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## Sensitivity of SWAT simulated streamflow to climatic changes within the Eastern Nile River basin

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**Abstract.** The hydrological model SWAT was run with daily station based precipitation and temperature data for the whole Eastern Nile basin including the three subbasins: the Abbay (Blue Nile), BaroAkobo and Tekeze. The daily and monthly streamflows were calibrated and validated at six outlets with station-based streamflow data in the three different subbasins. The model performed very well in simulating the monthly variability while the validation against daily data revealed a more diverse performance. The simulations indicated that around 60% of the average annual rainfalls of the subbasins were lost through evaporation while the estimated runoff coefficients were 0.24, 0.30 and 0.18 for Abbay, BaroAkobo and Tekeze subbasins, respectively. About half to two-thirds of the runoff could be attributed to surface runoff while the other contributions came from groundwater.

Twenty hypothetical climate change scenarios (perturbed temperatures and precipitation) were conducted to test the sensitivity of SWAT simulated annual streamflow. The result revealed that the annual streamflow sensitivity to changes in precipitation and temperature differed among the basins and the dependence of the response on the strength of the changes was not linear. On average the annual streamflow responses to a change in precipitation with no temperature change were 19 %, 17 %, and 26 % per 10 % change in precipitation while the average annual streamflow responses to a change in temperature and no precipitation change were  $-4.4 \% \text{ K}^{-1}$ ,  $-6.4 \% \text{ K}^{-1}$ , and  $-1.3 \% \text{ K}^{-1}$  for Abbay, BaroAkobo and Tekeze river basins, respectively.

47 temperature and precipitation scenarios from 19 AOGCMs participating inCMIP3 were used to estimate future changes in streamflow due to climate changes. The climate models disagreed on both the strength and the direction of future precipitation changes. Thus, no clear conclusions could be made about future changes in the Eastern Nile streamflow. However, such types of assessment are important as they emphasise the need to use several an ensemble of AOGCMs as the results strongly dependent on the choice of climate models.

## 1 Introduction

Numerous studies have been conducted at different scales ranging from small watersheds to the entire globe to assess the impacts of climate change on hydrologic systems (Jha et al., 2006). As Jha et al. (2006) noted with reference Arnell et al. (2001), nearly 80 studies were published in the late 1990s in which climate change impacts for one or more watersheds were analysed using a coupled climate model hydrologic model approach. However, more than half of the studies were carried out for river basins in Europe (Jha et al., 2006) and relatively few studies have been conducted in tropical region in Africa. The River Nile is already under great pressure from various competing applications as well as social, political and legal conditions within the riparian countries (Taye et al., 2011). To understand and resolve the potential water resource management problems associated with water supply, power generation, and agricultural practices as well as for future water resource planning, reservoir design and management, and protection of the natural environment, it is necessary to provide quantitative estimates of the hydrological effects of climate change. In this regard as Taye et al. (2011) stated several studies have been conducted on the sensitivity of streamflow to climate changes for many parts of the Nile. Among these studies, Elsahmay et al. (2009) run an ensemble of climate change scenarios using the Nile Forecasting Model with bias corrected precipitation and temperatures from 17 coupled general circulation models (AOGCMs) for the 2081-2098 period to assess the effects on the streamflow of the Blue Nile at Diem which belongs to Eastern Nile basin. One of the conclusions in Elshamy et al. (2009) was that the uncertainty in future precipitation change due to increased greenhouse gas emissions are large, making the future changes in streamflow very uncertain. Recently Taye et al. (2011) simulated the climate change impact on hydrological extremes in two regions (Nyando basin found in white Nile and Lake Tana catchment located in upper Blue Nile subbasin) and noted that for Lake Tana catchment the GCM uncertainty was more important than the hydrological models uncertainty.

Abbay (Blue Nile), BaroAkobo (Sobat) and Tekeze (Atbara) are the three major river basins in the Eastern Nile which all originated from the Ethiopian Highlands. 86% (or 82 km<sup>3</sup>) of the total average flow of the Nile at Aswan is estimated to origin from these three river basins (Arsano, 2005). Several attempts have been made to implement hydrological models for the Blue Nile basin. Sutcliffe et al. (1989) and Dugale et al. (1991) used a simple daily hydrological model calibrated by METOSAT derived rainfall estimates and the National Oceanic and Atmospheric Administration, USA in collaboration with the Egyptian Ministry of Public Works has developed a comprehensive model of the Nile to predict the inflow to the Aswan Dam (Barrett et al., 1993; Schaake et al., 1993; Johanson and Curtis, 1994; Todd et al., 1995). However, as Conway (1997) stated, both of these investigations suffered by the lack of in situ data, in particular subbasin discharge data to calibrate the hydrological models and gauge estimates of daily rainfall to calibrate the METEOSAT derived estimates of rainfall. Conway (1997) applied a gridbased water balance model with limited meteorological and hydrological data inputs on a monthly time step for the Blue Nile catchment. According to Conway (1997) the correlation between observed and simulated annual flows was 0.74 for a 76-yr data period and the mean error was 14%, although relatively large errors occurred in individual years. Furthermore, Mohamed et al. (2005) focused on the interaction between the climatic processes and the hydrological processes on the land surface in the subbasins of Nile (White, Blue Nile, Atbara and the main Nile) using a regional atmospheric model to show that the model could reproduce runoff reasonably well over the subbasins of the Nile. The above studies except the latter, have all been investigating the upper Blue Nile basin but there are still very few published studies on the two other basins (Tekeze and BaroAkobo). Recently, Setegen et al. (2008) investigated the Lake Tana Basin (part of the Blue Nile) using the hydrological model (SWAT) and studies applying the same model have also been conducted for the Meki basin (Central Ethiopia) and the upper Awash basin (western catchment of the Awash basin in Ethiopia) by Zeray et al. (2007) and Checkol (2006), respectively. These three studies showed that the SWAT model was able to describe the study areas with a quality that makes it suitable for water resource management use.

The aim of this paper is to test the applicability of the Soil and Water Assessment Tool (SWAT) physically distributed model over the three major subbasins in Eastern Nile at larger watershed scale and thereby complementing other older studies that have simulated parts of the catchment. Sensitivity studies to assess the potential impacts of climate change on the annual streamflow is performed using twenty hypothetical climate change perturbations in temperature, precipitation or both. In addition, the sensitivities found above together with 47 temperature-precipitation scenarios from 19 AOGCMs which were participating inpahse 3 of the Coupled Model Inercomparison Project (CMIP3) are used to assess the uncertainty in future streamflow changes for the Eastern Nile.

## 2 Description of the study area

The Eastern Nile and their tributaries all originate on the Ethiopian plateau and the three subbasins of the Eastern Nile lies between 5° N 33' E and 15° N 39' E with altitude ranges from 390 m in part of BaroAkobo to over 4500 m in the Tekeze river basin (MoWR, 2002). The total average annual flows are estimated to be 50.0, 23.6 and 8.2 billion cubic meters from the Abbay, BaroAkobo and Tekeze river basins, respectively (Arsano et al., 2004; MoWR, 2002). They provide 86% of the waters of the Nile (Abbay 59%, BaroAkobo 14%, Tekeze 13%, Swain, 1997).

According to materials published by the Ethiopian Central Statistical Agency, the Blue Nile has a total length of 1450 kilometers, of which 800 km are inside Ethiopia. The Blue Nile flows south from Lake Tana and then west across Ethiopia and northwest into Sudan. Although there are several feeder streams that flow into Lake Tana, the source of the river is generally considered to be a small spring at Gish Abbay (Lesser Abbay) north of Lake Tana at an altitude of approximately 2744 m. Other affluent streams of this lake include, from Gorgora, Magech, Gumara, Ribb, and Kilti Rivers. Lake Tana's outflow then flows 30 km before plunging over the Tis Issat Falls. The river then loops across northwest Ethiopia through a series of deep valleys and canyons and join Rahad and Dinder rivers downstream of Roseires in Sudan, after which it is known as the Blue Nile. There are numerous tributaries of Abbay between Lake Tana and the Sudanese border. Some of these are Bashilo, Walaka, Jamma, Muger, Guder, Anger, Didessa, and Dabus Rivers from the left bank, and Muga, Temcha, Lah, Chamoga, Fettam and Beles Rivers from right bank of the main Abbay River. After flowing past Roseires inside Sudan, the Blue Nile joins the White Nile at Khartoum and, as the River Nile, flows through Egypt to the Mediterranean Sea at Alexandria. Due to the high seasonal variability in rainfall over the Ethiopian plateau, the seasonal variation of the flow of the Abbay is large with maximum runoff is in August when it is about 60 times greater than its minimum in the month of February (Arsano, 2005).

The Baro-Akobo (Sobat) river system marks a 380 km frontier between Ethiopia and Sudan and originates in the Western Ethiopian Highlands. The Baro River is created by the confluence of the Birbir and Gebba Rivers, east of Metu in the Illubabor Zone of the Oromia Region, Ethiopia. It then flows west through the Gambela Region to join with the Pibor River from Sudan and Rivers from Northern Uganda to form the Sobat. Other notable tributaries of the Baro include the Alwero and Gilo Rivers. Of the Sobat River tributaries, the Baro River is the largest, contributing 83% of the total water flowing into the Sobat. During the rainy season, between June and October, the Baro River alone contributes about 14% of the Nile's water at Aswan, Egypt. In contrast, these rivers have very low flow during the dry season.

The Tekeze (Atbara), rises in Northern Ethiopia Highlands and have the Angereb and Guang as its major tributaries, it replenishes the main Nile north of Khartoum. The Tekeze joins the Atbara River after entering northeastern Sudan. The climatic pattern and physical environment of the Tekeze subsystem are very similar to those of the Abbay subbasin.

The climate varies from warm, desert-like climate at the Sudan border, to wet in the Ethiopian Highlands. The annual rainfall ranges from 800 mm to 2200 mm with an average of about 1420 mm for the Abbay river basin. The annual rainfall reaches at maximum of 3000 mm over the highlands and a minimum of 600 mm in the lowlands with annual average rainfall of about 1419 for the case of BaroAkobo Basin. In contrast to the Abbay and BaroAkobo river basins, the annual rainfall for Tekeze is much lower, ranging from 600 mm to 1200 mm with an average of about 900 mm. Most of rainfall occurs from June to September for all the three subbasins (MoWR, 2002).

## **3** Methods and materials

### 3.1 Model description

We used the physically based, distributed parameter model-SWAT (Soil and Water Assessment tool, version SWAT2005) which operates on daily time step and uses physiographical data such as elevation, land use and soil properties as well as meteorological data and, river discharge data for calibration (Arnold and Allen, 1996).

#### 3.2 Hydrological processes

The hydrological processes included in the model are evapotranspiration (ET), surface runoff, infiltration, percolation, shallow and deep aquifers flow, and channel routing (Arnold et al., 1998). The effects of spatial variations in topography, land use, soil and other characteristics of watershed hydrology are incorporated by dividing a basin into several subbasins based on drainage areas of tributaries and is further divided the subbasins into a number of hydrological response unit (HRUs) within each subbasin, based on land cover and soils. Each HRU is assumed spatially uniform in terms of land use, soil, topography and climate. The subdivision of the watershed enables the model to reflect differences in evapotranspiration for various crops and soils. All model computations are performed at the HRUs level.

The fundamental hydrology of a watershed in SWAT is based on the following water balance equation

$$\frac{\partial SW}{\partial t} = R_{day} - Q_{surf} - E_a - W_{seep} - Q_{gw}$$
(1)

Where SW is the soil water content (mm),  $R_{day}$  is the amount of precipitation on (mm),  $Q_{surf}$  is the amount of surface runoff (mm),  $E_a$  is the amount of evapotranspiration (mm),  $W_{seep}$  is the amount of water entering the vadose zone from the soil profile (mm), and  $Q_{gw}$  is the amount of ground flow (mm). A detail descriptions of the different model components can be found in Arnold et al. (1998) and Neitsch et al. (2002a).

#### 3.3 Physiographical data for the three subbasins

A range of spatially distributed data such as topographic features, soil types, land use and the stream network (optional) are needed for the model. Table 1 summarizes the input data use in the AVSWAT-X interface.

### 3.3.1 Digital elevation model

A DEM was created using a 1 km<sup>2</sup> resolution topographic database obtained from the Ethiopian Ministry of Water Resources. The DEM (see Fig. 2) was used to delineate the watershed and the drainage patterns of the surface area analysis. Subbasin parameters such as slope gradient, slope length of the terrain, and the stream network characteristics such as channel slope, length, and width were derived from DEM.

## 3.3.2 Land use and soil maps

Land use is one of the main factors affecting surface erosion, and evapotranspiration in a watershed. The source of

**Table 1.** Data sources for the Eastern Nile basin.

Data Type	Scale	Data Descriptions
DEM (Topographical data)	$1 \mathrm{km} \times 1 \mathrm{km}$	Elevation data from Ethiopia ministry of water resources
Soil	$10 \mathrm{km} \times 10 \mathrm{km}$	Soil texture data from ministry of water resources supplemented by the FAO soil data base
Land use	$1 \text{ km} \times 1 \text{ km}$	Land classification and their attributes from Ethiopia ministry of water resources



**Fig. 1.** Map showing an outline of Ethiopia and the water sources of Eastern Nile basin including stream gauges at the major tributaries (dots) and stream gauges for calibration and validation of the model (boxes).

land use map of the study is the Ministry of Water Resources Ethiopia and land use/land cover map was taken from the global Hydro1K dataset (Hansen, 1998) and modified to correspond with the SWAT predefined land uses classification (Fig. 3).

More than 50%, 23% and 15.7% of Abbay, Tekeze and BaroAkobo subbasin, respectively, are used for agriculture whereas forest, grass, bush and shrubs cover the rest. For detail see Fig. 3. Land use of the study area has changed over time (Rientjes et al., 2011) due to over increasing population density, changing agricultural practices, urbanization and water related infrastructure such as irrigation and hydropower production. As no detailed mapping of these changes exists for the whole region it is not taken into account.



**Fig. 2.** Topography (m) of the eastern Nile basin based on a  $1 \times 1$  km digital elevation model.

Different types of soil texture and physical-chemical properties are required for SWAT simulations. These data were obtained from various sources. The soil map obtained from Ministry of Water Resources of Ethiopian at Water Resources Information and Metadata Base Centre department. However, several properties like moisture bulk density, saturated hydraulic conductivity, percent clay content, percent silt content and percentage sand content of the soil which are required by SWAT model were not incorporated. These additional data were substantiated from various sources such as Wambeke (2003); USDA (1999) and FAO (1995). As it is shown in Fig. 4, the major soil types are lithosols and Eutric Cambisols for Tekeze subbasin: Chrome Acid Luvisols, Eutric Vertisol, Luvisols and lithic Leptosols for Abbay and Dystric cambisols and orthic Acrisols for BaroAkobo subbasin.



**Fig. 3.** Map of landuse of the three sub-basins of the Eastern Nile (Tekeze, Abbay and Baro Akobo).



**Fig. 4.** Map of soil types of the three sub-basins of the Eastern Nile (Tekeze, Abbay and Baro Akobo).

#### 3.3.3 Meteorological data

SWAT requires daily meteorological data, which were collected from the Ethiopian National Meteorological Agency (NMSA) for the period 1987–2006. We use 60 and 97 stations with temperature and precipitation, respectively. Figure 5 shows the stations used in this study and Table 2 sum-



Fig. 5. Main rivers and meteorological stations in the eastern Nile basin.

marize the number of stations in each subbasin. The average percentage of missing data in the observed datasets was less than 10% and 5% of precipitation and temperature, respectively. Missing values were filled using the SWAT built-in weather generator developed by Nicks (1974). The weather generator used a first-order Markov chain model. For each subbasin input to the weather generator was observed precipitation data for the weather station that was nearest the centroid of the subbasin and having a record length from 1967-2006. Given the observed wet and dry days frequencies, the model determine stochastically if precipitation occurs or not. When a precipitation event occurs, the amount is determined by generating values from a skewed normal daily precipitation distribution or a modified exponential distribution which is calculated based on the observed data. The amount of daily precipitation is partitioned between rainfall and snowfall using average daily air temperature.

## 3.3.4 River discharge

Hydrological discharge data were collected from the Ministry of Water Resources of Ethiopia. Table 3 summarizes the number of stream gauges with the date of the record length used for calibration and validation. All the flow data were daily except at Diem (Abbay, Sudan Border) where only monthly data was available.

## 3.4 Model setup

The Abbay, BaroAkobo and Tekeze stream network and sub watersheds were delineated using ARCSAWT-X with the SWAT suggested drainage area required to form the origin of the stream. 24, 29, 25 sub watersheds; and 309, 128 and 313 HRUs of Abbay, BaroAkobo and Tekeze river basin

Data type	Number of stations	Data descriptions
Temperature $(T_{\text{max}} \text{ and } T_{\text{min}})$	Abbay; 42 stations BaroAkobo; 8 stations Tekeze; 10 stations	Daily data from the Ethiopian National Meteorological Agency (NMSA)
Precipitation	Abbay; 74 stations BaroAkobo; 12 stations Tekeze; 11station	Daily data from the Ethiopian National Meteorological Agency (NMSA)

**Table 2.** Meteorological data sources for Eastern Nile basin.

Table 3. Streams gauges and their corresponding drainage area with calibration and validation dates used for model simulations.

Stream gauge name (basin)	Drainage Area (km <sup>2</sup> )	Calibration date	Validation date
Tana outlet (Abbay)	15 321	1 January 1991–31 December 1996	1 January 1997–31 December 2000
Kessie (Abbay)	65784	1 January 1991–31 December 1996	1 January 1997–31 December 2000
Diem (Abbay)	17400	1 January 1991–31 December 1996	1 January 1997–31 December 2000
Embamadre (Tekeze)	45 694	1 January 1994–31 December 1999	1 January 2000–31 January 2003
Gambella (BaroAkobo)	23 461	1 January 1990–31 December 1998	1 January 1999–31 December 2004
Gilo (BaroAkobo)	10137	1 January 1990–31 December 1998	No recorded data

as a function of 2 % land use and 5 % soil types within a given watershed, respectively were delineated up to the point of outlets for each subbasin. These points constituent of a drainage area of 174 000, 43 906, and 76 343 km<sup>2</sup> that drain about 86 %, 60 % and 93 % of the entire Abbay (201 340 km<sup>2</sup>), BaroAkobo (74 102 km<sup>2</sup>) and Tekeze (82 350 km<sup>2</sup>) subbasins, respectively which all are found in Ethiopia.

The Soil Conservation Service (SCS) curve number procedure (USDA-SCS,1972) was applied to estimate surface runoff volumes due to the unavailability of sub daily rainfall data required for the Green and Ampt method that SWAT offers a different option to estimate surface runoff. The potential evapotranspiration (PET) estimates and channel routing were performed using Hargreaves and Muskingum methods, respectively.

## 3.5 Sensitivity analysis

After pre-processing of the data and SWAT model set up, simulation was done for the periods indicated in Table 3 for the three subbasins. The built-in SWAT sensitivity analysis tool that uses the Latin Hypercube One-factor-AT-a-Time (LH-OAT) (Van Griensvenet al., 2002, 2005) was used. Six outlets (Fig. 1) were selected for the sensitivity analysis; three of them (Tana outlet, Kessie and Diem) in the Abbay, and two in BaroAkobo (Gambella and Gilo) and one in Tekeze (Embamadre).

According to Lenhart et al. (2002) the sensitivity of a flow to a parameter can be categorized into four classes. If the relative sensitivity lies between 0-0.05 and 0.05-0.2, then the parameter are classified as negligible and medium, respectively, whereas if it is varying between 0.2–1.0 and greater than 1 then categorized as high and very high class, respectively. Out of 28 selected parameters the curve number, available water capacity, average slope steepness, saturated hydraulic conductivity, soil evaporation compensation factor, soil depth, maximum canopy storage, threshold water depth in the shallow aquifer for flow, and baseflow alpha factor were identified as being parameters to which the flow has medium, high or very high sensitivity. The ranking of the parameters were different at various outlets where sensitivity test was carried out. However the curve number (CN<sub>2</sub>) was the main sensitivity parameter for all outlets. This is due to the fact that the curve number depends on several factors including soil types, soil textures, soil permeability, land use properties etc. In addition, the relative sensitivity of the available water capacity (Sol-AWC), the soil evaporation compensation factor (ESCO) and the saturated hydraulic conductivity (Sol-K) were also high in all outlets. From the sensitivity test, eight parameters having a relative sensitivity greater than 0.05 (sensitivity of the flow to the parameter categorized as medium or higher) were selected for the calibration process.

**Table 4.** List of adjusted parameters with calibrated values after manual and automatic calibration at the selected outlets for three subbasins of Eastern Nile using SWAT 2005 model.

Id	Parameter	Description	Range	Initial values	Cal	lues	
					Abbay	Baro	Tekeze
1	CN <sub>2</sub>	Initial SCS CN II value	±25 %	*	-10 %	-12 %	-24 %
2	Sol_K	Saturated Hydraulic conductivity (mm mm <sup><math>-1</math></sup> )	$\pm 25$ %	**	-4%	1.3 %	19 %
3	ESCO	Soil evaporation compensation factor	0.0 - 1.0	0.95	0.7	0.58	0.8
4	SOL_AWC	Available water capacity (mm water mm soil <sup><math>-1</math></sup> )	±25 %	**	+25 %	7 %	9.4 %
5	SOL_Z	Soil depth (mm)	±25 %	**	-4%	25 %	13 %
6	GWQMN	Threshold water depth in the shallow aquifer for flow (mm)	0.0-5000	0.0	200	319	53
7	CANMX	Maximum canopy storage	0-10	0.0	9.7	2.4	0.31
8	ALPHA_BF	Base flow alpha factor	0.0 - 1.0	0.048	0.048	0.01	0.002

The ranges are based primarily on recommendations given in the SWAT User's Manual (Neitsch et al., 2002a). \* SWAT default parameters and SWAT driven parameters were used. \*\* Field measured and from literature collected parameters.

## 3.6 Calibration and validation

Watershed models contain many parameters; these parameters are classified into two groups: physical and process parameters. A physical parameter represents physically measurable properties of the watershed (e.g. areas of the catchment, fraction of impervious area and surface area of water bodies, surface slope etc) while process parameters represents properties of the watershed which are not directly measurable e.g. average or effective depth of surface soil moisture storage, the effective lateral inflow rate, the coefficient of non-linearity controlling the rate of percolation to the groundwater (Sorooshian and Gupta, 1995). Thus, calibrations against available streamflow observations are often conducted to tune the model. Because automatic calibration relies heavily on the optimization algorithm and the specified objective function we follow the recommendations of Gan (1998) to use both manual and automatic calibration procedures. We first conducted manual calibration of daily stream using the procedure developed by Santhi et al. (2001). Parameters identified from the sensitivity analysis were varied in sequence of their relative sensitivity within their ranges (Table 4) until the volume is adjusted to the required quantity (Zeray et al., 2007). This process continued till the volume simulated is within  $\pm 15$  % of the gauged volume. The surface runoff adjustment was then followed by that of the baseflow. Here, the same apporach was followed being the adjustment made to the most sensitivity parameters affecting the baseflow. Each time the baseflow calibration is finalized, the surface runoff volume was also checked as adjustment of the baseflow parameters can also affect the surface runoff volume. The same procedure was followed to calibrate the water balance of the monthly flows. After each calibartion, the coefficient of determintation (proportion of the variance in the observations explained by the model,  $R^2$ ) and Nash-Sutcliffe effficeny value (ENS) were checked ( $R^2 > 0.6$  and ENS > 0.5, Santhi et al., 2001). Finally, the automatic calibration algorithm in SWAT is used for fine tuning the calibration. This is based on the Shuffled Complex Evolution algorithm developed at the University of Arizona (SCE-UA) which is a global search algorithm that minimizes a single objective function for up to 16 model parameters (Duan et al., 1992).

The performance of SWAT was evaluated using the Nash-Sutcliffe efficiency value (ENS) and the coefficient of determination ( $R^2$ ). The difference between the ENS and the  $R^2$  is that the ENS can interpret the model performance in the replicating individually observed values while the  $R^2$  does not (Rossi et al., 2008). It is only measuring the deviation from the best fit line. In addition systematic difference between the model and observations in the percentage (PBias) and the ratio of the root mean square error between the simulated and observed values to the standard deviation of the observations (RSR) was used. The equations and the interpretation of the values are given in Table 5. After manual and automatic calibration the daily, monthly and annual streamflow were compared against the observed data.

## 3.7 Climate sensitivity scenarios

Climate sensitivity scenarios were performed by perturbing the baseline simulation (the validated simulation forced with observed station data) as input. The climate perturbations are given as a percentage change in precipitation (precipitation is multiplied with a given factor). Thus, the number of wet and dry days was not perturbed, only the precipitation intensity. The temperature perturbation is applied by adding the prescribed change to the baseline simulation temperatures (Varanou et al., 2002). Each scenario was then run for the same simulation period as the baseline simulation. The perturbations applied are with temperature increases of 0, +2 and +4 °C and precipitation changes of -20%, -10%,

Formulae	Value	Rating		
	> 0.65	Very good		
ENS = 1 - $\begin{bmatrix} \sum_{i=1}^{n} (x_{obs}(i) - y_{mod el}(i))^{2} \\ \sum_{i=1}^{n} (x_{obs}(i) - \overline{x_{obs}})^{2} \end{bmatrix}$	0.54 to 0.65	Adequate		
	> 0.50	Satisfactory		
	$<\pm20$ %	Good		
$PBIAS = \begin{bmatrix} \sum_{i=1}^{n} (x_{obs}(i) - y_{mod el}(i)) \\ \sum_{i=1}^{n} (x_{obs}(i)) \\ \cdot 100 \end{bmatrix}$	$\pm 20$ % to 40 %	Satisfactory		
	$> \pm 40\%$	Unsatisfactory		
	$0.0 \le RSR \le 0.5$	Very good		
$\left[\sqrt{\sum_{i=1}^{n} (x_{\text{obs}}(i) - y_{\text{mod el}}(i))^2}\right]$	$0.5 < RSR \le 0.6$	Good		
$RSR = \frac{\lfloor \gamma_{i=1} \\ \sqrt{\sum_{i=1}^{n} (x_{obs}(i) - \overline{x_{obs}})^2}}$	$0.6 < \mathrm{RSR} \le 0.7$	Satisfactory		
1	$RSR \ge 0.70$	Unsatisfactory		
$R^{2} = \frac{\left[\sum_{i}^{n} (x_{\text{obs}}(i) - \overline{x}_{\text{obs}})(y_{\text{mod el}}(i) - \overline{y}_{\text{mod el}})\right]^{2}}{\sum_{i}^{n} (x_{\text{obs}}(i) - \overline{x}_{\text{obs}})^{2} \sum_{i}^{n} (y_{\text{mod el}}(i) - \overline{y}_{\text{mod el}})^{2}}$		Satisfactory		

**Table 5.** General reported ratings for Nash-Sutcliffe efficiency (ENS), Mean relative bias (PBIAS), Root mean square error-standard deviation ratio (RSR) and Coefficient of determination ( $R^2$ ) for calibration and validation process (adopted from Rossi et al., 2008).

-5%, 0%, +5, +10% and +20% and combination of the above temperature and precipitation perturbations. Climatic variables such as relative humidity, wind speed, cloud cover and solar radiation were considered to be unchanged.

The CMIP3 (Meehl et al., 2007) global coupled climate models (AOGCMs) were also applied to calculate annual mean temperature and precipitation changes from the base period 1980–2000 to 2080–2100 for the three subbasins. A total of 47 climate change simulations were assessed for each subbasin using three different emission scenarios (SRES A2, A1B and B1) and 19 models. Together with the sensitivity tests mentioned above and estimate of the impact of the AOGCMs temperature and precipitation changes on the annual streamflow of the different subbasins were conducted.

#### 3.8 Sensitivity of annual streamflow to climate change

The relative sensitivity of the streamflow  $(\Delta Q_{\Delta P,\Delta T})$  to either a precipitation  $(\Delta P)$  or a temperature  $(\Delta T)$  change or a combination of the two is calculated as:

$$\Delta Q_{\Delta P,\Delta T} = \frac{\left(Q_{\Delta P,\Delta T} - Q_{\Delta P=0,\Delta T=0}\right)}{Q_{\Delta P=0,\Delta T=0}} \cdot 100 \tag{2}$$

where Q is the annual or seasonal streamflow calculated using Eq. (1).

To be able to investigate if there is any nonlinearity in the streamflow change when both precipitation and temperature are changed we estimate the linear combination of the two.

$$\Delta Q_{\Delta T,\Delta P} = \left. \frac{\partial Q}{\partial P} \right|_{\Delta P,\Delta T=0} \Delta P + \left. \frac{\partial Q}{\partial T} \right|_{\Delta T,\Delta P=0} \Delta T \qquad (3)$$

where the local derivatives for each parameter is calculated as the sensitivity response when the other factor is kept unchanged. For example  $(\partial Q/\partial P)|_{\Delta P, \Delta T=0}$  are the responses in m<sup>3</sup>/% of the simulations covering the precipitation perturbations ±5, 10 and 20% and no temperature perturbation. Any deviation from this will indicate nonlinear effects that may arise as precipitation and temperature is changed simultaneously.

## 4 Results and discussion

The result part starts with a validation of the SWAT model in the three different sub-basins, then estimates of the individual sensitivity of the streamflow to temperature and precipitation in conducted before we investigate if the combined effect of temperature and precipitation changes may provide any non-linearities in the streamflow response. Finally we combine the sensitivity simulations with temperature and



Fig. 6. Daily observed (blue) and simulated (red) streamflow during the calibration and validation periods for the (a) Baro Akobo at Gambella and (b) Tekeze at Embamadre.

precipitation changes from the CMIP3 coupled climate models to investigate the range of possible streamflow responses given the uncertainty in the global model's temperature and precipitation change.

## 4.1 Model calibration and validation

### 4.1.1 Abbay calibration and validation

The model was calibrated for the Abbay subbasin with one upstream (Tana), one mid-way (Kessie) and one downstream (at the Sudan Border) gauging station. It slightly overestimated the flow in the upper and middle part of the basin and underestimated it in the lower part (Table 6) during the calibration period (the calibration and validations periods are given in Table 3). The overestimation of these simulations was particularly pronounced during extreme events (not shown). However, there were good agreements between simulated and observed flows on both daily and monthly time scale (Fig. 7a) for most of the years except 1995, when little precipitation was recorded at Tana outlet. The ENS and  $R^2$ ranged from 0.62 to 0.90 and 0.90 to 0.97, respectively for the monthly calibration (see Table 7 for further details). The daily calibration statistics were lower ranging from 0.62 to 0.65 and 0.77 for ENS and  $R^2$ , respectively (see Table 6).

In the validation period, the model similarly overestimated the flow at Tana outlet and at Kessie for the year 2000 giving a slightly higher bias than in the validation period. Thus, the daily and monthly ENS simulation efficiency was between 0.55 to 0.57 and. 0.53 to 0.65, respectively.

#### 4.1.2 BaroAkobo calibration and validation

Figures 6a and 7b show the time-series comparison of predicted and measured daily and monthly streamflows for the BaroAkobo subbasin at River Baro near Gambella over the 9 yr (1990-1998) calibration period. In general, SWAT accurately tracked the measured streamflows for the time, although some peak flow months were over predicted. The time series comparison of predicted and measured cumulative daily and monthly streamflows for the 6 yr (1999–2004) validation period is shown in the right side of the dashed line of Figs. 6a and 7b. The predicted flows closely followed the corresponding measured flows, with less over prediction of peak flow months, as compared to the calibration period. Daily and monthly statistics computed for the calibration and validation periods. (Tables 3 and 4) also show strong correlations between the simulated and measured flows. The validation period statistics were weaker than those computed for the calibration period (e.g. for daily data the Nash-Sutcliffe efficiency value (ENS) ranged from 0.70 to 0.81 for the calibration period and was only 0.64 for the validation period (Table 6), whereas, the monthly values were higher than 0.80 for both of the periods).



**Fig. 7.** Monthly observed (blue) and simulated (black) streamflow for the calibration and validation periods at **(a)** Diem (Abbay), **(b)** Gambella (Baro Akobo) and **(c)** Embamadre (Tekeze).

**Table 6.** Summary of daily streamflow statistics for the calibration and validation simulations for the Eastern Nile subbasins: ENS: Nash-Sutcliffe efficiency, PBIAS: mean relative bias, RSR: root mean square error-standard deviation ratio and  $R^2$ : coefficient of determination (see Table 5 for details).Dates for calibration and validation period is given in Table 3.

Location name (basin)		Cali	bration		Validation						
	ENS	RSR	PBIAS	$R^2$	ENS	RSR	PBIAS	$R^2$			
Tana outlet (Abbay)	0.65	0.48	38	0.77	0.55	0.74	25	0.78			
Kessie (Abbay)	0.62	0.57	14.2	0.77	0.57	0.66	9.9	0.71			
Embamadre (Tekeze)	0.50	0.74	20	0.60	0.8	0.60	6.9	0.68			
Gambella (BaroAkobo)	0.70	0.45	-10.9	0.65	0.64	0.40	-25.0	0.79			
Gilo (BaroAkobo)	0.81	0.46	-11.1	0.86							



**Fig. 8.** Annual streamflow changes (%) to precipitation change (%) holding temperature fixed for the three basins.

## 4.1.3 Tekeze calibration and validation

Calibration and validation of the Tekeze subbasin were carried out at Tekeze River near Embamadre and the predicted streamflow closely followed the measured flows, with an ENS of 0.8 and 0.5, and with a  $R^2$  of 0.81 and 0.60 for monthly and daily values during the calibration and validation periods (Tables 7 and 6), respectively. Further, a bias of 2 % in the calibration period also indicated a good agreement between measured and simulated monthly flows (Table 7).

#### 4.2 The annual water balance of the eastern Nile

Table 8 illustrates the average annual water balance components of the Eastern Nile Basin during the calibration and validation periods. 58/57 percent (calibration period/validation period), 56/58 percent and 62/64 percent of the average annual rainfalls were lost through evaporation in Abbay, BaroAkobo and Tekeze subbasin of the Eastern Nile during calibration and validation period, respectively. The average runoff coefficients were estimated to be 0.24, 0.30 and 0.18 for Abbay, BaroAkobo and Tekeze subbasins respectively. Surface runoff carried 55/58.5 percent, 71.6/74 percent and 51/54 percent of the water yield during the calibration and validation process for Abbay, BaroAkobo and Tekeze subbasins respectively. While, the groundwater contributions were 46/43 percent for Abbay, 31.7/30 percent for BaroAkobo and 50/47 percent for Tekeze during calibration and validation period respectively.

## **4.3** Sensitivity of annual Eastern Nile streamflow to climate change

The impact of the perturbed temperature and precipitation scenarios on annual streamflows in the three subbasins are shown in Table 9 and details are given in the sections below.



**Fig. 9.** Annual streamflow changes (%) to temperature change (°C) holding precipitation fixed for the three basins.

#### 4.3.1 Sensitivity to precipitation changes

Sensitivity of annual streamflow to changes in precipitation, holding the temperatures fixed (Eq. 2) was different among the three subbasins. As a first approximation, a linear regression analysis of the streamflow responses for the various scenarios indicated that a 10% change in precipitation would produce a 19%, 17%, and 26% change in streamflow for Abbay, BaroAkobo and Tekeze river basin respectively (Fig. 8). Table 9 and Fig. 10 shows that the Abbay subbasin is equally sensitive to a reduction and increase in precipitation and the sensitivity is changing linearly with the precipitation change. This was not the case for Tekeze. The sensitivity to a precipitation increase was larger than to a decrease in precipitation (-42 % and 63 % change for a -20 % and +20 % precipitation changes, respectively). For the BaroAkobo subbasin, this was the opposite. Sensitivity was stronger to a decline in precipitation (-38% and 29% for -20 and +20%precipitation change, respectively). See Table 9 and Fig. 10 for details. The change in sensitivity was likely due to the difference in topography and catchment characteristics of the subbasins. In the case of Tekeze basin, most of the region is categorized with a gentle slope, where a sheetflow change is dominating during an increase in precipitation. This is in contrast to BaroAkobo where 2/3 of the total drainage area is a plain. The land use and soil types of the two basins are also quite different. The depth of the soil in the Tekeze subbasin is shallower than BaroAkobo subbasin. Therefore, with an increase in precipitation, the response of the catchment generating direct streamflow will be smaller since more water infiltrated down to recharge the groundwater in the case of BaroAkobo subbasin. Thus, the sensitivity of BaroAkobo to an increase in precipitation will be smaller.

#### 4.3.2 Sensitivity to temperature change

The relative sensitivity of streamflow to changes in temperature, holding the precipitation fixed (Eq. 2) was relatively modest in all the three subbasins (Fig. 9). A linear regression analysis of the streamflow responses for the various temperature scenarios indicated that a  $1^{\circ}$ C increase in temperature would produce a 4.4 %, 6.4 %, and 1.3 % reduction in



Fig. 10. Change in annual streamflow (%) for different temperature and precipitation scenarios. (a) Baro Akobo, (b) Abbay and (c) Tekeze. Black dots indicate the linear sensitivity estimate based on Eq. (3).

**Table 7.** Summary of monthly streamflow statistics for the calibration and validation simulations for the Eastern Nile subbasins. ENS: Nash-Sutcliffe efficiency, PBIAS: mean relative bias, RSR: root mean square error-standard deviation ratio and  $R^2$ : coefficient of determination (see Table 5 for details). Dates for calibration and validation period are given in Table 3.

Location		Cali	bration			Validation						
	ENS	RSR	PBIAS	<i>R</i> <sup>2</sup>	ENS	RSR	PBIAS	$R^2$				
Tana outlet	0.85	0.32	7.2	0.90		0.53	0.71	21	0.86			
Kessie	0.62	0.58	28	0.90		0.54	0.80	37	0.86			
Diem	0.90	0.31	-11.3	0.97		0.65	0.39	8.2	0.92			
Embamadre	0.80	0.45	2.2	0.81		0.83	0.42	-13.9	0.88			
Gambella	0.90	0.31	-3.8	0.92		0.81	0.44	-23.0	0.89			
Gilo	0.93	0.40	-2.4	0.91		-	_	-	-			

**Table 8.** Annual averaged calibrated/validated hydrological balances and percent contribution of water balance components for the Eastern Nile basin SURQ<sup>I</sup>: surface runoff, LATQ<sup>II</sup>: lateral flow into stream, GW<sub>-</sub>Q<sup>III</sup>: groundwater in the shallow aquifer, ET<sup>IV</sup>: evapotanspiration, PET<sup>V</sup>: potential evapotranspiration (Hargreaves method is used), PERC<sup>VI</sup>: percolation below root zone (groundwater recharge), TLOS<sup>VII</sup>: transmission losses.

Subbasin	Period	Rainfall	SURQ <sup>I</sup>	LATQ <sup>II</sup>	GW_Q <sup>III</sup>	ETIV	$PET^V$	PERCVI	TLOS <sup>VII</sup>	
		(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	
Abbay	Calibration/validation	1422/1547	314.4/410	1.63/1.7	264.8/302	820.9/816	1585/1558	1585/1558 286/327		
	%	100/100	22/26	0.1/0.1	19/20	58/57		20/21	0.8/0.8	
BaroAkobo	Calibration/validation	1774/1682	527/492	0.3/0.24	233/199	997/979	1519/1542	253/215	24/23	
	%	100/100	30/29	0.2/0.1	13/12	56/58		14/13	1/1	
Tekeze	Calibration/validation	931/872	169/162	1.3/1.0	164/140	579/556	1396/1419	179/154	5/4	
	%	100/100	18/19	0.1/0.1	18/16	62/64		19/18	0.5/0.5	

streamflow for Abbay, BaroAkobo and Tekeze river basin respectively (Fig. 9). However, the sensitivity was not linear. Two of the subbasins (Abbay and BaroAkobo) showed a larger sensitivity from 0 to +2 °C than from +2 °C to +4 °C. The reason was mainly due to the evaporation losses from the soil. When the temperature rises, the available water at the top surface of the soil gets lost easily whereas it is difficult to evaporate water from the deeper layers of the soil. Thus, a small change in temperature dries out the upper soil layer while a larger change will be less efficient in changing evaporation as the upper soil is already tried out. The Tekeze basin was less sensitive to temperature change compared to the other basins because the basin already had limited moisture for approximately 2/3 of the year with today's temperatures.

## 4.3.3 Sensitivity to the combined effect of temperature and precipitation

Comparing the relative sensitivities of the streamflows when both temperature and precipitation were changed with the linear combination of sensitivities for the separate temperature and precipitation changes (Eq. 3) revealed that all regions shows a combined response that is very similar to the linear combination of the separate temperature and precipitation response (Fig. 10). The only hint of a non-linear effect is in the Tekeze basin where combining a 4 °C temperature increase with a positive precipitation increase gave a response that was around 2 % smaller than the linear combination of the sensitivities (Fig. 10c).

# 4.4 Estimation of future streamflow using CMIP3 simulations

To assess the uncertainty in future streamflow changes for the Eastern Nile we calculated the temperature and precipitation changes in the CMIP3, global coupled climate models (AOGCMs) with three different emission scenarios (SRES A2, A1B and B1). A total of 47 simulations with 19 different models were conducted. As the AOGCMs often have, large biases when it comes to reproducing the regional climatic features (e.g. Elshamy et al., 2009), they are not well suited to force hydrological models without extensive bias corrections. An alternative approach is to use the combined temperature and precipitation changes of the AOGCMs, with the sensitivities of the above simulations  $\Delta Q_{\Delta P,\Delta T}$ (Eq. 2), where  $\Delta P$  and  $\Delta T$  are taken from the AOGCMs and  $\Delta Q_{\Delta P,\Delta T}$  is the linearly interpolated results of the sensitivity simulations. For example, if the temperature change 404

**Table 9.** Percentage change in simulated average annual streamflow for each of twenty climate change scenarios compared with the baseline scenario (Eq. 2).

	Precipitation change (%)																				
Temp. change	p. ge Abbay BaroAkobo											Te	keze								
(°C)	-20	-10	-5	0	5	10	20	-20	-10	-5	0	5	10	20	-20	-10	-5	0	5	10	20
0 +2 +4	-34.9 -38.6 -40.4	-18.2 -22.3 -24.4	-9.3 -13.5 -15.7	$0.0 \\ -4.4 \\ -6.6$	9.8 5.2 2.9	19.6 14.9 12.5	40.3 35.4 32.8	-37.6 -43.0 -43.5	-22.5 -28.4 -29.1	-14.6 -20.6 -21.4	0.0 -6.4 -7.3	2.2 -5.3 -4.3	10.9 4.2 3.3	28.9 21.8 20.8	-42.1 -41.4 -44.9	-19.9 -19.1 -23.5	-10.8 -9.5 -14.0	0.0 1.3 -3.4	12.6 13.9 8.8	33.0 33.8 27.9	62.7 63.5 57.0



**Fig. 11.** Change in temperature (°C) and precipitation (%) for the period 2081-2100 compared to 1981-2000 from 19 AOGCMs and three emission scenarios (totally 47 simulations). Red square indicates the mean change over all simulations.

is 3.1 °C and precipitation change is 18%;  $\Delta Q_{\Delta P,\Delta T}$  is the linear interpolation for the four sensitivity simulations +2 °C and +10%, +2°C and +20%, +4°C and +10% and +4°C and +20%. The results revealed that all models agreed on a temperature rise, but they disagreed on the direction of precipitation change (Fig. 11). The large uncertainty in the models precipitation change translated into large uncertainties in the streamflow changes (Fig. 12). Around 60%, 40% and 55% of the estimates indicated an increased annual flow in the Abbay, BaroAkobo and Tekeze, respectively and the ensemble mean changes were modest in all three basins (5%, -1%, and 12% the Abbay, BaroAkobo and Tekeze, respectively). However, the extremes ranged from a 152 % increase in streamflow in the Tekeze basin using the CCSM 3.0 SRES A2 scenario changes to a 55% reduction in the same basin using the same scenario, but the values were from the GFDL CM2.0 model (Fig. 12c). This is in line with the large spread found for the Abbay in Elshamy et al. (2009).

## 5 Summary and conclusion

This study report on a first attempt to use a physically based, distributed hydrological model (SWAT) run with daily station based precipitation and temperature data and calibrated with daily streamflow measurements to simulate the Eastern Nile streamflow.

SWAT2005 adequately simulated monthly variability in flows for the Eastern Nile basin. The total simulated monthly streamflow ranged from good ( $0.65 < E_{NS} < 0.75$  to very good ( $E_{\rm NS} > 0.75$ ). The average daily and monthly difference between the observed and simulated flow (PBIAS) was good (PBIAS  $\leq \pm 20\%$ ) for the calibration period with the exception of the Abbay subbasin where it was only satisfactory ( $\pm 20\% < PBIAS \le \pm 40\%$ ). In summary, good performance of the model in the validation period indicate that the fitted parameters during calibration period listed in Table 4 can be taken as a representative set of parameters for the Eastern Nile watershed and further simulation and evaluation of alternative scenario analysis for other periods using the SWAT model. The model simulated monthly flows better than daily flows and the model was probably not adequate for studies of single sever events in small catchments.

Sixty percent of the average annual rainfalls were estimated to be lost through evaporation. The simulations estimated the runoff coefficients to be 0.24, 0.30 and 0.18 for Abbay, BaroAkobo and Tekeze subbasin respectively. Surface runoff carried around 55% of the streamflow in the Abbay and Tekeze while in BaroAkobo the percentage was about 72. The remaining contribution was from groundwater.

The streamflow sensitivity to changes in precipitation and temperature differed among the basins and depended on the strength of the changes. The annual streamflow responses to a 10% change in precipitation with no temperature change were on average 19%, 17%, and 26% for Abbay, BaroAkobo and Tekeze river basin respectively. However, the responses to a reduction and increase in precipitation were not the same. While BaroAkobo was more sensitive to a reduction in precipitation, Tekeze showed a larger sensitivity to an increase.

The streamflow sensitivity to temperature was moderate. The average annual streamflow responses to a 1 °C change in temperature and no precipitation change were -4.4%, -6.4%, and -1.3% for the Abbay, BaroAkobo and Tekeze



**Fig. 12.** Change in annual streamflow (%) for the (a) Baro Akobo, (b) Abbay and (c) Tekeze basins using the calculated combined temperature-precipitation sensitivities and precipitation and temperature changes (2081–2100 compared to 1981–2000) from 19 AOGCMs and three emission scenarios (totally 47 simulations for each sub-basin).

river basin respectively. The very low sensitivity of the Tekeze basin indicated that flows were moisture limited for a large part of the year.

The overall assessment made by coducting 20 hypothetical climate sensitivity scenarios is that the annual streamflow of the Eastern Nile is very sensitive to variations in precipitation and moderately sensitive to temperature changes. In addition, we showed that the modelled response of a combined temperature and precipitation change was very similar to adding the responses from the temperature change only and precipitation change only simulations.

Applying the combined temperature-precipitation sensitivities and 47 temperature and precipitation scenarios from 19 AOGCMs participating in CMIP3, we estimated the future streamflow change to be very uncertain and strongly dependent on the choice of climate model. The reason was the disagreement between the different climate models on both the strength and the direction of future precipitation changes. Thus, based on the state of the art climate models little can be said about future changes in Eastern Nile streamflow. However, our analysis emphasis the need for doing ensemble runs using different climate models in this type of assessment. This uncertainty may have implications for longterm water resource planning, estimation of the future hydropower potential, reservoir design and to which extent development of agriculture should utilize river or groundwater based irrigation systems.

Finally we note a few of the weaknesses of this analysis. The first is that it tried to address the climate change impact with only one hydrological model and two forcing variables (precipitation and temperature), neglecting all other variables (such as vegetation or radiation changes) which might affect the runoff generation. In our sensitivity studies, we multiplied the precipitation with a fraction. This means that we assumed the wet-day frequency was unchanged and the whole precipitation change was given as a change in intensity. For temperature, we added a constant for the whole year and thereby assuming that the changes were not depending on season. Finally, we used a rather simple procedure to link the CMIP3 climate change scenarios to changes in streamflow. These were all crude assumptions. However, we feel that given the huge uncertainty in the future precipitation changes partly justifies this crude treatment.

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