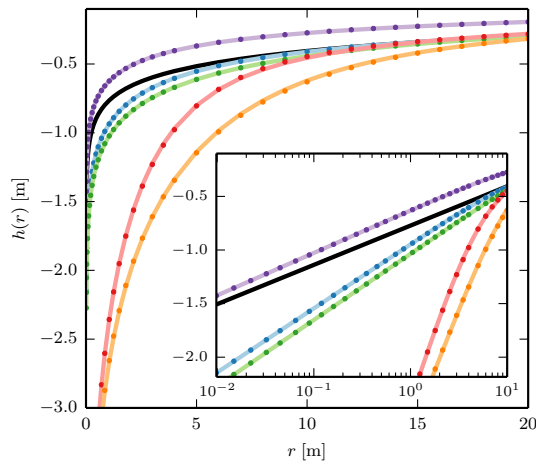|   | $T_G$ | $\hat{T}_G$ ($10^{-4}\,\text{m}^2\,\text{s}^{-1}$) | $\sigma^2$ | $\hat{\sigma}^2$ [$-$] | $\ell$ | $\hat{\ell}$ (m) |
|---|---|---|---|---|---|---|
| A | 1.0 | 1.03 ($\pm$0.0011) | 1.0 | 1.04 ($\pm$0.0022) | 10 | 9.80 ($\pm$0.086) |
| B | 1.0 | 1.08 ($\pm$0.0013) | 1.0 | 1.19 ($\pm$0.0022) | 20 | 21.6 ($\pm$0.127) |
| C | 1.0 | 1.08 ($\pm$0.0021) | 2.25 | 2.49 ($\pm$0.0038) | 10 | 10.1 ($\pm$0.050) |
| D | 1.0 | 1.19 ($\pm$0.0024) | 2.25 | 2.67 ($\pm$0.0039) | 20 | 22.2 ($\pm$0.077) |
| E | 1.0 | 1.16 ($\pm$0.0046) | 4.0 | 4.34 ($\pm$0.0078) | 10 | 11.0 ($\pm$0.042) |
| F | 1.0 | 1.31 ($\pm$0.0088) | 4.0 | 4.27 ($\pm$0.0131) | 20 | 22.2 ($\pm$0.120) |
| G | 1.5 | 1.55 ($\pm$0.0012) | 1.0 | 1.03 ($\pm$0.0016) | 10 | 10.1 ($\pm$0.066) |



**Figure 2.** Simulated ensemble means $\overline{\langle h(r) \rangle}$ (dots) and $h_\text{efw}(r)$ with best-fitting estimates (lines) for multiple ensembles: A (blue), B (green), E (red), F (orange), G (purple). Parameter values are listed in Table 1. Black line shows $h_\text{Thiem}(r)$ with $T_G = 10^{-4}\,\text{m}^2\,\text{s}^{-1}$.

transmissivity at the well nor fully levelled out as in the far field. The geometric mean $T_G$ and the correlation length $\ell$ for a single realization should therefore be interpreted as local values, not necessarily representing the mean values of the entire field but those of the pumping well vicinity. Owing to the nature of the pumping test, the drawdown signal does not sample the heterogeneity in transmissivity in a symmetric way, but the shape of the drawdown is mainly determined by the local heterogeneity close to the well.

### 2.5 Impact of parameters

The analytical form of $h_\text{efw}(r)$ allows analysing the impact of the statistical parameters $T_G$, $\sigma^2$, and $\ell$ on the drawdown. The drawdown behaviour for different choices of parameters can be seen in Fig. 2, which is discussed in detail later on.

Every parameter impacts on the drawdown in a different region. The geometric mean $T_G$ as a representative value for mean uniform flow determines the far-field behaviour. The variance $\sigma^2$ determines the drawdown at the well due to the dependence of the near-well asymptotic value $T_H =$

$T_G \exp\left(-\frac{1}{2}\sigma^2\right)$. The larger the variance, the larger are the differences between $T_G$ and $T_H$ and the steeper is the drawdown at the well, whereas the correlation length $\ell$ determines the transition from near to far-field behaviour. Therefore, fluctuation in the hydraulic head in the transition zone can affect estimation errors in the correlation length.

The asymptotic behaviour of $h_\text{efw}(r)$ can easily be analysed using the approximate functional description in Eq. (7): for distances close to the well, i.e. $r \ll \ell$, $h_\text{efw}(r)$ converges to Thiem's solution with $T_H$ as a constant transmissivity value. All terms, except the first one in Eq. (7), tend to zero or become constant. Thus, they are negligible compared to the logarithmic first term for very small $r$,

$$
\begin{aligned}
h_\text{efw}^\text{approx}(r \ll \ell) &\approx -\frac{Q_w}{2\pi T_H} \ln \frac{r}{R} - \frac{Q_w}{4\pi T_G}\left(e^{\frac{\sigma^2}{2}} - 1\right) \\
&\quad \cdot \left(\ln\left(1 + \zeta^2 R^2/\ell^2\right) + \frac{\sigma^2}{2}\right) + h_R \\
&\approx -\frac{Q_w}{2\pi T_H} \ln \frac{r}{R} + h_R.
\end{aligned}
$$

For large distances from the well, i.e. $r \gg \ell$, the solution converges to Thiem's solution with $T_G$ as a constant transmissivity value. The third and fourth term in Eq. (7) tend to zero and cancel out. The ones in the second term can be neglected; thus

$$
\begin{aligned}
h_\text{efw}^\text{approx}(r \gg \ell) &\approx -\frac{Q_w}{2\pi T_H} \ln \frac{r}{R} - \left(\frac{Q_w}{4\pi T_H} - \frac{Q_w}{4\pi T_G}\right) \\
&\quad \cdot \ln\left(\frac{\zeta^2 R^2/\ell^2}{\zeta^2 r^2/\ell^2}\right) + h_R \\
&\approx -\frac{Q_w}{2\pi T_G} \ln \frac{r}{R} + h_R.
\end{aligned}
$$

The larger the correlation length $\ell$, the longer the transition of the drawdown takes from near-well to far-field behaviour. The influence of $\ell$ on $h_\text{efw}(r)$ vanishes quickly with increasing distance to the well. The drawdown reaches the far-field behaviour after approximately two correlation lengths, $h^\text{efw}(r > 2\ell) = h_\text{Thiem}(r > 2\ell)$, with $T_G$ as a constant transmissivity value (Fig. 1b). These findings are in line with the results of Neuman et al. (2004).

# 3 Robust estimation of statistical parameters

## 3.1 Numerical pumping tests

Numerical pumping tests in heterogeneous porous media were generated as artificial measurements. They were used to test the capability of $h_{\mathrm{efw}}(r)$ in reproducing the mean drawdown and in estimating the underlying parameters of heterogeneity. Pumping tests were simulated using the finite-element software OpenGeoSys. The software was successfully tested against a wide range of benchmarks (Kolditz et al., 2012). Results of a steady-state simulation with homogeneous transmissivity were in perfect agreement with Thiem's analytical solution Eq. (1).

The numerical grid was constructed as a square of $256 \times 256$ elements with a uniform grid cell size of 1 m except for cells in the vicinity of the pumping well. The mesh was refined in the range of 4 m around the well, which ensures a fine resolution of the steep head gradients at the well. The well in the centre of the mesh was included as a hollow cylinder with radius $r_{\mathrm{w}} = 0.01$ m. The constant pumping rate of $Q_{\mathrm{w}} = -10^{-4} \, \mathrm{m}^3 \, \mathrm{s}^{-1}$ was distributed equally to all elements at the well. At the radial distance $R = 128$ m a constant head of $h(R) = 0$ m was applied, giving a circular outer head boundary condition.

Log-normally distributed, Gaussian-correlated transmissivity fields were generated using a statistical field generator based on the randomization method (Heße et al., 2014). Multiple ensembles with different statistical parameter values were generated, including high variances up to $\sigma^2 = 4$ (Table 1). Ensemble A with $T_{\mathrm{G}} = 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$, $\sigma^2 = 1$, and $\ell = 10$ m served as a reference ensemble for specific cases. Every ensemble consists of $N = 5000$ realizations, which was tested as sufficiently large to ensure ensemble convergence.

For the ensemble analysis, pumping test simulations were post-processed by performing an angular and an ensemble average. For every realization $i$, the simulated drawdown $\langle h_i(r, \phi) \rangle$ at the radial and angular location $(r, \phi)$ in polar coordinates was averaged over the four axial directions: $\langle h_i(r) \rangle = \sum_{\phi_j} \langle h_i(r, \phi_j) \rangle$. The ensemble mean was the sum over the angular mean of all individual realizations: $\overline{\langle h(r) \rangle} = \sum_{i=1}^{N} \langle h_i(r) \rangle$.

Non-linear regression was used to find the best-fitting values for the statistical parameters, denoted by $\hat{T}_{\mathrm{G}}$, $\hat{\sigma}^2$, and $\hat{\ell}$. The best-fitting estimates were determined by minimizing the mean square error of the difference between the analytical solution $h_{\mathrm{efw}}(r)$ and the measured drawdown samples $h(r)$: $\min_{T_{\mathrm{G}}, \sigma^2, \ell} \sum_r (h(r) - h_{\mathrm{efw}}(r))^2$, making use of the Levenberg–Marquardt algorithm. The reliability of the estimated parameters was evaluated using 95 %-confidence intervals.

The estimation procedure was applied to the head measurements at every 1 m distance starting at the well up to a distance of 80 m. The range beyond 80 m was not taken

into account to avoid boundary effects. The range of 80 m includes at least four correlation lengths for all tested ensembles, which is sufficient to ensure convergence to the far-field behaviour. The question of the applicability of $h_{\mathrm{efw}}(r)$ on limited head data is of quite complex nature. For a detailed discussion on that issue the reader is referred to Zech et al. (2015).

## 3.2 Ensemble pumping test interpretation

First, the simulated ensemble means were analysed, making use of the ensemble version of $T_{\mathrm{RCG}}(r)$ and $h_{\mathrm{efw}}(r)$ (Eqs. 4 and 6). Simulated ensemble means $\overline{\langle h(r) \rangle}$ for multiple choices of statistical parameters $T_{\mathrm{G}}$, $\sigma^2$, and $\ell$ are visualized in Fig. 2 in combination with $h_{\mathrm{efw}}(r)$ for the best-fitting parameter estimates $\hat{T}_{\mathrm{G}}$, $\hat{\sigma}^2$, and $\hat{\ell}$. Input parameters as well as inverse estimation results for all tested ensembles are listed in Table 1.

The best-fitting estimates show that all three parameters could be inferred from the ensemble mean with a high degree of accuracy. The deviation of the geometric mean from the input value is in general less than 10 %; only for high variances are the deviations up to 30 %. Variances deviate in a range of 20 %, and estimated correlation lengths are accurate within 10 % of the initial input parameter.

The confidence intervals of the estimates $\hat{T}_{\mathrm{G}}$ and $\hat{\sigma}^2$ are very small, showing a high sensitivity of the effective well flow solution $h_{\mathrm{efw}}(r)$ towards geometric mean and variance. The confidence intervals of the correlation length are larger due to the dependence of the estimate of $\hat{\ell}$ on the estimates $\hat{T}_{\mathrm{G}}$ and $\hat{\sigma}^2$. This is due to the fact that the correlation length determines the transition from $\hat{T}_{\mathrm{well}} = \hat{T}_{\mathrm{G}} \exp\left(-\frac{1}{2}\hat{\sigma}^2\right)$ to $\hat{T}_{\mathrm{G}}$, which results in larger uncertainties in the estimates of $\hat{\ell}$.

## 3.3 Individual pumping test interpretation

In the following, pumping test drawdowns of individual transmissivity fields are interpreted based on the adaption version $h_{\mathrm{efw}}^{\mathrm{local}}(r)$ as discussed in Sect. 2.4. The drawdowns along the four axial directions as well as the radial mean for two realizations from ensemble A ($T_{\mathrm{G}} = 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$, $\sigma^2 = 1$, $\ell = 10$ m) are visualized in Fig. 3a and b.

The realizations from Fig. 3a and b differ significantly in the value of the local transmissivity at the well. The analysis of the transmissivity fields at the well gave sampled values of $< T_{\mathrm{well}}^{(a)} > = 0.204 \times 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$ and $< T_{\mathrm{well}}^{(b)} > = 1.11 \times 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$, which is in both cases far from having the theoretical harmonic mean value $T_{\mathrm{H}} = 0.61 \times 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$ as the representative value for the near-well behaviour.

Inverse estimation results for the realization in Fig. 3a differ for the drawdowns along the four axial directions $\langle h(r, \phi_j) \rangle$ and the radial mean $\langle h(r) \rangle$: the estimated geometric mean ranges between $1.03 \times 10^{-4}$ and $1.45 \times 10^{-4} \, \mathrm{m}^2 \, \mathrm{s}^{-1}$ for the four axial directions, with an average value of $\hat{T}_{\mathrm{G}} =$

**Figure 4.** Histogram on the best-fitting estimates ($\hat{T}_{\text{G}}$, $\hat{T}_{\text{well}}$, $\hat{\ell}$) versus the theoretical input values ($T_{\text{G}}$, $T_{\text{H}}$, $\ell$) and the sampled transmissivity at the pumping well ($< T_{\text{well}} >$) for the $N = 5000$ realizations of ensemble A.
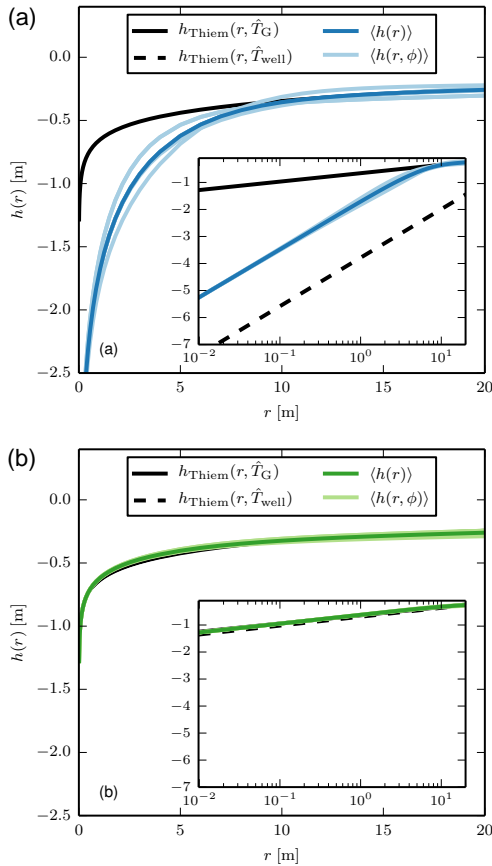
**Figure 3.** Drawdowns simulated for two individual transmissivity field realizations of ensemble A ($T_{\text{G}} = 10^{-4}\,\text{m}^2\,\text{s}^{-1}$, $\sigma^2 = 1$, $\ell = 10\,\text{m}$): **(a)** realization with $T_{\text{well}} = 0.204 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$ and **(b)** realization with $T_{\text{well}} = 1.11 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$. $\langle h(r) \rangle$ (dark color) is the radial mean, $\langle h(r, \phi) \rangle$ (light color) denotes the drawdowns along the four axes ($\phi = 0°$, $90°$, $180°$, $270°$), and in black is Thiem's solution for constant values.

$1.17 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$. The estimates for the local transmissivity at the well are between $0.195 \times 10^{-4}$ and $0.212 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$, with an average value of $\hat{T}_{\text{well}} = 0.204 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$, which is exactly the sampled local transmissivity $< T_{\text{well}}^{(a)} >$. The value of $\hat{T}_{\text{well}} = 0.204 \times 10^{-4}\,\text{m}^2\,\text{s}^{-1}$ is equivalent to a local variance of $\hat{\sigma}^2 = 3.49$. The estimated correlation length ranges between $7.95$ and $18.15\,\text{m}$, with an average of $\hat{\ell} = 12.77\,\text{m}$. It shows that the randomness of hydraulic heads due to the heterogeneity of transmissivity impacts the estimation results of the correlation length. The differences in the estimates for the drawdowns in different direction for the same realization of transmissivity shows that the parameter estimates reflect local heterogeneity in the vicinity of the well rather than the global statistical parameters of the transmissivity field. This was studied and discussed in detail for pumping tests in three-dimensional heterogeneous media by Zech et al. (2015).
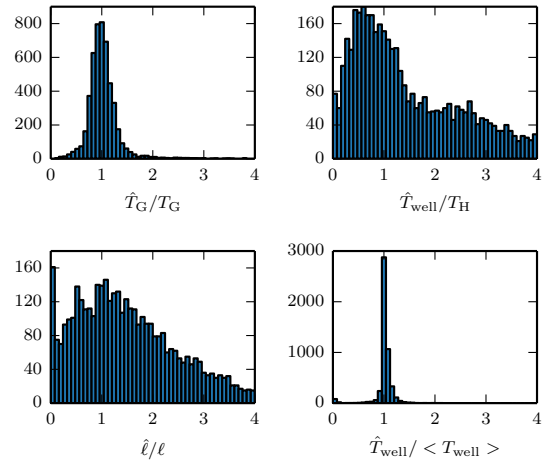
The realization in Fig. 3b does not allow the parameters of variance and correlation length to be inferred, due to the similarity of $T_{\text{well}}$ and $T_{\text{G}}$. Near-well and far-field representative transmissivities are nearly identical; thus the pumping test appears to behave like in a homogeneous medium (Fig. 3b). However, the behaviour is not representative but a result of the coincidental choice of the location of the pumping well.

A statistical analysis of the estimation results is presented in Fig. 4 for all 5000 realizations of ensemble A. A histogram on the best-fitting estimates in normalized form is shown, where normalization of results means that they were divided by the input parameters. It can be inferred that the estimate of the geometric mean $\hat{T}_{\text{G}}$ is in general close to the input value $T_{\text{G}}$. The estimate of the local transmissivity at the well $\hat{T}_{\text{well}}$ is very close to the sampled values $< T_{\text{well}} >$ for nearly all realizations. Thus, the method reproduced very well the local transmissivity at the well. However, the local value $T_{\text{well}}$ of every realization can be far from the theoretical value of $T_{\text{H}}$, where both realizations in Fig. 3 serve as an example. The estimates of the correlation length show a very large scatter. Exceptionally large and small values for $\hat{\ell}$ refer to realizations where it was nearly impossible to infer it due to the similarity of $T_{\text{well}}$ and $T_{\text{G}}$, as for the realization of Fig. 3b. The large range of estimated correlation lengths also points towards the fact that $\hat{\ell}$ of a single drawdown needs to be interpreted as a local value, which is determined by the transmissivity distribution in the vicinity of the well rather than the distribution of the entire field. However, the median of the normalized estimated correlation lengths is close to one, pointing to the fact that representative values can be inferred by taking the mean from multiple pumping tests.

## 4  Application example: single-aquifer analysis

Pumping test campaigns in the field often include the performance of multiple pumping tests within one aquifer. Drawdown measurements at multiple test locations can be used to gain representative parameters of the heterogeneous transmissivity field. The sampled area increases, and the effect of local heterogeneity through randomness of heads reduces. In the following, it is shown how mean $T_G$, variance $\sigma^2$, and the correlation length $\ell$ of an individual transmissivity field can be inferred by making use of a sampling strategy in combination with $h_{efw}^{local}(r)$.

### 4.1  Sampling Strategy

The sampling strategy was constructed as a pumping test campaign in a virtual aquifer with heterogeneous transmissivity. A series of steady-state pumping tests was performed at $n$ different wells. For each test, drawdowns were measured at all $n$ wells and at $m$ additional observation wells. A similar sampling strategy to infer the aquifer statistics from drawdown measurements has been pursued by e.g. Neuman et al. (2004), Copty and Findikakis (2004), and Firmani et al. (2006).

The used sampling strategy includes $n = 8$ pumping wells and $m = 4$ observation wells. The specific location of all wells is indicated in Fig. 5. All eight pumping wells are located within a distance of 18 m. The observation wells are located at larger distances and in all four directions. The well locations were designed to gain numerous drawdown measurements in the vicinity of each pumping well to allow a reliable estimation of $T_{well}$ (or $\sigma_{local}^2$) and $\ell$ by reducing the impact of head fluctuations on the estimation results. The additional observation wells provide head observations in the far field to gain a representative value for $T_G$. The choice of the well locations does not interfere with the refinement of the numerical grid at the pumping well.

Each of the eight pumping tests was analysed with $h_{efw}^{local}(r)$ (Sect. 2.4). The best-fitting estimates $\hat{T}_G$, $\hat{T}_{well}$, and $\hat{\ell}$ for all tests were inferred by minimizing the difference between the analytical solution and the 12 measurements. Additionally, parameter estimates were inferred by analysing the drawdown measurements of all tests jointly.

### 4.2  Aquifer analysis

The sampling strategy was applied to fields of all ensembles A–G (Table 1). Results are presented for two fields: D1 out of ensemble D ($\sigma^2 = 2.25$, $\ell = 20$ m) and E1 out of ensemble E ($\sigma^2 = 4.0$, $\ell = 10$ m). Each field was generated according to the theoretical values defined for the particular ensemble and afterwards analysed geostatistically to determine the sampled values. The fields D1 and E1 are visualized in Fig. 5. The drawdown measurements for all eight pumping tests at both fields are given in Fig. 6. The inverse estimates as well as
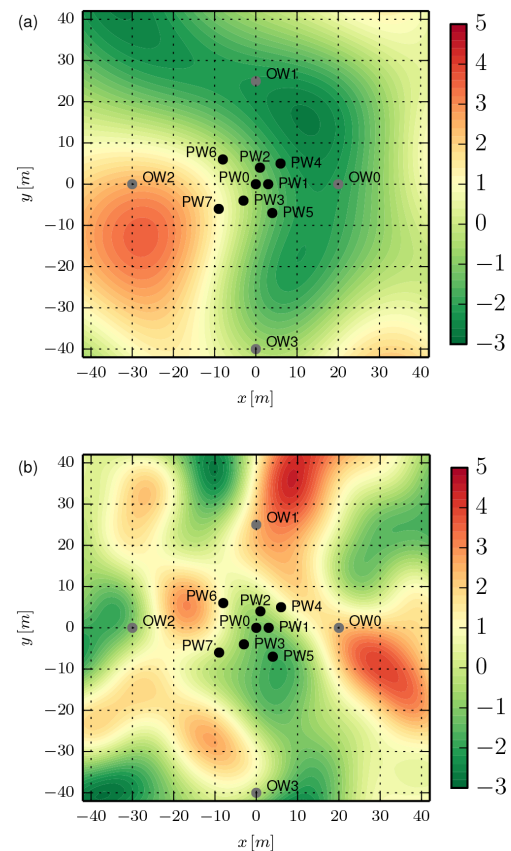


**Figure 5.** Spatial distribution of log-transmissivity for fields **(a)** D1 and **(b)** E1 and locations of the eight pumping wells (PW$_0$, …, PW$_7$ in black) and the four observation wells (OW$_0$, …, OW$_3$ in grey).

theoretical input and sampling values for the statistical parameters are summarized in Table 2.

Analysing the data from all eight pumping tests at field D1 jointly yields very close estimates of all parameters $\hat{T}_G$, $\hat{T}_{well}$ (corresponding to $\hat{\sigma}^2 = 2.255$), and $\hat{\ell}$ to the theoretical and sampled values. The geometric mean estimate is similar for all of the eight individual pumping tests. In contrast, the values of $\hat{T}_{well}$ vary within one order of magnitude. This behaviour was expected, since $\hat{T}_{well}$ represents the local transmissivity value at the pumping well. The wide range of estimates is a results of the high variance of the transmissivity field. The estimates of the correlation length $\hat{\ell}$ differ between the individual tests within a reasonable range of a few meters. The only exception is the estimate for pumping at PW$_5$. For this specific pumping test is highly uncertain due to the coincidence of the values of $\hat{T}_{well}$ and $\hat{T}_G$, similar to the realizations in Fig. 3b, as discussed in Sect. 3.3. However, the mean value over the individual tests as well as the estimate from the joint analysis of all measurements gave reliable estimates for the correlation length.

The analysis of the sampling strategy at field E1 yields similar results to those for D1. The geometric mean val-

**Table 2.** Parameter estimates of geometric mean transmissivity $\hat{T}_{\mathrm{G}}$ ($10^{-4}\,\mathrm{m^2\,s^{-1}}$), local transmissivity at the well $\hat{T}_{\mathrm{well}}$ ($10^{-4}\,\mathrm{m^2\,s^{-1}}$), and correlation length $\hat{\ell}$ (m) for the eight pumping tests at fields D1 (from ensemble D, $\sigma^2 = 2.25$) and E1 (from ensemble E, $\sigma^2 = 4.0$). Additionally, the theoretical and the sampled values ($T_{\mathrm{well}} \equiv T_{\mathrm{H}}$) are given.

|         | D1 | | | E1 | | |
|---------|--------------------|---------------------|-----------|--------------------|---------------------|-----------|
|         | $\hat{T}_{\mathrm{G}}$ | $\hat{T}_{\mathrm{well}}$ | $\hat{\ell}$ | $\hat{T}_{\mathrm{G}}$ | $\hat{T}_{\mathrm{well}}$ | $\hat{\ell}$ |
| $PW_0$  | 1.025 | 0.434 | 29.51 | 1.945 | 0.313 | 9.56  |
| $PW_1$  | 1.023 | 0.362 | 27.23 | 2.202 | 0.445 | 11.55 |
| $PW_2$  | 1.076 | 0.220 | 23.68 | 2.093 | 0.437 | 10.03 |
| $PW_3$  | 0.898 | 1.057 | 9.51  | 2.052 | 0.520 | 15.34 |
| $PW_4$  | 1.001 | 0.147 | 20.53 | 2.174 | 1.847 | 12.30 |
| $PW_5$  | 0.889 | 1.071 | 5.33  | 1.980 | 1.117 | 5.43  |
| $PW_6$  | 1.038 | 0.177 | 20.39 | 1.840 | 0.148 | 8.78  |
| $PW_7$  | 0.901 | 1.700 | 16.48 | 1.969 | 0.476 | 17.04 |
| Mean of 8 | 0.981 | 0.646 | 19.08 | 2.032 | 0.663 | 9.90 |
| Jointly | 1.013 | 0.328 | 22.38 | 2.010 | 0.409 | 9.97 |
| Theory  | 1.0   | 0.325 | 20.0  | 1.0   | 0.135 | 10.0 |
| Sampled | 0.985 | 0.333 | 23.43 | 1.999 | 0.491 | 12.66 |

ues $\hat{T}_{\mathrm{G}}$ differ little among the eight individual pumping tests and for the joint analysis. The mean value is double the value of the theoretical one, but close to the sampled geometric mean (Table 2). The local transmissivities $\hat{T}_{\mathrm{well}}$ again vary within one order of magnitude, reflecting the high variance of the field. The mean and jointly estimated values are higher than the theoretical one, which is in correspondence with the difference in the geometric mean. The estimates of the correlation length $\hat{\ell}$ deviate in a reasonable range of a few meters, which reflects the impact of the location of the pumping well with regard to the shape of the correlation structure around the well.

Finally, the analysis shows that representative values of the statistical parameters can be determined by performing a pumping test at multiple locations of an individual transmissivity field. It was shown that $h_{\mathrm{efw}}(r)$ is feasible to interpret steady-state pumping tests in highly heterogeneous fields.

## 5 Conclusions

The analytical effective well flow solution $h_{\mathrm{efw}}(r)$ is presented, which can be interpreted as an extension of Thiem's equation to heterogeneous media. $h_{\mathrm{efw}}(r)$ depends on the statistical parameters of log-normally distributed transmissivity: geometric mean $T_{\mathrm{G}}$, variance $\sigma^2$, and correlation length $\ell$. $h_{\mathrm{efw}}(r)$ was derived based on the radial coarse graining transmissivity $T_{\mathrm{RCG}}(r)$ introduced by Schneider and Attinger (2008), which interpolates between the near-well and far-field representative transmissivities for well flow. The effective well flow solution does not refer to an effective well flow equation directly but is an analytical solution of the groundwater flow equation under well flow conditions in combina-
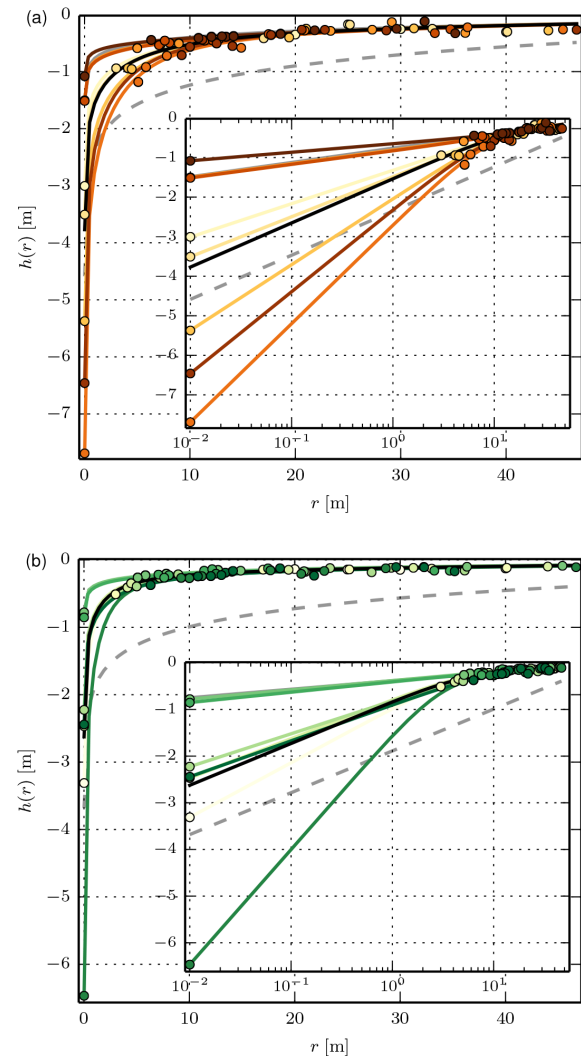


**Figure 6.** Simulated drawdown measurements (dots) and fitted effective well flow solution $h_{\mathrm{efw}}(r)$ (lines) for eight pumping tests within the heterogeneous transmissivity fields **(a)** D1 and **(b)** E1. Colours indicate the results for the individual pumping tests at $PW_0, \ldots, PW_7$ (from light to dark). The black line denotes the effective well flow solution $h_{\mathrm{efw}}(r)$ fitted to all measurements jointly. Grey lines denote Thiem's solution for $\hat{T}_{\mathrm{G}}$ (solid) and for $\hat{T}_{\mathrm{well}}$ (dashed). Statistical parameters are given in Table 2.

tion with the radial coarse graining transmissivity as an effective transmissivity. Simulation of pumping tests were performed in log-normally distributed transmissivity fields and compared with $h_{\mathrm{efw}}(r)$. Based on the results, the following conclusions can be drawn:

1. $h_{\mathrm{efw}}(r)$ describes the mean drawdown of a pumping test in two-dimensional heterogeneous isotropic media effectively. It is not limited to small variance but is tested to reproduce ensemble means for highly heterogeneous media with variances up to $\sigma^2 = 4$.

2. The analytical character of $h_{\mathrm{efw}}(r)$ allows performing inverse estimation of the statistical parameters of the transmissivity fields from measured drawdowns. Geometric mean $T_{\mathrm{G}}$, variances $\sigma^2$, and correlation length $\ell$ can be estimated for a wide range of parameters with high accuracy and certainty from ensemble mean drawdowns.

3. Parameter estimates from individual drawdowns reflect local heterogeneity at the well rather than the global statistical parameters of the transmissivity field.

4. Representative values of geometric mean, variance, and correlation length for an individual field of transmissivity can be determined by performing pumping tests at multiple locations of that field, estimating the parameters for every test separately, and then performing a statistical analysis of the results.

$h_{\mathrm{efw}}(r)$ is a promising tool with which to interpret steady-state pumping tests in order to infer the statistical parameters of the underlying transmissivity field without time- and cost-intensive laboratory investigations. Future steps will include the expansion of the method to interpret transient pumping test data.

## Appendix A

The effective well flow head $h_{\text{efw}}(r)$ as the solution of the well flow Eq. (2) is derived by solving the integral (Eq. 3) with the analytical expression of $T_{\text{RCG}}(r)$ from Eq. (4).

$$h(r_2) - h(r_1) = \frac{C_1}{T_G} \int_{r_1}^{r_2} \frac{1}{r} \exp\left(\frac{\sigma^2}{2} \frac{1}{(1+\zeta^2 r^2/\ell^2)}\right) \, dr \quad \text{(A1)}$$

The integral is evaluated analytically by making use of the exponential integral function

$$\Gamma(x) - \Gamma(X) = \int_X^x \frac{\exp(z)}{z} \, dz = \ln\frac{x}{X} + \sum_{k=1}^{\infty} \frac{x^k - X^k}{k! k} . \quad \text{(A2)}$$

The argument in the exponent in Eq. (A1) is substituted by $z(r) = \frac{\sigma^2}{2} \frac{1}{(1+\zeta^2 r^2/\ell^2)}$ with integrator $dr = -\frac{\ell \sigma^2}{4\zeta z^2}\left(\frac{\sigma^2}{2z} - 1\right)^{-\frac{1}{2}} dz$; furthermore partial fraction decomposition is used, resulting in

$$h(r_2) - h(r_1) = \frac{C_1}{T_G} \frac{\sigma^2}{4} \int_{z(r_1)}^{z(r_2)} \frac{\exp(z)}{z(z - \frac{\sigma^2}{2})} \, dz$$

$$= \frac{C_1}{2T_G} \int_{z(r_1)-\frac{\sigma^2}{2}}^{z(r_2)-\frac{\sigma^2}{2}} \frac{\exp\left(z + \frac{\sigma^2}{2}\right)}{z} \, dz$$

$$- \frac{C_1}{2T_G} \int_{z(r_1)}^{z(r_2)} \frac{\exp(z)}{z} \, dz \quad \text{(A3)}$$

$$= \frac{C_1}{2T_G} e^{\frac{\sigma^2}{2}} \left(\Gamma\left(z(r_2) - \frac{\sigma^2}{2}\right)\right.$$

$$\left. - \Gamma\left(z(r_1) - \frac{\sigma^2}{2}\right)\right)$$

$$- \frac{C_1}{2T_G} \left(\Gamma(z(r_2)) - \Gamma(z(r_1))\right) .$$

The final solution for the effective well flow head as given in Eq. (6) results by re-substituting the abbreviation $z(r) = \frac{\sigma^2}{2} \frac{1}{(1+\zeta^2 r^2/\ell^2)}$ with $r_2 = r$ and $r_1 = R$ and inserting $C_1 = -\frac{Q_w}{2\pi}$ as derived from the constant flux boundary condition (Sect. 2.1).

An approximate formulation of Eq. (A3) can be derived by using the definition of the exponential integral function as an infinite sum, given in Eq. (A2) in combination with the relationship $z(r) - \frac{\sigma^2}{2} = \frac{\sigma^2}{2} \frac{-\zeta^2 r^2/\ell^2}{1-\zeta^2 r^2/\ell^2} = z(r)\left(-\frac{\zeta^2 r^2}{\ell^2}\right)$:

$$h(r_2) - h(r_1)$$

$$= \frac{C_1}{2T_G} e^{\frac{\sigma^2}{2}} \left(\ln\frac{z(r_2) - \frac{\sigma^2}{2}}{z(r_1) - \frac{\sigma^2}{2}} + \sum_{k=1}^{\infty} \frac{\left(z(r_2) - \frac{\sigma^2}{2}\right)^k - \left(z(r_1) - \frac{\sigma^2}{2}\right)^k}{k! k}\right)$$

$$- \frac{C_1}{2T_G} \left(\ln\frac{z(r_2)}{z(r_1)} + \sum_{k=1}^{\infty} \frac{z(r_2)^k - z(r_1)^k}{k! k}\right)$$

$$= \frac{C_1}{T_G} e^{\frac{\sigma^2}{2}} \ln\frac{r_2}{r_1} + \frac{C_1}{2T_G}\left(e^{\frac{\sigma^2}{2}} - 1\right)\ln\frac{z(r_2)}{z(r_1)}$$

$$+ \frac{C_1}{2T_G} \sum_{k=1}^{\infty} \frac{z(r_2)^k\left(e^{\frac{\sigma^2}{2}}(-\zeta^2 r_2^2/\ell^2)^k - 1\right) - z(r_1)^k\left(e^{\frac{\sigma^2}{2}}(-\zeta^2 r_1^2/\ell^2)^k - 1\right)}{k! k}$$

$$\approx \frac{C_1}{T_G} e^{\frac{\sigma^2}{2}} \ln\frac{r_2}{r_1} + \frac{C_1}{2T_G}\left(e^{\frac{\sigma^2}{2}} - 1\right)\ln\frac{z(r_2)}{z(r_1)}$$

$$+ \frac{C_1}{2T_G}\left(e^{\frac{\sigma^2}{2}} - 1\right)(z(r_2) - z(r_1)) .$$

$$\text{(A4)}$$

The final approximate solution as given in Eq. (7) results by re-substituting $z(r)$ with $r_2 = r$ and $r_1 = R$ and inserting $C_1 = -\frac{Q_w}{2\pi}$.

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